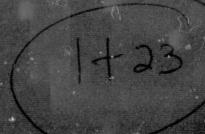
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Middle Atmosphere Program

HANDBOOK FOR MAP VOLUME 16

Edited by K. Labitzke J. J. Barnett B. Edwards



MIDDLE ATMOSPHERE PROGRAM

HANDBOOK FOR MAP

Volume 16

Edited by

K. Labitzke J. J. Barnett

B. Edwards

July 1985

Published for the ICSU Scientific Committee on Solar-Terrestrial Physics (SCOSTEP) with financial assistance from the National Aeronautics and Space Administration under P.O. W-15,897 and Unesco Subvertion 1984-1985

Copies available from SCOSTEP Secretariat, University of Illinois, 1406 W. Green Street, Urbana, Illinois 61801

ATMOSPHERIC STRUCTURE AND ITS VARIATION IN THE REGION 20 TO 120 KM DRAFT OF A NEW REFERENCE MIDDLE ATMOSPHERE

TABLE OF CONTENTS

TABLE OF CONTENTS	iii
1. INTRODUCTION, K. Labitzke	1
2. ATMOSPHERIC STRUCTURE 20 to 80 km	3
2.1 <u>Discussion on Available Data and on Errors</u>	3
M. Corney	3
F. J. Schmidlin	12
Southern Hemisphere, Yu. P. Koshelkov	15
by M. F. Radars, A. H. Manson, C. E. Meek, R. A. Vincent, and M. J. Smith	36
2.2 Middle Atmosphere Reference Model Derived from Satellite Data, J. J. Barnett, and M. Corney	47
2.3 Discussion on Variability in Time and Space	86
2.3.1 Planetary waves	86
b) Interannual variability, K. Labitzke and J. J. Barnett	138
2.3.2 Gravity waves	144
T. E. VanZandt	149
2.3.3 Atmospheric tides below 80 km, J. M. Forbes and G. V. Groves	157
2.3.4 Comparison of time-periodic variations in temperature and wind from meteorological rockets and satellites, A. D. Belmont	164
2.3.5 Annual and semiannual cycles based on the middle atmosphere reference model in section 2.2,	104
J. J. Barnett, M. Corney, and K. Labitzke	175 181
temperature in the middle atmosphere, K. Labitzke and B. Naujokat	183
2.4 A Proposed International Tropical Reference Atmosphere up to 80 km, M. R. Ananthasayanam and R. Narasimha	197
2.5 Interim Reference Ozone Models for the Middle Atmosphere, G. M. Keating and D. F. Young	205

3.1.1	Temperature structure of the 80 km to 120 km region, J. M. Forbes
3.1.2	Mean winds of the upper middle atmosphere (60-100 km):
	A global distribution from radar systems (M. F., meteor, VHF), A. H. Manson, C. E. Meek, M. Massebeuf, J. L.
	Fellous, W. G. Elford, R. A. Vincent, R. L. Craig,
	R. G. Roper, S. Avery, B. B. Balsley, G. J. Fraser, M. J. Smith, R. R. Clark, S. Kato, T. Tsuda, and A. Ebel 2
	scussion on Variability in Time and Space
3.2.1	Planetary and gravity waves in the mesosphere and lower thermosphere, R. A. Vincent
3.2.2	Atmospheric tides between 80 and 120 km, J. M. Forbes 2
	Turbulence in the altitude region 80 to 120 km,
	W. K. Hocking
4. NEW T	ECHNOLOGIES
	attribution to the CIRA Model from Ground-Based Lidar,

1. INTRODUCTION

Since the preparation of the last COSPAR Reference Atmosphere (CIRA 1972), there has been a substantial increase in the number of measurements of atmospheric structure by different satellite experiments as well as by meteorological rockets and different ground-based techniques. Therefore, a "COSPAR Task Group for the Preparation of a New CIRA" was formed in Ottawa in 1982, and one part of this group was charged with the task of preparing a "Reference Atmosphere for the Middle Atmosphere".

It is the purpose of this MAP Handbook to present a <u>draft</u> of the new Reference Atmosphere for the region between 20 and 80 km, which depends largely on recent satellite experiments covering the globe from 80°S to 80°N.

A separate "International Tropical Reference Atmosphere" is presented in Section 2.4, as well as "Interim Reference Ozone Models for the Middle Atmosphere" in Section 2.5. Both types of Reference Atmospheres are new for the CIRA, but it was thought to be timely and feasible on the basis of available data to include them.

Section 3 deals with the "Atmospheric Structure between 80 and 120 km" and is based largely on ground-based observation techniques.

"New Technologies" such as lidar and MST radar are discussed only briefly in Section 4. Note, however, that Handbook for MAP, Vol. 13 gives an up-to-date and very complete description of these new methods.

ACKNOWLEDGEMENTS

Members of the "COSPAR Task Group for the Preparation of a New CIRA".

Members of IAMAP's ICMUA (International Commission for the Meteorology of the Upper Atmosphere) were invited to contribute short papers on selected subjects to accompany the new Reference Models. Their enthusiasm and constructive help is very much acknowledged.

K. Labitzke and J. J. Barnett, Chairmen of COSPAR'S Task Group

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2.1.1 TEMPERATURE DATA FROM SATELLITES

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INTRODUCTION

Middle atmosphere temperature has been measured by a variety of sensors, notably the SIRS, VTPR, ITPR, HIRS/1, HIRS/2, MSU, SSU, SCRs, PMR, LRIR, LIMS, and SAMS. Some of these have been primarily tropospheric sounding instruments, developed to provide forecasting data, but having mid- and lower stratospheric channels to help sharpen tropospheric weighting functions.

Others have been aimed solely at the middle atmosphere. Of these some have been short duration research orientated experiments, e.g., the LRIR and LIMS, while others have been part of a long operational programme, e.g. the SSU. The current US operational sounding system, called the TOVS, is carried by the current NOAA series of satellites and comprises three sensors: the HIRS/2, MSU and SSU. Each makes stratospheric measurements, although the SSU weighting functions reach the greatest altitudes. Each scans across the satellite track to obtain global coverage with a resolution of 200 km or better. Such resolution is considered essential for the troposphere, but for the middle atmosphere where horizontal scales are larger, and particularly for the purposes of climatology, much coarser resolution is adequate. This is fortunate since many of the middle atmosphere sounders, particularly those which reach the highest altitudes, do not scan across the track and have a longitudinal resolution of 2000-3000 km, depending on latitude.

Satellite data from a single sounder are generally reduced by several different algorithms or with different coefficients. Results from experimental sounders are usually processed several times as techniques are improved, giving rise to different generations of results. Operational data are typically processed only once, with improvements in the algorithm being made as necessary and different algorithms used at different analysis centres. In the case of the TOVS, stratospheric values are given in the SATEMS distributed for tropospheric analysis, but the Upper Air Branch of NOAA and the British Meteorological Office separately reduce the data to obtain results which can be expected to be superior.

Satellite data have the advantage of giving uniform global coverage. The last CIRA reference atmosphere (CIRA, 1972) did not use satellite data for the middle atmosphere, but measurements are now sufficiently mature for them to make a valuable contribution.

DATA USED FOR THE PROPOSED SATELLITE-BASED REFERENCE ATMOSPHERE

Table I lists the sensors which have been used to produce a proposed revised reference atmosphere, with the time and space domains over which the data were available. As will be described later, only the SCR and PMR were used directly to obtain the climatic means. The SAMS and LIMS, together with, to some extent, the Stratospheric Sounder Units (SSR) on the Tiros-N series satellites and conventional radio/rocketsondes, were used as a check that the means were satisfactory.

The SCR, PMR, SAMS, LIMS, and SSU all measure the infrared emission from the carbon dioxide v_2 band at about 15 microns in order to determine the temperature profile. The SCR and PMR are essentially vertical sounders which use measurements at wavelengths of differing opacity to measure emissions

Table 1. Data sets and their domains

Sounder type	Altitude	Latitude	Time	used
Nadir)	100-0.3 mb (15-55 km)	80S-80N	-	1973- 1974
Nadir (R)	10-0.01 mb (30-80 km)	80S-80N		1975- 1978
Limb	50-0.05 mb (20-70 km)	50S-70N		1978- 1981
Limb	100-0.1 mb (16-66 km)	67S-84N	200	1978- 1979
	Nadir Nadir Limb	Nadir 100-0.3 mb (15-55 km) Nadir 10-0.01 mb (30-80 km) Limb 50-0.05 mb (20-70 km) Limb 100-0.1 mb (16-66 km)	Nadir 100-0.3 mb 80S-80N (15-55 km) Nadir 10-0.01 mb 80S-80N (30-80 km) Limb 50-0.05 mb (20-70 km) Limb 100-0.1 mb 67S-84N (16-66 km)	Nadir 100-0.3 mb 80S-80N Jan (15-55 km) Dec Nadir 10-0.01 mb 80S-80N Jun (30-80 km) Jul Limb 50-0.05 mb 50S-70N Oct (20-70 km) Dec Limb 100-0.1 mb 67S-84N Oct (16-66 km) May

originating in different layers of the atmosphere. This technique has an inherent limit to the vertical resolution of about 10 km, and the resolution achieved in practice varies from about 12 km in the low stratosphere to about 20 km in the upper mesosphere. The SAMS and LIMS view the atmospheric limb and scan vertically with a narrow field of view. A much better vertical resolution is theoretically possible (the limit is probably about 1-2 km) and the SAMS and LIMS achieve about 8 km and about 3 km, respectively.

RETRIEVAL METHODS

Retrieval is the process of obtaining the temperature profile (or 3-D field) which best fits the measurements of infrared emission. In the case of the SCR and PMR, climatology is used as additional information to give the result that is both consistent with the measurements and statistically most likely. The climatological profile used as an initial estimate was a combination of the CIRA 1972 monthly means for the mesosphere and upper stratosphere, and data by NEWELL (1977) for the lower and mid-stratosphere. These fields were derived from rocketsonde and radiosonde data. A separate field was available for the Northern Hemisphere for each month, and they were used for the Southern Hemisphere displaced by six months. This has the advantage that hemispheric differences apparent in the retrieved temperatures can only be ascribed to differences in the measurements. Values for each individual day were obtained by linear interpolation between the monthly fields in order that the fields varied smoothly with time. The initial estimate was independent of longitude, so that longitudinal structure arises totally from the data and not the initial estimate.

a) The Nimbus 5 SCR

The retrieval method was that due to CRANE (1977, 1979) for the study of a few months of winter SCR data. Its use was extended by VYAS (1984) to the complete years of 1973 and 1974. Channels Bl2, B34, and Al of the radiometer were used, these having weighting functions peaking at about 1.5, 8, and 60 mb, respectively. Radiances were Fourier analysed around latitude circles (at 4 deg latitude intervals) into the zonal mean and components of waves 1 to 4. Each component was retrieved separately to obtain the zonal mean and wave components of the temperature profile. This was done with daily analyses and

the resulting retrieved temperature coefficients were averaged over calendar months, with each field containing the mean over the corresponding months in 1973 and 1974.

b) The Nimbus 6 PMR

Channels 1000, 1015, 2100, and 2115 were used, these being radiances obtained from modulators 1 and 2 at 0 deg and 14.5 deg Doppler Scan angles. The highest altitude weighting function obtained from the PMR peaks at about 80 km, after taking into account nonlocal thermodynamic equilibrium effects; it is for a linear combination of channels 1000 and 2100 and is referred to as channel 3000. Thus although channel 3000 radiances are not explicitly used in the retrieval, the information is implicitly available from channels which are used. The radiances were initially available on latitude-longitude grids (at intervals of 4 deg and 10 deg, respectively) for each day, and were averaged to give mean fields on the same grid for each month from July 1975 to June 1978 (36 months). The data were then retrieved at each grid point separately using a maximum probability estimator as described by RODGERS (1976).

The weighting functions of the PMR have a significant temperature dependence, and for levels above about 75 km an allowance must be made in the retrieval process for the \$\frac{1}{2}\$ band of carbon dioxide not being in local thermodynamic equilibrium. These effects were taken into account by HEASEMAN (1981) who obtained mean weighting functions and coefficients of their dependence on the Planck function profile. In the retrieval process two kinds of weighting function are necessary: (1) those used to calculate the radiation emitted by the initial estimate Planck function profile; (2) differential weighting functions which give the changes of emitted radiation which arise from deviations from the initial estimate Planck function profile. The two weighting functions would be equal if there were no temperature dependence. Both are readily calculated from Heaseman's parameterization for any Planck function profile, and since the same initial estimate (hence the same weighting functions) are used at all longitudes for a given latitude, little additional computation is required.

c) The SAMS and LIMS

For limb sounders, temperature retrieval is closely associated with the problem of determining the viewing pressure of each measurement. This renders the process highly nonlinear, so retrieval is performed on individual scans or closely related groupings of data, rather than on gridded radiances. The SAMS and LIMS retrieval methods are described by RODGERS et al. (1984) and GILLE et al. (1984), respectively.

GEOPOTENTIAL HEIGHT DATA

The three-dimensional geopotential height field was obtained by integrating temperature vertically (using the hydrostatic relation) and adding to 30 mb monthly mean geopotential height analyses made by the Berlin Free University, based largely on radiosonde data. In the case of the Northern Hemisphere these had been made by averaging daily analyses to give means for each month for which satellite data were available (STRATOSPHERIC ANALYSIS GROUP). For the Southern Hemisphere, monthly mean fields were made directly from average radiosonde reports (KNITTEL, 1974). These data were available from January 1968 to December 1972, a different period from the satellite data, and therefore they were averaged to give a single mean field for each month.

MERGING OF DATA SETS

Because the data sets cover different time and space domains, averaging over all available data sets for any point was found to lead to discontinuities at data set boundaries. The problem was particularly severe at vertical lines of discontinuity, such as at 70 deg N at the edge of the SAMS data, because the thermal wind equation implied a zonal wind jet. Smoothing out the discontinuity merely broadened and smoothed the jet, without removing it. For this reason only the SCR and PMR data sets were used to give the proposed climatology, since they both measure nearly pole-to-pole. A further reason for not using the LIMS was the lack of data for a complete year, since comparison between corresponding seasons in the two hemispheres would have been misleading.

A smooth transition was made in the vertical between the SCR and PMR data sets by taking a weighted mean of the two where the weight, w, varied linearly between 6 and 8 pressure scale heights, z, (approximately 40 and 56 km, repectively):

$$T(z) = T(SCR)$$
 $z < 6$
 $T(z) = (1 - w)*T(SCR) + w*T(PMR)$ $6 < z < 8$
 $T(z) = T(PMR)$ $z > 8$

where w = (z-6)/2 and T is the zonal mean temperature or a sin or cos component of zonal temperature wave. Thus the two temperature fields were smoothly merged over a range of about 16 km. This will inevitably lead to lapse rate errors in this region, but this problem was felt to be acceptable and much less serious than the wind errors produced by a vertical discontinuity.

For both the SCR and PMR the temperature fields were averaged over their respective periods (2 and 3 years, respectively) before combination. For the Northern Hemisphere, 30 mb height fields averaged over the same five years were used for the reference level. For the SCR, retrievals made by A. D. Belmont were also available for the mid- and upper stratosphere. Since they were for the same time period, they were not averaged with the Oxford retrievals but were merely compared.

It was thought important to include tropospheric temperature in the mean climatology because many middle atmosphere applications require data below the tropopause, hence radiosonde data were used for the surface to 30 mb for the zonal mean. The Berlin temperature analyses were used for 30 mb and for 1000, 900, 800, 700, 600, 500, 400, 300, 200, 100, and 50 mb values given in the climatology by OORT (1983). The latter were given for latitudes 80 deg S to 80 deg N and for each calendar month, and are primarily averages over the 1960s and early 1970s. Linear interpolation on a log(pressure) scale was used to obtain values on the grid used for this work. Between 30 mb and 10 mb a smooth transition was made to satellite-only data, so above 10 mb SCR/PMR data were used exclusively. Radiosonde data were not used for the eddy components, apart from the 30 mb geopotential base level, so wave components at all levels were derived from satellite data.

COMPARISON AND VALIDATION

Figure 1 is an example showing the agreement obtained between the SCR retrievals and radiosonde measurements. Temperature around the 60 deg N latitude circle is given as a deviation from the zonal mean as a function of time for a 30-day period in January and Feruary 1973. Agreement is generally excellent both of the longitudinal location and the amplitude of perturbations. However detailed comparisons by VYAS (1984) showed that the SCR zonal mean values at this level were generally about 5 K colder than Berlin radiosonde

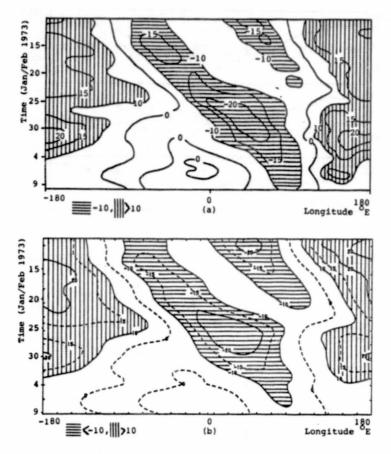


Figure 1. Longitude - time sections of deviations of temperature (K) from the zonal mean for that day at 50 mb 60 deg N; (a) taken from the Berlin Free University radiosonde analyses; (b) from SCR retrievals. Taken from VYAS (1984).

analyses and there is a case for making an empirical adjustment to the SCR zonal mean values to make them agree. BARNETT et al. (1975) have compared the SCR with radiosonde and rocketsonde; the former agree to within 1 K in equivalent temperature whilst the latter are 1-2 K warmer than the SCR at higher levels and approximately 2 K cooler in the lower stratosphere.

Figure 2 shows comparisons between values of height and temperature found over the Volgograd and Fort Churchill rocket stations and the PMR retrievals during the year July 1975 - June 1976. The rocketsonde measurements are direct copies of figures given in NASA (1978), and the PMR monthly mean values for those months of the same years and for the same latitude and longitude have been superimposed. It should be noted that the Volgograd profiles had been corrected in a manner consistent with FINGER et al. (1975) to make them compatible with US rocketsondes. Temperature differences are generally largest at 0.4 mb (about 54 km) being up to about 8 K, while differences were up to about 5 K at lower levels. No consistent bias was apparent at 2 mb but at 5 mb (where the information content of the weighting functions is rather low) the PMR measurements are generally warmer. Geopotential heights generally agreed to within about 200 m, although it should be remembered that the

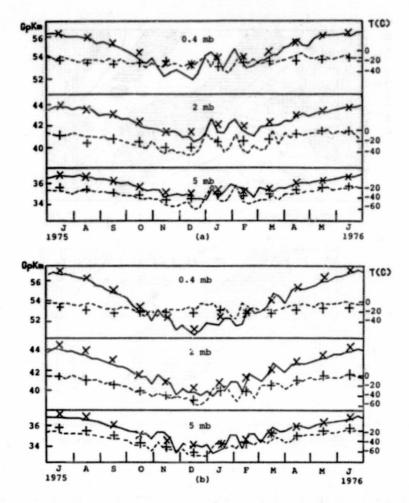


Figure 2. Comparisons between radio/rocketsonde measurements and retrievals for the same locations for (a) Volgograd (49 deg N, 44 deg E) and (b) Fort Churchill (59 deg N, 94 deg W). The rocket geopotential heights are given as solid lines with PMR monthly mean values marked with x. Rocket temperatures are given as dashed lines with PMR values marked by +. The upper, middle and lower boxes are for 0.4, 2, and 5 mb, respectively. The rocket data were extracted from analysed fields made by the Upper Air Branch of NOAA, and the figure is reproduced from NASA (STAFF, UPPER AIR BRANCH NATIONAL WEATHER SERVICE, 1978).

reference level of 30 mb used to determine heights was rather lower than ideal for use with the PMR weighting functions.

Figure 3 shows a comparison between the SAMS means (averaged over the years 1979-1981) and the SCR/PMR mean. For the zonal mean, differences of the SCR/PMR mean for 1973-78 minus SAMS are given. There are large differences, up to 12 K, near the north pole, which is taken to be due to sudden warming-type activity, but at other locations differences are less than about 5 K. The SAMS has been the subject of extensive comparisons. BARNETT and CORNEY (1984) compared the SAMS with the SSU, rocketsondes and radiosondes. The Pre-MAP

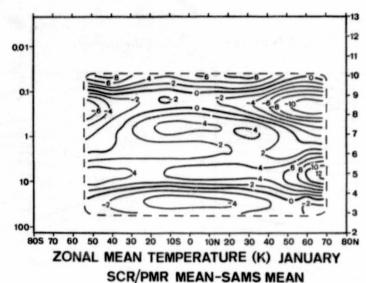


Figure 3. Difference between the SAMS average January zonal mean temperature for 1979, 1980, 1981 and that of the SCR/PMR combined mean, given as SCR/PMR - SAMS (K).

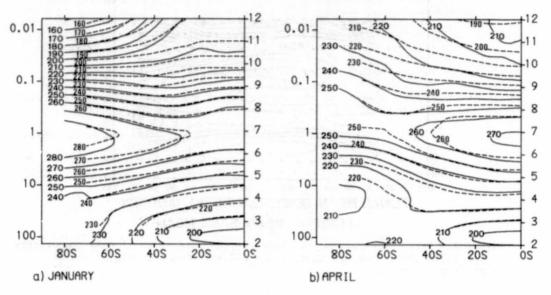
working group PMP-1 has intercompared SAMS, LIMS, SSU and analyses from Berlin Free University, the National Meteorological Center in Washington, and the European Centre for Medium-Range Weather Forecasting for various days and months during the Northern Hemisphere winters of 1979-81. Part of the study has been published as Handbook for MAP, Vol. 12 by RODGERS (1984), and the remainder will be published in a future handbook. The conclusion (for nominally simultaneous measurements) was that agreement was typically within a few K.

Figure 4a-d shows comparisons for January, April, July and October, between the SCR/PMR mean and the Southern Hemisphere Reference Atmosphere proposed by KOSHELKOV (1984) and given in Section 2.1.3) which is based on rocketsondes in the Southern Hemisphere and, to some extent, PMR measurements. In January agreement is excellent with maximum differences of about 5 K, but with values typically within 2 K, and features of the two fields are closely matched. Larger differences occur in April, exceeding 10 K at the top levels, but the geneal temperature patterns are again very alike. Similar agreement is found in July, and it should be noted that the cold belt around 45 deg S at 1 mb is present in both fields. Agreement in October is comparable with April and July. It is interesting to note that the temperature maximum at the stratopause in July at 80 deg S is very much warmer than that for the Northern Hemisphere 6 months later (see Section 2.2 Figure 1), and that a cold midlatitude belt occurs in the Northern Hemisphere winter, but that it is less marked than in the Southern Hemisphere.

RELATIONSHIP TO LONG-TERM TRENDS

Section 2.3.7 gives an analysis of long-term temperature trends observed in the stratosphere. The satellite data are for only a relatively short period (see Table 1), but Figures 10 and 13 of Section 2.3.7 show that this period, 1973-1978, is representative of the long-term average over the last 20 years.

SCR/PMR (solid); KOSHELKOV(dashed)



SCR/PMR (solid); KOSHELKOV (dashed)

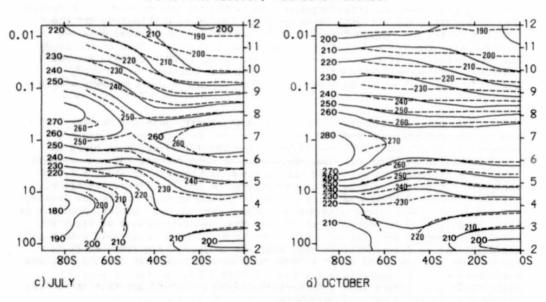


Figure 4. Comparison between the SCR/PMR combined temperature means (K) for (a) January, (b) April, (c) July and (d) October and that given by KOSHELKOV (1984) and Section 2.1.3 for the Southern Hemisphere.

N86-12816

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2.1.2 TEMPERATURE AND WIND DATA FROM METEOROLOGICAL ROCKETS

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Guided by the historical belief that the upper atmosphere is quiescent and steady when compared to the lower atmosphere, meteorologists of the 1950s and early 1960s found it difficult to accept the measurements provided by early rocket measurements. These early measurements were characterized by poor data resolution in every scale: vertical (\sim 8-10 km), horizontal (\sim 5-10000 km), and temporal (\sim weekly to monthly). Heavy, sophisticated and complex sounding rocket techniques deployed during this early period were costly, and tended to produce oversmooth data.

Development of small, single stage easy to handle meteorological rocket systems led to an increased frequency of launchings; from 1-2 every three months to as many as 3-5 every week from United States rocket ranges. Early efforts saw the development of a coordinated launch schedule from independently scheduled launchings from the different launch ranges. Meteorological rockets also were being developed and in use in other countries, such as the United Kingdom, Japan, France, Australia, and the USSR. The coordinated aspects of rocketsonde launchings in the US led to the formation of the Meteorological Rocket Network. The number of launch sites grew from four in 1950 to 30 in the late 1960s; only about ten sites are still operated by the US today, four by the USSR, and one by Japan. Australia launches an occasional rocketsonde for research studies, as does India.

During the mid-1960s to early 1970s a cooperative effort between Argentina, Brazil, France, and the United States established a schedule of rocketsonde launchings growing from one per month to one per week. The effort of these countries fostered a suggestion that a cooperative series of measurements from two meridional chains of launch sites take place. One chain was established in the Americas (near 70°W) and one in the Eastern Hemisphere (near 70°E). The Eastern Hemisphere network was established and maintained by the USSR. Thus, the Meteorological Rocket Network and the two North-South networks provided a considerable quantity of rocketsonde data between 20 km to 60 km with some launch sites providing data to 90 km.

The number of rocket ranges operated by the United States has diminished critically during the past few years. However, when one considers the frequent requests for data that are received for many reasons and is aware of research planned in the middle atmosphere, it is apparent that the importance of the meteorological rocketsonde continues.

Meteorological rocketsonde data have been published since the autumn of 1959. Initially, reports were published each quarter by the Schellenger Research Laboratory of the University of Texas at El Paso. In 1966, this activity became the responsibility of the World Data Center for Meteorology located in Asheville, North Carolina. In 1969, the archival format was changed by the World Meteorological Organization. This change made it simple to provide a unified format on magnetic tape to any investigator requesting data.

Many tens of thousands of observations are on file in the World Data Center (WDC) in the unified format which began in 1969. For the years of 1959-1968 an almost equal amount of data exists in a somewhat different format. Additionally, thousands of rocketsonde reports in manuscript or different formats, although not easily retrievable, also exist. The quantity of data so

far gathered permits a relatively detailed look at stratospheric and lower mesospheric structure and has led to the partitioning of the Northern Hemisphere atmosphere into climatological seasons as shown in Table 1 (WEBB, 1969). An example of the utility of rocketsonde data also can be noted in the reversal that occurs each spring and autumn. Rocketsonde wind data have shown that each spring the middle atmosphere (between 30-60 km) winds reverse from westerly to easterly beginning in the polar latitudes and progresses equatorward. The upper levels progressing faster than the lower levels. The autumn reversal follows the same pattern, i.e., pole to equator as the wind changes from easterly to westerly.

In recent times the most significant amount of rocket data available in the WDC archives has been obtained from the United States rocketsonde system. Although the problem of data quality may be addressed differently for each rocketsonde system, only the US system is discussed because of the quantity of data archived.

Questions concerning measurment errors and data quality often are asked. Differences have been noted in measurements made within minutes of each other, sometimes looking as if individual measurements were obtained hours, or even days apart. These observed differences generally are considered to be caused by atmospheric small-scale variations, but unless reliable information about the instruments is available, the differences could be instrumental.

Studies of the precision of the US rocketsonde instrument (see BOLLERMAN (1970) for a description of the US Super Loki Datasonde) have been carried out. Accuracy, while not very easy to confirm, can only be judged in relation to measurements from rocketsonde instruments of all countries (FINGER et al., 1975). A comparison of rocketsondes of Great Britain, France, Japan, USSR, and the United States showed that all instruments (except that of the USSR) agreed to within 5°C up to 60 km. Measurements obtained from the USSR rocketsonde became progressively colder than the others above 45 km, the difference in temperature reaching approximately 12°C at 60 km.

Repeatability of the US instrument has been shown by SCHMIDLIN (1981) to be 1°C at 53 km and lower altitudes. This precision decreases to about 4°C at 65 km. This test used paired observations where the second rocketsonde was launched 5 minutes after the first of the pair. Other efforts to understand differences and the quality of high altitude temperature measurements were conducted by HOXIT and HENRY (1973), who evaluated rocketsonde temperatures relative to altitude and solar angle, by KRUMINS and LYONS (1972) and KRUMINS (1978), who developed optimum correction values for the raw temperature measurements.

Validity of rocketsonde temperature measurements also depends on calibration data. Calibrations from a random sample of 18 instruments were checked using laboratory techniques (SCHMIDLIN, 1981); results were positive. The manufacturer supplied calibrations showing no change after 2-3 years.

The quality of wind information obtained from a falling target depends on the quality of the tracking system, sample rate, editing and filtering used with the raw tracking data, the type of sensor, and sensor fall speed. Winds obtained from various targets, whether parachute, chaff, or sphere can be made comparable after suitable corrections. The slower the target falls, the more precise the wind measurements. Thus, the magnitude of the error is a function of the target's fall velocity. At fast fall velocities and large wind shears the magnitude of the measurement difference between the sensor's horizontal velocity and actual wind increases. Additionally, the faster a target falls the more smoothing that must be applied, consequently slow targets have greater wind resolving capability.

Table 1. Climatological periods of the Northern Hemisphere derived from meteorological rocketsonde data.

Period	Date
Winter storm period	16 December - 15 February
Late winter	16 February - 31 March
Spring reversal	1 April - 15 June
Summer	16 June - 15 August
Fall reversal	16 August - 15 October
Early winter	16 October - 15 December

Although it is not possible to establish an exact error for wind measurements based on the previous discussion, unpublished information from studies conducted at White Sands Missile Range and Wallops Island indicate the wind errors may be as large as 7 meters per second near 60-65 km.

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2.1.3 OBSERVED WINDS AND TEMPERATURES IN THE SOUTHERN HEMISPHERE

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(Shortened for this publication by K. Labitzke, Ed.)

(a) TEMPERATURE IN THE SOUTHERN HEMISPHERE BASED ON ROCKET DATA

The presence of hemispheric asymmetry in the structure of the middle atmosphere has been confirmed in a number of papers based on rocketsonde and satellite data (BOROKIKOV et al., 1962; GAIGEROV, 1973; GAIGEROV and KOSHELKOV, 1973; GAIGEROV et al., 1969; ELLIS et al., 1970; KOSHELKOV, 1971a, 1974a; FRITZ and SOULES, 1970; LABITZKE, 1974; 1977a,b; LABITZKE and BARNETT, 1973, 1979; BARNETT, 1974, 1975, 1981; BARNETT et al., 1978; HARWOOD, 1975; NASTROM and BELMONT, 1975; HARTMANN, 1976; LEOVY and WEBSTER, 1976; HOUGHTON, 1978; CRANE, 1979; HIROTA et al., 1983). Therefore the middle atmosphere of the Southern Hemisphere cannot be regarded as indentical to that of the Northern Hemisphere, but as a region with its own specific features of circulation and structure. This fact makes it necessary to compile separate reference atmospheres for two hemispheres. However there were not sufficient observational rocket data for this purpose during the time when CIRA 1972 was compiled. Most of the studies on meteorology of the middle atmosphere of the Southern Hemisphere were confined to regional analyses -- for Australia (GROVES, 1965; PEARSON, 1966; ROFE, 1966), South America (ERYNSZTEIN, 1972), Southern Ocean (FINGER and WOOLF, 1967; KOSHELKOV, 1969), and Antarctica (GAIGEROV, 1973; GAIGEROV and KOSHELKOV, 1973; BRIGGS, 1965). Later in the 1970s first attempts were made to generalize the accumulated information for the whole of the Southern Hemisphere. In particular, empirical wind and temperature models for the stratosphere and mesosphere of the Southern Hemisphere were compiled in the Central Aerological Observatory (CAO) based on rocketsonde as well as aerological information (KOSHELKOV, 1983a,b)

These results are analyzed briefly below as a part of the new CIRA. It should be noted also that some attempts are being made in CAO to provide an analytical presentation of the climatic distribution of meteorological parameters.

The available rocketsonde data were collected both at stations and from vessels. The number of temperature measurements conducted by means of the Soviet rocketsondes and published in Bulletins of Results of the Rocket Sounding of the Atmosphere (1960-1982) is presented in Table 1. Besides this, data obtained at Woomera (31°S, 137°E) were used including 28 dropsonde measurements during 1968-1972 (HIND, 1973) and 31 falling sphere observations during 1970-1974 (WEAPONS RESEARCH ESTABLISHMENT, 1962-1974). At other sites, most of the observations were by Arcasondes and Datasondes and the data were obtained from WDC-A (1965-1978); NASA (1968-1970, 1972-1977) and ROCOB exchange. The profiles were corrected according to DREWS (1966); EZEMENARI (1972); and KRUMINS and LYONS (1972). The number of measurements avilable (at 50 km) are 129 for Mar Chiquita (38°S, 57°W) in 1967-1980, about 1200 profiles for Ascension Is. (8°S, 14°W) in 1965-1980 and about 200 measurements for Natal (6°S, 55°W) in 1966-1980. The results obtained at Chamical (30°S, 60°W) in 1966-1968, at Tartagal (23°S, 64°W) in 1966 and the vessel "Croatan" near the western coast of South America in 1965 (FINGER and WOOLF, 1967; MANNING and CHAMBERLIAN, 1968) were also used. Fort Sherman (9°N, 80°W) data for 1967-1978, Kwajalein Is. (9°N, 168°E) data for 1970-1981 and Thumba (8°N, 77°E)

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Table 1. The number of successful temperature measurements by means of Soviet rocketsondes from research vessels and at Molodezhnaya and Kerguelen Is. (up to January 1982). Top - for the 75-km level, bottom - for the 50-km level.

Station						Mon	th						Annua1
	J	F	М	Α	М	J	J	Α	S	0	N	D	
Vessels: 5°N-15°S	48 63	76 85	24 35	5	19 33	22 41	7 10	11 17	6 8	5 7	20 35	23 32	266 379
15°S-25°S	26 31	6	11 13	1	9 14	8 10	-	22 21	6	9 14	4	11 14	113 140
25°S-35°S	7 10	15 16	9	4	8 9	7 8	8 10	0	11 12	8 10	6	7 13	90 118
35°S-45°S	2	13 16	11 13	8	7 10	3	8 13	0	4	6 8	10 14	9 10	81 105
45°S-55°S	1 5	11	3 4	-	2	0	2	0	2 4	-	4 8	4 5	18 51
(Kerguelen) 49°S	-	9 11	29 32	31 34	23 26	29 32	14 16	6 8	2	-	-	-	143 164
(Molodezhnaya) 68°S	42 47	35 41	35 41	33 41	32 45	42 62	51 72	52 68	30 42	42 52	37 45	46 54	477 610

data for 1970-1981 were of help in the analysis of the equatorial region. Some results of mesospheric measurements by means of grenades and Pitot probes were published (MANNING and CHAMBERLAIN, 1968; NASA, 1966-1972; THEON et al., 1972).

It is known that at altitudes higher than 45 km, temperature readings obtained by means of different rocket systems reveal systematic_discrepancies. These were confirmed in the course of direct intercomparison tests (FINGER et al., 1975; IVANOVSKY et al., 1979; SCHMIDLIN et al., 1980) and later were revised (KOSHELKOV, 1983a) by means of indirect comparisons of climatic temperature means at different sites. As a result, adjustments have been worked out to make different sets of data compatible; some of them used in the data analysis for the Southern Hemisphere are presented in Table 2. Nefore applying such adjustment to the Soviet rocketsonde data, the mean temperatures obtained prior to 1979 had been fitted to the results of 1979-1981 when a modified payload was used: for the equator the bias in the former results proved to be 1.5°C at 50 km, 14°C at 60 km, 13°C at 70 km and 7°C at 75 km and for higher latitudes seasonal variations of the bias were taken into account. Data obtained at Molodezhnaya and Kerguelen Is. were corrected also for the wind effect in temperature readings by approximately -5°C for Molodezhnaya and 3-4°C for Kerguelen data for the lower mesosphere. Arcasonde data accumulated in the Northern Hemisphere and near the equator during 1965-1969 have revealed somewhat higher temperatures at altitudes 30 to 40 km than Datasonde data for

Table 2. Empirical adjustments (°C) for obtaining compatibility of different sets of temperature measurements in the mesosphere with grenade measurements.

	Table in the second	Technique										
Alt., km	M 100B (1979-1981)	Datasonde (corrected (44)) 	Arcasonde (corrected (42,43))	Australian dropsonde (corrected (37))								
80	0	-	•									
70	6	-7		to bole								
60	9	-2	-4	-11								
50	5	0	-1	-3								

1971-1980; to make both sets compatible, Arcsonde data for the Southern Hemisphere sites were lowered by about 2°C and then united with the Datasonde data. It cannot be ruled out however that the discrepancy between the lean temperatures in different years is related to the solar activity cycle (ANGELL and KORSHOVER, 1978; QUIROZ, 1979; KOKIN et al., 1981).

The Australian sphere temperatures for 1970-1974 did not differ significantly from grenade temperatures for corresponding latitudes in the Northern Hemisphere up to the height of 70 km; above this level, the usefulness of the 1970-1974 sphere data was limited since seasonal variations were not in agreement with earlier rocket results (ROFE, 1966) or PMR data (LABITZKE and BARNETT, 1981). The dropsonde temperature data were adjusted (KOSHELKOV, 1977) to the sphere data in the lower mesosphere (Table 2).

Compilation of the reference model from sets of data was achieved by application of both temporal and spatial smoothing. Seasonal variations were approximated for each station by two (for Mar Chiquita and Woomera) or three (for Molodezhnaya and Ascension Is.) harmonics of the annual cycle. In case of the incomplete annual cycle of observations (Kerguelen Is., vessels) smoothing by hand provided better results.

Latitudinal smoothing was based on an application of either third degree polynomials (mainly in the stratosphere where the data amount was greater) or hand smoothing (in the mesosphere); in the latter case, the vertical wind shear and PMR radiance (LABITZKE and BARNETT, 1981) latitudinal variations could be taken into account.

Vertical consistency of the smoothed (in time and space) values was then considered for various latitudes and required usually insignificant (1-2°) changes to provide smooth vertical variation. The lower part of the rocket-based mean profiles was adjusted to zonal mean temperatures based on aerological observations (KHANEVSKAYA, 1971; ZASTAVENKO, 1975; KOSHELKOV, 1971b, 1980b; VAN LOON et al., 1975; KNITTEL, 1976; MONTHLY CLIMATIC DATA FOR THE WORLD, 1957-1977). The rms error of the monthly mean temperatures in the Southern Hemisphere is estimated to be in the stratosphere about 1°C in summer and 2-2.5°C in winter while in the mesosphere appropriate values are about 1.5-2°C and 3°C, respectively. Systematic bias of the model data must be small in

the stratosphere and of the order of 5°C in the mesosphere; exact values are difficult to assess since the nature of discrepancies between different rocket measurements has not been finalized (FINGER et al., 1975; IVANOVSKY et al., 1979; SCHMIDLIN et al., 1980; KOKIN and GAIGEROV, 1981). However, the use of the common reference (grenade) in the mesosphere for the Northern and Southern Hemisphere Reference Atmospheres enables one to define hemispheric asymmetry in thermal structure. The accuracy of the analysis applied for the compilation of the Southern Hemisphere Reference Tables is estimated to be about 1-2°C in the stratosphere. The total uncertainty in the reference temperature values amounts to 2-3°C in the stratosphere and 5-7°C in the mesosphere.

The tables for latitudes 40 °S to 70 °S represent characteristic values for the Indian Ocean sector of the Southern Hemisphere, since the main contributing sites in extratropical latitudes (Molodezhnaya, Kerguelen Is.) are located in this sector and the bulk of vessel sounding data is also for the Indian Ocean area (usually for 65-70 °E). From satellite information it is found that the upper stratosphere in this sector of the Subantarctic in winter is slightly warmer than mean zonal temperatures (cf. Section 2.3.1). For latitudes lower than 40 °S data from various sectors of the Southern Hemisphere have been used and the model should describe conditions close to the zonal mean.

Figure 1 shows a comparison of the model temperatures for $70\,^{\circ}$ S with (a) the Molodezhnaya data for 1982-1983 at the 40-km level, and (b) with the Reference Atmosphere data as presented in Section 2.2. The agreement is generally good.

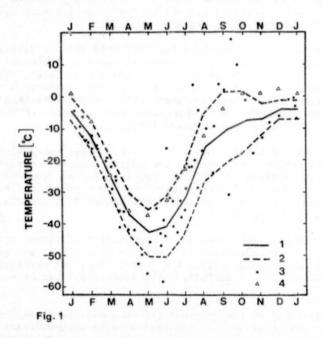


Figure 1. Comparison of the model temperatures for 70°S with the Molodezhnaya data for 1982-83 at the 40-km level, and with the data given in Section 2.2. 1 - temperature, in the CAO model; 2 - standard deviation of temperature from the model values; 3 - temperature at Molodezhnaya (1982-1983); 4 - temperature data of new Reference Atmosphere, Section 2.2.

(b) WIND IN THE SOUTHERN HEMISPHERE FROM ROCKET DATA

The wind structure of the stratosphere and mesosphere is not identical in the Northern and Southern Hemispheres as it has been revealed in recent years from both rocket (GAIGEROV and KOSHELKOV, 1973; ROFE, 1966; KOSHELKOV, 1969, 1974b, 1975; BUGAEVA and RYAZANOVA, 1969; BELMONT et al., 1974; GAIGEROV et al., 1975; TARASENKO et al., 1976) and satellite (HARTMANN, 1976; HIROTA, et al., 1983; and others) observations. Compilation of reference atmospheres is easier in the case of wind than in the case of temperature due to the absence of systematic discrepancies between wind velocities measured by means of different techniques. However for the Southern Hemisphere the main difficulty arises due to the scanty amount of observations, particularly above 60 km, where diurnal variations are great (e.g. ELFORD, 1974; GROVES, 1974; BOUTKO et al., 1976).

As in the case of temperature models, the information (EOROVIKOV et al., 1962; FINGER and WOOLF, 1967; BRIGGS, 1965; BULLETINS OF RESULTS OF THE ROCKET SOUNDING OF THE ATMOSPHERE, 1960-1982; Hind, 1273; WEAPONS RESEARCH ESTABLISHMENT, 1962-1974; WDC-A, 1965-1978; NASA, 1968, 1969, 1970; NASA, 1972-1977; MANNING and CHAMBERLAIN, 1968; NASA, 1966-1972; THEON et al., 1972) used for compiling reference tables for the Southern Hemisphere has been collected mainly from observations conducted in the southern regions of the Indian Ocean (and partly, of the Pacific), in the Australian and South American sectors of the hemisphere. The number of rocket wind measurements for main sites is clear from Table 3. Additionally, measurements from on board vessels "Ob" in 1958 and "Croatan" in 1965 were used, as well as the results of 28 launchings at McMurdo (78°S, 168°E) in 1962-1973 in Antarctica and a number of firings at Tartagal and Chamical in Argentina in 1966. Most valuable proved to be 24 mesospheric measurements (at the altitude of 80 km) of wind velocity at Natal in 1966-1973.

Table 3. The number of wind measurements for main rocket sites in the Southern Hemisphere up to January 1982, used for compiling the reference atmosphere.

1		l A	ltitude, kn	1
Site	Period of obs.	40	60	80
Vessels:	1961-1981	<u>'</u>		
5°N - 5°S		359	92	
5°S - 15°S		92	7	-
15°S - 25°S		173		
25°S - 35°S		128	9	-
35°S - 45°S		99	8	
45°S - 55°S		121	5	
Kerguelen Is.	1973-1981	171	158	72
Woomera	1962-1974	111	78	43
Mar Chiquita	1966-1977	164	64	
Ascension Is.	1964-1978	1684	804	42
Molodezhnaya	1969-1981	688	511	240

Wind measurements at South American sites, Ascension Is. and McMurdo have been conducted mainly by tracking parachutes of the Arcasonde or Datasonde below 60-65 km and chaff measurements in some cases (at Chamical). Falling spheres were applied at Ascension Is. and Woomera for mesospheric heights in addition to rocketsonde parachute measurements in the stratosphere and lower mesosphere over Natal. In the case of Soviet rocketsondes, winds below 60 km were determined by means of parachute and above that height with the help of chaff. A 6-year series (ELFORD, 1974) of radiometeor measurements of wind at Adelaide (35°S, 139°E) was a help for the wind analysis in the meteor layer. Radiosonde data (MONTHLY CLIMATIC DATA FOR THE WORLD, 1957-1977; MONTHLY CLIMATIC DATA - UPPER AIR, 1969-1974; ATLAS OF WIND CHARACTERISTICS OF THE SOUTHERN HEMISPHERE, 1967) provided the basis for the analysis in the middle stratosphere; zonal mean geostrophic winds at 50 and 30 mbar levels (KOSHELKOV, 1971b; KNITTEL, 1976; KOSHELKOV and KOVSHOVA, 1982) were also taken into consideration.

As for the temperature model, the procedure of compiling wind tables involved temporal and latitudinal smoothing of the data. The resulting reference values are of regional character south of 40 °S (the Indian Ocean sector) and more closely approach zonal means north of this latitude. Only the zonal component has been considered since for a meaningful analysis of the mean meridional circulation, one should have greater information than has been available. (Some information on the meridional component is given in Section 2.1.4).

An addition of new rocket data to the first version of the model (KOSHELKOV, 1975) did not result in a substantial change of mean values of stratospheric winds (no more than by 5 m/s). However, in the mesosphere certain difficulties were encountered in combining different sets of wind data, e.g., relatively low values of radiometeor winds at Adelaide in winter below 80 km and greater speeds measured by means of the falling spheres at Woomera, or rather weak westerlies above 60-65 km in winter over Kerguelen Is. and greater values over Molodezhnaya (chaff data at both sites). The introduction of the Kerguelen chaff data resulted in a reduction (by 10 m/s of the westerly flow in the present model as compared to the earlier (KOSHELKOV, 1975) version. It seems that values 5 and 10 m/s may reasonably reflect the uncertainty of the present model in the stratosphere and mesosphere, respectively.

Gross features of the latitudinal distribution of zonal wind are common for the two hemispheres, including the dominance of the easterly flow in the strato-mesosphere in summer and westerly flow in winter. A specific feature of the southern atmosphere circulation in summer is an extension of the maximum easterly flow at the heights of 45 to 55 km from 30° latitude into the equatorial region (HIROTA et al., 1983; BARNETT, 1981; KOSHELKOV, 1975) (Figure 2).

Hemispheric differences are insignificant in autumn. However, in winter these are quite pronounced: maximum values of the westerly flow in the Southern Hemisphere are higher than those in the Northern Hemisphere, and the latitude of the core of the flow is lower in the Southern Hemisphere; the subtropical high pressure ridge (determining the division of easterlies and westerlies) in the stratosphere of the Southern Hemisphere is weaker and closer to the equator than its Northern Hemisphere counterpart. In spring, a gradual shift of the core of maximum speeds towards higher latitudes and downward into the stratosphere is typical for the Southern Hemisphere; the easterly flow in the mesosphere of the Southern Hemisphere may appear as early as October, while a delay by 1-1.5 months is observed in the stratosphere.

Seasonal variation of zonal wind in the equatorial atmosphere (Figure 3) revealed that the CAO data deviate from the CIRA 1972 data; first, there is a

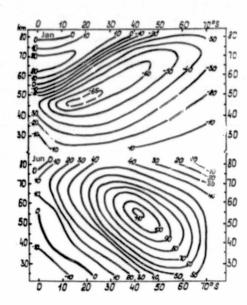


Figure 2. Cross sections of mean zonal wind (m/s) in the middle atmosphere of the Southern Hemisphere; upper part - January; lower part - June.

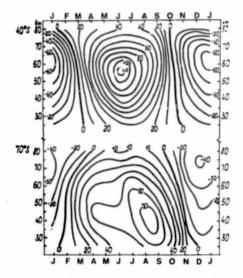


Figure 3. Seasonal variations of mean values of zonal wind at latitudes 40°S and 70°S (CAO mod \approx 1).

variation with a 12-month period (in addition to the predominant 6-month wave): second, the downward spread of the westerly wind arising within the semiannual wave is confined to 35-40 km.

In higher latitudes, the amplitude of the annual wave is greater in the Southern than in the Northern Hemisphere. The amplitude of the semiannual wave is minimum near 40-50°S and no secondary maximum has been found near 50-60°S similar to that described (BELMONT et al., 1974) for the Northern Hemisphere. Maximum speeds of the westerly flow in the middle atmosphere of the Southern Hemisphere are observed in early winter in middle latitudes and in late winter in the polar region. In the Antarctic, there is a time lag of the occurrence of maximum speed values in the stratosphere with decreasing altitude; (cf. also Sections 2.3.4 and 2.3.5).

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(c) MONTHLY MEAN TABULATIONS OF ZONAL MEAN TEMPERATURES (°C) AND GEOPOTENTIAL HEIGHTS (DAM) FOR THE MID-SEASON MONTHS

MEAN TEMPERATURES (°C) AT CONSTANT PRESSURES LEVELS IN THE SOUTHERN HEMISPHERE BASED ON ROCKET DATA

Pressure	-			La	titude,	S				
mbar	1	0	10	20	30	40	50	60	70	
		- 10-1							of the D	
				J	anuary					
0.01		-76	-76	-77	-81	-88	-96	-102	-107	
0.02		-72	-72	-72	-75	-80	-84	-88	-92	
0.05		-55	-55	-55	-58	-62	-64	-65	-66	
0.1		-39	-39	-41	-45	-48	-48	-46	-44	
0.2		-23	-24	-27	-31	-32	-30	-27	-23	
0.5		-6	-7	-10	-12	-10	-6	-2	1	
1		-4	-4	-3	-1	1	6	9	11	
2		-13	-12	-10	-6	-3	- 1	4	6	
5		-32	-30	-27	-24	-20	-17	-14	-12	
10		-43	-41	-39	-36	-34	-31	-28	-25	
20		-52	-51	-49	-47	-44	-41	-37	-34	
30		-58	-57	-55	-53	-50	-46	-42	-38	
50		-69	-67	-64	-61	-55	-49	-44	-40	
					April					
0.01		-81	-81	-80	-78	-74	-69	-65	-62	
0.02		-77	-76	-74	-71	-67	-63	-58	-54	
0.05		-63	-62	-59	-56	-53	-50	-46	-41	
0.1		-46	-45	-44	-42	-41	-39	-36	-32	
0.2		-30	-29	-29	-29	-30	-31	-28	-24	
0.5		-11	-11	-11	-12	-16	-21	-21	-19	
1		-3	-3	-5	-8	-13	-19	-24	-26	
2		-7	-8	-10	-14	-20	-26	-32	-35	
5		-24	-24	-26	-30	-34	-40	-45	-49	
10		-38	-37	-38	-40	-44	-48	-52	-57	
20		-49	-48	-48	-49	-50	-53	-56	-60	
30		-55	-54	-53	-53	-53	-54	-56	-60	
50		-66	-65	-63	-60	-57	-56	-56	-56	

Pressure	1			L	atitude,	S			
mbar	1	0	10	20	30	40	50	60	70
197	38			72	July	M T			
0.01		-83	-83	-83	-80	-76	-70	-64	-58
0.02		-77	-76	-75	-72	-68	-61	-54	-49
0.05		-63	-62	-62	-59	-53	-46	-40	-34
0.1		-48	-47	-48	-47	-42	-36	-30	-24
0.2		-31	-31	-33	-34	-31	-28	-22	-17
0.5		-11	-12	-13	-17	-19	-21	-15	-11
1		-6	-6	-6	-12	-19	-25	-24	-22
2		-13	-12	-14	-19	-27	-36	-38	-39
5		-30	-28	-30	-34	-41	-50	-55	-60
10		-41	-39	-41	-43	-48	-57	-66	-73
20		-50	-48	-49	-50	-53	-61	-71	-81
30		-55	-54	-53	-53	-55	-61	-70	-81
50		-64	-63	-61	-59	-57	-60	-70	-81
					October				
0.01		-81	-81	-81	-80	-81	-81	-81	-81
0.02		-76	-76	-75	-74	-74	-74	-73	-71
0.05		-63	-62	-60	-59	-59	-58	-57	-54
0.1		-47	-46	-45	-44	-44	-44	-43	-40
0.2		-30	-30	-30	-30	-30	-30	-29	-26
0.5		-11	-11	-11	-12	-12	-13	-11	-8
1		-3	-3	-3	-4	-4	-4	-2	-1
2		-8	-8	-8	-9	-9	-9	-6	-4
5		-25	-25	-27	-28	-27	-25	-21	-18
10		-38	-38	-39	-41	-41	-38	-34	-31
20		-49	-49	-49	-49	-49	-47	-46	-46
30		-56	-55	-54	-53	-52	-50	-51	-55
50		-65	-64	-62	-58	-54	-51	-52	-58

MEAN HEIGHTS (DAM) OF CONSTANT PRESSURE LEVELS IN THE SOUTHERN HEMISPHERE BASED ON ROCKET DATA

									7.10
Pressur	e			Lat	itude,	S			
mbar	1	0	10	20	30	40	50	60	70
	23	er.	14	Ja	anuary		Charles and the Charles and th		
0.01		7931	7941	7944	7950	7960	7995	8044	8087
0.02		7525	7534	7541	7551	7573	7615	7670	7718
0.05		6966	6973	6981	6997	7033	7085	7146	7203
0.1		6510	6517	6527	6550	6592	6648	6707	6762
0.2		6016	6027	6042	6073	6120	6174	6230	6277
0.5		5323	5335	5361	5399	5445	5496	5539	5577
1		4781	4794	4821	4857	4899	4942	4977	5011
2		4247	4254	4279	4310	4347	4383	4412	4436
5		3571	3579	3596	3619	3645	3670	3695	3716
10		3092	3099	3111	3127	3147	3165	3184	3200
20		2633	2640	2648	2660	2673	2684	2695	2705
30		2373	2378	2385	2394	2403	2410	2417	2422
50		2061	2063	2066	2071	2072	2072	2071	2073
					April				
				,	Apr 11				
0.01		7906	7914	7923	7912	7877	7818	7779	7748
0.02		7512	7518	7523	7508	7465	7400	7352	7314
0.05		6967	6974	6972	6950	6897	6816	6758	6709
0.1		6525	6525	6524	6495	6438	6356	6289	6228
0.2		6048	6049	6042	6015	5959	5872	5799	5731
0.5		5370	5374	5366	5337	5284	5209	5131	5057
1		4831	4838	4828	4805	4759	4697	4624	4547
2		4288	4294	4289	4275	4239	4191	4129	4056
5		3597	3603	3607	3601	3581	3546	3500	3439
10		3105	3112	3118	3118	3108	3082	3046	2992
20		2640	2647	2653	2656	2650	2631	2601	2560
30		2377	2382	2388	2391	2388	2375	2344	2306
							20.0		2000

Pressure	1	le" ker	256 图	L	atitude,	S	TELE LEV		
mbar	1	0	10	20	30	40	50	60	70
					July				
0.01		7859	7863	7864	7828	7783	7707	7646	7586
0.02		7468	7472	7469	7430	7378	7287	7211	7139
0.05		6927	6929	6924	6876	6807	6698	6608	6520
0.1		6485	6485	6482	6431	6352	6228	6125	6023
0.2		6012	6012	6009	5960	5873	5740	5626	5514
0.5		5337	5341	5340	5292	5209	5072	4942	4816
1		4802	4807	4808	4769	4694	4566	4429	4296
2		4267	4270	4276	4248	4187	4076	3938	3806
5		3592	3595	3600	3586	3546	3458	3335	3207
10		3109	3114	3120	3111	3085	3018	2905	2789
20		2649	2653	2658	2653	2635	2584	2490	2391
30		2388	2390	2392	2389	2375	2334	2253	2164
50		2067	2070	2071	2066	2051	2014	1948	1876
				(October				
0.01		7901	7908	7917	7924	7926	7927	7917	7875
0.02		7507	7513	7520	7522	7524	7526	7518	7477
0.05		6964	6968	6970	6968	6972	6974	6961	6913
0.1		6524	6526	6524	6524	6522	6523	6510	6454
0.2		6048	6049	6046	6042	6045	6045	6028	5968
0.5		5370	5371	5371	5368	5369	5371	5350	5284
1		4831	4833	4832	4830	4831	4834	4810	4739
2		4289	4290	4290	4288	4290	4293	4264	4191
5		3600	3602	3604	3605	3608	3605	3567	3489
10		3111	3113	3117	3119	3122	3115	3070	2986
20		2646	2649	2655	2658	2660	2648	2599	2512
20		2382	2386	2390	2395	2396	2382	2330	2250
30						-050			

(d) MEAN TEMPERATURES (°C) IN THE SOUTHERN HEMISPHERE

MEAN TEMPERATURE IN THE SOUTHERN HEMISPHERE (°C)

Height	- 1												
km	1	J	F	М	Α	М	J	J	Α	S	0	N	D
	'					Equa	tor						
80		-76	-77	-80	-81	-82	-83	-83	-84	-83	-81	-78	-76
75		-69	-71	-73	-75	-77	-76	-76	-76	-76	-74	-73	-70
70		-53	-55	-58	-60	-62	-63	-63	-63	-64	-61	-60	-56
65		-35	-38	-40	-42	-44	-45	-45	-44	-45	-43	-42	-38
60		-20	-23	-24	-26	-28	-28	-28	-27	-27	-26	-26	-23
55		-8	-9	-10	-12	-14	-14	-14	-13	-13	-13	-13	-11
50		-4	-2	-2	-4	-5	-6	-6	-6	-4	-4	-5	-6
45		-8	-4	-3	-5	-7	-9	-9	-7	-6	-5	-5	-7
40		-20	-17	-13	-13	-15	-18	-20	-19	-16	-15	-15	-19
35		-34	-33	-30	-28	-28	-30	-33	-33	-30	-29	-29	-32
30		-45	-44	-42	-41	-41	-43	-44	-44	-43	-41	-41	-43
25		-55	-54	-54	-52	-52	-53	-53	-53	-53	-53	-53	-54
20		-70	-71	-71	-69	-67	-66	-66	-66	-66	-67	-68	-69
						10	°S						
80		-76	-77	-80	-81	-82	-83	-83	-84	-82	-81	-78	-76
75		-69	-70	-72	-74	-76	-75	-75	-75	-75	-73	-72	-70
70		-52	-54	-57	-59	-61	-62	-62	-62	-63	-60	-59	-56
65		-35	-38	-39	-41	-43	-45	-45	-44	-45	-42	-42	-39
60		-21	-23	-24	-26	-28	-29	-29	-28	-28	-26	-26	-23
55		-9	-10	-11	-13	-14	-14	-14	-13	-13	-13	-13	-11
50		-4	-3	-3	-4	-6	-6	-6	-6	-4	-4	-5	-6
45		-7	-5	-4	-5	-7	-9	-9	-7	-6	-5	-5	-6
40		-19	-17	-15	-14	-15	-18	-19	-19	-16	-15	-15	-18
35		-33	-32	-30	-28	-28	-30	-33	-33	-31	-29	-29	-31
30		-44	-43	-42	-41	-41	-43	-44	-44	-43	-41	-41	-42
25		-55	-54	-53	-52	-52	-52	-52	-53	-53	-53	-53	-53
20		-69	-70	-70	-68	-66	-65	-65	-65	-65	-66	-67	-68

Height km	1	J	F	м	А	м	J	J	A	s	0	N	D
KIII	i	·			^	"	Ü	Ü	^	3	U	"	U
	_'-						20°S	-					
80		-77	-78	-79	-79	-81	-82	-83	-83	-81	-81	-79	-77
75		-69	-69	-70	-72	-74	-74	-74	-74	-73	-72	-72	-71
70		-53	-54	-56	-57	-60	-61	-61	-61	-61	-58	-58	-57
65		-38	-39	-40	-40	-43	-45	-46	-45	-45	-42	-42	-41
60		-24	-25	-25	-26	-28	-30	-31	-29	-28	-26	-26	-25
55		-12	-12	-12	-13	-15	-16	-16	-15	-14	-13	-12	-12
50		-4	-4	-5	-5	-6	-7	-7	-7	-5	-4	-4	-4
45		-5	-6	-6	-7	-8	-10	-10	-9	-7	-5	-4	-4
40		-17	-16	-16	-17	-17	-19	-20	-20	-18	-15	-15	-16
35		-31	-31	-31	-30	-30	-31	-33	-33	-32	-30	-29	-30
30		-42	-42	-41	-41	-42	-43	-44	-44	-43	-42	-42	-42
25		-53	-53	-52	-52	-52	-52	-52	-53	-53	-53	-53	-53
20		-66	-67	-66	-65	-64	-63	-63	-63	-63	-64	-65	-66
							30°S						
80		-80	-80	-79	-78	-79	-80	-81	-81	-79	-80	-81	-81
75		-71	-70	-69	-69	-70	-71	-72	-71	-70	-71	-72	-72
70		-56	-56	-56	-55	-57	-58	-60	-59	-59	-57	-59	-59
65		-41	-41	-41	-40	-42	-44	-47	-46	-44	-41	-42	-42
60		-27	-27	-27	-27	-29	-31	-33	-32	-29	-27	-25	-25
55		-13	-13	-13	-14	-17	-18	-20	-19	-16	-14	-11	-11
50		-2	-5	-7	-8	-10	-11	-12	-11	-9	-5	-2	-1
45		-3	-6	-9	-11	-13	-14	-15	-13	-9	-5	-3	-2
40		-14	-15	-18	-21	-23	-24	-24	-22	-20	-17	-14	-13
35		-28	-29	-31	-33	-35	-36	-36	-35	-34	-31	-29	-27
30		-40	-41	-41	-43	-44	-46	-46	-45	-44	-44	-43	-41
25		-51	-51	-51	-52	-52	-53	-53	-53	-53	-53	-52	-52
20		-62	-63	-62	-61	-61	-60	-60	-59	-59	-60	-61	-62

Height												
km	J	F	М	Α	М	J	J	Α	S	0	N	D
						40°S						
80	-87	-85	-79	-74	-74	-75	-77	-78	-78	-80	-85	-88
75	-75	-73	-69	-66	-65	-66	-69	-69	-68	-71	-74	-77
70	-58	-59	-58	-54	-53	-53	-56	-58	-57	-57	-60	-60
65	-42	-44	-44	-41	-40	-40	-44	-46	-43	-41	-41	-42
60	-26	-28	-30	-29	-29	-30	-33	-34	-30	-27	-24	-24
55	-10	-12	-16	-18	-20	-22	-23	-23	-18	-14	-9	-9
50	1	-4	-9	-13	-16	-18	-17	-15	-11	-5	-1	2
45	-1	-5	-10	-16	-19	-22	-22	-17	-11	-6	-2	0
40	-11	-14	-19	-25	-29	-32	-31	-27	-21	-17	-13	-11
35	-25	-28	-32	-37	-41	-44	-43	-39	-35	-31	-27	-25
30	-38	-39	-42	-46	-49	-51	-50	-48	-46	-44	-41	-39
25	-48	-49	-50	-52	-54	-55	-55	-53	-52	-51	-50	-49
20	-56	-57	-58	-58	-58	-57	-57	-56	-55	-55	-56	-56
						50°S						
80	-94	-90	-79	-70	-67	-69	-72	-74	-77	-81	-89	-95
7 5	-77	-76	-69	-63	-59	-60	-64	-66	-67	-71	-77	-79
70	-59	-60	-58	-53	-48	-47	-52	-56	-56	-57	-60	-60
65	-40	-44	-46	-41	-36	-35	-40	-45	-43	-41	-40	-40
60	-22	-27	-32	-32	-29	-28	-31	-34	-31	-27	-22	-21
55	-5	-10	-18	-24	-25	-24	-24	-24	-21	-15	-7	-5
50	6	-1	-10	-19	-23	-23	-21	-18	-12	-5	1	6
45	3	-3	-11	-22	-28	-31	-27	-20	-11	-6	0	3
40	-8	-13	-21	-30	-39	-42	-39	-28	-21	-15	-10	-8
35	-23	-27	-33	-41	-49	-54	-50	-41	-34	-28	-24	-22
30	-35	-38	-43	-49	-55	-60	-58	-52	-46	-41	-38	-35
25	-44	-46	-49	-54	-57	-61	-61	-59	-54	-49	-47	-45
20	-50	-52	-54	-56	-57	-59	-60	-58	-56	-52	-51	-50

Height	1												
km	J	F	М	Α	М	J	J	A	S	0	N	D	
						60°S						-	
80	-98	-95	-80	-66	-61	-64	-68	-71	-76	-81	-93	-100	
75	-78	-77	-69	-60	-53	-53	-59	-63	-66	-70	-78	-80	
70	-56	-58	-56	-50	-43	-42	-48	-53	-54	-56	-59	-58	
65	-35	-40	-43	-39	-32	-30	-36	-41	-41	-41	-38	-36	
60	-17	-24	-30	-30	-26	-24	-27	-30	-29	-27	-20	-16	
55	0	-8	-19	-23	-24	-21	-20	-21	-18	-14	-5	0	
50	9	1	-10	-21	-23	-20	-15	-13	-9	-4	3	9	
45	5	-2	-13	-27	-30	-30	-23	-14	-8	-3	1	6	
40	-6	-12	-23	-35	-43	-44	-37	-24	-17	-11	-8	-6	
35	-20	-26	-35	-45	-55	-57	-51	-39	-30	-23	-21	-20	
30	-32	-37	-44	-53	-62	-67	-65	-55	-46	-36	-33	-32	
25	-40	-44	-49	-56	-64	-70	-71	-67	-58	-48	-41	-40	
20	-44	-47	-51	-56	-61	-66	-70	-68	-63	-53	-45	-44	
						70°S							
80	-101	-98	-81	-64	-56	-59	-64	-70	-75	-82	-96	-103	
75	-78	-77	-68	-57	-47	-48	-55	-61	-64	-70	-78	-80	
70	-52	-55	-54	-46	-37	-37	-44	-50	-52	-55	-56	-52	
65	-30	-36	-40	-36	-27	-26	-32	-38	-40	-40	-35	-29	
60	-10	-21	-28	-27	-22	-21	-23	-26	-28	-26	-18	-10	
55	4	-7	-17	-21	-20	-18	-16	-16	-17	-13	-3	5	
50	12	3	-10	-19	-21	-17	-10	-6	-6	-2	6	12	
45	7	-2	-15	-27	-28	-25	-16	-6	-5	-2	2	8	
40	-4	-12	-25	-37	-43	-41	-32	-16	-11	-8	-7	-4	
35	-18	-26	-36	-48	-58	-57	-50	-35	-25	-18	-19	-18	
30	-29	-36	-44	-57	-69	-73	-68	-57	-42	-31	-28	-28	
25	-37	-41	-50	-60	-71	-80	-80	-75	-60	-47	-35	-35	
20	-40	-43	-49	-58	-67	-76	-81	-80	-73	-58	-41	-39	

(e) MEAN ZONAL WIND (m/s) IN THE SOUTHERN HEMISPHERE

MEAN ZONAL WIND IN THE SOUTHERN HEMISPHERE (m/s)

Height	!	,	_				,	,		s				
km	1	J	F	М	Α	М	J	J	Α	5	0	N	D	
						Eq	uator							
80		-2	-43	-42	-34	-20	-9	9	-6	-31	-35	-17	3	
75		8	-13	-16	-17	-10	1	10	2	-16	-20	-15	11	
70		22	23	18	7	4	11	10	12	3	8	3	15	
65		23	27	27	22	12	12	8	13	15	23	21	11	
60		12	22	26	32	13	6	-1	7	15	27	15	0	
55		-5	15	25	29	13	0	-11	-2	10	22	7	-15	
50		-34	0	18	23	14	-3	-22	-11	4	17	5	-26	
45		-38	-22	6	16	12	-3	-24	-18	-3	12	5	-21	
40		-26	-32	-16	-1	4	-7	-20	-21	-11	2	2	-15	
35		-16	-22	-22	-13	-10	-11	-17	-18	-14	-7	-5	-14	
30		-9	-12	-12	-12	-15	-15	-15	-15	-15	-12	-11	-11	
25		-6	-7	-7	-8	-12	-17	-15	-15	-15	-15	-13	-8	
20		-2	-1	0	1	1	1	0	-1	-3	-3	-3	-3	
							1000							
							10°S							
80		-4	-48	-38	-14	9	17	29	3	-15	-27	-13	10	
75		10	-10	-13	-4	18	26	30	22	5	-18	-13	13	
70		23	20	14	19	26	32	28	31	25	2	-7	7	
65		16	22	24	37	34	35	24	23	31	16	-2	-4	
60		1	14	25	40	32	29	16	4	20	19	-11	-21	
55		-22	2	21	34	27	18	-1	5	12	15	-12	-42	
50		-56	-20	10	28	19	11	-12	-4	5	14	-8	-49	
45		-63	-43	-9	20	16	7	-12	-7	-1	10	-3	-36	
40		-49	-44	-28	7	12	4	-8	-8	-4	3	-4	-21	
35		-35	-36	-31	-10	-1	0	-6	-8	-7	-3	-8	-18	
30		-27	-25	-21	-15	-11	-8	-8	-9	-9	-9	-12	-17	
25		-18	-17	-15	-14	-12	-12	-10	-11	-12	-13	-14	-16	
20		-12	-12	-10	-5	-1	0	-1	-2	-4	-6	-8	-10	

Height km	1	J	F	м	A	м	J	J	A	s	0	N	D	
KIII	i				^	"		•	^	,	•			
							20°S							
80		13	-5	12	16	34	37	40	29	10	-15	-10	12	
75		18	13	21	28	45	47	44	40	27	-10	-15	3	
70		10	14	23	40	53	56	43	43	40	2	-19	-14	
65		-13	5	18	45	57	59	40	36	40	10	-21	-32	
60		-40	-13	11	42	53	53	31	26	36	14	-21	-47	
55		-56	-31	-2	36	46	47	22	16	23	14	-19	-53	
50		-65	-42	-14	30	37	38	14	9	13	13	-12	-50	
45		-62	-48	-24	20	28	31	10	4	5	9	-7	-39	
40		-50	-43	-30	10	18	22	9	0	-1	4	-5	-30	
35		-38	-36	-30	-3	5	11	7	0	-3	0	-5	-20	
30		-27	-28	-25	-9	-3	3	4	-1	-4	-5	-7	-17	
25		-19	-20	-18	-11	-5	-2	0	-3	-5	-8	-10	-14	
20		-14	-14	-12	-6	-1	1	1	0	-2	-4	-6	-9	
							30°S							
80		15	16	21	32	43	47	50	46	24	-1	-4	7	
75		0	12	21	37	55	60	58	54	36	-2	-20	-18	
70		-29	1	18	44	70	73	68	63	47	-1	-26	-36	
65		-47	-23	12	50	78	86	72	65	47	4	-28	-51	
60		-58	-35	5	45	74	88	68	52	44	11	-27	-54	
55		-63	-41	-1	39	67	84	60	48	38	14	-20	-52	
50		-59	-42	-8	32	57	73	51	38	30	13	-15	-46	
45		-53	-39	-11	24	43	58	39	28	20	9	-11	-37	
40		-45	-32	-13	15	30	36	28	19	12	4	-9	-29	
		-35	-27	-13	7	20	24	18	14	8	1	-8	-21	
35			-22	-12	1	9	16	13	11	6	-1	-7	-15	
35 30		-24	22	1.6	•	-						-		
		-14	-18	-11	-2	4	9	9	8	3	-2	-5	-10	

Height	1									1.77				
km	1	J	F	М	Α	М	J	J	Α	S	0	N	D	
	'						40°S							
80		-4	-11	17	26	32	40	43	36	25	-2	-7	-10	
75		-32	-4	20	35	46	53	54	48	36	-2	-,15	-35	
70		-50	-22	17	41	59	66	66	63	45	-1	-32	-50	
65		-63	-32	12	47	74	87	82	72	52	2	-31	-55	
60		-63	-36	7	48	83	105	92	78	52	6	-29	-54	
55		-59	-35	2	44	84	110	97	76	48	7	-25	-49	
50		-52	-32	0	39	73	101	91	70	43	7	-19	-43	
45		-43	-27	-1	32	64	89	83	61	39	6	-17	-35	
40		-36	-21	-2	24	50	74	72	51	30	5	-14	-28	
35		-29	-17	-2	17	36	56	59	41	22	5	-11	-20	
30		-19	-12	-3	12	25	37	42	33	18	6	-7	-14	
25		-10	-7	-2	8	18	23	30	25	15	6	-3	-8	
20		1	2	5	9	13	18	20	18	15	10	5	3	
							50°S							
80		-26	-9	13	18	25	28	30	25	19	-5	-19	-31	
75		-46	-21	15	26	35	42	44	37	28	-3	-31	-47	
70		-57	-27	17	34	46	54	55	50	37	-1	-37	-52	
65		-57	-27	17	41	58	66	67	62	46	0	-33	-53	
60		-52	-25	17	46	70	82	81	72	54	3	-28	-51	
55		-46	-22	16	48	77	93	93	81	56	5	-24	-44	
50		-38	-18	13	48	77	100	101	84	56	8	-20	-37	
45		-31	-15	11	42	71	98	101	82	54	10	-16	-31	
40		-25	-12	10	34	60	87	93	76	51	13	-13	-25	
35		-20	-8	9	27	49	76	84	71	49	17	-9	-19	
30		-14	-5	7	20	38	63	72	64	48	22	-4	-13	
25		-7	-2	7	17	30	43	56	53	46	26	1	-7	
20		3	7	11	16	22	30	36	37	32	24	9	4	

	The same		the second	100	24						19		_
Height	1												
km	J	F	М	Α	М	J	J	A	S	0	N	D	
	'					60°5							
80	-32	-20	-4	8	19	18	20	18	12	-8	-26	-38	
75	-43	-27	5	21	27	30	34	26	19	-5	-37	-46	
70	-48	-27	12	30	37	44	47	39	29	-1	-36	-50	
65	-45	-21	20	38	47	53	58	53	38	4	-30	-47	
60	-39	-16	26	46	56	62	68	63	48	8	-24	-42	
55	-33	-12	30	52	62	71	78	73	57	12	-20	-36	
50	-28	-10	29	54	66	79	86	82	64	18	-15	-30	
45	-22	-8	25	52	68	80	92	90	70	24		-25	
40	-18	-6	21	46	64	79	88	89	73	30	8	-20	
35	-14	-4	17	38	58	75	82	83	74	38	-3	15	
30	-9	-2	14	30	50	65	74	76	71	45	1	-11	
25	-4	2	12	25	42	54	64	69	67	44	6	-5	
20	1	6	13	19	28	37	47	52	49 *	41	13	2	
						70°S							
						70-3							
80	-29	-26	-17	0	12	4	14	13	5	-9	-30	-36	
75	-34	-24	-9	10	20	16	23	18	9	-5	-34	-41	
70	-35	-17	1	24	29	31	35	28	17	0	-30	-40	
65	-32	-10	14	33	37	40	50	38	26	7	-27	-36	
60	-27	-5	22	39	42	45	57	49	36	13	-21	-32	
55	-23	-3	26	44	45	46	62	60	44	19	-15	-28	
50	-19	-2	27	51	47	48	64	67	52	24	-10	-23	
45	-15	-2	26	52	49	50	64	75	61	30	-6	-19	
40	-13	-1	24	47	52	51	61	76	67	37	-3	-16	
35	-9	0	20	41	49	50	56	71	69	43	0	-13	
30	-6	1	16	32	44	47	50	65	66	48	5	-8	
25	-3	3	12	27	37	43	45	55	58	43	10	-3	
20	-1	4	9	17	24	29	33	36	37	28	13	0	

2.1.4 MEAN WINDS OF THE MESOSPHERE (60-80 KM), AS MEASURED BY MF RADARS

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ABSTRACT

Winds data obtained from medium frequency (MF) radars for heights of 60-80 km are discussed: locations are Saskatoon (52°N, 107°W), Christchurch (44°S, 173°W), Adelaide (35°S, 183°E) and Townsville (20°S, 147°E). Whereas well-defined summer easterly jets centred near 70 km develop in summer, no regular buildups and decays are observed in winter at midlatitudes. Part of this variability can be associated with stratospheric warmings, which develop into breakdowns of the polar vortex in the Northern Hemisphere. Amplitude and phase profiles of the annual and semiannual oscillations are also presented.

The radar winds from Saskatoon are compared and combined with rocket-derived winds up to 60 km from Primrose Lake (54°N, 110° W) to give consistent cross sections from 20-110 km. The SH radar winds are compared with a model based on rocket winds (Koshelkov, Section 2.1.3) which extends up to 80 km. The latter evidence considerable smoothing, as no winter variability is evident. The other consistent difference is that heights of the summer easterly maxima for the model are 5-10 km lower than the radar winds at all latitudes.

INTRODUCTION

Very little winds data have been gathered in the last decade in the height range from 60-80 km. Small rocket systems (e.g. datasondes used within the Meteorological Rocket Network, MRN) provide data to 60 km regularly, but above that height with less regularity and probably more error. Few stations are now operational. These data are discussed in Section 2.1.2. The best source of tidally corrected winds at and above 80 km are radars: these include medium frequency (MF) or partial reflection systems, meteor radars with height ranging (unfortunately a minority); and VHF radars or MST systems. Until now the latter have provided little data of this type due to limitations in the heights and hours of the day for which suitable echoes are available. A new data set from the MST at Poker Flat including winds from meteor and turbulence echoes (BALSLEY and RIDDLE, 1984) is discussed in Section 3.1.2.

As well as giving excellent almost continuous winds data in height and time above 80 km, MF radars provide winds almost continuously with height from 55/70 - 80 km (the lowest height depending on latitude and season), and for at least the daylight hours. An example of data yield for summer and winter months has been shown for Saskatoon (GREGORY et al., 1982) depending on season, 8 -12 hours may be represented near 60 km, and approaching ~ 20 hours near 80 km. Thus daily means of the winds, obtained from simple means of all measured values or from harmonic analysis should have negligible contributions from the 12-hour tide, and small (although often not estimated) contributions from the 24-hour tide. At present there are MF radars producing winds by the spaced antenna drifts method at Adelaide (35°S), Christchurch (44°S) and Saskatoon (52 N), with new systems at Scott Base (78°S) and Mawson (68°S). Data from the first three systems and one which operated for several years at

Townsville (20°S), are presented here.

The winds for 60-80 km are discussed from several viewpoints. Firstly, comparisons are made between MF radar and rocket winds. A detailed comparison between Saskatoon radar and Primrose rocket $(54^{\circ}N, 110^{\circ}W)$ winds has been completed (MEEK and MANSON, 1984) and is summarized here. Also a comparison is made between radar winds from Christchurch, Adelaide, and Townsville, and rocket winds in a Southern Hemisphere data model obtained by Russian workers (KOSHELKOV, 1983 and Section 2.1.3). It is vital to estimate the difference between zonal mean winds and those for the Oceanian region (~140°E); and to check for the presence of tidal contamination in a data set derived from rocket systems. Secondly, and within each of these presentations the nature of the variability in the wind cross sections, especially during the winter seasons, will be discussed. Although in many cases the summer winds at 60 km could be interpolated to those at 80 km, due to the regularity and smoothness of the contours, that would seldom be possible in winter, even in the Southern Hemisphere (SH). The planetary waves, especially those associated with the stratwarms of the NH, lead to significant winter variability, much of which is not evident above 80 km in the meteor winds data. There is also strong evidence for 12-, 6-month oscillations (annual, semiannual) in these radar winds and these profiles may be compared with, and added to, rocket-derived profiles for 20-60 km shown in Section 2.3.4.

WIND CROSS SECTIONS (20-110 km) FROM SASKATOON AND PRIMROSE LAKE ($\sim 53\,^{\circ}$ N, $\sim 109\,^{\circ}$ W), 1979-1982

Winds for Primrose Lake, obtained by radar tracking of starutes released from Loki Darts have provided coverage from 20-65 km, with 8-12 firings per month in 1978/9 reducing to 4-5 per month by 1983. The firings are near 1000 h local time (LT). The radar winds for Saskatoon are obtained continuously, as described in the Introduction: below 75 km the daylight means (8-19h) are calculated, and then tidal corrections made; while above 74 km harmonic analysis is applied to 1 or 4d sets to obtain tidal amplitudes and phases and the mean wind (GREGORY et al., 1981; MANSON et al., 1981a,b, 1982; MANSON and MEEK, 1984). Careful selection of harmonic analysis data from 60-75 km has shown that the diurnal tide dominates there (~7 m/s amplitudes, northward/ eastward maxima at ~12 h/18 h local solar time). These parameters are very consistent with the rocket-derived tides for 60 km shown in Section 2.3.3. Detailed corrections, also allowing for seasonal and height variations, and 12-h tides, have been applied to the Saskatoon radar winds and Primrose Lake rocket winds, so that a true daily mean may be obtained (MEEK and MANSON, 1984). The corrections are up to 5 m/s in magnitude, and are vital for the small meridional flow.

There was also evidence for noise in both data sets. Correlations of the 65 km rocket data with lower heights, and with the radar winds, demonstrated that a strong ballistic effect was still present above 60 km, despite smoothing and analysis corrections. The upper heights of all MRN data sets should thus be treated with caution. Finally, the radar winds (<70 km) for the same hour as the rocket firing were smaller by 20-30% in summer months only. Careful study and modelling showed that reduced radar-echo signal-to-noise ratios in summer were the cause of this reduction. Empirical corrections were applied to the radar data from 60-70 km mainly for summer months (MEEK and MANSON, 1984). With these corrections and tidal adjustments the two data sets could be combined.

We show winds for a combination of 4 years (1979-1982) in Figure 1 and for CIRA-72 and a compilation by GROVES (1969) in Figure 2. Ten-day means have been used for the radar winds and monthly means for the rocket winds. The adjustments have led to an extremely good match of radar and rocket data.

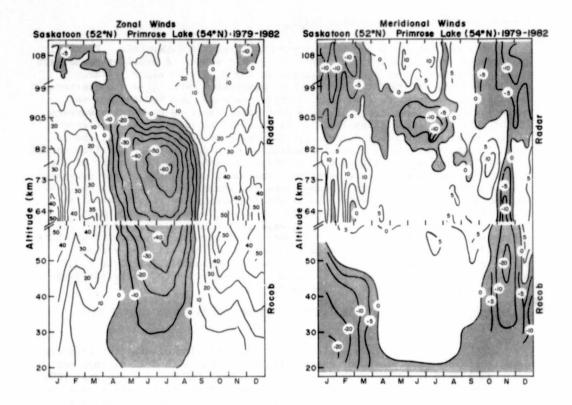


Figure 1. Zonal and meridional winds: 10d means above 60 km. Above 100 km the data apply to a ~ 5 km layer. The s.d. are typically 6 m/s near 90 km.

Temporal features of periods less than 30-d clearly emerge in the radar winds. There are also small differences in the relative positions of contours during the equinoxes and in magnitudes during the solstices, consistent with the latitudinal separation of 340 km. Individual years are available elsewhere (MEEK and MANSON, 1984). Consider first the zonal winds. For the composite the summer-centred months are dominated by a strong and smoothly contoured easterly flow 20-95 km. The 50° contour from CIRA-72 is very similar, although its easterly maximum and zero line are \(\dagger \) km lower. Also its westerly flow near 100 km is stronger probably due to tidal contamination (MANSON et al., 1981b). The equinoctial transitions are very regular and rapid. Hence, unlike CIRA, May is more summer-like and September more winter-like. For the winter-centred Canadian months the westerly maxima are somewhat weaker than the December/January maximum of CIRA. However, there is much more structured variability in these months than in CIRA: causes are planetary waves and stratwarms (MANSON et al., 1981a; MANSON and MEEK, 1984), but also long period oscillations (12-, 6-month) (MANSON et al., 1981b) e.g. the maxima of December and October, respectively. These latter are discussed below in more detail. Because of the regularity of the stratwarm dates, (4 years and temperature perturbations near January 31 and/or February 28) the composite (Figure 1) shows westerly minima near those times, and also small northerly cells. In CIRA-72 the 60 km transition between mainly MRN rocket data and rocket/radar data is almost discontinuous in December-March, indicating strong longitudinal differences and stratwarm effects. The CIRA-72 February winds above 60 km are

quite unrealistic when compared to those from Canada. Also note that there is a considerable bias toward North America in CIRA-72, so even there a zonal mean is probably not available.

The meridional cross sections are also very consistent from year to year, so that each closely resembles the composite of Figure 1. In summer there is poleward flow 20-80 km and above 95 km, with equatorward flow between. cell is quite strong (10 m/s) and maximizes in June/July; this has been detected at all longitudes near 50/60°N (NASTROM et al., 1982; DARTT et al, 1983). Here is an appropriate place to explain the westerly vertical gradient (thermal wind) of the zonal flows above ~75 km. For December-March there is poleward flow from ~50 to ~87 with reverse flow above and below. One explanation is for similar flow to summer, with upward motion at high latitudes from ~75-95 km, although this is inconsistent with the thermal wind associated with the zonal flow. A second is for two cells, one in the thermosphere and one in the mesosphere, giving downward motions throughout the upper middle atmosphere (60-110 km) (GROVES, 1980). The rocket data show an appropriate stratospheric equatorward flow. The Canadian meridional cross sections differ significantly from the data model of GROVES (1969) shown in Figure 2. His contour is dominated by the summer-centred equatorward flow. The transition between ROCOB and radar meridional winds is definitely made more continuous by the tidal and noise corrections. This is especially evident in the fall months, when a narrow equatorward tongue is established.

WIND CROSS SECTIONS FOR CHRISTCHURCH (44°S, 173°E), ADELAIDE (35°S, 138°E) AND TOWNSVILLE (20°S, 147°E) for \sim 1978-1983

The zonal cross sections for these locations (Figures 3, 4, 5) are quite similar to Saskatoon's, and may best be described as midlatitude in their characteristics. There are some tropical features in the Townsville data, but overall they differ considerably from CIRA-72 at 20°. There is a more detailed

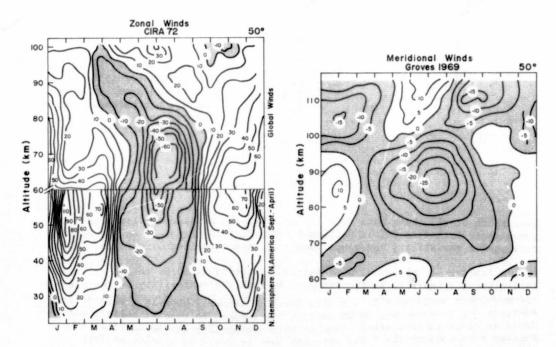


Figure 2. CIRA (1972); Groves (1969)

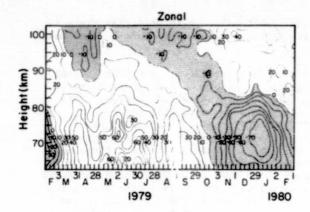


Figure 3. Christchurch, 44°S, 173°E: 7 d means; s.d. typically 7 m/s at 90 km, increasing to 10 m/s at 80 km.

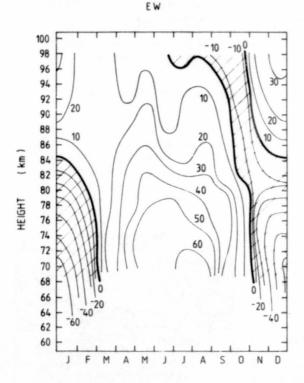


Figure 4. Adelaide, 35°S, 138°E: zonal winds for 1978-1983. Data extend down to ∿70 km; contours are extended for numbering only. The s.d. are typically 7 m/s at 90 km.

discussion of all these data (\sim 60-110 km) plus the meridional flow, and comparisons with CIRA-72, in Section 3.1.2. Here the focus is on the 60-80 km data; their variability and comparison with rocket-derived winds data.

A feature of the annual wind pattern in the 65 to 80 km region at Christchurch (Figure 3) is the contrast between the variability of the winds in autumn/winter compared with the steadiness in summer. Whereas a well-defined easterly jet centred near 80 km develops in summer, no regular buildup and decay is observed in winter. Some of this variability can be ascribed to regular wave motion: the 2-day wave has been detected in a coherent form throughout the 67 to 100 km range. Transitory responses, however, are more

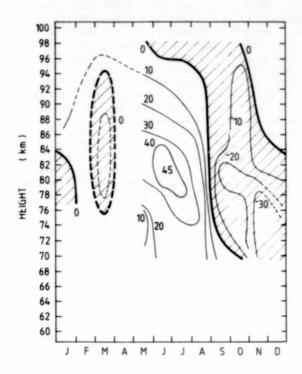


Figure 5. Townsville, 20°S, 147°E. Zonal winds for 1978-1980.

important in winter. For the 1979 data shown, a particular example of this is in early August, when winds were reversed from their usual westerly values for a period of 5 days over most of the 65-100 km range; the thermal wind at this time also suggested a high latitude cooling in the mesosphere. Stratospheric radiance charts from TIROS-N indicated a wave number 2 thermal centre moving eastward across New Zealand. As is usual for the Southern Hemisphere warmings, this did not lead to a strong polar heating. So while Southern Hemisphere warmings do not result in a breakdown of the polar vortex, very strong disturbances of the local mean flow can occur. The effects of this are most evident at heights below 75 km.

At Adelaide (Figure 4) also there is considerable variability in the prevailing winds in winter compared with the situation in summer. Both the EW and NS winds vary in a quasi-periodic manner with the maximum variability occurring in the period May-August and peaking in June-July. Amplitudes can be up to 20-30 m/s in each component with the amplitudes appearing to maximize at or below 75 km altitude. The variations have time scales of between one week and a month and are presumably associated with the passage of large-scale planetary waves.

These zonal winds are now compared with a detailed empirical model for the Southern Hemisphere, based on rocketsonde data from the USSR (KOSHELKOV, 1983). A summary of these data due to Koshelkov appears in Section 2.1.3. We consider Christchurch (44°S) first, and compare with Koshelkov's 40 and 50° data. Contours based on the latter are very smooth and symmetrical, and show none of the winter variability visible in Figure 3. There is evidently much smoothing in the model. The model gives a westerly winter flow of ~ 80 m/s at 65 km compared with ~ 60 m/s in Figure 3. Values are similar at 80 km (~ 30 m/s), meaning that the thermal wind in the model is stronger. In summer, Koshelkov's

peak is at a lower altitude (60/65 km vs 70 km), it is weaker (60 m/s vs 75 m/s), and the thermal wind is less. The 80 km easterly flow is weaker in the rocket-based model, inferring reversal to westerlies at a lower altitude. The spring and autumn transitions are similarly placed. Data from Adelaide (35° S) are available from 69 km (Figure 4). Comparing with Koshelkov's 30 and 40° data, the winter variability is greater at Adelaide despite the limited time resolution there (10-30d). The westerly flow is greater in the model at 70 km (70 m/s vs 60 m/s), the peak is earlier (June vs July/August), but the flows are comparable at 80 km. In summer, Koshelkov's peak is at a low 55/60 km (60 m/s) giving a flow of ~40 m/s at 70 km. Adelaide's flow is 60 m/s at 70 km, suggesting a higher altitude peak, as was found at Christchurch. The rocket-based model has a transition to westerly flow near 80 km, rather than Adelaide's 85 km. Finally, considering Townsville (20°), the winter flow is similar to the model (Figure 5). However the summer flow differs seriously, following the trend at 44° and 35° (Figures 3, 4). The model has a peak near 50 km, and the reversal to westerly flow is near 68 km. However Townsville has easterly flow from 70 km (~30 m/s), and a reversal near 83 km.

These differences in the summer flow between the rocket-based empirical model and the radar data are also illustrated by January (1980-82) data from the same three stations, plus new data from Mawson (68°) and Scott Base (78°S) (VINCENT, 1984; FRASER, 1984) (Figure 6). There is an upward tilt of the easterly peak with latitude, varying from 75 m/s at 70 km and 40° , to $^{\circ}30$ m/s at 80 km and 80° . The model also shows this upward tilt, but the peak is 5-10 km lower in height. The new summer data from the Antarctic are quite similar to those from Poker Flat (65°N), shown in Section 3.1.2, and differ from CIRA which shows a peak below 70 km (Figure 14, Section 3.1.2).

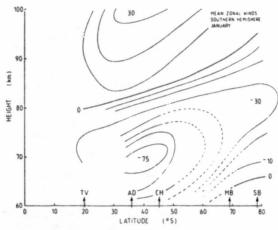


Figure 6. Contours of the zonal winds for January, Southern Hemisphere. New stations are Mawson and Scott Base.

In conclusion, the radar and rocket-based model show quite serious differences, and the major source of these is not clear. There will be differences due to comparing one longitude (Oceania) with a zonal average of some type; but until the amplitude of standing waves at these heights is known, this effect cannot be estimated. Other differences will be due to the years involved in the data sets, and comparatively small quantities of rocket data above 60 km.

ANNUAL AND SEMIANNUAL OSCILLATIONS

The presence of strong annual and semiannual oscillations in the midlatitude mesosphere and lower thermosphere are already evident from careful study of the high resolution cross sections from Saskatoon, Christchurch and

Adelaide. Harmonic analysis of the daily (Saskatoon) or approximately weekly values gives the profiles for these harmonics, for EW and NS components, (MANSON et al., 1981b; SMITH, 1981)(Figures 7, 8, and 9). Considering first Saskatoon: below 80 km the annual zonal oscillation is dominant (45 m/s), and the December maximum (westerly) is clearly evident in the zonal cross section of Figure 1. For the semiannual oscillation (20 m/s at 70 km) the maximum in mid-October and minimum in January are also evident in Figure 1. Above 90 km the oscillations are shifted by $\sim 180\,^\circ$ and the small easterly cells of April and October are clearly associated with the 6-month oscillation. Near 90 km, the semiannual oscillation dominates the annual oscillation (Figures 1, 7). Barmonics for individual years from 1979-1981 show excellent agreement with Figure 7; interannual fluctuations are typically less than 15 days.

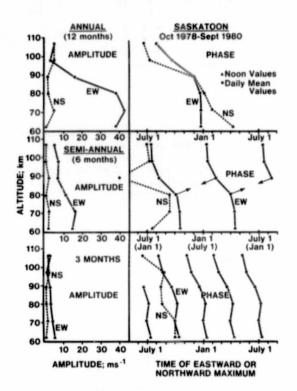
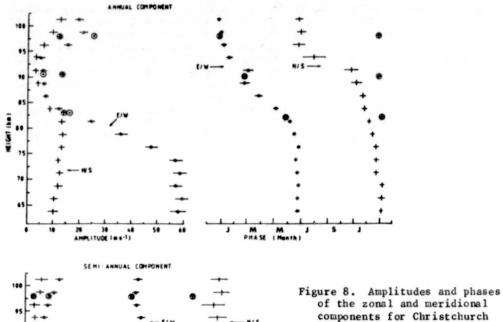
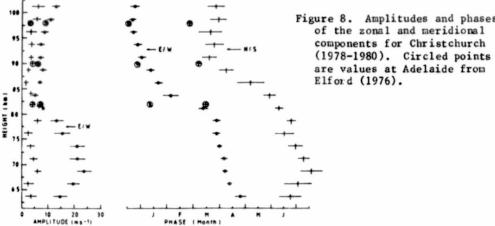


Figure 7. Amplitudes and phases of the zonal (EW) and meridional (NS) components for Saskatoon.

For Christchurch: spectral analysis of weekly wind data covering more than a year indicate that the principal long-term seasonal components are harmonics of an annual oscillation (Figure 8). The annual variation dominates below 80 km with a zonal amplitude of 60 m/s maximising at the end of June. Its strength decreases with increasing height, with minimum values in the 88-95 km region. The circulation above 95 km is 180° out of phase with that of the mesosphere. The annual variation of the zonal wind at Adelaide was very similar for early data also shown in Figure 8, but the meridional component there did not show such a large phase variation as at Christchurch (ELFORD, 1976). The semiannual oscillation achieves largest amplitude near 70 km (23 m/s). It assumes an additional importance in the 86-95 km region where it exceeds the annual variation; in this region easterly winds are observed at two intervals each year (Figure 3). A 3-monthly zonal component, with amplitudes less than 10 m/s, is also evident with a constant phase slope with height.

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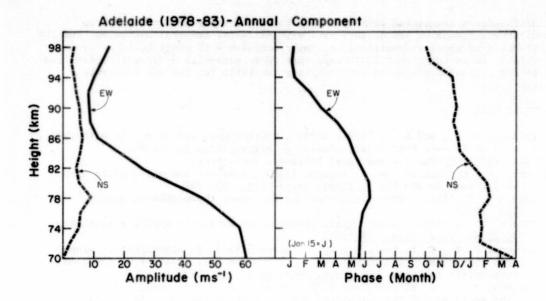




regular over time and geographical location.

The recent data from Adelaide, used in the cross section of Figure 4, provide profiles of annual and semiannual oscillations (Figure 9) which are remarkably similar to those from Christchurch, and also Elford's earlier analysis. The main differences are that the meridional annual oscillation is smaller in amplitude, and has a smaller phase variation near 95 km; amplitudes of both components of the semiannual oscillation are smaller, and the phase variation of the NS is again small. These oscillations appear to be very

Overall, the profiles of Figures 7 and 8 are similar to those shown by GROVES (1972), although the resolution here is improved. However, the comparison with Adelaide is not good, as Groves shows major differences in the positions of maxima and phase gradients below 40°, whereas the data of Figure 9 are quite midlatitude in character. Also, differences above 90 km at the three locations are likely due to tidal contamination in the earlier data analysis.



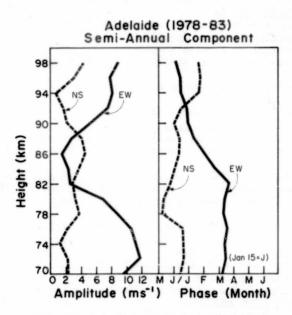


Figure 9. Amplitudes and phases of the zonal and meridional components for Adelaide (1978-1983)

CONCLUS ION

The heights of 60-80 km are of considerable interest in the middle atmosphere, as they include the maxima of the summer and winter zonal cells at midlatitudes. MF radar winds data (60-80 km) usefully extend the small-rocket (MNR) winds data so that, supplemented by radar data for above 80 km (MF, meteor, VHF/MST), winds data continuity from 20-110 km is available.

Differences between Southern and Northern Hemisphere winds, and with CIRA-72, highlight the need for a global reference atmosphere. The

difficulties associated with this task include the use of data sets from different groups of years, data sets with different temporal averaging, and the presence of zonal asymmetries. A comparison with a SH model based on rocket data to 80 km (Section 2.1.3) shows that these potential difficulties can lead to significant differences in winds data available for the new reference atmosphere.

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2.2 MIDDLE ATMOSPHERE REFERENCE MODEL DERIVED FROM SATELLITE DATA

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Table I and Figures 1.1 - 1.12 give zonally averaged temperature and geostrophic zonal wind for each month and for latitudes from 80°S to 80°N with pressure scale height as a vertical coordinate. The pressure scale height is defined as -ln(p/p₀) where p is pressure and p₀ is surface pressure. The height interval corresponding to one pressure scale height is proportional to absolute temperature, and is 7 km at 240 K. Values in Table I are given at intervals of 0.5 pressure scale heights, i.e., approximately 3,5 km. Figure 2 gives the geopotential height fields for the principal seasons.

Table II gives temperature, pressure and density with geometric height as the vertical coordinate at intervals of $5\ km$.

The temperature values have been obtained from a combination of satellite data above 30 mb with values supplied by the Berlin Free University at 30 mb and the climatology derived by OORT (1983) for 50 mb and below. The geopotential height fields were obtained from these temperature fields by integrating up and down from the 30 mb geopotential height supplied by Berlin Free University. The geostrophic winds were obtained by differentiating these geopotential height fields.

In order to derive Table II it was necessary to obtain the geometric height from the geopotential height. This was done using the scaling factors given in the Smithsonian Meteorological Tables (LIST, 1958). For some applications users may wish to use geometric and geopotential heights interchangeably. The following table which gives the geopotential height for different geometric heights and latitudes will show whether such an approximation is satisfactory for their purposes:

Geomagnetic				
Height (m)	0°	40 °	80 °	latitude
	Geope	otential	Height	
20000	19897	19941	20000	
40000	39669	39756	39874	
60000	59318	59449	59626	
80000	78844	79018	79255	

The basic grid used for the calculations, interpolation and plotting had intervals of 0.2 in ln(pressure) and 4 deg in latitude. Values were interpolated to a coarser resolution of 10 deg latitude and 0.5 intervals in ln(pressure) and 5 km for tabulation.

It must be emphasised that the zonal wind values given are geostrophic. Below about 60 km they can be expected to be within a few m/s of the true zonal wind, but above that level increasing departures can be expected because of forcing by tides and gravity waves.

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Values are tabulated to at least one significant figure more than their accuracy justifies. This is to avoid truncation problems where the data are to be used in calculations which demand particularly smooth fields.

Temperature values in Table I for 70°S and 80°S at 1013 mb and 0 km are left blank because these levels are within the Antarctic land mass. Wind values for 80°S and 80°N have been left blank because the geopotential height was not available nearer to the pole for a gradient to be found. Between 16°S and 16°N wind values were omitted because the large values of Coriolis parameter near the equator causes the wind calculation to be very sensitive to errors in the geopotential height gradient.

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								Table				OF	PC	OR	QU	ALI	TY	
TABLE					***		PRES	SURE C	XXXX IN	MES								
JANUARY			TEMPER				**			TITUDE		20	**	40	50	60	70	80
HEIGHT	(mb)		-70	-60	-50	-40	-30	-20	-10	0	10	20	30					
10.5 10.5 9.05 9.05 8.00 7.5 6.5 6.5 5.5 5.5 4.0 2.5 2.5 2.5 2.5 2.5 2.5 2.5 2.5 2.5 2.5	3/2.00																	225.1 225.5 226.4 228.1 231.4 237.4 245.3 252.7 256.0 255.1 251.7 244.9 236.4 225.2 212.3 202.3 201.6 207.8 210.7 244.1 225.2 212.3 225.2 212.3 225.3 25.3
JANUAR	r ZONAL	MEAN	GEOPOT	ENTIAL	HEIGH	T (m)												
SCALE HEIGHT	PRESSURE (mb)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
12.0	0.0062 0.0103 0.0169 0.0279 0.0279 0.0260 0.1250 0.2061 0.3398 0.5603 0.9237 1.52 2.51 4.14 6.83 11.25 18.55 30.59 50.43	81385 78945 76277 73381 70236 66864 63257 59446 55439 51289 47067 42876 38880 31139 27577 24116 20673 17242	81098 78617 75915 72995 69838 66470 62884 59108 55146 51051 46884 42736 38698 34802 31077 27526 24087 20671 17259	80746 78202 75454 72504 69338 65981 62428 58694 54783 50750 46646 42551 38560 31015 27469 24043 17312	80302 77615 74766 71763 68595 65275 61776 58100 54257 50288 46241 42211 38281 34488 30851 27354 23960 217427	79836 76982 74024 70978 67828 64553 61103 57479 45783 41806 37938 34213 30651 27223 23905 20681	79513 76529 73492 70411 67261 63995 60555 56942 53172 49281 45326 41407 37608 33950 30455 27087 23820 23655 17605	79418 76379 73308 70200 67015 63700 60200 56538 52744 48855 44926 41055 37320 33714 30267 26950 237605 17607	79403 76378 73322 70212 66999 63639 60074 56336 52481 48570 44671 40845 37133 33563 30142 26846 23644 20545 17580	79426 76395 73332 70216 66994 63615 60037 56290 52414 48495 44602 40780 37071 33495 30082 26797 23605 20518 17568	79375 76334 73259 70138 66924 63565 60020 56309 952459 48544 44642 40811 37103 335531 30113 26815 23616 20525 17571	82245 79224 76162 73064 69929 66714 63374 59883 56251 52465 48575 44562 40814 37102 33535 30120 26819 23616 14581	78993 75875 72720 69534 66290 62965 59531 55976 48436 44553 40728 37048 33519 30117 26807 23590 20454 17399	78592 75404 72184 68951 65686 62368 58987 55513 51879 48104 44277 40520 36903 33411 30031 26734 23514 617210	78168 74898 71614 68321 65017 61696 58324 54860 51254 47543 43811 40141 36581 33130 29778 26507 23036 16957	78006 74699 71380 68047 64697 61316 57872 54342 50695 46981 43285 39642 36094 32656 29332 26118 22986 19851 16684	77703 74409 71101 67771 64393 60942 57385 53736 50020 46294 42610 38979 35442 32028 28763 25639 22636 19536 16408	77453 74145 70818 67455 64023 50491 53108 49362 4565 41598 38369 34845 31459 28260 25227 22280 19291 16221
JANUARY	MEAN	ZONAL	MEAN G	EOSTRO	PHIC W	IND (m	s ⁻¹)											
	PRESSURE (mb)		-70	-60		-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
11.5 11.0 10.5	0.0460 0.0758 0.1250 0.2061 0.3398 0.5603 0.9237 1.52 2.51 4.14 6.63 11.25 18.55 30.59		-9.8 -13.6 -16.9 -19.4 -21.1 -21.9 -21.4 -17.0 -13.7 -5.5 -2.3 0.5 -2.4 -1.1 1.7	-21.7 -30.2 -37.3 -42.3 -45.8 -44.1 -41.0 -37.5 -33.5 -29.2 -25.1 -11.4 -10.3 -7.2 -3.8 0.6 6.0	-20.3 -35.4 -47.9 -56.3 -59.7 -56.3 -47.8 -42.7 -37.9 -33.6 -29.0 -24.2 -9.6 -5.4 0.7 9.0	-20.9 -39.4 -54.1 -63.4 -67.1 -66.0 -62.9 -59.5 -55.9 -52.2 -48.4 -44.1 -38.8 -32.6 -26.0 -19.0 -12.7 -7.5 -1.0 9.0	-12.3 -27.1 -37.8 -48.1 -50.2 -52.8 -56.0 -58.6 -59.4 -7.1 -31.1 -23.8 -10.7 -4.7 -3.5	3.4 -3.2 -6.4 -8.1 -11.2 -17.9 -27.8 -40.5 -53.4 -59.5 -50.6 -41.9 -34.0 -27.3 -21.0 -15.5 -10.2 -2.9 6.7				27.4	31.4 40.3 48.5 56.5 66.5 66.5 58.4 48.0 37.8 30.1 24.4 12.1 7.1 4.9 6.0 9.7 18.8 32.3	42.0 51.9 60.0 66.1 67.1 62.0 55.7 43.2 35.3 27.3 21.1 17.3 15.1 13.5 12.8 15.1	31.2 34.5 37.7 40.4 43.5 46.5 47.8 45.7 40.6 36.0 32.8 30.3 27.8 24.4 20.9 19.5 20.6	10.8 11.7 12.6 14.6 16.8 21.7 28.5 35.3 39.3 40.0 38.9 38.5 38.5 36.3 31.4 25.6 21.5	18.0 17.6 18.1 20.5 32.7 40.1 44.3 45.2 44.6 43.8 42.7 40.4 35.6 29.0 22.8 315.1	

TABLE I	(contln	ued)					PRESS	SURE CO	DORD1N/	TES								
FEBRUAR	Y ZONAL I	MEAN TE	MPERA"	TURE (()				LAT	TITUDE								
SCALE HEIGHT	PRESSURE (mb)			-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
11.5 11.6 10.0 9.5 9.0 8.5 8.0 7.0 6.5 5.0 4.5 4.5 4.5 3.5 3.0 2.5 2.5	0.0062 0.0169 0.0169 0.0279 0.0758 0.1230 0.2061 0.3398 0.5603 0.5603 1.522 2.51 4.143 6.83 11.25 18.55 50.59 50.43 83.15 137.09 226.03 372.66 614.42 1013.0	198.0 211.2 225.5 240.5 253.0 263.6 272.4 278.6 278.2 272.1 262.6 252.3 241.9 234.0 232.8 232.3 241.9 232.3 231.4 230.2	198.8 211.3 224.5 237.6 249.4 260.0 269.4 275.9 276.2 270.5 261.4 233.4 230.9 230.8 230.2 229.4	171, 2 178, 6 188, 5 200, 0 212, 0 223, 5 24, 4 266, 4 273, 1 274, 4 268, 9 259, 9 250, 5 240, 9 252, 7 228, 7 228, 7 225, 7 225	204.2 211.1 230.2 240.9 252.1 263.0 271.3 267.2 258.3 248.6 239.0 230.6 225.5 222.2 219.7 219.4 223.4	208.2 213.4 219.7 227.9 238.6 249.4 259.8 268.7 270.4 266.0 256.3 245.5	210.3 214.3 220.7 229.7 240.1 249.7 259.5 267.7 268.3 262.8 253.6 226.2 219.8 223.6 226.2 219.8 212.0 205.1	210,5 215,3 222,8 232,7 243,8 252,7 261,0 268,2 268,7 261,9 252,5 243,6 244,6	209,9 215,2 2233,0 245,1 256,5 265,8 270,5 268,6 262,2 252,2 240,9 229,8 222,3 215,9 201,2 201,2 201,2	209,9 214,7 222,4 232,6 244,6 257,7 268,1 271,9 269,9 263,3 252,8 2240,8 221,9 215,2 205,6 196,9	211, 6 215, 1 221, 7 231, 4 243, 0 256, 0 266, 9 271, 9 270, 5 263, 6 252, 7 240, 9 229, 7 222, 2 215, 0 206, 4 197, 6 201, 3 226, 2	214.3 217.0 222.3 229.6 239.0 251.2 263.2 270.4 270.2 263.1 229.9 222.1 215.3 208.4 200.8 203.9 225.5	217 0 219 5 223 7 228 7 236 8 247 7 259 2 266 5 266 9 259 8 249 1 1 238 6 229 4 222 2 216 1 207 1 207 6 222 7	222, 6 222, 6 229, 1 234, 1 243, 3 254, 8 262, 4 261, 8 262, 4 261, 8 27, 27, 27, 27, 27, 27, 27, 27, 27, 27,	226 8 228 8 231 5 236 0 243 7 252 4 252 4 256 8 254 1 246 1 226 1 221 8 217 6 217 6 218 3 218 6 218 5 228 5	2231,4 2333,9 237,5 243,0 249,2 253,0 252,5 248,0 241,6 221,5 227,6 221,5 217,1 217,1 217,8 217,8 217,8 217,8	233 1 233 1 246 1 253 3 257 6 249 5 249 5 243 4 238 4 238 6 222 2 215 0 212 2 214 1 214 6 214 8 215 5	236.4 245.4 254.9 265.2 265.2 247.8 240.2 235.6 227.0 219.9 211.4 208.3 210.2 211.2 211.2 213.6
FEBRUAR	Y ZONAL	MEAN	GEOPOT	ENTIAL	HEIGH	T (m)												
SCALE HEIGHT	PRESSURE (mb)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
12.0 11.5 11.0 10.0 9.5 9.0 8.5 7.0 6.5 6.5 5.5 5.5 4.0 3.5 3.5 3.5 2.5	0.0062 0.0103 0.0169 0.0279 0.0469 0.1250 0.2061 0.3398 0.5603 0.9237 1.52 2.51 4.14 6.83 11.25 18.55 9.50 9.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1	80562 77930 75118 72126 68925 65516 61896 58114 54185 50146 46062 42026 38112 27243 23830 20422 17026	80296 77645 74819 71820 68626 65245 61673 57944 50068 46017 42006 38113 34353 30744 27269 23875 17119	82601 80040 77357 74510 74510 68304 64953 61436 57764 53931 49977 45961 41974 38104 34363 30768 27300 23931 17264 13950	79831 77029 74099 71048 67869 64568 61116 57503 49819 45830 41871 38024 30741 27303 23967 17455	79616 76688 73677 70592 67420 64147 60729 57157 53425 49552 45597 41661 37837 34159 30640 27243 23943 20726 17593	79491 76485 73428 70322 67138 63846 60403 56818 53088 49224 45291 41394 33968 30479 27112 23848 20682 17630	79470 76455 73396 70280 67073 63744 60250 56615 52853 48976 45036 41143 37380 33751 30285 26957 23732 20605 17607	79452 76443 73395 70285 67075 63741 60237 56565 52734 48801 44848 40955 331576 30133 26824 23616 20513 17550	79485 76464 73408 70297 67094 63765 60268 56595 52742 48786 44814 40904 331512 30077 26778 23580 20493 17545	79517 76477 73398 70277 67080 63767 60291 56641 52804 48853 44875 40957 331560 30120 26811 23612 20523 17567	794 10 76331 73210 70055 66840 63534 60102 56519 52745 48833 44867 40953 33563 30119 26810 23611 20506 17510	79131 76023 72864 69668 66427 63120 59711 56168 52450 48597 44683 40818 37098 26789 23585 17396	78690 75522 72305 69059 65777 62449 59059 55566 48125 44277 40490 33345 29991 26725 23522 20358 17216	78273 75026 71740 68432 65097 61728 58308 54800 51162 47428 43680 40011 36477 29784 26555 23360 20174 16983	78264 74964 71627 68255 64848 61398 57880 54277 50595 46888 43222 39633 32149 3276 29478 26267 23099 19931 16745	78226 74936 71610 68232 64774 61224 57565 53820 50063 46365 42757 39228 35773 32385 29085 25883 22762 19645	78214 74928 71592 68182 68182 60991 57194 53319 4245791 42223 38741 35320 35320 25527 22462 19407 16332
	Y MEAN																	
HEIGHT	PRESSURE (mb)		-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
12.0 11.5 11.0 10.5 10.0 9.5 8.5 7.5 7.0 6.5 6.5 5.5 5.0 4.5 4.5 4.5 4.5 4.5 4.5	0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603 0.9237 1.52 2.51 4.14 6.83 11.25 18.55 50.43 83.15		-14.2 -16.7 -18.7 -20.7 -20.7 -20.4 -18.2 -14.3 -7.0 -4.2 -2.0 3.3 1.2 2.2 2.8 3.3 6.0 8.0 9.9	-9.3 -15.4 -20.5 -24.0 -25.7 -25.2 -22.5 -18.4 -10.7 -8.0 -6.0 -4.2 -2.8 -1.4 -0.1 1.1 3.5 7.3 13.2	-5.4 -17.2 -27.1 -35.9 -36.1 -32.9 -28.8 -24.7 -20.6 -17.2 -14.8 -8.2 -5.1 -2.5 5.1 12.5 21.5	-5.2 -17.7 -27.8 -34.5 -36.4 -35.7 -35.7 -33.8 -31.7 -29.2 -26.5 -20.1 -16.5 -12.6 -9.2 -5.9 -0.5 8.6	1.2 -6.8 -12.1 -17.2 -19.9 -24.1 -29.3 -35.5 -35.5 -34.7 -28.2 -25.1 -21.8 -17.5 -12.9 -7.7 0.2	0.6 -1.4 0.2 2.3 2.4 -0.3 -4.7 -11.3 -20.4 -30.5 -37.3 -39.5 -38.1 -35.4 -31.1 -25.8 -20.9 -15.2 -7.1				28.6 32.6 38.5 45.7 56.5 56.5 55.6 48.8 27.1 18.1 12.5 8.4 8.2 1.1 1.4 7.2 5.6 6.6 7.6 1.4 7.6 7.6 7.6 7.6 7.6 7.6 7.6 7.6 7.6 7.6	36.0 42.2 48.4 54.9 60.8 65.1 663.5 57.3 49.7 42.1 34.8 27.2 19.5 12.4 7.3 5.0 8.9 18.3	45.0 51.3 57.2 62.7 67.6 71.6 71.6 72.0 67.5 61.4 53.0 42.7 32.3 22.8 10.8 10.8 10.8 10.8 10.8	10.8 16.7 22.5 27.5 37.6 37.6 42.3 47.2 51.6 52.7 49.3 42.1 27.6 23.0 20.1 18.0 16.8 18.4	-1.6 -0.1 1.0 2.1 4.3 8.3 14.4 22.8 35.9 35.0 30.4 25.8 23.7 25.8 24.9 24.9 24.9 24.9	7.2 6.8 6.1 5.8 8.6 14.0 21.6 29.4 33.7 27.5 25.8 25.5 25.5 25.4 13.1 19.5	

TABLE	(contin	(beu					PRESS	SURE CO	DORDINA	TES								
MARCH	ZONAL	MEAN '	TEMPER/	ATURE	(K)					TITUDE							20	-
SCALE HEIGHT	PRESSURE (mb)		-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
12.0 11.5 11.5 10.5 9.0 9.0 8.0 7.5 6.5 6.5 5.5 5.5 5.5 5.0 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5	0.0062 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.5398 0.5603 1.52 2.51 2.51 2.51 3.59 30	203 9 209 6 215 8 223 3 241 2 248 1 255 0 261 8 263 6 258 8 239 2 231 4 222 8 221 3 222 8 224 2 225 7 224 8	203.6 209.0 214.9 221.6 229.3 237.1 244.4 251.7 260.5 264.5 259.9 250.6 241.1 233.6 241.1 233.6 241.1 233.6 241.1 233.6 241.7 222.3 223.7 222.3 223.7 224.4	202 1 207 6 213 5 220 1 226 2 233 2 241 2 248 9 259 1 265 7 263 2 244 8 236 6 229 1 224 3 222 9 222 3 222 3 222 3	203 6 207 9 212 1 216 5 221 7 228 8 237 9 247 7 259 2 267 4 258 6 248 7 238 8 230 2 225 0 222 5 222 5 221 7 218 7 218 7	205.4 208.7 211.7 215.3 221.1 228.3 237.0 247.3 259.6 268.8 260.2 250.1 239.7 225.2 221.3 216.3 216.3 216.3	209, 2 208, 5 211, 8 216, 5 223, 7 231, 9 239, 4 248, 4 259, 9 266, 6 260, 0 250, 7 240, 8 225, 1 219, 7 212, 5 207, 4 224, 0	207.2 211.1 216.7 224.1 233.2 242.3 250.5 260.3 268.6 268.6 268.7 262.5 252.3 241.6 218.3 209.4 203.0 225.6	207,6 207,0 207,8 2110,8 2110,8 2110,8 2110,8 2110,8 2210,8 221,0 221,0 211,0 211,0 211,0 217,5 207,7 197,7 200,8 226,9 217,5 207,7	208.8 210.5 214.5 221.2 230.5 242.0 254.5 265.9 254.7 242.2 230.6 230.6 230.9 217.1 207.0 200.4 226.5	209.1 211.0 214.6 221.4 230.3 240.4 252.9 264.9 271.6 265.3 254.6 230.7 223.3 216.0 207.3 197.9 201.2 226.2	211, 2 214, 1 218, 3 223, 8 230, 3 249, 9 262, 1 269, 7 270, 3 263, 8 253, 0 241, 8 253, 2 216, 3 201, 8 201, 8 201, 2 204, 2 204, 2 204, 2	214, 4 218, 2 221, 9 226, 3 231, 5 238, 1 248, 2 259, 7 267, 2 267, 6 260, 5 250, 0 239, 6 250, 0 222, 8 216, 8 210, 6 209, 7 222, 2	215.4 220.1 223.7 227.5 237.8 247.4 258.9 266.4 265.7 258.3 247.4 236.0 255.8 220.5 217.4 215.3 214.8 215.5 219.0	219.1 224.1 227.0 230.3 247.8 258.2 264.2 264.2 264.2 264.2 264.2 264.2 264.3 218.7 218.7 218.7 218.7 218.7 218.7	221,4 225,0 227,6 233,8 240,2 249,0 258,4 262,6 258,2 248,3 237,6 227,9 220,8 218,1 218,5 218,8 219,2 219,3 218,8	218,9 222,3 225,5 229,0 234,6 243,3 253,5 260,4 253,3 242,7 234,7 227,6 222,0 219,3 218,4 217,1 217,7 217,7	216.3 219.6 223.3 227.8 234.8 245.5 257.1 261.9 258.8 249.8 249.8 223.7 228.6 223.8 220.6 218.1 214.3 213.9 215.0 215.9
MARCH	ZONAL	MEAN	GEOPOT	ENTIAL	HEIGH	T (m)											,	
SCALE HEIGHT	PRESSURE (mb)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
12.0 11.5 11.5 10.5 10.5 9.5 8.5 7.7 6.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5	0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1256 0.2061 0.3398 0.5603 0.9237 1.52 2.51 4.14 6.83 11.25 18.55 30.59 50.43 83.15	78815 75788 72670 669459 66122 62653 59067 55385 51597 47742 43919 40204 36634 33189 29844 26578 23329 20055 16764	78872 75852 72766 69553 66250 62837 59308 55678 51923 48071 44227 40483 36887 36411 30037 26751 23026 20236 16950	79045 76047 72962 69788 66519 63158 59682 56096 52373 48524 44644 40848 37198 33671 30264 26947 23675 17157	79170 76158 73081 669943 66734 63439 60020 56467 52752 48891 44977 41128 37416 33845 30415 27084 23610 217357	79297 76265 73186 70061 66866 63578 60170 56628 52913 49043 45119 41253 37511 33929 30485 27144 23876 20668 17531	79408 76378 73300 70167 66944 63610 60157 52866 48995 45073 41211 37474 33871 30417 27074 23818 20649 17588	79499 76483 73420 70291 67063 63718 60232 56625 52884 49008 45065 41168 37401 33782 30320 26978 23736 20599 17601	82596 79561 76526 73461 70344 67139 63816 60346 56726 52927 49003 45031 41102 37307 33674 30215 26884 23650 20532 17566 14680	79592 76565 73465 70352 67158 63848 60358 52943 49001 45010 41065 37257 33615 30158 26834 23613 20506 17546	79526 76469 73394 70282 67090 63785 60337 56731 52930 49000 45016 41076 33626 30167 26843 23628 20528 17560	79484 76408 73293 70130 66892 63569 60139 56571 52816 48918 44956 41037 37254 33628 30170 26844 23628 217512	79415 76305 73136 69915 66634 63283 59845 52564 48702 44777 40901 37165 33576 30142 26825 23611 20474 17408	79168 76055 72863 69614 66309 62948 59513 55967 52254 48403 44498 40653 33409 30035 26768 23565 20397 17250	78973 75815 72566 69263 65915 62515 59050 551779 47948 44083 40292 36660 33191 29882 26659 23463 17071	78625 75422 72150 68836 65485 62091 58622 55045 47502 43682 39965 33001 29722 26511 23315 316906	76251 75071 71636 668561 665233 61843 58344 54709 50938 47117 43352 39715 36223 32837 29550 26321 23117 19927 16748	77944 74797 71605 68363 65059 61677 58160 54480 50671 46849 43123 39540 36081 32694 29385 26131 22919 19751 16619
MARCH	MEAN	ZONAL	MEAN G	EOSTRO	PHIC W	IND (m	s ⁻¹)											
SCALE HE IGHT	PRESSURE (mb)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
12.0 11.5 11.0 10.0 9.5 9.5 9.5 9.5 6.5 6.5 5.0 4.5 4.5 3.5 2.5	0.0062 0.0105 0.0169 0.0279 0.0458 0.1250 0.2061 0.3398 0.5063 0.9237 1.52 2.51 4.14 6.83 11.25 18.55 50.59 83.15			11.7 11.2 11.5 12.6 14.6 18.0 22.3 26.3 29.1 30.3 29.9 27.2 18.6 14.8 11.6 11.1 11.8 14.2 17.8		12.2 11.3 11.1 11.0 9.7 7.0 4.7 3.6 2.9 2.5 2.6 2.7 2.1 1.0 0.1	14.2 14.0 12.0 8.5 3.8 -0.1 -1.5 -1.8 -3.0 -5.2 -7.4 -9.3 -10.4 -10.1 -8.5 -4.1	10.2 11.1 13.5 16.0 18.5 20.4 19.1 13.9 6.1 0.6 4.4 -10.7 -15.8 -18.2 -17.2 -17.2 -17.2				3.2 4.1 9.5 18.7 29.3 38.2 42.8 42.3 37.9 24.7 19.0 13.2 2.6 1.2 1.1 1.2 4.1 1.2 4.1		10.0 11.2 14.5 19.8 25.4 30.5 35.0 38.1 39.0 37.5 34.6 30.7 25.7 19.6 12.9 10.0 16.8 24.7		22.3 24.1 24.9 24.2 23.3 22.5 22.2 23.4 28.8 28.7 25.3 19.8 15.1 112.4 111.8 12.3 111.8		

TABLE 1	(contin	(beu					PRES	SURE CO	XORDINA	TES								
APRIL	ZONAL	MEAN '	TEMPER	ATURE	(K)				1.47	TITUDE								
SCALE HEIGHT	PRESSURE (mb)		-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
12.0 11.5 11.5 10.0 9.5 9.0 8.5 7.0 6.5 6.5 5.5 5.5 5.5 5.0 2.5 0.0	0.0062 0.0105 0.0169 0.0279 0.0450 0.1250 0.2061 0.2061 0.23398 0.5603 0.9237 1.51 2.51 2.51 11.29 18.59 30.59 50.43 83.15 137.09 226.03 372.66 614.42 1013.0	231.4 236.0 242.6 249.1 253.0 256.2 258.9 254.4 243.1 231.3	223.0 225.7 227.2 229.3 233.0 238.4 244.0 255.0 257.2 257.2 244.6 231.9 220.9 211.7 211.7 217.6 218.9 220.9 214.2 210.5 244.6	226.5 229.7 233.7 238.4 243.6 247.9 254.4 255.5 248.0 236.6 226.6	220.1 223.0 226.9 232.8 240.4 247.7 255.3 258.8 254.4 244.9 234.6	216.1 219.4 224.6 231.3 239.2 248.4 258.8 264.3 260.4 251.3 241.2	217.2 224.4 232.5 239.4 248.6 260.2 266.8 264.0 255.7 245.9	214.2 221.1 230.4 239.7 250.3 261.3 267.8 267.4 260.7 250.5	209.7 211.7 217.9 227.5 239.0 251.4 263.0 269.7 269.8 264.1 254.4	210.1 216.6 226.9 239.5 252.5 263.9 270.2 270.6 265.2 255.9	211.9 219.0 228.4 239.0 250.7 262.3 269.8 270.1 264.5 255.3	217.1 224.0 230.9 238.2 247.9 260.1 269.1 269.4 263.0 253.3	220.3 226.6 233.2 239.6 248.8 260.5 269.3 269.6 262.6 252.5	221.8 228.2 235.0 241.6 251.1 262.7 270.7 270.6 264.1 253.3	224.1 230.2 236.4 243.1 252.8 263.5 270.8 271.0 263.3 251.4	225.7 231.1 236.9 243.9 252.9 263.8 270.6 268.5 259.3 247.1	225.7 230.9 235.9 244.3 254.4 264.8 269.7 264.9 254.7 242.6	225.4 230.1 234.8 243.9 255.0 265.1 268.8 262.5 251.8 240.2
APRIL	ZONAL	MEAN (GEOPOT	ENTIAL	HEIGH	(m)												
SCALE HEIGHT	PRESSURE (mb)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
12.0 11.5 11.0 10.5 10.5 9.5 9.5 8.0 7.5 6.0 6.5 6.5 6.5 4.0 3.5 2.5 2.0	0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603 1.9237 1.52 2.51 4.14 6.83 11.25 50.59 50.43 83.15	77573 74213 70839 67421 63914 60313 56633 52905 49130 45359 41718 38241 34941 34941 34945 28695 25703 22697 196477	64193 60661 57052 53386 49650	77977 74736 71442 68103 64709 61254 57722 54124 50443 46700 43010 39455 32805 29633 26490 23321 20139 16954	78367 75196 71990 68746 65451 62089 58623 55050 417593 43830 40168 336861 30025 26805 23588 20385 17203	78902 75790 72643 69456 62868 59422 55836 48299 44450 40697 37094 33626 30276 26996 23753 17425	79188 76125 73022 69872 66639 63293 59836 56269 52537 48672 44779 40966 37297 33761 30353 27031 23768 17539	79298 76260 73195 70089 66903 63600 60155 56571 52818 48940 45014 41140 37380 333801 30348 26999 23744 20597 17589	79395 76316 73247 70164 67021 63764 60346 56758 52984 49079 45123 41206 337411 33761 30278 26925 23678 17570	79388 76303 73242 70172 67039 63789 60371 56778 52996 49084 45118 41190 37378 337311 30225 26882 23646 20526 17558	79331 76272 73223 70150 66996 63726 60301 56719 52956 49055 45094 41173 37368 33705 30228 26891 23658 17560	79438 76382 73303 70166 66934 63605 60169 56616 52891 49012 45061 41154 33737 30258 26907 23669 20529 17513	79598 76543 73425 70240 66967 63602 60140 56569 52637 48955 45000 41096 33703 30240 23663 20510 17433	79684 76669 73593 70351 67054 63664 63664 60174 55572 52806 48896 44924 41001 37213 33591 30158 26853 23632 20461 17317	79706 76716 73586 67024 63610 60100 56475 52689 48774 44798 40876 37110 33516 30112 26829 23606 20402 17201	79637 76632 73483 70227 66880 63455 59935 56302 52514 48596 44640 40765 37061 33524 30149 26868 23622 20382 17145	79475 76484 73351 70100 66753 63338 59822 56174 52366 48444 44522 40710 37071 33596 30253 26965 23681 20403 17141	79377 76394 73271 70027 66687 63286 59782 56131 52316 48397 44500 40729 33685 30359 27061 23742 20430 17154
APRIL	MEAN	ZONAL	MEAN G	EOSTRO													Calcon	
SCALE HE IGHT	PRESSURE (mb)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
11.5	0.0062 0.0105 0.0169 0.0279 0.0460 0.1250 0.2061 0.3398 0.5603 0.9237 1.52 2.51 4.14 6.83 11.25 18.55 50.43 83.15		14.5	16.8 22.2 27.5 32.4 37.5 43.4 50.0 55.8 60.6 60.6 56.9 50.9 43.0 35.9 30.3 21.0 18.2 17.1 17.5	39.0 44.3 50.1 56.0 61.3 65.5 68.3 69.0 67.4 49.4 40.7 25.3 19.9 17.1 16.8	40.5	22.0 27.1 32.8 38.2 44.7 44.7 43.5 41.0 38.5 33.9 26.6 18.1 10.0 -0.7 210.0	13.4 17.1 24.1 33.3 42.7 47.0 45.1 40.7 36.9 31.0 21.5 10.0 -0.2 -7.1 -9.9 -9.4				-26.2 -25.0 -17.2	-10.9 -18.5 -21.0 -18.8 -14.8 -10.8 -6.8 -3.2 0.1 3.0 5.1 6.7 8.0 8.8 8.3 5.8 3.2 2.1 4.0 11.8 23.8	-6.9	6.7 3.9 3.3 4.4 8.2 9.4 10.7 12.6 11.7 12.6 10.1 6.6 3.0 5 0.5 0.4 3.0 9.4	7.2 6.9 7.1 7.3 8.7 8.8 9.2 11.1 11.3 9.3 9.4 0.8 -3.4 -5.0 -2.8 -0.1 1.8	10.4 10.6 10.3 9.8 9.8 9.0 8.5 9.0 8.7 6.4 -1.3 -4.7 -6.6 -0.3 0.6	

TABLE I	(contin	ued)					PRES	SURE CO	DORDIN	ATES								
MAY	ZONAL	MEAN '	TEMPER	ATURE	(K)				1.65	TITIME								
SCALE P	RESSURE (mb)		-70	-60	-50	-40	-30	-20	-10	O	10	20	30	40	50	60	70	80
11.5 11.0 10.5 10.5 9.0 8.5 9.0 8.5 7.0 6.5 6.0 5.5 5.0 2.5 2.0	6.83	206.2 194.8	206.3 198.6	207.7	214.6	225.6	233.6	239.7	243.5	233.1	243.9	242.9	233.3	243.7	232.3	245.2	245.7	162.7 174.0 187.4 201.8 216.4 227.9 257.3 250.1 263.0 273.9 280.6 278.4 270.9 258.0 245.2 236.4 230.0 229.1 1230.0 229.1 230.0 229.1 230.6 229.1 230.6
MAY	ZONAL	MEAN (GEOPOT	ENTIAL	HE IGH	r (m)												
SCALE P	RESSURE (mb)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
11.5 11.0 10.5 10.0 9.5 9.0 8.5 8.0 7.5	0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.503 0.5603 0.5603 0.5603 0.5603 1.52 2.51 4.14 6.83 11.25 18.55 30.59 50.43 85.15	76372 72948 69519 66056 62524 58901 55173 51385 47576 43830 40259 336852 336512 27573 24792 22000 19111 16144	76965 73587 70177 66717 667181 59561 55849 52078 44539 40959 37548 34313 31222 26260 25382 22475 119507	77496 74164 70757 67286 63739 60125 56457 52750 49021 45331 41771 38362 35127 32028 29018 26024 22988 19914 16816	77847 74585 71270 67897 64454 60947 57373 53740 50060 46378 42770 39289 359745 29662 26542 23401 20250 17098	78366 75206 75206 68746 68746 65423 62028 58553 54987 51313 47570 43823 40181 36705 333349 30082 26856 23645 23645 17321	78750 75691 72596 669458 66237 62899 59437 55864 52157 48347 44509 40742 37121 33636 30263 26962 23718 17459	78878 75872 72873 69809 66691 63435 60006 56419 952672 48820 44923 41073 333768 30327 26988 23734 20578 17552	78901 75878 72863 69886 66827 63631 60229 56630 52856 48977 45066 41202 37438 33798 30311 26953 23762 17572	78962 75929 72930 669932 66867 63660 60247 56846 48985 45073 41203 33774 30283 26931 23680 17578	79088 76067 73052 70020 66904 63653 60220 56622 52871 49003 45087 41212 33789 30308 26962 23717 20582 17592	79278 76286 73261 70180 67001 63701 60256 56680 52955 49081 45144 41262 37498 33866 30384 27019 23756 17568	79448 76493 73478 70385 67183 63865 60413 56830 53091 49202 45238 41322 33390 30417 27051 23789 20613 17525	79543 76678 73703 70625 67424 64099 60640 57048 45352 45354 41387 37555 33890 30413 27064 23809 17458	79793 77006 74056 67746 64392 60891 57247 45452 41462 37615 37615 23837 27106 23837 27106 17383	80098 77365 74430 68068 64682 61149 57467 53615 49632 45585 41583 37731 34048 27180 23887 20810 17330	82857 80353 77674 74786 68441 65041 65041 657763 53869 49846 45775 41758 33687 34195 30676 27280 23956 20635 17306 13988	80546 77904 75051 71991 68731 65327 61757 58001 54064 49997 41868 37996 34310 27374 24018 20658 17293
MAY	MEAN	ZONAL	MEAN G	EOSTRO	PHIC W	IND (m	s ⁻¹)											
SCALE P	RESSURE (mb)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
11.5 11.0 10.5 10.0 3.5 9.0 8.5 8.0 7.5	0.0062 0.0103 0.0169 0.0279 0.0458 0.1250 0.2061 0.3398 0.5603 0.9237 1.52 2.51 4.14 6.83 11.25 30.59 50.43 83.15 11.25		32.2 37.4 40.3 41.1 40.5 40.8 42.6 47.7 49.5 50.8 51.9 52.3 41.7 31.9 221.0	28.5 32.2 35.2 37.7 40.4 43.9 48.4 53.4 53.4 59.6 61.3 61.3 61.3 61.3 49.2 41.2 33.4 49.2	33.1 39.9 48.0 57.0 666.9 84.3 90.4 92.9 90.7 83.0 52.5 42.1 32.8 25.9 21.7	49.9	28.3 38.9 50.7 64.1 86.2 89.3 88.1 83.4 76.7 54.5 39.4 25.3 14.7 7.9 3	11.4 13.6 22.1 34.3 48.6 61.5 66.9 64.3 58.7 52.8 46.9 38.7 26.7 13.3 3.5 -1.4				-33.9 -39.1 -38.6 -33.1 -25.1 -18.8 -16.9 -18.0 -19.5 -17.8	-16.4 -24.4 -27.7 -28.1 -27.0 -25.8 -25.3 -24.5 -21.5 -18.3	-20.9 -28.6 -31.2 -31.0 -29.7 -27.5 -24.7 -21.3 -17.0 -13.6	-20.8 -26.1 -27.7 -26.7 -24.4 -21.9 -18.9 -15.4 -12.7 -10.6	-16.0 -20.6 -24.0 -26.1 -24.6 -22.9 -18.5 -13.5 -12.0 -11.0 -9.9 -7.8 -6.2 -1.2 -1.2 -1.2 -1.2 -1.2 -1.2 -1.2 -1	-14.6 -17.5 -20.2 -21.7 -21.6 -21.0 -19.8 -17.4 -14.4 -11.3 -9.5 -8.7 -8.4 -8.7 -8.4	

TABLE I	(contin	ued)					PRESS	SURE CO	XXX INA	TES								
JUNE	ZONAL	MEAN	TEMPER	ATURE	(K)													
SCALE HEIGHT	PRESSURE (mb)	-80	-70	-60	-50	-40	-30	-20	-10	O	10	20	30	40	50	60	70	80
12.0 11.5 11.5 10.5 9.5 9.0 6.5 6.5 5.5 5.5 4.0 2.5 2.5 2.0 0.5	0.0062 0.0105 0.0169 0.0279 0.0464 0.1250 0.2061 0.3398 0.5605 1.52 2.51 1.52 2.51 1.25 18.55 30.9257 1.709 226.03 372.66 614.42	241.1 248.4 257.7 265.4 267.9	247.9 256.3 263.1 266.0 262.2	241.0 248.0 253.9 257.9 259.8 258.4	214 6 218 5 223 3 235 7 241 7 251 4 253 8 254 4 249 8 254 6 260 6 212 9 214 7 206 6 8 209 5 212 9 215 7 215 7 215 7 215 7 215 7 215 7 216 4 260 2	225.7 232.4 238.5 243.3 248.7 253.7	215.3 223.6 233.2 241.4 248.9 256.9	207.2 215.7 228.0 239.5 249.9 259.6	204.7 212.6 225.2 239.7 252.0 261.2	204.6 212.8 226.0 240.3 252.4 261.3	206.6 214.6 226.9 240.7 251.5 260.4	208.8 215.9 226.8 239.3 250.0 259.8	209.1 216.4 226.4 238.6 250.2 260.7	208.1 217.9 229.1 240.5 251.8 262.4	208.2 219.4 231.5 244.0 256.2 267.0	208.6 221.9 235.0 247.7 259.7 270.1	207.4 222.3 235.9 249.7 263.3 274.1	206.4 222.2 236.3 251.0 265.8 277.4
JUNE	ZONAL	MEAN	GEOPOT	ENTIAL	HE I GH	T (m)												
SCALE HEIGHT	PRESSURE (1b)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
12.0 11.5 11.0 10.5 10.0 9.5 9.0 7.5 9.0 6.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5	0.0062 0.0169 0.0279 0.0460 0.02758 0.1250 0.2061 0.3590 0.5603 0.9237 1.52 2.51 4.14 6.83 11.25 18.55 30.59 90.43 83.15	75799 72439 69028 65542 61957 58254 54416 50504 46615 42854 39283 35871 326454 26848 24199 21481 116830	76616 73300 69915 66443 62866 59176 55367 51488 47614 43842 40240 36793 33528 30457 27595 24834 22009 19107 16160	77260 73977 70597 67121 63537 59862 56110 52317 44780 41195 37769 34538 31476 28535 25631 22671 19650	80746 77574 74341 71026 67623 64125 60548 56895 53194 49468 42182 38755 335526 32439 29410 20149 173859	78055 74917 71713 68447 65091 61643 58113 54512 50829 47098 43391 39816 33184 29993 26811 23618 20441 17291	78469 75449 72389 69276 66063 62719 59240 55651 51944 48144 44328 40595 37024 33594 30256 26967 23728 20753 17454	78602 75640 72656 69645 66954 63309 59880 56298 52561 48714 44833 41013 33769 30350 27024 23773 20612 17569	78608 75639 72680 69706 66654 63456 60046 52680 48821 44949 41136 33814 30348 27004 23762 20615 17601	78637 75656 72686 69710 66653 63445 60026 55419 52652 48797 44930 41116 333781 30314 26974 23736 20598 17593	78711 75743 72770 69771 66690 63464 60034 56428 52673 48820 44944 41125 33809 30349 27005 237610 17600	78906 75951 72962 69932 66825 63590 60172 56389 48992 45085 41237 335915 30449 27087 23822 20656 17617	79112 76208 73247 70224 67108 63872 60464 56886 53141 49265 45327 41433 30553 27179 23904 20718 17631	79309 76556 73685 70701 67580 64310 60868 57266 49598 45621 41670 374186 30671 27275 23984 20766 17606	79781 77131 74317 71349 68217 64919 61434 57774 53936 49975 45951 41950 38072 30799 27381 24066 20803 17563	80288 77753 75005 768898 65556 62018 58305 54420 50412 46335 42278 33544 34569 30971 27513 24160 17540	80756 78281 75580 72660 72660 69508 66156 62597 58842 54901 50832 46695 42586 334774 31135 27643 24254 24254 217533	81091 78656 75987 73089 63943 66589 63017 59235 55251 51130 46944 42795 384936 31280 27761 24335 17536
JUNE	MEAN	ZONAL	MEAN G	EOSTRO	PHIC W	IND (m	s ⁻¹)											
SCALE HE IGHT	PRESSURE (mb)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
12.0 11.5 11.0 10.5 9.0 8.5 7.5 7.5 6.0 5.5 6.0 5.5 4.5 3.5 3.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5	0.0062 0.0109 0.0169 0.0279 0.0460 0.1250 0.2061 0.3398 0.5603 0.9237 1.52 2.51 4.14 6.83 11.25 18.55 50.59 50.43		41.4 45.6 48.3 49.6 50.6 51.8 59.0 61.9 62.3 62.0 61.8 62.3 54.4 45.9 38.5 31.8 25.2	33.0 34.6 36.1 37.9 46.1 52.3 58.0 61.4 63.6 68.9 70.2 65.5 55.7 37.7	27.6 33.1 40.1 48.5 57.9 67.4 76.7 84.8 89.2 85.6 80.0 74.4 67.1	102.6 113.7 121.9 127.1 127.5 121.8 109.4 92.8 74.0 55.7	33.7 45.1 59.3 75.6 92.5 105.7 112.2 113.3 109.6 90.1 74.2 54.6	55.6 51.0 47.2 41.7 30.7 16.4 6.1 2.1 2.3 5.1				-33.5 -38.1 -38.7 -36.5 -34.2 -34.3 -37.4 -40.7 -41.7 -39.8 -34.4 -27.9 -23.1 -20.1	-28.1 -39.3 -45.8 -48.1 -47.1 -44.9 -43.5 -42.5 -40.4 -38.2 -33.7 -27.0 -21.1 -16.6	-35.4 -46.5 -52.5 -54.1 -51.6 -48.3 -44.4 -39.2 -34.1 -29.5 -24.4 -19.0 -11.4 -9.3 -7.5 -3.4	-49.8 -51.7 -50.5 -47.7 -43.9 -39.7 -35.6 -31.9 -28.3 -24.2 -19.3 -15.0 -11.7 -9.4 -7.0	-36.4 -42.9 -47.2 -49.0 -48.1 -45.7 -32.0 -35.4 -32.0 -28.2 -24.2 -19.9 -15.8	-28.1 -30.9 -33.0 -34.3 -34.2 -33.3 -31.7 -29.2 -25.7 -21.5 -17.8 -15.0 -13.0	

TABLE	(contin	(beu					PRES	SURE CO	OORDINA	ATES								
JULY	ZONAL	MEAN	TEMPER	ATURE	(K)					TITUDE					1 20			
SCALE HEIGHT	PRESSURE (mb)		-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
12.0 11.5 10.0 9.0 8.5 9.0 7.5 6.5 5.0 4.0 2.5 2.5 2.5 0.0	0.0103	222.2 226.3 231.9 239.8 250.4 261.8 273.1 266.0 256.6 236.9 222.3 204.4 185.1 178.0 187.0	217.3 219.9 224.0 229.6 237.0 246.3 256.7 265.5 269.7 266.6 258.9 239.9 239.9 225.2 208.5 192.3 186.7 192.5 195.0 197.2 200.5 3 205.8 220.4 243.0	218.8 223.07 228.7 235.2 249.8 256.8 262.1 263.7 258.8 250.3 225.3 211.5 200.7 1201.3 205.3 207.3 210.0 224.3	216,4 220,1 224,6 229,6 235,1 240,9 247,1 253,3 257,8 256,9 249,7 238,0 210,0 210,0 210,2 212,3 211,3 211,3 211,3 211,8 214,2 215,1 225,1	210 5 214 1 217 2 220 5 226 3 232 5 238 4 246 5 259 9 254 9 254 9 254 9 257 2 20 4 223 7 218 6 215 3 214 7 215 3 217 3 218 3 219 3 219 3 219 3	205, 4 208, 0 210, 8 214, 2 220, 1 227, 9 236, 9 247, 0 257, 6 263, 2 260, 4 251, 0 239, 7 231, 5 227, 3 219, 5 210, 0 222, 4 242, 8 267, 8	202.1 204.5 206.6 209.8 217.2 227.4 237.9 249.3 260.4 265.7 263.1 254.9 245.2 236.5 229.5 229.5 224.2 205.3 212.7 204.2 205.3 212.7 204.2 205.3 212.7 204.2 205.3 212.7 204.2 205.3 212.7 204.2 205.3 212.7 204.2 205.3 212.7 207.3 212.7 207.3 212.7 207.3 212.7 207.3 212.7 207.3 212.7 207.3 212.7 207.3 212.7 207.3 212.7 207.3	201, 7 203, 5 205, 5 208, 8 216, 5 227, 8 240, 5 252, 5 262, 1 265, 4 262, 3 255, 4 262, 3 257, 4 201, 9 211, 4 201, 9 203, 0 224, 9 252, 5	201.9 203.0 204.9 208.9 217.4 229.5 242.2 254.0 262.4 264.1 255.3 248.1 239.3 229.4 223.1 217.3 210.3 201.3 203.0 225.9 25.9	202.7 203.6 205.8 209.9 217.6 228.9 242.6 253.1 261.0 264.4 238.2 241.1 254.3 246.4 238.2 241.1 254.3 246.4 238.2 240.2 253.8 217.9 211.1 201.8 203.4 225.7 253.1 203.4 225.7 253.1	202 7 204 7 206 7 216 6 227 5 239 9 250 2 258 9 264 7 265 5 238 7 230 4 224 6 219 0 212 6 203 7 205 7 205 7	198.7 202.4 205.7 209.0 215.4 225.4 237.8 248.6 265.2 265.0 249.0 240.2 232.0 240.2 232.0 240.2 232.0 240.2 232.0 240.2 232.0 240.2 232.0 240.2 232.0 240.2 232.0 240.2 232.0 240.2 232.0 240.2 240.2 250.5 250.2 250.5	188 9 195 8 202 2 215 8 225 8 238 3 249 8 259 9 267 4 252 8 243 1 234 6 222 4 217 8 212 8 213 8 212 8 213 8 225 9 227 4	175.9 185.9 196.6 207.4 218.2 229.4 242.0 253.8 271.8	165-3 177-7 191-5 205-9 220-0 223-3 33-246-4 258-7 274-8 276-3 271-6 262-1 251-3 241-0 232-5 227-8 226-6 225-5 227-8 226-6 225-5 225-5 226-6 225-5 226-6 225-5 226-6 225-5 226-6 225-5 226-6 225-6 226-6 225-6 226-6 225-6 226-6 2 2 2 2	100.5 174.0 189.2 204.9 220.7 236.0 250.2 263.1 279.7 280.5 275.4 265.6 254.5 234.9 230.5 230.0 230.0 229.1 227.9 227.4 237.6	172.7 188.3 204.7 221.2 237.3 252.2 265.8 283.7 283.8 277.5 267.2 255.4 244.6 8 233.0 232.5 230.7 229.6 235.9 260.4
JULY	ZONAL	MEAN	GEOPOT	ENTIAL	HEIGH	T (m)												
SCALE HEIGHT	PRESSURE (mb)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
12.0 11.5 10.5 10.0 9.0 8.5 9.0 7.5 5.0 4.5 4.5 3.5 2.5 2.0	0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603	75990 72709 69363 665903 665903 58565 54657 50665 446714 42889 39212 35667 32305 24330 23689 21031 18299 15521	79809 76608 773600 70039 66626 63086 55576 51651 43864 40142 36550 33146 29964 27040 24278 21503 11665 15793 12886	77352 74119 70811 67417 63920 60319 56606 52805 48948 45114 41388 37793 34390 28178 25275 22359 16407	77732 74537 71280 67957 64552 61069 57494 53830 50081 46304 42592 39013 35627 32407 29303 26230 23134 20030 16927	78075 74967 71807 68604 65332 61973 58525 54980 51299 47517 43739 40084 36617 33287 30039 26817 23607 20427 17280	78411 75385 72317 69207 66027 62750 59345 55806 52105 48286 44445 40692 37103 33656 30301 26995 23750 20569 17461	78632 75654 72643 69596 66471 63218 59899 56246 48648 44769 40968 37309 33781 30373 27049 23800 20633 17580	78705 75740 72740 669720 66607 63360 59927 56314 48675 44806 41010 37333 33776 30347 27022 23789 17615	78712 75744 72754 669724 66603 63340 59885 56255 48607 44754 40969 37290 33724 30297 26982 23758 20622 17605	78724 75750 72753 69713 66584 63321 59863 56231 52461 48608 44756 40978 37314 33763 30338 27016 23783 20639 17616	78776 75793 72781 69734 66615 63370 59943 56353 52619 48781 44906 41100 37432 33875 30444 27112 23865 20702 17653	78895 75958 72967 66932 66826 63605 60210 56645 52924 49085 41356 37644 34060 30607 27249 23979 217706	79143 76328 73411 70407 67302 64074 60672 57099 53362 49498 45567 41672 37901 34268 30773 27386 24091 20868 17716	79567 76922 74117 71161 68041 64768 61314 57685 53891 49975 42044 38206 34506 30951 27520 24192 20920 17682	80084 77577 74870 71965 68841 65524 62007 58311 50461 46419 42397 38490 38490 38490 212660 24295 20970 17660	80639 78195 75532 72651 69529 66188 62623 58867 54936 46779 42700 38739 34927 31288 27785 24384 21016 17654	81062 78642 75994 75121 69996 66643 63052 59261 55282 51174 47011 42893 38905 31420 27894 24459 17655
JULY	MEAN	ZONAL	MEAN G	EOSTRO	PHIC W	IND (m	s ⁻¹)											
SCALE HEIGHT	PRESSURE (mb)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
11.5 11.0 10.5	0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1256 0.2061 0.3590 0.5603 0.9237 1.522 2.51 4.14 6.83 11.25 18.55 50.59 50.43 83.15		44.2 46.4 49.8 55.1 61.9 68.4 71.5 71.1 69.3 67.5 65.7 62.9 56.9 49.1 36.9	45.5 49.5 55.7 64.4 73.7 80.8 85.3 86.9 89.0 89.1 83.7 72.5 60.1 41.3	24.2 29.0 34.8 42.4 51.5 61.5 72.6 83.5 90.9 93.5 92.1 90.3 88.2 73.6 60.9 49.3	36.3 45.1 54.8 65.6.9 87.2 95.4 101.2 103.0 100.1 92.7 82.8 71.3 59.1 46.2 34.7 27.9 24.7	36.3 44.5 53.7 63.3 78.3 80.3 78.9 69.9 63.1 53.6 41.3 15.7 11.6 12.8	37.6 44.4 49.9 51.8 48.2 40.7 32.7				-15.3 -14.8 -14.7 -16.9 -21.2 -27.8 -34.8 -40.0 -42.0 -39.2 -33.9 -29.5 -26.3 -24.0 -20.9 -17.6 -13.9	-20.3 -30.3 -36.2 -39.1 -40.4 -42.2 -44.4 -46.0 -45.9 -44.4 -40.8 -35.2 -28.8 -23.8 -19.9 -16.5 -13.7	-31.9 -46.7 -56.1 -59.9 -59.1 -56.4 -53.2 -50.0 -46.7 -43.0 -38.7 -33.2 -27.1 -21.6 -16.6 -12.9 -10.1	-23.2 -38.1 -50.5 -58.8 -62.7 -61.9 -53.5 -48.3 -22.9 -38.2 -23.4 -18.2 -14.0 -10.8 -8.1 -4.0 9.8	-38.3 -45.0 -49.7 -51.9 -49.0 -45.1 -40.8 -36.2 -31.8 -27.5 -23.1 -18.7 -14.7 -9.3 -6.8	-31.9 -35.3 -37.7 -39.3 -39.5 -38.1 -35.3 -31.8 -27.7 -23.3 -19.1 -15.9 -13.3 -11.2 -9.6 -7.6	

TABLE	(contin	ued)					PRES	SURE O	OORDIN	ATES								
AUGUST	ZONAL	MEAN	TEMPER	ATURE	(K)													
SCALE HEIGHT	PRESSURE (mb)	-80	-70	-60	-50	-40	-30	-20	-10	O O	10	20	30	40	50	60	70	80
12.0 11.5 10.5 10.5 10.0 9.5 9.5 6.5 7.5 6.5 5.6 6.5 5.6 6.5 5.6 6.5 5.6 6.5 6.5	0.0103 0.0169 0.0279 0.0460 0.0758 0.1250	219.8 222.5 226.4 233.2 243.4 255.5 267.8 267.1 269.0 249.8 234.9 215.7 192.7 1192.7 1192.7 1193.0 1186.2 1188.3 1190.9 1195.0 202.0 2017.5	216.6 219.3 221.4 224.2 229.0 236.3 246.1 257.8 267.6 270.5 268.0 262.2 254.7 241.3 203.7 191.5 194.7 196.0 198.0 198.0 204.7 220.8 243.8	219.7 222.3 224.9 227.7 231.4 237.1 245.8 255.7 262.7 262.7 264.2 260.4 253.7 241.8 227.5 204.5 204.5 204.5 204.5 204.5 204.5 204.5 204.8 205.4 206.4 209.4	216.6 220.0 222.8 225.2 228.5 237.3 237.3 237.6 245.6 257.8 227.6 219.6 219.6 211.3 211.3 211.3 215.5 229.8 227.6 215.6 215.6 215.6 216.6 217.6	211 9 215 7 218 8 220 9 224 2 228 1 253 0 241 7 252 1 258 3 247 8 238 3 247 8 238 3 247 8 220 1 222 8 220 1 2217 3 216 2 216 2 215 4 253 4	208.2 211.7 214.7 217.1 220.9 226.3 245.1 256.3 262.5 262.5 262.2 242.2 228.7 224.9 220.3 215.7 210.7 211.7 211.7 212.8	205.3 208.4 211.1 214.1 219.6 227.2 236.5 260.5 265.5 265.5 257.1 246.9 237.5 229.4 224.3 219.0 213.1 205.4 224.4 224.4 224.4	202.7 205.1 208.1 211.9 218.8 228.6 239.9 252.5 263.1 267.9 266.0 258.7 248.6 238.6 229.7 223.3 217.4 211.9 202.3 203.0 224.7 252.3	202.9 204.5 207.7 212.7 220.5 230.5 241.9 254.1 264.0 267.4 265.3 258.3 248.6 228.9 222.4 216.4 211.2 202.0 203.0 225.1 252.1	204 .4 206 .0 209 .4 214 .7 222 .1 231 .5 242 .7 253 .0 262 .2 266 .5 264 .0 256 .7 247 .3 237 .9 229 .4 222 .7 216 .8 211 .3 202 .1 203 .3 225 .6 255 .6 255 .7 247 .3 257 .9 258 .7 258 .7 268 .7 26	205.1 207.6 211.0 215.6 222.7 232.1 242.3 250.2 258.2 264.8 263.9 255.6 246.4 238.2 229.8 229.8 229.8 217.8 212.4 205.7 205.0 226.6 255.5	203.6 207.3 210.9 215.1 221.6 230.3 239.8 248.0 256.8 263.3 265.3 265.3 265.3 265.3 247.0 238.3 247.0 238.3 247.0 252.2 219.6 214.5 207.9 227.0 252.8 277.1	196.4 202.3 208.0 213.8 220.3 228.4 238.3 247.6 256.8 265.3 259.7 250.1 240.2 252.5 221.5 221.5 221.5 217.5 217.5 217.5 213.0 225.8 247.6	186.8 194.9 203.7 212.2 220.9 229.7 239.6 249.6 259.5 267.7 261.8 252.8 243.9 223.7 221.6 228.3 223.7 221.6 219.4 244.4 244.4 243.6 268.9	177 .8 187 .6 199 .3 211 .8 223 .5 234 .5 254 .1 262 .8 269 .1 270 .3 264 .6 255 .4 246 .3 270 .2 270 .2 270 .2 270 .3 264 .6 255 .4 246 .3 257 .2 229 .8 225 .8 225 .8 225 .8 225 .1 224 .5 223 .7 224 .5 224 .5 224 .6 225 .8	174 0 184 9 197 5 210 9 224 9 238 4 249 7 258 7 266 3 272 2 272 8 266 9 257 5 247 7 238 3 230 9 227 6 227 8 227 8 227 8 227 8 227 8 227 8 227 8 227 8	174.3 185.6 198.4 212.1 226.7 241.5 253.2 269.7 275.3 274.7 267.9 238.8 229.8 229.8 229.8 229.8 229.8 229.2 227.9 234.0 228.1
AUGUST	ZONAL	MEAN	GEOPOT	ENTIAL	HE I GH	T (m)												
SCALE HEIGHT	PRESSURE (mb)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
12.0 11.5 11.5 10.0 9.0 8.5 6.0 5.5 6.0 5.5 4.5 4.5 4.5 2.0	0.0062 0.0169 0.0169 0.0279 0.0469 0.1250 0.2061 0.3398 0.5603 1.52 2.51 4.14 6.83 11.25 18.55 50.59 50.43 83.15 137.09	76624 73386 70101 66740 63248 59601 55763 51778 47752 43788 39937 36206 32656 29348 26363 23660 20992 18246 15470	80517 77323 74096 70834 67520 64112 60585 56892 53042 45145 41262 37473 33842 30426 27301 24420 21604 18755 15896 13007	77898 74661 71386 68072 64711 61284 57748 54077 50273 46409 42564 38795 35166 25460 22465 19469 16473	78085 74889 716486 66364 66364 665042 61668 58228 54693 51031 47279 43514 39821 36266 29589 26400 23246 20111 16985	78311 75181 71996 68777 62206 58831 55360 51739 47999 44224 40526 36970 33538 30210 26930 23689 20485 17314	78665 75591 72467 69306 66098 62826 59453 55948 52270 48467 44625 40859 37243 33756 30371 27047 23791 17475	78975 75945 72871 66759 66584 63316 59920 56374 52640 48773 44866 41031 37345 337345 30381 27060 23816 20649 17590	79016 76033 73006 69933 66780 63509 60077 56475 52691 48797 44881 41032 37321 33752 30329 27011 23787 20642 17607	79045 76059 73035 669955 66781 63483 60023 56397 52599 48705 44799 40960 37253 33685 30266 26959 237519 17591	79099 76097 73056 69954 66756 63440 59964 56335 52555 48677 44787 40967 37278 33725 30305 26995 23780 20644 17616	79127 76106 73041 669921 66712 63387 59910 56303 52578 48745 44865 41051 37381 37381 37382 30407 27088 23859 17660	79143 76134 73071 69954 66757 63452 60006 56434 52735 48918 45050 41238 37555 34000 30568 27227 23973 20794 17709	79191 76273 73266 70180 67001 63720 60300 56742 53046 49228 45341 41489 37757 34165 30708 27348 24072 20857 17709	79397 76605 73684 67467 64170 60732 57152 53421 49562 45637 41753 37987 34348 30840 27442 24137 27649	79740 77068 74236 68034 64683 61174 57524 49838 45882 41955 38149 34472 30935 27516 24186 20887 17595	80149 77526 74723 71737 68542 65152 61571 57849 54002 50056 46059 42099 38261 34558 31004 27569 24218 20887 17554	80576 77946 75136 68912 65486 61857 58084 50192 46159 42178 38328 34520 31061 27615 24243 20884 17519
AUGUST	MEAN	ZONAL	MEAN G	EOSTRO	PHIC W	IND (m	s ⁻¹)											
SCALE HEIGHT	PRESSURE (mb)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
12.0 11.5 11.5 10.5 10.5 9.0 8.5 7.5 6.0 5.5 4.5 4.5 3.5 3.5 2.5	0.0062 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603 1.52 2.51 4.14 6.83 11.25 18.55 30.59 50.43		39.6 39.8 40.0 40.6 47.6 55.8 66.4 77.3 84.9 88.3 84.5 79.6 71.2 58.8 47.7 39.4 31.7 25.1	25.1 25.8 25.8 26.3 28.2 32.6 40.9 52.0 62.9 71.0 85.1 86.6	16.4 19.8 23.4 27.5 32.3 39.0	32.0 38.0 43.7 49.3 54.7 59.4		21, 1 28, 9 38, 4 48, 0 56, 6 61, 4 60, 8 54, 3 44, 7 34, 8 20, 5 13, 4 5, 0 -2, 1 -5, 1 11, 8 25, 1				3.3 3.6 3.3 1.0 -4.3 -12.3 -18.8 -21.6 -22.9 -24.1 -24.4 -23.3	-1.6 -7.0 -10.1 -12.1 -14.3 -17.7 -22.2 -26.2 -28.6 -29.7 -29.4 -27.0 -23.2 -20.7 -18.5 -15.9	-14.9 -25.8 -32.7 -36.2 -37.0 -37.1 -36.2 -34.4 -32.1 -29.2 -25.5 -21.1 -16.8 -12.8	-11.5 -22.9 -32.5 -39.0 -41.3 -38.6 -35.1 -51.5 -27.8 -24.6 -21.7 -15.7 -15.7 -12.3 -9.0 -6.7 -4.6	-22.4 -28.0 -32.0 -34.1 -33.8 -31.1 -26.8 -22.4 -18.6 -15.9	-29.8 -32.5 -34.2 -34.9 -33.8 -30.5 -25.2 -20.0 -15.8 -12.6	

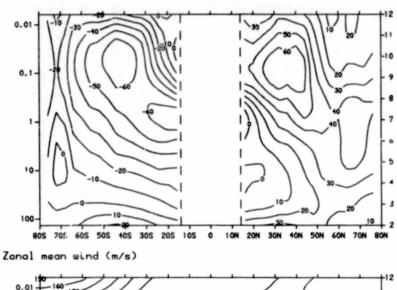
TABLE	(con rin	(beu					PRESS	SURE CO	XXXX	ATES								
SEPTEME	BER ZONAL	MEAN	TEMPER	ATURE	(K)													
SCALE HEIGHT	PRESSURE (mb)	-80	-70	-60	-50	-40	-30	-20	-10	O	10	20	30	40	50	60	70	80
12.0 11.5 11.0 10.5 9.0 8.5 9.0 6.5 6.5 5.5 5.0 2.5 2.5 2.5 0.0	0.0062 0.0103 0.0169 0.0279 0.0460 0.1250 0.1250 0.5603 0.5603 0.5603 1.52 2.51 1.52 2.51 1.53 1.53 1.53 1.53 1.53 1.53 1.53 1	209 .1 214 .1 217 .7 222 .2 227 .8 234 .9 258 .7 277 .8 277 .8 277 .9 275 .3 271 .5 259 .5 240 .6 215 .9 198 .5 197 .7 194 .4 196 .1 202 .8 218 .4 240 .2	209.4 214.9 219.0 222.9 227.1 232.0 239.2 249.9 261.7 268.3 271.1 257.4 242.2 267.2 249.9 249.9 207.1 1202.3 199.9 205.1 200.1	208.8 215.8 225.5 228.6 225.5 231.6 242.0 256.4 256.4 256.4 256.4 262.8 258.3 249.7 210.5 207.4 210.3 225.0 249.3 249.3	206.5 212.4 219.1 224.3 227.5 230.6 234.1 238.2 245.4 253.5 250.6 241.4 252.3 225.1 219.7 216.9 215.6 216.8 230.5 255.6	205.0 209.9 215.3 220.2 224.0 227.7 231.6 236.6 244.8 254.5 260.4 258.8 250.6 241.2 232.5 262.1 218.7 217.0 220.8 256.1 286.1 286.1 286.1	204.3 207.8 211.7 215.7 219.4 224.1 229.6 236.4 257.8 264.3 263.4 255.2 245.2 236.5 224.7 220.4 215.7 220.4 215.7 220.4 223.0 243.5 243.0 243.5 243.0 243.5 243.0 243.5 243.0 243.5 268.7 290.9	204.4 208.4 211.4 211.4 211.5 7 221.4 228.1 256.3 267.5 260.5 267.5 260.5 260.5 260.5 240.3 230.9 224.1 218.4 212.6 204.4 205.4 205.4 209.9 249.9 249.9 249.9 249.9 249.9	205.4 205.5 206.1 208.2 212.0 219.1 228.1 228.3 250.9 262.5 262.2 252.3 241.6 231.1 223.9 217.0 211.1 201.5 202.6 252.1 252.5 202.6	207.0 205.9 207.8 211.9 228.2 259.6 252.2 263.3 269.2 268.9 262.3 251.9 240.9 230.8 2216.4 2110.4 201.0 202.5 225.6 257.6 200.0 202.5 203.6 203.	206,9 206,3 207,1 210,0 214,3 221,2 239,9 251,1 267,5 260,8 250,6 240,1 223,0 216,1 210,3 202,8 277,0 301,2	205.0 205.9 207.8 211.4 216.4 223.5 232.1 241.1 247.4 259.1 267.0 258.7 248.8 239.2 230.9 223.5 217.2 212.1 203.0 204.2 226.2 230.9 223.5 217.2 212.1 203.0 204.2 226.2	203.7 206.6 209.4 212.6 212.4 0 231.9 239.1 247.7 258.6 3247.7 256.3 247.7 218.7 218.7 218.7 218.7 218.7 217.2 225.6 238.1 230.0 256.3 247.2 238.1 238.1 238.1 238.7 218.7 218.7 218.7 218.7 218.7 218.7 218.7 219.0 219	201.8 205.2 208.7 212.0 216.0 221.9 229.2 237.3 246.7 257.7 255.4 263.6 256.7 246.9 227.3 230.0 224.0 212.5 212.7 223.5 212.7 223.5 246.9	198.0 202.0 206.6 211.2 216.0 221.6 229.0 257.3 264.6 263.0 255.7 246.3 229.7 224.1 1220.9 218.6 218.4 222.2 240.3 265.4	195.0 199.7 205.3 211.7 218.5 225.5 232.5 240.7 248.2 257.6 263.5 260.9 252.5 229.1 223.6 221.7 222.6 221.7 222.6 225.8 229.1	195,6 201,1 206,7 212,9 220,0 228,2 236,5 243,9 251,1 259,0 262,4 239,6 248,4 239,6 248,4 222,9 221,8 222,8 222,8 223,5 225,8	194.1 199.9 205.9 212.8 220.9 240.5 247.7 254.5 260.2 261.3 255.3 224.7 230.6 222.1 226.0 222.1 224.5 226.3 26.3
SEPTEM	BER ZONAL	MEAN	GEOPOT	ENTIAL	HEIGH	T (m)												
SCALE HEIGHT	PRESSURE (mb)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
12.0 11.5 11.0 10.5 9.0 9.0 7.5 8.0 7.0 6.5 6.5 4.0 5.5 3.0 2.0	0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603 0.9237 1.52 2.51 4.14 6.83 11.25 18.55	78295 75135 719136 68621 65233 61728 58038 54150 50113 46038 41987 37980 34089 30414 27077 24053 21162 18289 15452	78379 75202 71965 68671 65310 61863 58281 54537 50651 46697 42731 38791 34947 31278 24736 21748 18891	78547 75344 72067 68741 65370 61951 58453 54853 51124 47300 43442 39620 32334 28946 25716 22601 19537 16498	78688 75531 72279 68972 65619 62216 58758 55222 51565 47811 44024 40295 36694 33223 29879 26607 23373 20175 17009	78900 75788 72596 69343 66035 62673 59246 55727 52066 48291 44481 40745 33676 30326 27030 237632 17345	79103 76032 729016 669716 66469 63148 59737 56203 48676 44804 40998 3733810 30405 27082 23625 17507	79228 76191 73116 69992 66790 63501 60101 56560 52829 48961 45036 41161 37422 33826 30380 27049 23812 20654 17600	79211 76198 73164 70091 66935 63664 60248 56672 52905 49011 45070 41176 2137411 33791 30336 27005 23780 17620	79194 76179 73145 70067 66905 63628 60198 56605 52827 48926 44982 41089 37388 33718 30268 26944 23730 17593	79232 76208 73155 70052 66864 63561 60117 56526 52759 48871 44942 41066 373723 30282 26958 23747 20621 17603	79275 76249 73180 70051 66830 63498 60029 56439 52714 48857 44946 41097 373807 30367 27039 23815 20671 17630	79242 76197 73107 66963 66734 63397 59946 56366 52675 48823 44933 41116 37432 27129 23893 20721 17636	79100 76070 72986 69856 66650 63349 59931 55390 52695 48858 44977 41161 33928 30510 27186 23938 20738 17593	78967 75977 72916 669789 66585 63290 56324 52630 48803 44932 41126 33909 30493 27172 23917 17481	78947 75984 72929 69781 66529 63181 59714 56135 52429 48607 44760 40993 37363 37363 37363 3745 27126 23862 217370	31795 78889 75905 72832 69665 66382 62982 55839 52101 48276 44463 40752 37183 33724 30357 27060 23808 20555 17285	78860 75890 72822 69650 66340 62888 59310 55634 51862 48036 40574 37037 33611 30270 26990 23745 20492 17213
SEPTEM	BER MEAN	ZONAL	MEAN G	EOSTRO	PHIC W	IND (m	s ⁻¹)											
SCALE HE IGHT	PRESSURE (mb)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
	30.59 50.43		4.3 3.5 1.7 -0.9 -1.5 1.4 8.1 29.1 38.3 45.7 52.6 58.9 62.5 53.1 46.6 41.5 28.2	10.0	13.8 17.5 21.0 23.9 26.4 28.7 31.4 34.5 36.6 40.4 43.7 48.3 52.3 54.0 51.7	28.5	23.3 28.5 36.2 44.4 51.0 55.5 56.9 44.8 37.0 27.7 17.9 9.3 3.1	9.7 18.3 28.1 36.4 40.3 36.7 31.2 25.7 20.5 13.5 4.9 -2.7 -4.9				-1.7 -3.0 -0.2 3.9 8.0 12.0 15.6 16.3 7.7 4.3 -4.8 -9.9 -15.1 -15.4 -13.3 -9.1 -2.7 4.3	12.4 12.7 13.6 13.8 13.0 11.2 7.9 4.6 2.5 1.0 -1.1 -3.4	19.8 16.0 13.1 11.2 9.6 7.3 3.9 1.5 -0.3 -1.9 -2.0 -1.9 -2.1 -2.2 -2.0 -1.1 1.5 7.9	0.9 0.1 1.1 3.3 5.5 7.7 9.2 9.6 8.9 7.7 6.0	2.4 1.6 1.4 1.8 3.3 6.0 9.8 13.3 15.9 17.6 17.5 12.3 8.8 6.1 4.6 3.9 4.0 7.1	3.9 4.1 4.8 5.6 6.7 9.0 12.8 20.4 22.9 23.2 21.1 17.5 13.3 9.1 4.5 4.0 4.7 5.8	

TABLE I	(contin	ued)					PRES	SURE C	OORDIN	ATES								
OCTOBER	ZONAL	MEAN	TEMPER	ATURE	(K)													
SCALE HEIGHT	PRESSURE (mb)	-80	-70	-60	-50	-40	-30	-20	-10	TI TUDE 0	10	20	30	40	50	60	70	80
12.0 11.5 11.0 10.5 10.0 9.5 9.5 9.5 7.5 7.0 6.5 5.5 5.0 4.5 4.5 4.5 4.5 2.5 2.5 2.5 2.0	0.0062 0.0105 0.0169 0.0276 0.0261 0.2061 0.3398 0.5605 0.9237 1.52 2.51 4.14 6.83 11.25 18.55 30.59 50.43 18.25 30.59 50.43 18.25 1	217 6 226 2 232 2 238 4 249 8 263 5 273 3 281 6 284 2 283 8 255 0 217 0 212 7 207 7 207 7 207 7 205 7	190 .1 199 .9 209 .8 219 .1 227 .0 232 .6 238 .1 247 .1 258 .1 267 .2 275 .1 277 .2 275 .2 27	220 8 227 6 232 9 238 2 244 5 252 7 261 8 269 2 269 7 242 6 231 8 226 9 224 1 3 214 0 213 3 214 3	219 .5 226 .1 232 .0 237 .4 242 .8 250 .7 266 .2 266 .1 236 .2 227 .2 227 .2 225 .1 223 .9 218 .7 218 .2 218 .2 218 .2	216.9 229.2 235.5 241.0 249.1 260.1 267.4 266.3 258.2 247.2 235.5 224.0 222.2 216.9 217.0 221.2	213 8 219 4 226 11 233 0 239 6 248 6 260 2 268 5 267 9 259 7 249 2 240 1 210 2 211 0 222 9 244 5	209 8 215 6 2222 7 230 1 237 8 248 0 260 1 268 9 268 8 262 0 252 4 242 4 232 6 224 7 218 2 211 9 203 5 204 9 224 6	207 5 210 9 218 1 227 6 238 4 250 2 261 5 268 7 268 8 253 4 254 0 232 2 244 0 232 2 244 5 217 1 210 5 201 6 225 4	208 0 209 5 215 7 225 9 238 4 251 5 262 8 269 1 269 2 263 8 254 3 232 8 224 0 199 6 201 2 225 9	209 7 211 5 217 5 227 0 238 3 250 7 262 2 268 6 268 5 262 7 253 3 243 0 232 9 244 1 216 7 210 7	211.3 214.5 221.2 230.1 239.1 249.8 260.8 267.2 266.7 250.1 240.5 231.8 224.4 217.7 211.4 202.0 203.2 225.4	213.4 217.0 224.0 231.9 238.8 248.6 260.4 266.9 264.1 255.6 245.8 236.7 228.9 223.5 218.6 206.4 207.3 223.6 248.6	215.5 218.7 223.9 230.9 239.0 248.5 258.9 264.6 251.7 241.8 232.8 225.7 221.4 218.5 215.2 212.1 212.6 220.8 242.0	218 5 221 4 225 4 231 5 239 8 248 1 259 9 255 8 246 9 237 2 222 4 217 8 217 8 217 9 217 1 220 2 236 9	225.1 226.6 231.0 236.3 242.4 247.9 255.0 256.4 249.5 239.3 216.3 216.3 216.9 218.5 219.5 219.5 220.0 220.7	225 9 236 0 242 0 246 6 250 6 255 4 253 1 242 8 230 5 221 3 216 7 217 0 219 4 221 0 220 7 228 0	228.5 233.9 248.0 251.9 254.3 250.6 237.9 224.2 214.3 210.6 211.1 10.2 2:2.1 218.5 220.9 220.9 224.9
OCTOBER	ZONAL	MEAN	GEOPOTE	ENTIAL	HEIGHT	(m)												
SCALE HEIGHT	PRESSURE (mb)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
11.5 11.0 10.5	0.0062 0.0103 0.0169 0.0279 0.0460 0.2061 0.3398 0.5603 1.52 2.511 4.14 6.63 11.25 18.55 18.55 18.55 18.55 18.55	79766 76791 73670 67059 63618 60044 56290 52358 48291 44143 39980 35024 28452 25157 22020 18938	82653 79795 76798 73653 70387 67018 63575 60022 56326 52478 48504 44454 40404 36442 32652 225766 22558 19421 16359 13319	79745 76718 73544 70260 66886 63438 59903 56266 52497 48605 44651 40736 33309 29842 26488 23184 16810	79554 76541 73385 70121 66764 63327 59810 56201 52460 48606 44698 40849 37152 33610 30225 26917 23628 20375 17167	79546 76518 73387 70168 66855 63453 59963 56380 44864 41015 33776 30398 27101 23834 20601 17412	79509 76477 73380 70211 66947 63586 60124 56555 52826 48951 45014 41142 33842 30413 27086 23831 27086 17530	79367 76342 73293 70181 66970 63657 60230 56679 52954 9076 45131 41237 33845 30371 27023 23783 20632 17590	79244 76200 73167 70107 66967 63707 60293 52966 49080 45137 41233 337441 33783 30302 26959 23729 20597 17590	79256 76175 73119 70058 66936 63698 60292 52943 49046 45099 41190 37396 33738 30251 26907 23686 17563	79278 76195 73195 70045 66907 63657 60248 56672 52908 49017 41179 433763 30281 26934 23710 20584	79267 76212 73134 70020 66832 63531 60093 56517 52772 48901 44984 41119 333792 30338 26995 23761 20618 17591	79150 76079 72972 69823 66596 63258 59809 52513 48645 44750 40938 37271 33736 30330 27018 23784 20621 17549	78860 75756 72617 69441 66200 62872 59431 55865 52145 48304 44449 40689 37079 33602 30249 26977 23757 20580 17452	78461 75313 72131 68911 65641 62300 58847 55276 47791 44009 40321 36782 33375 30080 26848 23649 17285	78174 74984 71739 68448 65097 61679 58172 54582 50897 47142 43435 39850 36416 33093 29861 26680 23510 20324 17118	77847 74588 71298 67962 64548 61049 57468 53829 50121 46384 42751 39280 32775 29611 26472 23339 16983	77614 74314 70988 64127 60544 56879 53172 49430 45705 42129 38742 38742 29346 26263 23173 16871
OCTOBER			MEAN G															
SCALE HE I GHT	PRESSURE (mb)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
11.5 11.0 10.5 10.0 9.5 9.0 8.5 8.0	0.0062 0.0103 0.0169 0.0279 0.0450 0.1250 0.2061 0.3598 0.5603 0.9237 1.52 2.51 4.14 6.83 11.25 18.55 30.59 50.43 83.15		2.2 0.2 -1.9 -3.3 -4.0 -4.4 -3.2 0.8	-13.3 -13.9 -14.2 -13.6 -13.2 -12.0 -8.9 -5.2 -1.0 4.1 11.4 21.4 30.9 37.7 40.2 39.0 35.3 29.1 22.5	-3.1 -5.3 -5.3 -5.3 -0.9 1.4 3.0 4.6 6.4 7.5 8.3 9.4 11.6 14.7 18.2 21.7 24.1 25.6 25.5 23.7 21.9	2.6 1.2 3.8 8.3 12.9 16.6 19.5 21.4	-6.6 -11.2 -10.7 -5.3 1.7 8.1 13.7 17.7 19.8 20.2 19.6 17.7 10.3 4.6 -1.4 -4.8 -5.2 2.1 11.9 25.8	-25.1 -30.7 -30.9 -24.5 -13.9 -2.3 7.3 11.4 9.4 8.8 6.6 1.0 -5.8 -10.3 -11.6 -9.5 -4.4 5.0				14.9 8.6 7.1 10.5 17.0 25.9 35.0 39.3 38.2 35.3 32.8 21.1 11.3 2.1 11.3 2.7 9.7 2.2 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5	23.7 26.9 30.8 34.9 38.1 39.6 39.8 39.2 38.0 36.6 33.0	34.7 38.5 41.8 44.7 46.1 45.4 45.1	28.3 31.7 36.0 40.4 44.6 48.1 50.5 51.2 49.7 46.2 40.4	45.3 48.3 49.6 48.5 43.7 36.1	14.5 18.9 22.7 25.5 28.7 33.3 39.0 44.3 50.0 48.7 37.3 29.4 21.9 17.0 13.9 10.9 8.8 7.5 7.5	

T101 F 1 (200 B)	990	COURT COMPRIANTES	or roc	IN QUAL	LIII							
TABLE I (conflined) PRESSURE COORDINATES												
NOVEMBER ZONAL MEAN TEMPERATURE		LATITUDE										
SCALE PRESSURE -80 -70 -60 HEIGHT (mb)	-50 -40 -30	-20 -10 0	10 20	30 40	50 60	70 80						
12.0 0.0062 162.9 165.8 169.9 11.5 0.0103 174.1 177.1 181.4 11.0 0.0169 187.3 190.2 194.3 10.5 0.0279 201.6 204.0 207.1	177.1 188.0 198.1 186.8 194.3 201. 197.4 201.2 204. 207.3 208.6 208.	0 204.7 208.6 213.5 1 205.1 208.7 212.9 3 206.2 207.8 209.7 8 209.1 208.1 207.3	212.7 210.2 212.0 209.9 209.8 209.9 208.5 210.8	210.5 214.0 2 211.2 215.7 2 212.7 217.6 2 214.8 220.1 2	218.1 221.4 220.7 223.6 222.6 227.1 225.1 230.1	225.6 228.4 226.5 228.5 227.4 227.9 229.4 229.4						
10.0 0.0460 216.0 216.9 217.6 9.5 0.0758 227.4 227.1 226.3 9.0 0.1250 236.8 236.1 235.3 8.5 0.2061 250.0 247.9 245.2	216.8 216.1 215. 225.3 224.5 223. 234.6 233.4 231. 244.1 241.7 241.	0 204.7 208.6 213.5 1 205.1 208.7 212.6 5 206.2 207.8 209.7 8 209.1 208.1 207.3 2 214.0 211.5 208.5 0 221.6 219.0 215.6 7 230.9 230.0 227.6 1 240.5 242.1 241.8 0 250.0 252.4 253.5 9 261.1 261.2 262.4 5 270.5 267.6 267.0	209.7 212.8 216.4 219.5 227.6 229.8 241.1 240.3	217.7 223.3 2 224.2 227.8 2 232.2 233.1 2 240.0 239.9 2	228.2 233.3 231.9 237.4 236.5 241.5 243.1 246.5	232.9 233.1 238.1 238.9 244.7 246.8 251.2 254.1						
6,5 1,52 284,9 281,9 278,9	276.8 275.4 273.	1 270.3 267.9 266.9	266,9 267,1	263,3 257,5 2	248.9 243.2	240.0 237.3						
5.5 4.14 272.5 269.3 264.4 5.0 6.83 260.5 257.6 252.8 4.5 11.25 248.1 245.6 240.4 4.0 18.55 236.6 235.9 232.8	260.9 258.2 255. 247.6 244.3 243. 234.3 231.0 231. 228.5 224.8 224.	6 255.0 255.0 255.1 4 243.7 244.3 244.6 4 232.0 231.3 232.1 2 223.7 223.2 223.2	254.0 251.2 243.6 240.4 232.2 229.9 223.5 223.0	244.7 236.3 2 234.6 227.5 2 226.4 220.5 2 221.0 217.4 2	227.5 221.6 219.3 213.7 215.0 209.4 213.9 209.4	215.6 210.4 208.4 203.4 204.4 199.6 204.8 200.5						
3.5 30.59 235.8 254.4 229.7 5.0 50.45 235.7 252.0 228.2 2.5 83.15 228.9 228.0 225.5 2.0 137.09 221.8 222.4 221.8	226.2 221.8 219. 222.4 217.2 213. 220.9 215.0 208. 220.0 215.5 209.	3 217.8 216.8 216.2 0 210.5 209.4 208.6 0 202.0 198.6 197.9 1 203.8 200.4 200.0	216.6 217.2 208.8 210.2 198.3 201.2 200.5 202.8	217.1 216.5 2 211.8 214.1 2 206.3 212.4 2 207.7 213.0 2	215.2 212.8 215.5 215.2 216.1 217.0 216.7 218.2	209.4 206.2 212.3 208.9 215.2 212.5 217.3 215.7						
1.5 226,03 214,8 216,5 218,7 1.0 372,66 223,4 225,1 228,8 0.5 614,42 246,4 247,7 252,2 0.0 1013,0 275,0	220.5 221.0 222. 234.4 240.0 245. 258.9 265.6 271. 280.4 287.2 292.	5 264,6 263,2 262,7 6 255,0 255,0 255,1 243,7 244,5 244,5 4 232,0 231,3 232,1 2 223,7 223,2 223,2 3 217,8 216,8 216,2 0 202,0 198,6 197,9 4 203,8 200,4 200,0 5 224,6 225,5 226,7 7 250,5 252,8 253,6 4 275,2 276,3 276,7 9 297,2 299,9 300,5	225.7 224.3 253.2 250.9 277.0 275.7 301.0 299.7	222.0 219.2 2 245.2 238.1 2 270.6 263.5 2 295.2 288.3 2	218.7 218.9 232.6 228.2 256.8 251.1 281.4 272.3	218.1 217.0 225.0 222.9 246.6 243.8 261.3 255.7						
NOVEMBER ZONAL MEAN GEOPOTENTIAL												
SCALE PRESSURE -80 -70 -60 HEIGHT (mb)	-50 -40 -30	-20 -10 0	10 20	30 40	50 60	70 80						
11.5 0.0103 80860 80767 80489 11.0 0.0169 78219 78082 77744	80167 79906 7967 77358 77013 7/70	4 82478 82346 82311 1 79477 79288 79199 4 76467 76237 76110 0 73427 73194 73057	79184 79130 76095 76058	78927 78514 7 75824 75343 7	78052 77752 74806 74454	77298 76834 73976 73494						
9.0 0.1250 65661 65465 65059 8.5 0.2061 62096 61920 61539	68039 67674 6736 64674 64323 6404 61167 60842 6057	9 67143 66978 66893 2 63833 63695 63642 9 60378 60233 60196	66862 66717 63618 63432 60181 59987	66295 65589 6 62955 62216 6 59496 58753 5	54841 64266 51414 60762 57903 57188	63801 63309 60269 59754 56635 56082						
7.5 0.5603 54391 54302 54022 7.0 0.9237 50303 50265 50036 6.5 1.52 46136 46145 45962	53701 53435 5321: 49744 49493 4928: 45702 45468 4528:	8 56789 56612 56571 2 53045 52848 52792 9 49149 48972 48914 4 45180 45044 44999 3 41257 41150 41115	52790 52648 48914 48791 45000 44879	52195 51471 5 48358 47675 4 44485 43870 4	50576 49805 16819 46064 13119 42431	49124 48501 45352 44718 41742 41132						
5.5 4.14 37915 38016 37956 5.0 6.83 34010 34153 34163 4.5 11.25 30284 30470 30557	37773 37597 3750 34043 33911 3384 30522 30440 3037	1 37452 37355 37325 3 33795 33692 33662 2 30317 30215 30177 8 26981 2689 26847	37337 37252 33688 33648 30207 30208	37018 36636 3 33507 33238 3 30136 29962 2	56140 35632 32870 32445 29695 29351	35099 34515 31995 31587 28976 28640						
3.5 30.59 23289 23512 23713 3.0 50.43 19846 20094 20360 2.5 83.15 16458 16726 17037	23810 23837 2379 20523 20619 2062 17279 17458 1754	2 23749 23669 23630 3 20610 20546 20516 2 17591 17559 17557 9 14646 14670 14/57	23651 23671 20533 20536 17553 17526	23654 23582 2 20510 20426 2 17451 17305 1	23414 23197 20260 20063 17100 16897	22952 22738 19864 19697 16733 16611						
NOVEMBER MEAN ZONAL MEAN GEOSTRO SCALE PRESSURE -80 -70 -60	PHIC WIND (m s 1) -50 -40 -30	-20 -10 0	10 20	30 40	50 60	70 80						
HEIGHT (mb)			/									
12.0 0.0062 -5.5 -18.1 11.5 0.0103 -9.1 -23.2 11.0 0.0169 -12.6 -27.4 10.5 0.0279 -15.9 -30.2	-12.7 -9.7 -15. -21.8 -22.4 -27. -27.6 -30.2 -34. -29.9 -32.8 -36.	2 -29.1 2 -39.8 1 -46.6 3 -47.9	20.7 17.2 17.4 23.4	31.9 39.4 36.9 45.7 43.7 52.6 52.0 59.5	25.4 18.9 30.0 22.5 35.1 25.5 40.9 28.0	28.2 30.9 31.9 31.5						
10.0 0.0460 -17.8 -31.1 9.5 0.0758 -17.8 -30.4 9.0 0.1250 -17.1 -29.5 8.5 0.2061 -15.5 -28.3 8.0 0.3398 -12.3 -25.9	-28.7 -31.4 -32. -27.7 -29.6 -30. -26.2 -27.6 -28. -24.0 -25.2 -27.	9 -39,1 4 -35,5 7 -35,7	44.2 53.7 56.2	61.5 66.6 70.7 72.6 76.2 76.1 77.2 78.1 75.8 79.7	52.2 33.5 57.4 37.6 61.7 42.2	32.7						
7.5 0.5603 -8.7 -23.2 7.0 0.9237 -5.0 -20.6 6.5 1.52 -1.5 -18.1 6.0 2.5! 2.1 -15.0	-22.2 -22.7 -24. -20.8 -21.2 -21.0 -19.1 -19.6 -17. -17.1 -16.7 -12.0	1 -37.7 0 -33.2 2 -25.8 0 -18.9	48.3 45.0 41.7 36.0	73.2 79.4 69.2 75.6 62.4 66.9 51.5 55.3	65.4 48.9 63.1 49.5 56.2 46.5 47.6 41.4	43.1						
5.5 4.14 6.5 -11.0 5.0 6.83 10.8 -6.2 4.5 11.25 14.9 -0.2 4.0 18.55 14.6 5.7	-14.3 -12.9 -8. -10.3 -9.6 -6.1 -5.0 -7.3 -7. 0.3 -5.2 -7.	2 -29.1 2 -39.8 1 -46.6 3 -47.9 4 -44.6 9 -39.1 4 -55.5 7 -35.7 1 -37.7 1 -37.7 1 -37.7 1 -37.7 2 -37.7 1 -37.7 1 -37.7 2 -35.8 3 -10.9 1 -15.2 5 -14.5 1 -14.2 5 -13.0 3 -10.9 7 -6.9 2 1.5 1 15.9	26.2 14.8 5.6 0.5	37.9 42.6 25.1 30.6 15.0 21.0 8.1 14.4	39.1 35.7 30.8 30.5 23.7 25.5 18.4 20.4	34.1 28.6 23.5 18.5						
3.5 30.59 13.7 10.7 3.0 50.43 15.3 15.9 2.5 83.15 17.6 20.6 2.0 137.09 18.6 23.1	10.4 4.4 -0.1 16.8 12.3 8.2 22.0 21.5 21.	7 -6.9 2 1.5 1 15.9	1.6 8.8 20.5	5.3 11.4 6.5 12.2 13.3 17.5 24.8 25.2	15.2 16.6 14.4 14.2 16.1 13.3 19.2 13.3	14.8 11.6 8.6 6.6						

TABLE	TABLE 1 (continued) PRESSURE COORDINATES									OF POOR QUALIT								
DECEMBER ZONAL MEAN TEMPERATURE (K)																		
SCALE HE I GH	PRESSURE T (mb)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
12. 11. 10. 9. 8. 8. 7. 7. 6. 5. 4. 4. 4. 3. 3. 2. 2. 1. 1. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	5 0,0103 0,0169 0,0279 0 0,0460 0,0758 0 0,1250 0 0,2061 0 0,3398 5 0,5603 1,52 2,51 5 4,14 0 6,83 5 11,25 0 18,55 5 30,59 5 0,50 1,52 0 18,55 5 0,50 1,52 0 18,55 0 18,55 0 18,55 0 137,09 5 226,03 5 72,66 5 614,42	159.6 174.0 189.9 206.2 221.8 236.1 251.3 267.1 279.3 287.5 284.4 274.8 263.1 249.9 237.7 236.4 236.3 237.7 236.4 236.3 237.7 236.4 236.3 237.7 236.4 236.3 236.4 236.3 236.4	163.0 177.0 1792.4 207.8 222.3 235.9 250.0 264.3 275.6 283.6 283.6 281.9 272.7 261.3 235.1 234.3 235.1 234.3	168.2 181.6 195.9 209.6 222.3 235.0 247.9 260.8 271.5 279.5 279.5 269.1 257.4 257.4 245.6 236.3 231.8 229.6 225.8 225.8	167.9 177.5 188.3 199.4 210.1 221.2 235.4 245.9 258.7 276.0 278.8 275.1 265.3 252.9 240.6 257.1 222.7 221.7 221.7 221.7 221.7 221.7 221.7 221.7 221.7 221.7 221.7 221.7 231.9	188.5 195.4 202.8 210.5 219.9 231.1 242.8 254.9 265.5 273.5 271.9 261.3 249.3 249.3 228.5 222.9 216.7 213.9 221.3	198 1 2011 7 205 9 211 2 218 9 229 3 241 9 253 7 263 6 271 3 272 9 267 9 257 9 246 0 233 5 225 7 220 2 212 5 207 8 223 2	203, 7 205, 6 208, 3 212, 0 219, 5 230, 8 243, 4 254, 0 262, 6 269, 5 254, 0 242, 9 231, 6 223, 8 218, 2 210, 0 201, 0 203, 3 225, 2 251, 8	206.2 206.6 208.2 212.1 220.9 233.9 247.5 257.2 263.4 265.2 260.1 251.7 241.4 229.9 222.7 217.2 208.6 200.5 200.5	209.0 208.3 208.1 211.4 220.6 234.5 248.2 258.5 264.1 265.6 263.8 259.3 252.0 242.0 229.6 222.2 216.5 200.0 200.0 226.0	207.9 207.6 208.1 211.3 219.9 232.8 246.5 257.0 263.3 266.1 264.3 259.7 251.8 241.8 240.2 222.3 216.3 208.0 209.0 200.4 225.5	206 6 6 207 6 209 2 2 12 0 0 2 2 12 0 0 2 2 13 0 2 2 13 0 2 2 1 2 1 2 1 2 1 2 1 2 1 7 0 2 2 2 2 2 2 2 1 2 1 7 0 2 2 0 0 9 2 2 3 0 2 2 4 2 2 2 5 0 2 2 5 0 2	209,9 211,3 213,3 216,7 223,4 231,6 239,4 247,8 257,5 264,6 258,0 247,0 236,5 211,3 206,7 208,4 221,5 211,3 208,4 221,4	216.2 218.5 220.4 222.1 225.9 235.5 244.3 254.2 260.3 254.2 248.5 238.4 223.1 218.5 216.7 214.0 218.6 214.0 218.6	221,5 225,7 226,2 228,6 231,3 234,8 240,1 246,7 252,8 252,5 245,6 235,8 214,6 214,9 215,9	224,2 227,7 231,4 235,0 239,2 243,2 247,6 251,9 254,1 249,0 239,6 229,7 220,7 220,7 210,4 210,4 210,9 214,2 216,9 217,6 216,9	226.9 228.7 232.2 236.3 241.5 248.2 254.5 258.3 257.5 249.2 249.2 201.0 200.3 205.0 209.8 212.7 214.5 215.9 225.9	229,6 230,2 233,2 233,2 237,0 242,4 250,2 257,2 260,3 258,0 248,7 237,9 227,2 216,4 204,9 194,7 193,5 199,7 205,7 205,7 205,3 212,1 214,8 221,8
DECEM	BER ZONAL	MEAN	GEOPOT	ENTIAL	HE I GH	T (m)												
SCALE	PRESSURE (mb)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
12. 11. 11. 10. 9. 8. 8. 7. 6. 6. 5. 5.	5 0.0103 0.0169 0.0279 0.0460 0.0250 0.0255 0.2061 0.3398 5 0.5603 0.9237 1.52 0.9237 1.52 0.1855 1.52 0.1855 1.52 0.5603 1.52 0.5603 0.9237 0.92	81295 78858 76190 73295 70153 66803 63231 59438 55431 51278 47049 42844 387495 31047 27485 24019 20556 17109	81061 78577 75869 72943 69788 66436 62875 59113 51057 46880 42716 38654 31005 27445 23988 20551 17134	80690 78134 75366 72400 69233 65888 62349 58627 54724 50687 46566 42448 38436 354575 30896 27369 27369 27369 17219	82805 80275 77601 74759 71764 68602 65277 61764 58076 54212 50223 46154 42089 38131 34330 30722 27264 23906 20612 17364 14126	79915 77107 74186 61013 64714 61240 57600 53783 49835 45798 41771 37867 30569 27163 23660 20638 17494	79614 76557 737051 67503 64226 60773 57145 57145 45442 41474 37625 33930 30424 27063 23798 20626 17562	79416 76421 73390 10315 67158 63867 60340 52963 49063 45112 41206 37417 33774 30304 26971 23734 17586	79321 76299 73263 70191 67023 63699 60168 56470 52654 48768 44868 41017 37270 33653 30206 26896 23674 17574	79280 76232 73187 70117 66953 63627 60088 56379 52551 48668 44786 40949 37208 33588 30141 26837 23627 20518 17554	79202 76159 73116 70049 66894 63586 60070 52565 48685 44798 40758 332592 30140 26830 23619 20508 17538	79111 76080 73027 66947 66786 63476 59990 56362 52598 48733 44821 40944 37186 33576 30142 26840 23625 20498 17496	78879 75797 72686 69544 66323 62994 59542 55978 48448 44566 40731 37034 35492 30093 26801 23592 20453 17395	78351 75169 71956 68715 65435 62097 58690 551826 47753 43946 40228 33235 29921 26688 23503 20345 17215	77716 74456 71161 67830 64461 61052 57574 54013 50349 46641 42991 39460 32807 29610 26452 23309 16988	77498 74191 70829 67415 63942 60410 56815 53159 49447 45754 42177 38736 35443 2500 29154 26088 23019 19908 16756	77008 73674 70299 66870 63372 59789 56105 52348 48563 44844 41278 37869 34625 28530 25598 22631 116499	76563 73198 69806 66364 62855 59251 55531 51735 47932 44214 40655 37244 33999 27993 25161 22282 19316 16273
DECEM	BER MEAN	ZONAL	MEAN G	EOSTRO	PHIC W	IND (m	s ⁻¹)											
SCALE	PRESSURE T (mb)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
	5 0.0279 0.0460 0 0.0758 0 0.1250 0 0.2061 0 0.3398 5 0.5603 1 .52 0 2.51 6 .83 1 1.52 0 18.55 1 1.55 5 30.59 5 0.5043 1 1.55 5 30.59 5 0.443 1 1.55 5 30.59		-12.6 -16.5 -19.8 -22.1 -22.9 -21.6 -19.1 -15.4 -11.1 -7.3 -4.8 -2.9 -1.5	-31.8 -38.4 -43.0 -45.4 -44.5 -42.8 -40.2 -37.1 -33.6 -29.9 -26.3 -22.2 -17.6 -12.4 -7.3 -2.8 2.8 8.8	2.9 11.3	-30.3 -43.0 -50.3 -52.6 -50.0 -46.7 -43.4 -39.6 -36.2 -32.8 -28.5 -23.4 -18.5 -13.8 -9.3 -5.1 -6.0	-30.7 -41.8 -48.6 -51.8 -52.3 -52.5 -52.8 -50.9 -47.2 -34.7 -21.5 -16.2 -11.8 -2.8	-30.4 -37.5 -40.1 -43.7 -48.5 -56.4 -64.0 -64.7 -56.3 -44.9 -34.1 -19.2 -14.6 -10.9 -1.2					53.2 64.2 74.8 82.5 84.2 79.0	64.9 73.3 82.2 91.0 97.9 101.4 102.4 102.0 93.6 64.4 47.7 33.5 23.1 16.3 13.1	31.9 36.9 42.8 49.7 57.4 65.2 73.0 79.5 82.1 79.1 69.9 58.6	18.4 20.4 23.0 26.4 31.2 38.0 46.0 53.7 59.7 57.4 54.0 50.0 45.3 38.4 30.7 24.4	36.6 37.7 38.8 40.1 42.6 46.7 51.2 54.0 54.7 54.1 52.8 50.4 46.2 38.7 30.3 23.9	

ORIGINAL PAGE IS OF POOR QUALITY



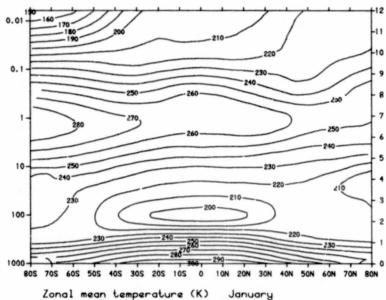


Figure 1.1.

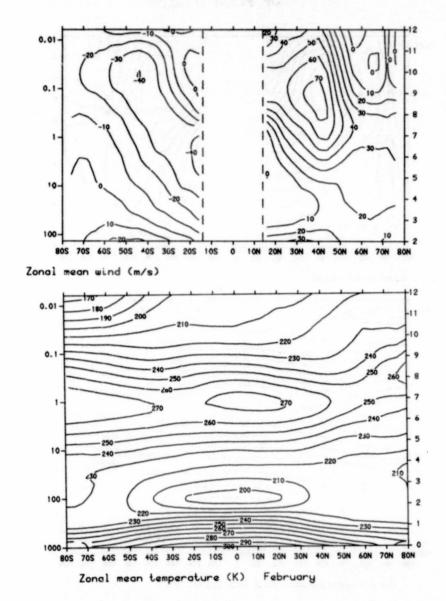


Figure 1.2.

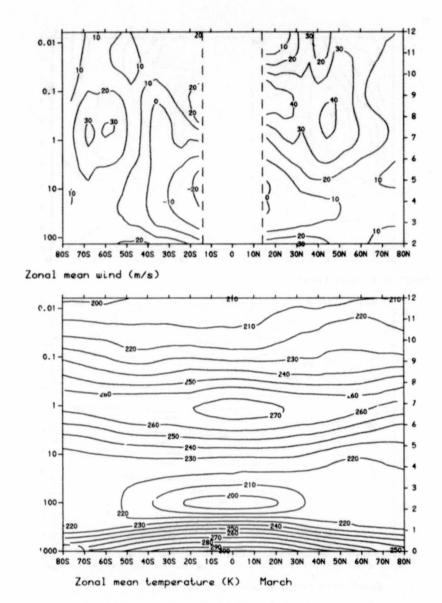
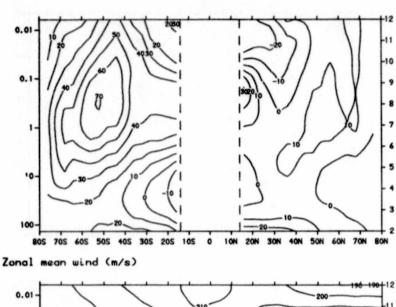


Figure 1.3.



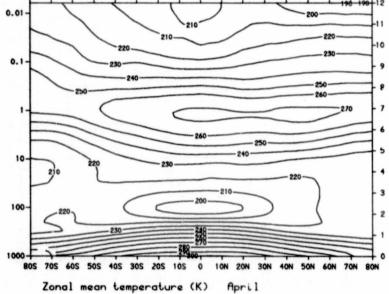


Figure 1.4.

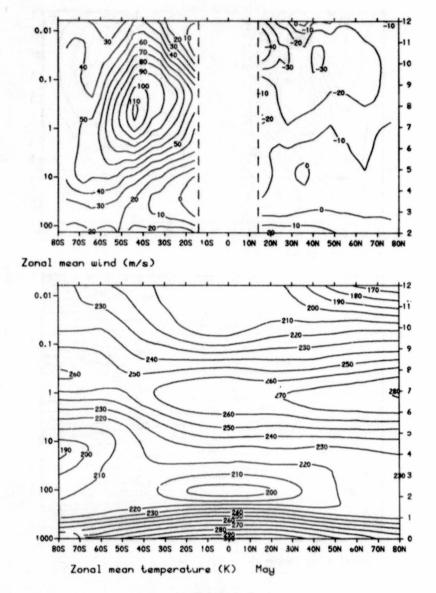


Figure 1.5.

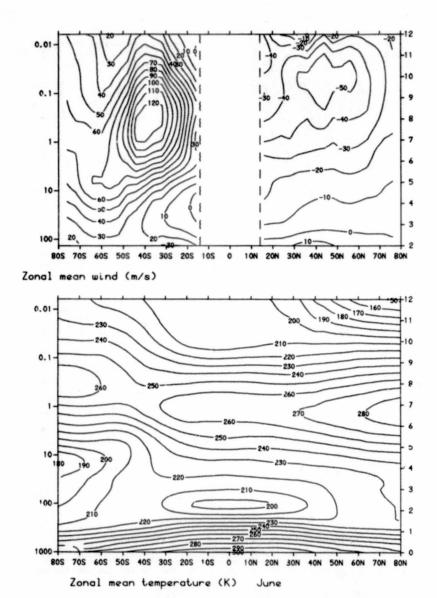
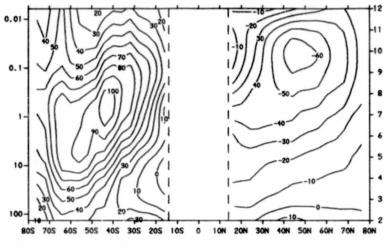


Figure 1.6.



Zonal mean wind (m/s)

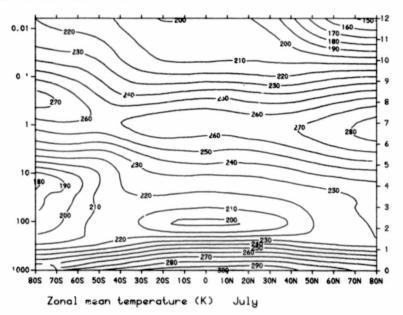


Figure 1.7.

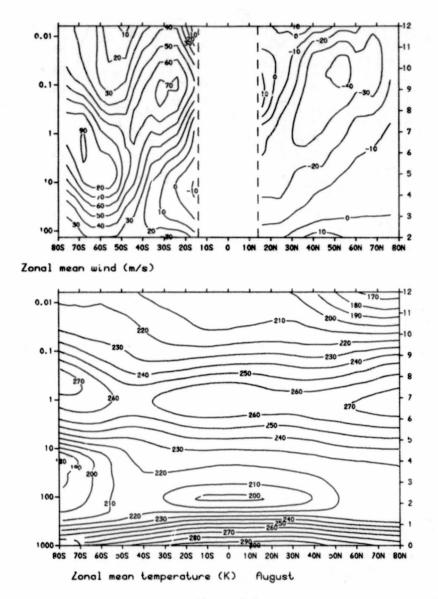
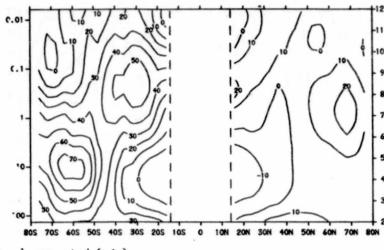


Figure 1.8.

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Zonal mean wind (m/s)

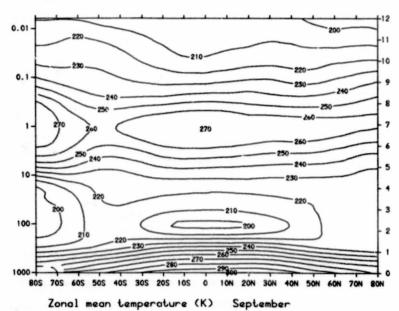


Figure 1.9.

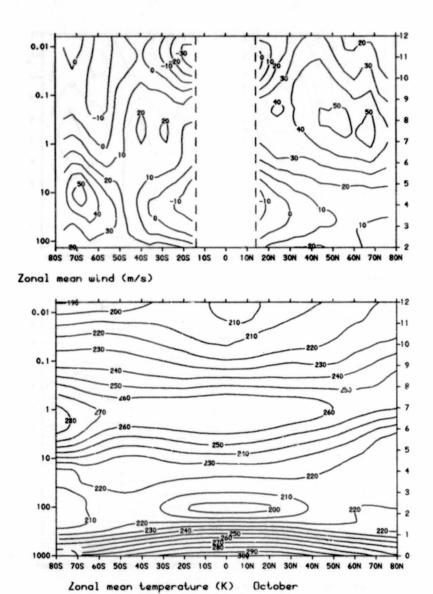
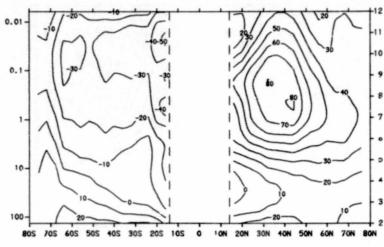


Figure 1.10.



Zonal mean wind (m/s)

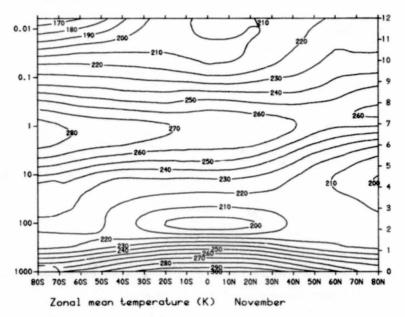


Figure 1.11.

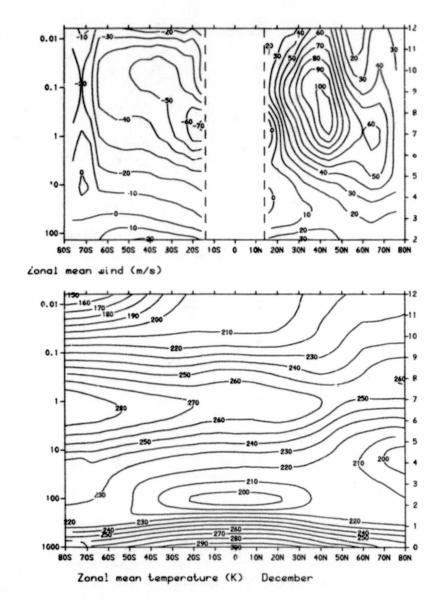


Figure 1.12.

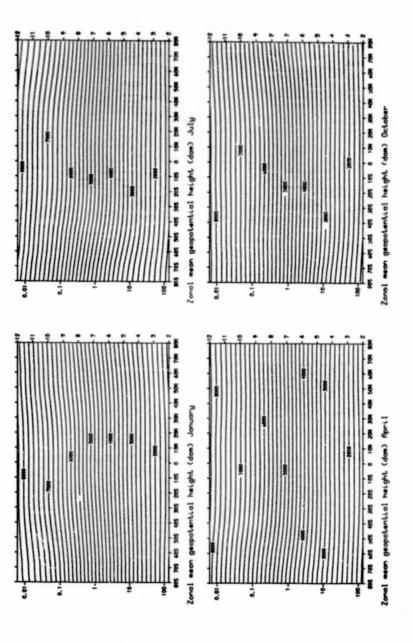


Figure 2.

Table II.

Height																			
## HEIGHT -80 -70 -60 -50 -40 -30 -20 -10 0 10 20 30 40 50 60 70 80 ## 172.2 173.5 175.5 183.2 193.5 202.7 206.8 206.1 206.5 207.1 208.0 211.8 216.2 223.3 225.0 224.4 225.2 75 200.2 204.8 202.0 204.8 206.3 210.5 206.3 207.9 201.0 211.9 215.5 219.2 223.0 227.7 227.5 226.3 70 226.4 224.8 224.9 227.7 219.0 215.2 214.2 215.9 217.8 216.3 217.7 217.5 219.5 224.0 225.0 227.7 227.5 229.3 56 228.5 225.5 215.5 229.5 225.2 225.3 226.5 30.6 226.5 228.4 224.8 227.7 219.0 215.2 214.2 215.9 217.8 216.3 217.7 217.5 219.5 221.2 225.0 227.7 227.5 229.3 56 228.5 225.5 225.5 225.5 225.2 227.8 225.8 2	ANUARY	ZONA	IL MEAN	TEMP	ERATURE	(K)													
80 172.2 173.3 175.5 183.2 193.5 202.7 206.8 206.1 206.5 207.1 208.0 211.8 216.2 222.3 225.0 224.4 225.2 75 200.9 200.3 200.4 202.0 204.8 208.3 210.3 209.3 209.3 209.9 210.5 211.9 215.5 219.8 224.0 226.2 227.5 225.3 226.5 70 226.4 224.8 222.7 210.0 212.3 217.8 218.2 217.5 220.3 224.8 222.7 219.0 212.5 217.8 218.5 218.2 226.2 227.5 220.4 225.5 220.4 235.6 235.1 235.2 236.3 236		-80	-70	-60	-50	-40	-30	-20			10	20	30	40	50	60	70	80	
206.7 292.9 298.7 292.8 287.4 285.0 287.7 292.6 287.7 292.6 287.7 292.6 282.9 298.5 238.7 232.5 232.5 244.7 284.2 250.7 295.5 281.2 276.8 272.1 265.3 281.4 288.7 297.4 257.8 267.8 267.8 267.9 267.0 265.4 265.2 287.2 274.7 284.2 250.7 255.5 255.4 267.2 268.2 267.8 267.9 267.0 265.4 266.2 267.8 267.8 267.0 265.4 266.2 267.2 267.0 265.4 266.2 267.3 267.8 267.2 267.8 267.2 267.8 267.2 267.8 267.2 267.8 267.2 267.8 267.2 267.8 267.2 267.8 267.2 267.8 267.2 267.8 267.2 267.8 267.2 267.8 267.2 267.8 267.2 267.8 267.2 267.8 267.2 267.8 267.2		172.2	173.3	175.5	183.2	193.5	202.7	206.8	206.1	206.5	207.1	208.0	211.8	216.2	222.3	225.0	224.4	225.2	
206.7 292.9 298.7 292.8 287.4 285.0 287.7 292.6 287.7 292.6 287.7 292.6 282.9 298.5 238.7 232.5 232.5 244.7 284.2 250.7 295.5 281.2 276.8 272.1 265.3 281.4 288.7 297.4 257.8 267.8 267.8 267.9 267.0 265.4 265.2 287.2 274.7 284.2 250.7 255.5 255.4 267.2 268.2 267.8 267.9 267.0 265.4 266.2 267.8 267.8 267.0 265.4 266.2 267.2 267.0 265.4 266.2 267.3 267.8 267.2 267.8 267.2 267.8 267.2 267.8 267.2 267.8 267.2 267.8 267.2 267.8 267.2 267.8 267.2 267.8 267.2 267.8 267.2 267.8 267.2 267.8 267.2 267.8 267.2 267.8 267.2 267.8 267.2 267.8 267.2	75	200.9	200.5	200.4	202.0	204.8	208.3	210.3	209.3	209.9	210.5	211.9	215.5	219.8	224.0	226.2	225.3	226.3	
206.7 292.9 298.7 292.8 287.4 285.0 287.7 292.6 287.7 292.6 287.7 292.6 282.9 298.5 238.7 232.5 232.5 244.7 284.2 250.7 295.5 281.2 276.8 272.1 265.3 281.4 288.7 297.4 257.8 267.8 267.8 267.9 267.0 265.4 265.2 287.2 274.7 284.2 250.7 255.5 255.4 267.2 268.2 267.8 267.9 267.0 265.4 266.2 267.8 267.8 267.0 265.4 266.2 267.2 267.0 265.4 266.2 267.3 267.8 267.2 267.8 267.2 267.8 267.2 267.8 267.2 267.8 267.2 267.8 267.2 267.8 267.2 267.8 267.2 267.8 267.2 267.8 267.2 267.8 267.2 267.8 267.2 267.8 267.2 267.8 267.2 267.8 267.2 267.8 267.2	70	226.4	224.8	222.7	219.0	215.2	214.1	215.9	217.8	218.3	217.7	217.5	219.5	221.2	225.0	227.7	227.3	229.3	
50 288,5 288,4 279,7 279,4 271,4 268,7 267,4 267,8 267,9 267,0 263,4 259,2 253,5 253,5 255,0 259,4 4 289,2 283,5 283,5 285,0 278, 272,2 286,2 286,5 284,4 282,3 252,0 231,0 40 276,2 274,1 271,2 267,9 264,1 260,2 256,5 254,9 259,2 259,8 254,0 230,0 246,4 282,3 252,0 231,0 246,2 244,1 271,2 267,9 264,8 284,1 282,5 274,2 281,7 271,2 281,2 271,2	65	248.3	245.3	241.5	255.5	229.8	227.5	230,4	233.0	235.1	255.1	230.7	227.8	220.3	220.2	229.0	241.0	230.4	
50 288,5 284,4 279,7 279,4 271,4 266,7 267,4 267,8 267,8 267,9 267,0 263,4 259,2 253,5 253,5 255,0 259,4 4 282,3 250,0 278,8 272,8 269,5 267,1 264,0 263,8 264,5 264,6 264,6 264,4 252,3 252,0 21,0 40 276,2 274,1 271,2 267,6 264,1 260,2 256,5 254,9 259,2 259,8 254,0 230,0 246,4 265,2 46,5 246,7 246,9 5 261,6 260,5 259,1 278,5 264,8 264,1 260,2 256,5 254,9 257,2 258,8 254,0 230,0 246,2 246,5 246,5 246,7 246,9 5 20,2 256,5 254,9 277,8 277,2 278,0 278,1 278,2 279		200.7	274 9	272 1	256.0	261 1	250 7	250 4	263 3	254.9	262 0	250 %	251 0	245 2	241 7	244 2	250 7	255 5	
40 276,2 274,1 271,2 267,6 264,1 260,2 296,5 284,9 285,2 285,2 285,8 284,0 290,0 246,2 446,5 246,5 246,7 246,9 5 261,8 260,5 289,1 224,6 224,6 224,6 224,7 227,2 286,0 5 261,8 241,2 243,7 240,7 236,1 232,0 228,9 227,8 227,2 228,0 228,1 228,5 227,5 226,2 224,7 221,7 219,1 225,2 255,5 255,5 255,5 252,5 226,2 228,1 228,2 218,1 227,5 218,2 218,5 217,5 218,5 218,5 219,3 219,5 218,2 218,5 217,2 218,1 217,5 218,0 218,5 219,3 219,5 218,2 218,5 217,2 218,1 217,5 218,0 218,5 218,5 218,5 218,5 211,4 205,9 218,2 218,5 217,2 228,5		201.1	284 4	270 7	275 4	271 4	268 7	267 4	267 8	267 8	267 0	267.0	263.4	259.2	253 5	253 5	255.0	255.4	
40 276,2 274,1 271,2 267,6 264,1 260,2 296,5 284,9 285,2 285,2 285,8 284,0 290,0 246,2 446,5 246,5 246,7 246,9 5 261,8 260,5 289,1 224,6 224,6 224,6 224,7 227,2 286,0 5 261,8 241,2 243,7 240,7 236,1 232,0 228,9 227,8 227,2 228,0 228,1 228,5 227,5 226,2 224,7 221,7 219,1 225,2 255,5 255,5 255,5 252,5 226,2 228,1 228,2 218,1 227,5 218,2 218,5 217,5 218,5 218,5 219,3 219,5 218,2 218,5 217,2 218,1 217,5 218,0 218,5 219,3 219,5 218,2 218,5 217,2 218,1 217,5 218,0 218,5 218,5 218,5 218,5 211,4 205,9 218,2 218,5 217,2 228,5		286.1	283.4	280.0	275.8	272.8	269.5	267.1	264.0	263.8	264.5	265.8	264.4	260.6	254.4	252.3	252.0	251.0	
30 244,5 244,1 243,7 240,7 236,1 232,0 228,9 227,8 227,2 228,0 228,1 228,5 227,5 222,2 224,7 221,7 219,1 25 225,2 234,6 233,6 232,6 229,6 222,2 242,7 221,7 219,2 218,2 217,5 218,0 218,5 219,5 218,2 213,8 207,8 202,0 20 234,6 253,2 229,6 222,2 242,7 221,7 219,2 110 226,9 225,2 231,5 227,3 220,3 212,3 206,0 202,0 199,8 199,3 199,7 202,2 208,1 214,2 17,9 217,0 214,1 211,2 110 226,9 225,5 224,8 239,7 229,8 235,0 238,3 239,0 239,2 238,6 235,4 228,6 221,5 218,8 217,1 215,2 214,0 24,0 240,8 243,7 248,3 235,8 265,8 269,4 271,9 272,5 272,4 2724,4 299,6 2618,8 227,5 244,5 239,1 234,8 231,9 0 240,8 243,7 248,1 248,5 295,8 265,8 269,4 271,9 272,5 2724,4 2724,9 29,6 2618,8 272,7 266,4 234,1 248,6 248,1 248,6 248,1 248,1 248,6 248,1 248	40	276.2	274.1	271.2	267.6	264.1	260.2	256.5	254.9	255.2	255.2	255.8	254.0	250.0	246.4	246.5	246.7	246.9	
30 244,5 244,1 243,7 240,7 236,1 232,0 228,9 227,8 227,2 228,0 228,1 228,5 227,5 222,2 224,7 221,7 219,1 25 225,2 234,6 233,6 232,6 229,6 222,2 242,7 221,7 219,2 218,2 217,5 218,0 218,5 219,5 218,2 213,8 207,8 202,0 20 234,6 253,2 229,6 222,2 242,7 221,7 219,2 110 226,9 225,2 231,5 227,3 220,3 212,3 206,0 202,0 199,8 199,3 199,7 202,2 208,1 214,2 17,9 217,0 214,1 211,2 110 226,9 225,5 224,8 239,7 229,8 235,0 238,3 239,0 239,2 238,6 235,4 228,6 221,5 218,8 217,1 215,2 214,0 24,0 240,8 243,7 248,3 235,8 265,8 269,4 271,9 272,5 272,4 2724,4 299,6 2618,8 227,5 244,5 239,1 234,8 231,9 0 240,8 243,7 248,1 248,5 295,8 265,8 269,4 271,9 272,5 2724,4 2724,9 29,6 2618,8 272,7 266,4 234,1 248,6 248,1 248,6 248,1 248,1 248,6 248,1 248	35	261.8	250.5	258,1	254.6	250.6	246.8	244.1	242.3	242.5	242.1	241.7	239.2	237,4	235.4	235.7	236.3	236,6	
20 234,6 233,2 229,6 222,8 215,5 210,2 207,4 205,3 204,3 204,5 206,7 210,0 214,5 216,8 215,5 211,4 205,9 15 225,25 231,3 237,3 220,3 212,3 206,0 202,0 199,8 1993, 1997, 202,2 208,1 214,7 217,9 217,0 214,1 211,2 10 226,9 225,5 224,8 225,9 229,8 235,0 238,5 239,0 239,2 239,6 235,4 228,6 221,5 218,8 217,1 215,2 214,0 5 240,8 243,7 248,3 255,8 265,8 267,1 271,9 272,3 272,4 272,4 299,6 261,8 224,5 239,1 234,8 231,9 0 275,2 281,4 289,5 295,9 298,9 300,5 300,6 300,0 297,1 291,7 284,7 277,7 266,4 254,1 248,6	30	244.5	244.1	243.7	240.7	236.1	232.0	228.9	227.8	227.2	228.0	228.1	228.5	227.5	226.2	224.7	221.7	219.1	
10 226,9 225,5 224,8 225,9 229,8 235,0 236,3 259,0 239,2 239,2 228,6 225,4 228,6 221,5 248,5 271,1 215,2 214,0 5 240,8 243,7 246,3 255,8 263,8 269,4 271,9 272,3 272,4 272,4 296,6 261,8 252,5 244,5 259,1 234,8 251,9 0 275,2 281,4 289,5 295,9 298,9 300,5 300,6 300,0 297,1 291,7 284,7 277,7 266,4 254,1 248,6 240,4 248,6 240,4 248,6 240,4 248,6 240,4 248,6 240,4 248,6 240,4 248,6 240,4 248,6 240,4 248,6 240,4 248,6 240,4 248,6 240,4 248,6 240,4 240,4 248,6 240,4	25	235.6	233.8	232.6	229.0	225.4	222.1	219.2	218.1	217.5	218.0	218.3	219.3	219.6	218.2	213.8	207.8	202.0	
10 226,9 225,5 224,8 225,9 229,8 235,0 236,3 259,0 239,2 239,2 228,6 225,4 228,6 221,5 248,5 271,1 215,2 214,0 5 240,8 243,7 246,3 255,8 263,8 269,4 271,9 272,3 272,4 272,4 296,6 261,8 252,5 244,5 259,1 234,8 251,9 0 275,2 281,4 289,5 295,9 298,9 300,5 300,6 300,0 297,1 291,7 284,7 277,7 266,4 254,1 248,6 240,4 248,6 240,4 248,6 240,4 248,6 240,4 248,6 240,4 248,6 240,4 248,6 240,4 248,6 240,4 248,6 240,4 248,6 240,4 248,6 240,4 248,6 240,4 240,4 248,6 240,4		234.6	233.2	229.6	222.8	215.5	210.2	207.4	205.3	204.3	204.6	206.7	210.0	214.5	216.8	215.5	211.4	205.9	
O 275.2 281.4 289.5 299.9 298.9 300.5 300.6 300.0 297.1 291.7 284.7 277.7 266.4 254.1 248.6 IANUARY ZONAL MEAN PRESSURE (N m^2) IEIGHT -80 -70 -60 -50 -40 -30 -20 -10 0 10 20 30 40 50 60 70 80 EXPON (K m) 1.590 1.504 1.408 1.290 1.186 1.129 1.119 1.123 1.130 1.118 1.083 1.035 0.960 0.890 0.861 0.815 0.781 E+0 75 3.903 3.680 3.421 3.069 2.737 2.537 2.486 2.503 2.514 2.480 2.391 2.293 2.060 1.880 1.806 1.714 1.659 E+0 70 8.541 8.080 7.545 6.786 6.067 5.592 5.440 5.473 5.486 5.408 5.206 4.884 4.392 5.965 3.769 3.591 5.417 E+0 65 1.730 1.647 1.552 1.417 1.288 1.195 1.152 1.148 1.146 1.135 1.099 1.025 0.928 0.831 0.784 0.745 0.703 E+1 60 3.221 3.189 3.032 2.814 2.597 2.426 2.319 2.282 2.273 2.267 2.219 2.101 1.926 1.733 1.616 1.513 1.410 E+1 50 6.130 5.940 5.710 5.372 5.019 4.713 4.483 4.359 4.353 4.346 4.320 4.163 3.893 3.332 3.262 2.993 2.749 E+1 50 1.107 1.081 1.049 0.988 0.942 0.890 0.847 0.818 0.812 0.816 0.817 0.797 0.797 0.797 0.695 0.660 0.682 0.351 E-2 40 3.624 3.579 3.524 3.410 3.266 3.127 3.006 2.935 2.912 2.922 2.914 2.872 2.785 2.566 2.447 2.222 2.203 E+2 30 1.326 1.318 1.311 1.288 1.260 1.231 1.203 1.184 1.174 1.178 1.177 1.173 1.154 1.106 1.030 0.937 0.861 E+3 EIGHT -80 -70 -60 -50 -40 -30 -20 -10 0 10 20 30 40 50 60 70 80 EXPON (K m) 3.217 3.022 2.794 2.452 2.136 1.941 1.886 1.898 1.996 1.880 1.814 1.770 1.754 1.3492 4.473 4.999 E+2 30 1.326 1.318 1.311 1.288 1.260 1.231 1.203 1.184 1.174 1.178 1.177 1.173 1.154 1.106 1.030 0.937 0.861 E+3 EIGHT -80 -70 -60 -50 -40 -30 -20 -10 0 10 20 30 40 50 60 70 80 EXPON (K m) 3.217 3.022 2.794 2.452 2.136 1.941 1.886 1.898 1.906 1.880 1.814 1.700 1.546 1.354 1.354 1.265 1.208 E-5 6.768 6.393 5.946 5.294 4.656 4.242 4.119 4.164 4.173 4.105 3.933 1.642 3.265 2.924 2.781 2.650 2.522 E-5 70 1.314 1.222 1.180 1.079 0.982 0.910 0.878 0.876 0.875 0.885 0.834 0.770 0.562 0.613 0.577 0.595 0.615 0.595 0.795 0		232.5	231.3	227.3	220.3	212.3	206.0	202.0	199.8	199.3	199.7	202.2	208.1	214.7	217.9	217.0	214.1	211.2	
O 275.2 281.4 289.5 299.9 298.9 300.5 300.6 300.0 297.1 291.7 284.7 277.7 266.4 254.1 248.6 IANUARY ZONAL MEAN PRESSURE (N m^2) IEIGHT -80 -70 -60 -50 -40 -30 -20 -10 0 10 20 30 40 50 60 70 80 EXPON (K m) 1.590 1.504 1.408 1.290 1.186 1.129 1.119 1.123 1.130 1.118 1.083 1.035 0.960 0.890 0.861 0.815 0.781 E+0 75 3.903 3.680 3.421 3.069 2.737 2.537 2.486 2.503 2.514 2.480 2.391 2.293 2.060 1.880 1.806 1.714 1.659 E+0 70 8.541 8.080 7.545 6.786 6.067 5.592 5.440 5.473 5.486 5.408 5.206 4.884 4.392 5.965 3.769 3.591 5.417 E+0 65 1.730 1.647 1.552 1.417 1.288 1.195 1.152 1.148 1.146 1.135 1.099 1.025 0.928 0.831 0.784 0.745 0.703 E+1 60 3.221 3.189 3.032 2.814 2.597 2.426 2.319 2.282 2.273 2.267 2.219 2.101 1.926 1.733 1.616 1.513 1.410 E+1 50 6.130 5.940 5.710 5.372 5.019 4.713 4.483 4.359 4.353 4.346 4.320 4.163 3.893 3.332 3.262 2.993 2.749 E+1 50 1.107 1.081 1.049 0.988 0.942 0.890 0.847 0.818 0.812 0.816 0.817 0.797 0.797 0.797 0.695 0.660 0.682 0.351 E-2 40 3.624 3.579 3.524 3.410 3.266 3.127 3.006 2.935 2.912 2.922 2.914 2.872 2.785 2.566 2.447 2.222 2.203 E+2 30 1.326 1.318 1.311 1.288 1.260 1.231 1.203 1.184 1.174 1.178 1.177 1.173 1.154 1.106 1.030 0.937 0.861 E+3 EIGHT -80 -70 -60 -50 -40 -30 -20 -10 0 10 20 30 40 50 60 70 80 EXPON (K m) 3.217 3.022 2.794 2.452 2.136 1.941 1.886 1.898 1.996 1.880 1.814 1.770 1.754 1.3492 4.473 4.999 E+2 30 1.326 1.318 1.311 1.288 1.260 1.231 1.203 1.184 1.174 1.178 1.177 1.173 1.154 1.106 1.030 0.937 0.861 E+3 EIGHT -80 -70 -60 -50 -40 -30 -20 -10 0 10 20 30 40 50 60 70 80 EXPON (K m) 3.217 3.022 2.794 2.452 2.136 1.941 1.886 1.898 1.906 1.880 1.814 1.700 1.546 1.354 1.354 1.265 1.208 E-5 6.768 6.393 5.946 5.294 4.656 4.242 4.119 4.164 4.173 4.105 3.933 1.642 3.265 2.924 2.781 2.650 2.522 E-5 70 1.314 1.222 1.180 1.079 0.982 0.910 0.878 0.876 0.875 0.885 0.834 0.770 0.562 0.613 0.577 0.595 0.615 0.595 0.795 0		226.9	225.5	224.8	225.9	229.8	235.0	238.3	239.0	239.2	238.6	235.4	228.6	221.6	218.8	217.1	215.2	214.0	
EIGHT -80 -70 -60 -50 -40 -30 -20 -10 0 10 20 30 40 50 60 70 80 EXPON 80 1.590 1.504 1.408 1.290 1.186 1.129 1.119 1.125 1.130 1.118 1.083 1.035 0.960 0.890 0.861 0.815 0.781 E+0 75 3.903 3.680 3.421 3.069 2.737 2.537 2.486 2.503 2.514 2.480 2.591 2.255 2.060 1.880 1.806 1.714 1.659 E+0 70 8.541 8.080 7.545 6.786 6.067 5.592 5.440 5.473 2.488 5.408 2.591 2.255 2.060 1.880 1.806 1.714 1.659 E+0 65 1.750 1.647 1.552 1.417 1.288 1.195 1.152 1.148 1.146 1.136 1.099 1.025 0.928 0.831 0.784 0.745 0.703 E+1 60 3.321 3.189 5.032 2.814 2.597 2.426 2.519 2.282 2.273 2.267 2.219 2.101 1.926 1.733 1.616 1.513 1.410 E+1 55 6.130 5.940 5.710 5.372 5.019 4.713 4.483 4.393 4.344 4.320 4.165 3.993 3.532 3.262 2.993 2.749 E+1 50 1.107 1.081 1.049 0.998 0.942 0.890 0.847 0.818 0.812 0.816 0.817 0.797 0.757 0.695 0.640 0.582 0.531 E+2 40 3.624 3.579 3.524 3.410 3.266 5.127 3.006 2.935 2.912 2.922 2.914 2.872 2.866 2.636 2.447 2.224 2.037 E+2 35 6.791 6.737 6.577 6.596 6.288 6.081 5.892 5.776 5.724 5.735 5.905 5.571 5.591 5.531 3.933 3.251 2.262 2.372 2.235 2.071 1.935 E+3 20 5.563 5.571 5.591 5.654 2.628 2.399 2.560 2.528 2.512 2.516 2.512 2.497 2.462 2.372 2.235 2.071 1.935 E+3 20 5.565 5.571 5.591 5.653 5.669 5.678 5.652 5.613 5.593 5.596 5.568 5.499 5.572 5.313 4.992 4.473 4.099 E+2 50 6.786 6.939 5.946 5.294 4.656 4.242 4.119 4.164 4.173 4.108 1.814 1.700 1.546 1.396 1.334 1.265 1.208 E-5 70 1.314 1.252 1.180 1.079 0.982 0.910 0.888 0.867 0.875 0.865 0.885 0.895 5.571 5.591 5.653 1.803 1.791 0.888 0.895 0.758 5.865 5.499 5.572 5.825 2.781 2.690 2.522 E-5 1.110		240.8	243.7	275.2	281.4	289.5	295.9	298.9	300.5	300.6	300.0	297.1	291.7	284.7	277.7	266.4	254.1	248.6	
HEIGHT	ANUARY	ZONA	AL MEAN	PRES	SURE (N	m ⁻²)													
80 1,590 1,504 1,408 1,290 1,186 1,129 1,119 1,123 1,130 1,118 1,083 1,033 0,960 0,890 0,861 0,815 0,781 E+0 75 3,903 3,880 3,421 3,069 2,737 2,537 2,537 2,486 2,503 2,514 2,480 2,391 2,233 2,060 1,880 1,806 1,714 1,639 E+0 70 8,541 8,080 7,545 6,786 6,067 5,592 5,440 5,473 5,484 5,408 2,206 4,854 4,392 5,956 3,769 3,991 3,417 E+0 65 1,730 1,647 1,552 1,417 1,288 1,195 1,152 1,148 1,146 1,136 1,099 1,025 0,928 0,831 0,784 0,745 0,703 E+1 65 3,321 3,189 3,032 2,814 2,597 2,426 2,319 2,282 2,273 2,267 2,199 2,101 1,926 1,733 1,616 1,513 1,410 E+1 65 6,130 5,940 5,710 5,372 5,019 4,713 4,483 4,359 4,333 4,346 4,320 4,163 3,893 3,532 3,262 2,993 2,749 E+1 65 1,107 1,081 1,049 0,998 0,942 0,890 0,847 0,818 0,812 0,816 0,817 0,797 0,757 0,659 0,640 0,582 0,531 E+2 45 1,989 1,956 1,913 1,835 1,747 1,658 1,584 1,537 1,525 1,531 1,531 1,503 1,443 1,345 1,244 1,130 1,033 E+2 40 3,624 3,579 3,524 3,410 3,266 3,127 3,006 2,935 2,912 2,922 2,914 2,872 2,786 2,656 2,447 2,224 2,037 E+2 30 1,326 1,318 1,311 1,288 1,260 1,231 1,203 1,184 1,174 1,178 1,177 1,173 1,154 1,106 1,030 0,937 0,861 E+3 25 2,700 2,690 2,675 2,654 2,628 2,595 2,560 2,528 2,512 2,516 2,2497 2,245 2,235 2,071 1,955 E+3 20 5,363 5,571 5,591 5,633 5,669 5,678 5,652 5,613 5,593 5,596 5,568 5,499 5,382 5,187 4,944 4,686 4,487 E+3 ANUARY ZONAL MEAN DENSITY (Kg m ⁻³) EIGHT -80 -70 -60 -50 -40 -30 -20 -10 0 10 20 30 40 50 60 70 80 EXPON 60 3,217 5,022 2,794 2,452 2,136 1,941 1,886 1,898 1,906 1,880 1,814 1,700 1,546 1,396 1,334 1,265 1,208 E-5 75 6,768 6,393 5,946 5,294 4,656 4,242 4,119 4,164 4,173 4,105 3,931 3,642 3,265 2,242 2,2781 2,650 2,522 E-5 70 1,514 1,222 1,180 1,079 0,982 0,910 0,878 0,876 0,875 0,885 0,834 0,770 0,692 0,613 0,577 0,590 0,519 E-4 65 2,428 2,339 2,238 2,096 1,933 1,830 1,741 1,711 1,198 1,697 1,699 1,567 1,429 1,280 1,190 1,116 1,037 E-4 65 1,597 7,476 7,511 7,028 6,697 6,346 6,020 5,766 5,768 5,769 5,756 5,535 5,756 5,531 5,090 4,635 4,160 3,748 E-5 0 1,537 1,334 1,349 4,327 4,439 4,368 4,866 4,083 4,010 5,774 1,598 1,398 3,882 3									LATIT	UDE									
75		-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80	EXPON
70 8,941 8,080 7,585 6,786 6,067 5,992 5,440 5,473 5,484 5,408 5,206 4,854 4,392 3,956 3,769 3,591 3,417 E+0 51 1,730 1,547 1,552 1,417 1,288 1,195 1,152 1,148 1,146 1,136 1,199 1,025 0,928 0,831 0,784 0,745 0,705 E+1 52 3,321 3,189 3,032 2,814 2,597 2,426 2,319 2,282 2,273 2,267 2,219 2,101 1,926 1,733 1,616 1,513 1,410 E+1 53 1,107 1,081 1,049 0,998 0,942 0,890 0,847 0,818 0,812 0,816 0,817 0,797 0,757 0,955 0,640 0,582 0,531 E+2 545 1,989 1,956 1,913 1,835 1,747 1,658 1,584 1,537 1,525 1,531 1,531 1,503 1,443 1,345 1,244 1,130 1,033 E+2 540 3,624 3,579 3,524 3,410 3,266 3,127 3,002 2,935 2,912 2,922 2,914 2,872 2,786 2,656 2,447 2,224 2,037 E+2 55 6,791 6,737 6,507 6,509 6,288 6,081 5,892 5,776 5,724 5,724 5,745 5,590 5,572 5,313 4,932 4,473 4,099 E+2 530 1,326 1,318 1,311 1,288 1,260 1,231 1,203 1,184 1,174 1,178 1,177 1,173 1,154 1,106 1,030 0,937 0,861 E+3 52 2,700 2,690 2,675 2,654 2,628 2,595 2,560 2,528 2,512 2,516 2,512 2,497 2,462 2,372 2,235 2,071 1,955 E+3 52 2,700 2,690 2,675 2,654 2,628 2,995 2,560 2,528 2,512 2,516 2,512 2,497 2,462 2,372 2,235 2,071 1,955 E+3 52 2,703 2,690 2,675 2,654 2,628 2,995 2,560 2,528 2,512 2,516 2,512 2,497 2,462 2,372 2,235 2,071 1,955 E+3 53 2,703 2,804 5,504 5,504 4,554 4,554 4,814 1,704 1,754 1,753 1,754 1,066 1,030 0,937 0,861 E+3 54 2,704 2,805 2,807 2,807 2,808 2,908 2,808 2,808 2,518 2,518 2,518 2,518 2,518 2,702 2,355 2,071 1,955 E+3 54 2,428 2,339 2,238 2,938 1,936 1,931 1,886 1,898 1,906 1,880 1,814 1,700 1,546 1,396 1,334 1,265 1,208 E-5 57 1,314 1,252 1,180 1,079 0,982 0,910 0,878 0,876 0,875 0,865 0,834 0,770 0,692 0,613 0,577 0,550 0,519 E-4 65 2,428 2,339 2,238 2,938 1,935 1,830 1,741 1,711 1,698 1,697 1,659 1,557 1,429 1,280 1,190 1,116 1,037 E-4 65 1,337 1,324 1,306 1,262 1,210 1,153 1,103 1,065 1,065 1,065 1,066 1,055 1,017 0,995 0,879 0,795 0,725 e-5 57 1,314 1,252 1,180 1,079 0,982 0,910 0,878 0,876 0,875 0,865 0,834 0,770 0,692 0,613 0,577 0,550 0,519 E-4 65 2,428 2,339 2,238 2,038 6 1,953 1,860 1,741 1,711 1,698 1,697 1,659 1,657 1,599 1,609 0,46		1.590	1.504	1.408	1.290	1.186	1.129	1.119	1,123	1.130	1.118	1.083	1.033	0.960	0.890	0.861	0.815	0.781	E+0
65 1.730 1.647 1.552 1.417 1.288 1.195 1.152 1.148 1.146 1.136 1.099 1.025 0.928 0.831 0.784 0.745 0.705 E+1 60 3.521 3.189 3.032 2.814 2.597 2.426 2.319 2.282 2.273 2.267 2.219 2.101 1.926 1.733 1.616 1.513 1.410 E+1 61 6.130 5.940 5.710 3.372 5.019 4.713 4.483 4.359 4.333 4.346 4.320 4.165 3.893 3.532 3.262 2.993 2.749 E+1 62 1.107 1.081 1.049 0.998 0.942 0.890 0.847 0.818 0.812 0.616 0.817 0.797 0.797 0.995 0.640 0.582 0.531 E+2 63 1.989 1.956 1.913 1.855 1.747 1.658 1.584 1.537 1.525 1.551 1.531 1.501 1.443 1.345 1.244 1.130 1.033 E+2 64 3.624 3.579 3.524 3.410 3.266 3.127 3.006 2.935 2.912 2.922 2.914 2.872 2.786 2.636 2.447 2.224 2.037 E+2 65 6.791 6.737 6.677 6.509 6.288 6.081 5.892 5.776 5.724 5.747 5.735 5.690 5.572 5.313 4.932 4.473 4.099 E+2 67 1.326 1.318 1.311 1.288 1.260 1.231 1.203 1.184 1.174 1.178 1.177 1.173 1.154 1.106 1.030 0.957 0.861 E+3 68 2.700 2.690 2.675 2.654 2.628 2.595 2.560 2.528 2.512 2.516 2.512 2.497 2.462 2.372 2.235 2.071 1.955 E+3 68 2.700 2.690 2.675 2.654 2.628 2.595 2.560 2.528 2.512 2.516 2.512 2.497 2.462 2.372 2.235 2.071 1.955 E+3 68 3.217 3.022 2.794 2.452 2.136 1.941 1.886 1.398 1.906 1.880 1.814 1.700 1.546 1.396 1.334 1.265 1.208 E-5 67 1.514 1.252 1.180 1.079 0.982 0.910 0.878 0.876 0.875 0.865 0.834 0.770 0.692 0.613 0.577 0.550 0.519 E-4 65 2.428 2.339 2.238 2.096 1.953 1.830 1.741 1.711 1.698 1.697 1.697 1.780 1.790 1.280 1.190 1.116 1.037 E-4 65 2.428 2.339 2.238 2.096 1.953 1.830 1.741 1.711 1.698 1.697 1.697 1.429 1.280 1.190 1.116 1.037 E-4 65 2.428 2.339 2.238 2.096 1.953 1.830 1.741 1.711 1.698 1.697 1.697 1.790 1.200 1.900 1.106 1.037 0.692 0.613 0.577 0.590 0.519 E-4 65 2.422 2.339 2.238 2.096 1.953 1.830 1.741 1.711 1.698 1.697 1.667 1.429 1.280 1.190 1.116 1.037 E-4 65 2.422 2.404 2.380 2.318 2.202 2.113 2.065 2.072 2.014 2.017 2.006 1.980 1.929 1.882 1.718 1.562 1.434 E-5 61 1.337 1.324 1.306 1.262 1.210 1.153 1.103 1.065 1.065 1.066 1.066 1.066 1.067 1.280 1.190 1.116 1.037 E-4 62 2.422 2.404 2.380 2.318 2.200 2.143 8.06 2.148 3.131 3.156 3.162 3.06		3.903	3,080	3,421	5.009	6 067	5 502	2,400	5 477	5 404	5.400	5 206	4 054	4 303	1.000	1.000	3 501	1,039	E+0
60 3.221 3.189 3.032 2.814 2.597 2.426 2.319 2.262 2.273 2.67 2.219 2.101 1.926 1.733 1.616 1.513 1.410 E+1 55 6.130 5.940 5.710 5.372 5.019 4.713 4.463 4.359 4.353 4.364 4.320 4.163 3.893 5.525 3.262 2.995 2.749 E+1 50 1.107 1.081 1.049 0.998 0.942 0.890 0.847 0.818 0.812 0.816 0.817 0.797 0.757 0.695 0.640 0.582 0.531 E+2 1.989 1.956 1.913 1.835 1.747 1.658 1.584 1.537 1.525 1.531 1.531 1.503 1.443 1.345 1.244 1.130 1.033 E+2 40 3.624 3.579 3.524 3.410 3.266 5.127 3.006 2.935 2.912 2.922 2.914 2.872 2.786 2.656 2.447 2.224 2.037 E+2 35 6.791 6.737 6.507 6.509 6.288 6.081 5.892 5.776 5.724 5.747 5.735 5.690 5.572 5.513 4.932 4.473 4.099 E+2 30 1.326 1.318 1.311 1.288 1.260 1.231 1.203 1.184 1.174 1.178 1.175 1.175 1.154 1.106 1.030 0.957 0.861 E+3 2 2.700 2.690 2.675 2.655 2.628 2.595 2.560 2.528 2.512 2.516 2.512 2.497 2.462 2.372 2.235 2.071 1.955 E+3 2 5.563 5.571 5.591 5.633 5.669 5.678 5.652 5.613 5.593 5.596 5.568 5.499 5.382 5.187 4.944 4.686 4.487 E+3 3 4 4 4 4 4.686 4.487 E+3 3 4 4 4 4 4.686 4.487 E+3 4 4 4 4.586 4.487 E+3 4 4 4 4 4.586 4.487 E+3 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4		1 730	1.647	1 552	1 417	1 288	1 105	1 152	1 148	1 146	1 136	1 000	1 025	0.028	0.930	0.784	0.745	0.703	E+1
5 6,130 5,940 5,710 5,372 5,019 4,713 4,483 4,359 4,333 4,364 4,320 4,163 3,893 3,532 3,262 2,993 2,749 E+1 5 1,107 1,081 1,049 0,998 0,942 0,990 0,847 0,818 0,818 0,816 0,817 0,797 0,757 0,695 0,640 0,582 0,531 E+2 4 1,989 1,956 1,913 1,835 1,747 1,658 1,584 1,537 1,525 1,531 1,531 1,503 1,443 1,345 1,244 1,130 1,033 E+2 4 0 3,624 3,579 3,524 3,410 3,266 3,127 3,006 2,935 2,912 2,922 2,914 2,872 2,786 2,656 2,447 2,224 2,037 E+2 5 6,916 6,737 6,677 6,509 6,288 6,081 5,892 5,776 5,724 5,747 5,735 5,690 5,727 5,313 4,932 4,473 4,099 E+2 5 1,326 1,318 1,311 1,288 1,260 1,231 1,203 1,184 1,174 1,178 1,177 1,175 1,154 1,106 1,030 0,937 0,861 E+3 2 2,700 2,690 2,675 2,654 2,628 2,595 2,560 2,528 2,512 2,516 2,512 2,497 2,462 2,372 2,235 2,071 1,955 E+3 2 5,563 5,571 5,591 5,633 5,669 5,678 5,652 5,613 5,593 5,596 5,568 5,499 5,382 5,187 4,944 4,686 4,487 E+3 ANNUARY ZONAL MEAN DENSITY (Kg m ⁻³) EIGHT -80 -70 -60 -50 -40 -30 -20 -10 0 10 20 30 40 50 60 70 80 EXPON 80 3,217 3,022 2,794 2,452 2,136 1,941 1,886 1,898 1,906 1,880 1,814 1,700 1,546 1,396 1,334 1,265 1,208 E-5 75 6,768 6,393 5,946 5,294 4,656 4,242 4,119 4,164 4,173 4,105 3,931 3,642 3,265 2,942 2,781 2,650 2,522 E-5 70 1,314 1,252 1,180 1,079 0,982 0,910 0,878 0,876 0,875 0,865 0,834 0,770 0,692 0,613 0,577 0,550 0,519 E-4 60 4,538 4,225 4,083 3,878 3,656 3,450 3,262 3,148 3,131 3,156 3,162 3,066 2,885 2,617 2,396 2,180 1,996 E-4 57 7,997 7,476 7,311 7,028 6,997 6,346 6,020 5,768 5,704 5,758 5,865 5,551 5,900 4,653 4,160 3,748 E-4 50 1,337 1,324 1,306 1,262 1,210 1,153 1,103 1,065 1,065 1,066 1,054 1,017 0,095 0,679 0,795 0,779 0,795 0,772 E-5 30 9,037 9,008 9,012 8,906 8,741 8,584 8,409 8,302 8,221 8,269 8,267 8,285 8,176 7,861 7,289 6,596 6,035 E-3 30 1,889 1,881 1,875 1,864 1,859 1,889 1,881 1,810 1,800 1,800 1,798 1,788 1,767 7,861 7,289 6,596 6,035 E-3 30 1,889 1,881 1,875 1,864 1,859 1,889 1,891 1,810 1,810 1,800 1,800 1,798 1,788 1,767 7,861 7,289 6,596 6,035 E-3 30 2,904 4,008 4,007 4,007 4,006 4,009 4,009 4,009 4,003 4,009 3,067 3,906 3,786 3		3 321	3 180	3 032	2 814	2 507	2.426	2.310	2 282	2 273	2 267	2.219	2.101	1.026	1.733	1.616	1.513	1.410	E41
50 1,107 1,081 1,049 0,998 0,942 0,890 0,847 0,818 0,812 0,816 0,817 0,797 0,797 0,797 0,695 0,640 0,582 0,531 E+2 45 1,898 1,995 1,915 1,835 1,747 1,558 1,984 1,537 1,525 1,551 1,531 1,503 1,483 1,345 1,244 1,130 1,033 E+2 40 3,624 3,579 3,524 3,410 3,266 3,127 3,006 2,935 2,912 2,922 2,914 2,872 2,786 2,636 2,447 2,224 2,037 E+2 35 6,791 6,737 6,597 6,599 6,288 6,081 5,892 5,776 5,724 5,747 5,735 5,690 5,752 5,313 4,932 4,473 4,099 E+2 30 1,326 1,318 1,311 1,288 1,260 1,231 1,203 1,141 1,174 1,178 1,177 1,173 1,514 1,106 1,030 0,937 0,861 E+3 25 2,700 2,690 2,675 2,654 2,628 2,595 2,560 2,528 2,512 2,516 2,512 2,497 2,462 2,372 2,235 2,071 1,955 E+3 20 5,563 5,571 5,591 5,633 5,669 5,678 5,652 5,613 5,593 5,596 5,568 5,499 5,382 5,187 4,944 4,686 4,487 E+5 ANUARY ZONAL MEAN DENSITY (Kg m ⁻³) **EIGHT		6.130	5.940	5.710	5.372	5-019	4.713	4.483	4.359	4.333	4.346	4.320	4.163	3.893	3,532	3.262	2.993	2.749	E+1
45 1,989 1,986 1,913 1,835 1,747 1,658 1,984 1,537 1,525 1,531 1,531 1,503 1,443 1,345 1,244 1,130 1,033 E+2 40 3,624 3,579 3,524 3,410 3,266 5,127 3,006 2,935 2,912 2,922 2,948 2,872 2,786 2,636 2,447 2,224 2,037 E+2 35 6,791 6,737 6,677 6,509 6,288 6,081 5,892 5,776 5,724 5,747 5,735 5,690 5,572 5,313 4,932 4,473 4,099 E+2 30 1,326 1,318 1,311 1,288 1,260 1,231 1,203 1,184 1,174 1,178 1,177 1,173 1,154 1,106 1,030 0,937 0,861 E+3 25 2,700 2,690 2,675 2,654 2,628 2,959 2,560 2,528 2,512 2,516 2,512 2,497 2,462 2,372 2,235 2,071 1,935 E+3 20 5,563 5,571 5,591 5,633 5,669 5,678 5,652 5,613 5,593 5,596 5,568 5,499 5,382 5,187 4,944 4,686 4,487 E+3 ANUARY ZONAL MEAN DENSITY (Kg m ⁻³) BEIGHT -80 -70 -60 -50 -40 -30 -20 LATITUDE (Km) 80 3,217 3,022 2,794 2,452 2,136 1,941 1,886 1,898 1,906 1,880 1,814 1,700 1,546 1,396 1,334 1,265 1,208 E-5 77 1,314 1,252 1,180 1,079 0,982 0,910 0,878 0,876 0,875 0,865 0,834 0,770 0,692 0,613 0,977 0,550 0,519 E-4 65 2,428 2,339 2,238 2,096 1,993 1,830 1,741 1,711 1,698 1,697 1,659 1,567 1,429 1,280 1,190 1,116 1,037 E-4 65 1,338 4,225 4,083 3,678 3,556 3,450 3,262 3,148 3,131 3,156 2,365 2,885 2,617 2,396 2,180 1,097 1,505 1,153 1,153 1,154 1,007 0,799 0,795 0,779 0,795 0	50	1,107	1.081	1.049	0.998	0.942	0,890	0.847	0.818	0.812	0.816	0.817	0.797	0.757	0.695	0.640	0.582	0.531	E+2
40		1,989	1,956	1.913	1,835	1.747	1,658	1.584	1.537	1,525	1.531	1.531	1.503	1.443	1.345	1.244	1.130	1.033	E+2
30 1,326 1,318 1,311 1,288 1,260 1,231 1,203 1,184 1,174 1,178 1,177 1,175 1,154 1,106 1,030 0,937 0,861 E+3 25 2,700 2,690 2,675 2,654 2,628 2,595 2,560 2,528 2,512 2,516 2,512 2,497 2,462 2,372 2,235 2,071 1,955 E+3 20 5,563 5,571 5,591 5,633 5,669 5,678 5,652 5,613 5,593 5,596 5,568 5,499 5,382 5,187 4,944 4,686 4,487 E+3 ANUARY ZONAL MEAN DENSITY (Kg m ⁻³) BEIGHT -80 -70 -60 -50 -40 -30 -20 -10 0 10 20 30 40 50 60 70 80 EXPON (Km) 80 3,217 3,022 2,794 2,452 2,136 1,941 1,886 1,898 1,906 1,880 1,814 1,700 1,546 1,396 1,334 1,265 1,208 E-5 75 6,768 6,593 5,946 5,294 4,656 4,242 4,119 4,164 4,173 4,105 3,931 3,642 3,265 2,942 2,781 2,650 2,522 E-5 70 1,314 1,252 1,180 1,079 0,982 0,910 0,878 0,876 0,875 0,865 0,834 0,770 0,692 0,613 0,577 0,550 0,519 E-4 65 2,428 2,339 2,238 2,096 1,933 1,830 1,741 1,711 1,698 1,697 1,659 1,567 1,429 1,200 1,100 1,116 1,037 E-4 60 4,538 4,225 4,083 3,878 3,656 3,450 3,262 3,148 3,131 3,156 3,162 3,066 2,885 2,617 2,396 2,180 1,996 E-4 57 7,977 7,476 7,311 7,028 6,997 6,346 6,020 5,768 5,704 5,758 5,865 5,756 5,531 5,090 4,653 4,160 3,748 E-4 50 1,337 1,324 1,306 1,262 1,210 1,153 1,103 1,065 1,051 1,066 1,054 1,017 0,955 0,879 0,799 0,772 E-5 45 2,422 2,404 2,380 2,318 2,230 2,143 2,065 2,017 2,014 2,017 2,006 1,980 1,929 1,882 1,178 1,562 1,434 E-3 45 2,422 2,404 2,380 2,318 2,230 2,143 2,065 2,017 2,014 2,017 2,006 1,980 1,929 1,882 1,178 1,562 1,434 E-3 57 9,037 9,008 9,012 8,906 8,741 8,584 8,409 8,302 8,221 8,269 8,267 8,285 8,176 7,861 7,289 6,596 6,035 E-3 58 9,037 9,008 9,012 8,906 8,741 8,584 8,409 8,302 8,221 8,269 8,267 8,285 8,176 7,861 7,289 6,596 6,035 E-3 59 9,037 9,008 9,012 8,906 8,741 8,584 8,409 8,302 8,221 8,269 8,267 8,285 8,176 7,861 7,289 6,596 6,035 E-3 59 9,037 9,008 9,012 8,906 8,741 8,584 8,409 8,302 8,221 8,269 8,267 8,285 8,176 7,861 7,289 6,596 6,035 E-3 50 1,889 1,881 1,875 1,864 1,859 1,864 1,859 1,804 1,800 1,800 1,708 1,		3.624	3,579	3.524	3,410	3.266	3.127	3,006	2,935	2.912	2.922	2.914	2.872	2.786	2.636	2.447	2.224	2.037	E+2
25 2,700 2,690 2,675 2,654 2,628 2,995 2,560 2,528 2,512 2,516 2,512 2,497 2,462 2,372 2,235 2,071 1,935 E+3 5 5,563 5,571 5,591 5,633 5,669 5,678 5,652 5,613 5,593 5,596 5,568 5,499 5,382 5,187 4,944 4,686 4,487 E+3 ANUARY ZONAL MEAN DENSITY (Kg m ⁻³) EIGHT		6.791	6.737	6,677	6.509	6,288	6.081	5,892	5.776	5.724	5.747	5.735	5,690	5.572	5.313	4.932	4.473	4.099	E+2
20 5.563 5.571 5.591 5.633 5.669 5.678 5.652 5.613 5.593 5.596 5.568 5.499 5.382 5.187 4.944 4.686 4.487 E+3 ANUARY ZONAL MEAN DENSITY (Kg m ⁻³) EIGHT -80 -70 -60 -50 -40 -30 -20 -10 0 10 20 30 40 50 60 70 80 EXPONI (Km) 80 3.217 3.022 2.794 2.452 2.136 1.941 1.886 1.898 1.906 1.880 1.814 1.700 1.546 1.396 1.334 1.265 1.208 E-5 75 6.768 6.393 5.946 5.294 4.656 4.242 4.119 4.164 4.173 4.105 3.931 3.642 3.265 2.924 2.781 2.650 2.522 E-5 70 1.314 1.252 1.180 1.079 0.982 0.910 0.878 0.876 0.875 0.865 0.834 0.770 0.692 0.613 0.577 0.550 0.519 E-4 65 2.428 2.339 2.238 2.096 1.935 1.830 1.741 1.711 1.698 1.697 1.595 1.567 1.429 1.208 1.101 1.101 1.037 E-4 60 4.338 4.225 4.083 3.878 3.656 3.450 3.262 3.148 3.131 3.156 3.162 3.066 2.885 2.617 2.396 2.180 1.986 E-4 57 7.597 7.476 7.311 7.028 6.697 6.346 6.020 5.768 5.704 5.758 5.826 5.756 5.551 5.090 4.653 4.160 3.748 E-4 50 1.357 1.354 1.306 1.262 1.210 1.155 1.103 1.065 1.056 1.066 1.054 1.017 0.955 0.879 0.799 0.779 0.724 E-3 45 2.422 2.404 2.380 2.318 2.230 2.143 2.065 2.072 2.014 2.017 2.006 1.980 1.929 1.882 1.718 1.562 1.434 E-3 45 2.422 2.404 4.527 4.439 4.308 4.186 4.085 4.010 5.778 3.988 3.986 3.993 3.882 3.726 3.458 3.140 2.875 E-3 30 9.037 9.008 9.012 8.906 8.741 8.584 8.409 8.302 8.221 8.269 8.267 8.285 8.176 7.861 7.289 6.596 6.035 E-3 30 1.889 1.881 1.875 1.864 1.859 1.849 1.831 1.810 1.800 1.800 1.788 1.786 1.705 1.705 1.596 1.472 1.359 E-2 25 3.992 4.008 4.007 4.037 4.061 4.069 4.069 4.039 4.023 4.021 4.009 3.967 3.906 3.616 3.616 3.611 3.672 3.772 3.7737 E-2																			
EIGHT -80 -70 -60 -50 -40 -30 -20 -10 0 10 20 30 40 50 60 70 80 EXPONENTS (Km) 80 3.217 3.022 2.794 2.452 2.136 1.941 1.886 1.398 1.906 1.880 1.814 1.700 1.546 1.396 1.334 1.265 1.208 E-5 75 6.768 6.593 5.946 5.294 4.656 4.242 4.119 4.164 4.173 4.105 3.931 3.642 3.265 2.924 2.781 2.650 2.522 E-5 70 1.514 1.252 1.180 1.079 0.982 0.910 0.878 0.875 0.875 0.875 0.870 0.652 0.613 0.577 0.550 0.519 E-4 65 2.428 2.339 2.238 2.096 1.953 1.830 1.741 1.711 1.698 1.697 1.659 1.567 1.429 1.280 1.190 1.116 1.037 E-4 64 4.338 4.225 4.083 3.878 3.656 3.450 3.262 3.148 3.131 3.156 3.162 3.066 2.885 2.617 2.396 2.180 1.986 E-4 75 7.597 7.476 7.511 7.028 6.697 6.346 6.020 5.768 5.704 5.758 5.826 5.756 5.531 5.090 4.653 4.160 3.748 E-4 75 7.337 1.354 1.306 1.262 1.210 1.153 1.103 1.065 1.056 1.061 1.066 1.054 1.017 0.955 0.879 0.795 0.772 E-5 75 2.422 2.404 2.380 2.318 2.230 2.143 2.065 2.072 2.014 2.017 2.006 1.980 1.929 1.842 1.718 1.562 1.436 E-5 75 9.037 9.008 9.012 8.906 8.741 8.584 8.409 8.302 8.221 8.269 8.267 8.285 8.176 7.861 7.289 6.596 6.035 E-3 75 9.037 9.008 9.012 8.906 8.741 8.584 8.409 8.302 8.221 8.229 8.267 8.285 8.176 7.861 7.289 6.596 6.035 E-3 75 9.992 4.008 4.007 4.037 4.061 4.069 4.069 4.039 4.023 4.021 4.009 3.967 3.906 3.546 3.641 3.472 1.357 E-2		2.700 5.563	2.690 5.571	2.675 5.591	5,633	2,628 5,669	5,678	2.560 5.652	5,613	5.593	2.516 5.596	2.512 5.568	2.497 5.499	2.462 5.382	2.372 5.187	4.944	4.686	4.487	E+3
EIGHT -80 -70 -60 -50 -40 -30 -20 -10 0 10 20 30 40 50 60 70 80 EXPONENTS (Km) 80 3.217 3.022 2.794 2.452 2.136 1.941 1.886 1.898 1.906 1.880 1.814 1.700 1.546 1.396 1.334 1.265 1.208 E-5 75 6.768 6.593 5.946 5.294 4.656 4.242 4.119 4.164 4.173 4.105 3.951 3.642 3.265 2.924 2.781 2.650 2.522 E-5 70 1.514 1.252 1.180 1.079 0.982 0.910 0.878 0.876 0.875 0.865 0.834 0.770 0.692 0.613 0.577 0.550 0.519 E-4 65 2.428 2.339 2.238 2.096 1.953 1.830 1.741 1.711 1.698 1.697 1.657 1.429 1.280 1.190 1.116 1.037 E-4 60 4.338 4.225 4.083 3.878 3.656 3.450 3.262 3.148 3.131 3.156 3.162 3.065 2.885 2.617 2.396 2.180 1.986 E-4 7.597 7.476 7.511 7.028 6.697 6.346 6.020 5.788 5.704 5.758 5.826 5.756 5.531 5.090 4.653 4.160 3.748 E-4 7.337 1.324 1.306 1.262 1.210 1.153 1.103 1.065 1.055 1.061 1.066 1.055 1.017 0.955 0.879 0.795 0.752 E-5 45 2.422 2.404 2.380 2.318 2.230 2.143 2.065 2.072 2.014 2.017 2.006 1.980 1.929 1.842 1.718 1.562 1.434 E-5 4.571 4.349 4.527 4.439 4.508 4.186 4.083 4.010 5.974 3.988 3.969 3.939 3.882 3.726 3.458 3.140 2.875 E-3 30 1.889 1.881 1.875 1.864 1.859 1.849 1.831 1.831 1.801 1.800 1.800 1.788 1.786 1.786 1.705 1.596 1.472 1.369 E-2 2 3.992 4.008 4.007 4.007 4.009 4.009 4.003 4.009 4.007 4.003 3.967 3.906 3.904 4.007 4.007 4.009 3.967 3.906 3.641 3.472 3.337 E-2	ANUARY	ZONA	L MEAN	DENS	TY (Kg	m ⁻³)													
3.217 3.022 2.794 2.452 2.136 1.941 1.886 1.898 1.906 1.880 1.814 1.700 1.546 1.596 1.334 1.265 1.208 E-5 6.768 6.393 5.946 5.294 4.656 4.242 4.119 4.164 4.173 4.105 3.931 3.642 3.265 2.924 2.781 2.650 2.522 E-5 70 1.514 1.252 1.180 1.079 0.982 0.910 0.878 0.875 0.865 0.834 0.770 0.692 0.613 0.577 0.550 0.519 E-4 65 2.428 2.339 2.238 2.096 1.953 1.830 1.741 1.711 1.698 1.697 1.659 1.557 1.429 1.280 1.190 1.116 1.037 E-4 60 4.338 4.225 4.083 3.878 3.656 3.450 3.262 3.148 3.131 3.156 3.162 3.066 2.885 2.617 2.396 2.180 1.906 E-4 7.597 7.476 7.311 7.028 6.697 6.346 6.020 3.768 5.704 5.758 5.826 5.758 5.551 5.090 4.653 4.160 3.748 E-4 7.597 7.476 7.311 7.028 6.697 6.346 6.020 3.768 5.704 5.758 5.826 5.758 5.551 5.090 4.653 4.160 3.748 E-4 7.597 7.476 7.311 7.028 6.481 7.051	EIGHT	-80	-70	-60	-50	-40	-30	-20			10	20	30	40	50	60	70	80	EXPONE
75 6.768 6.393 5.946 5.294 4.656 4.242 4.119 4.164 4.173 4.105 3.931 3.642 3.265 2.924 2.781 2.650 2.522 E-5 70 1.514 1.252 1.180 1.079 0.982 0.910 0.878 0.876 0.875 0.865 0.834 0.770 0.692 0.613 0.577 0.550 0.519 E-4 65 2.428 2.339 2.236 2.096 1.953 1.830 1.741 1.711 1.698 1.697 1.659 1.567 1.429 1.280 1.190 1.116 1.037 E-4 66 4.338 4.225 4.085 3.878 3.656 3.450 3.262 3.148 3.131 3.156 3.162 3.066 2.885 2.617 2.396 2.180 1.986 E-4 7.597 7.476 7.311 7.028 6.697 6.346 6.020 5.768 5.704 5.758 5.826 5.756 5.551 5.000 4.653 4.160 3.748 E-4 50 1.337 1.324 1.306 1.262 1.210 1.153 1.103 1.665 1.056 1.066 1.054 1.017 0.955 0.879 0.795 0.724 E-3 45 2.422 2.404 2.380 2.318 2.230 2.143 2.065 2.072 2.014 2.017 2.006 1.980 1.929 1.842 1.718 1.562 1.434 E-3 44 5.71 4.549 4.527 4.439 4.308 4.186 4.085 4.010 3.974 3.988 3.969 3.493 3.862 3.726 3.458 3.140 2.875 E-3 50 9.037 9.008 9.012 8.906 8.741 8.584 8.409 8.302 8.221 8.269 8.267 8.285 8.176 7.861 7.289 6.596 6.055 E-3 51 8.891 1.881 1.875 1.864 1.859 1.889 1.831 1.851 1.801 1.800 1.800 1.788 1.786 1.788 1.767 1.703 1.596 1.472 1.369 E-2 53 9.992 4.008 4.007 4.007 4.061 4.069 4.069 4.039 4.023 4.021 4.009 3.967 3.906 3.786 3.541 3.472 3.375 E-2	(Km)																		
70 1,314 1,252 1,180 1,079 0,982 0,910 0,878 0,875 0,875 0,865 0,834 0,770 0,692 0,613 0,577 0,590 0,519 E-4 65 2,428 2,339 2,238 2,096 1,953 1,830 1,741 1,711 1,698 1,697 1,659 1,567 1,429 1,280 1,190 1,116 1,037 E-4 60 4,338 4,225 4,083 3,878 3,656 3,450 3,262 3,148 3,131 3,156 3,162 3,066 2,885 2,617 2,396 2,180 1,986 E-4 7,597 7,476 7,511 7,028 6,697 6,346 6,020 5,768 5,704 5,758 5,866 5,756 5,531 5,090 4,655 4,160 3,748 E-4 6,000 5,737 1,324 1,306 1,262 1,210 1,153 1,103 1,065 1,051 1,061 1,065 1,061 1,017 0,955 0,879 0,795 0,772 E-5 6,000 5,748 2,756 5,758 5	80	3.217	3.022	2.794	2.452	2.136	1.941	1.886	1.898	1.906	1.880	1.814	1.700	1.546	1.396	1.334	1.265	1.208	E-5
65		0.768	1 252	1 100	1.070	4.030	0.010	0.070	0.036	0.075	0.055	0.951	0.042	0.600	0.617	0.577	0.550	0.522	E-3
60 4.338 4.225 4.083 3.878 3.656 3.450 3.262 3.148 3.131 3.156 3.162 3.066 2.885 2.617 2.396 2.180 1.986 E-4 55 7.597 7.476 7.311 7.028 6.697 6.346 6.020 5.768 5.704 5.758 5.826 5.756 5.551 5.090 4.653 4.160 3.748 E-4 50 1.337 1.324 1.306 1.262 1.210 1.153 1.103 1.065 1.056 1.066 1.054 1.017 0.955 0.879 0.795 0.724 E-3 45 2.422 2.404 2.380 2.318 2.230 2.143 2.065 2.027 2.014 2.017 2.006 1.980 1.929 1.842 1.718 1.562 1.434 E-3 45 2.71 4.549 4.527 4.439 4.308 4.186 4.083 4.010 3.974 3.988 3.969 3.493 3.882 3.726 3.458 3.140 2.875 E-3 50 9.037 9.008 9.012 8.906 8.741 8.584 8.409 8.302 8.221 8.269 8.267 8.285 8.176 7.861 7.289 6.596 6.055 E-3 51 8.89 1.881 1.875 1.864 1.859 1.889 1.831 1.631 1.800 1.800 1.798 1.788 1.767 1.703 1.596 1.472 1.369 E-2 52 3.992 4.008 4.007 4.007 4.061 4.069 4.069 4.039 4.023 4.021 4.009 3.967 3.906 3.786 3.561 3.472 2.373 E-2	65	2 420	2 330	2 230	2 006	1.953	1.830	1 741	1 711	1 600	1.607	1.650	1 567	1.420	1 280	1 100	1 116	1.077	E-4
55 7.597 7.476 7.311 7.028 6.697 6.346 6.020 5.768 5.704 5.758 5.826 5.756 5.531 5.090 4.653 4.160 3.748 E-4 50 1.337 1.324 1.306 1.262 1.210 1.153 1.103 1.065 1.056 1.061 1.066 1.054 1.017 0.955 0.879 0.795 0.772 E-5 45 2.422 2.404 2.380 2.318 2.230 2.143 2.065 2.027 2.014 2.017 2.006 1.980 1.929 1.842 1.718 1.562 1.434 E-3 4.571 4.349 4.527 4.439 4.308 4.186 4.083 4.010 3.974 3.988 3.969 3.939 3.882 3.726 3.458 3.140 2.875 E-3 59 0.37 9.008 9.012 8.906 8.741 8.584 8.409 8.302 8.221 8.269 8.267 8.285 8.176 7.861 7.289 6.596 6.035 E-3 30 1.889 1.881 1.875 1.864 1.859 1.849 1.831 1.810 1.800 1.800 1.798 1.788 1.767 1.705 7.596 1.472 1.369 E-2 5 3.992 4.008 4.007 4.037 4.061 4.069 4.069 4.039 4.023 4.021 4.009 3.967 3.906 3.768 5.541 3.472 3.337 E-2	60	4.330	4.225	4.083	1.878	3.656	3.450	3.262	3.148	3.131	3.156	3.162	3.066	2.885	2.617	2 305	2.180	1.086	E-4
50 1,337 1,324 1,366 1,262 1,210 1,153 1,103 1,065 1,056 1,066 1,054 1,017 0,955 0,879 0,795 0,724 E-3 45 2,422 2,404 2,380 2,318 2,230 2,143 2,065 2,027 2,014 2,017 2,006 1,980 1,929 1,842 1,718 1,562 1,434 E-3 40 4,571 4,549 4,527 4,439 4,308 4,186 4,083 4,010 3,974 3,988 3,969 3,939 3,882 3,726 3,458 3,140 2,875 E-3 55 9,037 9,008 9,012 8,906 8,741 8,584 8,409 8,302 8,221 8,269 8,267 8,285 8,176 7,861 7,289 6,596 6,035 E-3 1,889 1,881 1,875 1,864 1,859 1,849 1,831 1,810 1,800 1,800 1,788 1,767 1,703 1,596 1,472 1,369 E-2 25 3,992 4,008 4,007 4,037 4,061 4,069 4,069 4,039 4,023 4,021 4,009 3,967 3,906 3,786 3,641 3,472 3,337 E-2	55	7.597	7.476	7.311	7.028	6,697	6.346	6.020	5.768	5.704	5.758	5.826	5.756	5.531	5.090	4.653	4.160	3.748	E-4
45 2.422 2.404 2.380 2.318 2.230 2.143 2.065 2.027 2.014 2.017 2.006 1.980 1.929 1.842 1.718 1.562 1.434 E-3 4.571 4.549 4.527 4.439 4.508 4.186 4.083 4.010 3.974 3.988 3.969 3.939 3.882 3.726 3.458 3.140 2.875 E-3 59 9.037 9.008 9.012 8.906 8.741 8.584 8.409 8.302 8.221 8.269 8.267 8.285 8.176 7.861 7.289 6.596 6.055 E-3 30 1.889 1.881 1.875 1.864 1.859 1.849 1.831 1.831 1.800 1.800 1.708 1.788 1.767 1.705 1.596 1.472 1.369 E-2 53.992 4.008 4.007 4.037 4.061 4.069 4.069 4.039 4.023 4.021 4.009 3.967 3.906 3.786 3.641 3.472 3.337 E-2	50	1.337	1.324	1.306	1,262	1,210	1,153	1,103	1,065	1.056	1,061	1.066	1,054	1.017	0.955	0.879	0.795	0.724	E-3
40 4.571 4.549 4.527 4.439 4.308 4.186 4.083 4.010 5.974 3.988 3.969 3.959 3.882 3.726 3.458 3.140 2.875 E-3 9.037 9.008 9.012 8.906 8.741 8.584 8.409 8.302 8.221 8.269 8.267 8.285 8.176 7.661 7.289 6.596 6.035 E-3 1.889 1.881 1.875 1.864 1.859 1.849 1.831 1.610 1.800 1.800 1.798 1.788 1.767 1.703 1.596 1.472 1.369 E-2 3.992 4.008 4.007 4.037 4.061 4.069 4.069 4.039 4.023 4.021 4.009 3.967 3.906 3.786 3.641 3.472 3.337 E-2		2.422	2,404	2,380	2.318	2,230	2.143	2.065	2.027	2.014	2.017	2,006	1.980	1,929	1.842	1.718	1,562	1.434	E-3
35 9.037 9.008 9.012 8.906 8.741 8.584 8.409 8.302 8.221 8.269 8.267 8.285 8.176 7.861 7.289 6.596 6.035 E-3 50 1.889 1.881 1.875 1.864 1.859 1.849 1.831 1.810 1.800 1.800 1.798 1.788 1.767 1.703 1.596 1.472 1.369 E-2 5.3992 4.008 4.007 4.037 4.061 4.069 4.069 4.039 4.023 4.021 4.009 3.967 3.906 3.786 3.641 3.472 3.337 E-2	40	4.571	4.549	4.527	4.439	4.308	4.186	4.083	4.010	3.974	3,988	3,969	3,939	3.882	3.726	3.458	3,140	2.875	E-3
25 3.992 4.008 4.007 4.037 4.061 4.069 4.069 4.039 4.023 4.021 4.009 3.967 3.906 3.786 3.641 3.472 3.337 E-2	35	9.037	9,008	9.012	8,906	8.741	8,584	8,409	8,302	8.221	8.269	8.267	8.285	8.176	7.861	7.289	6,596	6.035	E-3
25 3.992 4.008 4.007 4.037 4.061 4.069 4.069 4.059 4.023 4.021 4.009 3.967 3.906 3.786 3.641 3.472 3.337 E-2 8.260 8.322 8.482 8.805 9.165 9.408 9.494 9.524 9.538 9.531 9.385 9.122 8.741 8.536 7.991 7.722 7.591 E-2	30	1.889	1.881	1.875	1.864	1.859	1.849	1.831	1.810	1.800	1.800	1.798	1.788	1.767	1.703	1.596	1.472	1.369	E-2
ZU 8.260 8.322 8.482 8.805 9.165 9.408 9.494 9.524 9.538 9.531 9.385 9.122 8.741 8.336 7.991 7.722 7.591 E-2		3.992	4.008	4.007	4.037	4.061	4.069	4.069	4.039	4.023	4.021	4.009	3.967	3.906	3.786	3,641	3.472	3.337	E-2
	20	0.260	6.522	8.482	8,805	9.165	9.408	9.494	9.524	9.558	9.551	9.385	9,122	8.741	8,336	7.991	1.122	7.591	E-2

TABLE I	1 (con	tinued)					FIGHT	COORDI	NATES								
EBRUAR	Y ZON	IAL MEA	N TEMP	PERATUR	E (K)													
								LATIT	UDE									
(Km)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80	
80 75	179.9	180.3	181.7	189.6	198.3	204.3	205.2	205.0	205.8	206.9	209.3	210.8	214.2	219.5	223.1	222.6	222.2	
70	223.1	221.2	219.8	203.9	216.0	216.2	217.6	217.9	217.6	217.1	218.2	216.0	219.0	225.9	230.7	220.2	233.7	
65	244.1	24D_2	235.0	230.7	227.5	778.4	231.1	251.5	231 3	230 n	228 D	226.7	227 1	220 A	234 2	230 A	245.7	
60	259.7	255.5	251.2	245.9 260.6 271.5 271.5	242.7	243.0	246.3	248.2	248.0	246.4	241.3	237.7	253.3	234.0	240.2	249.3	258.1	
55	271.4	268,1	264.8	260.6	256.8	255.8	257.3	262.2	363.9	262.9	258.2	253.3	246.7	244.3	248.6	257.1	265.4	
50	278.8	276.1	273.3	271.5	268.6	267.1	267,4	270.0	271.4	271.4	269.5	265,1	260.3	254.9	253.3	254.7	257.9	
45	276.9	275.1	273.5	271.5	270.0	267.9	268.3	268,4	269.7	270.2	270.0	266.8	262.3	255.6	250.2	246.8	245.5	
40	267.1	265.6	264.0	262.5 250.0 236.7 226.7	261.6	259.0	258,2	259.0	259.9	260.1	259.6	256,7	252.2	245.5	242.0	239.2	256.7	
35	255.9	255.0	251.8	250.0	247.4	245.8	245.5	244.0	244.9	244.9	245.0	242.3	238.0	232.4	231.9	232.5	231.3	
25	239.4	239.1	230.0	236.7	233.8	231,9	210 5	228.9	217 0	220.8	229.0	228.8	229.1	221,9	216 2	213 6	222.9	
20	232.0	231.2	227 7	221.5	215 1	210 3	207 3	205 3	204 1	204 6	207.0	210.3	214 8	217.6	217 1	213.0	200 1	
15	230 7	229.7	226 1	219.2	212 1	206.2	202.0	100 0	100 8	200 1	202 5	208 3	215 2	218 0	217 0	214 6	210 4	
10	226.1	226.1	225.3	226.5	230.7	235.5	238.7	239.1	239.1	238.9	236.0	228.9	221.6	219.0	217.5	215.6	213.7	
5	239.2	241.6	247.4	256.5	264.8	269.8	272.0	272.3	272.3	272.5	269.4	261.7	252.2	244.3	239.3	235.6	233.0	
0			276.2	226.5 256.5 282.2	290.0	296,3	299.5	300.7	300.6	299.8	295.7	291,2	284.3	277.6	266.5	254.0	247,4	
BRUAR	Y ZON	AL MEA	N PRES	SURE (N m ⁻²)													
								LATIT	UDE									
IGHT Km)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80	EXPONE
80 75	1.320	1.262	1.213	1.173	1.138	1.124	1,130	1.134	1.141	1.144	1.117	1.057	0.974	0.904	0.895	0.881	0.875	E+0
70	7.000	6.715	6,429	6.055	5.691	5.503	5,506	5,536	5.556	5.534	5.306	4.955	4.468	4.028	3.899	3,861	3.822	E+0
65				1,279														
60	2.791	2.729	2,670	2,584	2.473	2.377	2,336	2,338	2,351	2.358	2,294	2.157	1.947	1.733	1.626	1,564	1,500	E+1
55	5.255	5.185	5.121	5.014	4.837	4.652	4.537	4.503	4.517	4.546	4,483	4.268	3,921	3,500	3,236	3.035	2.844	E+1
50	9.682	9,614	9.557	9.419	9,164	8,831	8,596	8,438	8,434	8,497	8,442	8,144	7,601	6.857	6.317	5,849	5,405	E+1
45	1.773	1.769	1.766	1.748	1.707	1,651	1.606	1.572	1,565	1.577	1.571	1,529	1.443	1.322	1.232	1.145	1.056	E+2
35	5,299	5.302	5.300	6.345	5.214	5.120	5,030	5 703	5 744	5 702	5 770	2.903	2.772	2.589	4 004	2.290	2.131	E+2
30	1.255	1.261	1.270	1.271	1.250	1.236	1 206	1 182	1 173	1 170	1 177	1 170	1 147	1 107	1.051	0 987	0 026	E+2
25				2,645														
20	5.366	5,434	5,535	5.644	5,715	5.704	5,652	5,585	5,574	5,596	5,563	5,499	5,388	5,218	5,008	4.774	4.577	E+3
BRUAR	Y ZON	AL MEA	N DENS	ITY (K	g m ⁻³)													
	-80	-70	**	-50	40	-30	-20	LATIT	UDE 0					-				
(IGHT	-60	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80	EXPONE
80 75	2.557	2.439	2,325	2.156	1.998	1.917	1.918	1.926	1.932	1.927	1.860	1.747	1,584	1,435	1.397	1.379	1.372	E-5
70	1.003	1.058	1.019	0.970	0.918	0.887	0.881	0.885	0.890	0.888	0.847	0.785	0.699	0.620	0.589	0.581	0.570	F-4
65	2.044	2,012	1,980	1.932	1,857	1,783	1.748	1,752	1,762	1,770	1.716	1,610	1,442	1.276	1,192	1.144	1,091	E-4
60	3.743	3.720	3.703	3.660	3,549	3,407	3,303	3,281	3,302	3.334	3.312	3,161	2,907	2,580	2.359	2.186	2.024	E-4
55	6.746	6.737	6.736	6.701	6.561	6,336	6.143	5,984	5,962	6.023	6.048	5,869	5,536	4,991	4.534	4.113	3.733	E-4
50	1.210	1.213	1.218	1,209	1.189	1.152	1.120	1,089	1.083	1.091	1.091	1.070	1.017	0.937	0.869	0.800	0.730	E-3
45	2.231	2.241	2,249	2.243	2,202	2.147	2.085	2.040	2.022	2.033	2.027	1,996	1,916	1.802	1.715	1.616	1,499	E-3
40	4.303	4.331	4,362	4.358	4.281	4.203	4.097	3.994	3.956	3.974	3.974	3,939	3.829	3.673	3.518	3.343	3.137	E-3
35	1 824	1 870	1 854	8.840	1 875	1 856	1 827	1 700	1 701	1 704	1 701	5.201	1 774	1 737	1.490	7.046	0.014	E-3
25	3.866	3,922	3.994	4.064	4.101	4.091	4.063	4.014	4.000	4.021	4-014	3.982	3.927	3.822	3.677	3.502	3.350	F-2
20	8.051	8,203	8.468	8.875	9,256	9.448	9.499	9.477	9,511	9,531	9.362	9,109	8.737	8.353	8.036	7.778	7.626	E-2

TABLE I	I (con	tinued)				н	EIGHT	COORDI	NATES								
MARCH	ZON	AL MEA	N TEMP	ERATUR	E (K)													
								LATIT	UDE									
(Km)		-70		-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80	
80	203.1	202.9	201.9	203.7	205.8	205.9	205.3	206.9	208.6	208.6	209.5	211.1	210.2	212.2	214.9	213.8 219.7 224.6 229.9 239.9 253.6 261.2 256.6 243.1 231.8 222.4 218.8 217.2	212.0	
70	223.3	221.8	220.9	217.4	216.6	218.5	219.1	217.7	217.2	216.8	219.8	222.8	224.1	226.9	227.2	224.6	222.1	
65	236.8	233.3	230.3	226.5	226.6	230.3	231.7	230.6	229.8	229.1	229.0	229.9	229.9	232.0	231.0	229.9	228.6	
60	247.1	243.8	241.5	239.3	238,9	241.1	244.4	244.9	245.4	243.6	240.5	239,2	237.9	238.4	238.2	239.9	240.8	
55	256.3	254.2	252.9	253.5	254.2	254.9	256.0	260.6	261,9	260.8	257.2	254.2	252.1	250.5	250.1	253.6	256.5	
50	263.6	263.8	264.5	266.3	267.3	267.3	267.8	270.2	271.5	270.7	268,8	265.9	264.7	262.4	261.1	261.2	261.9	
45	259.7	261.0	263.4	265.7	266.5	266.1	268.3	270.5	271.6	271.5	270.0	267.5	266.0	263.5	260.2	250.0	254.4	
35	235.0	236.7	230 4	241.5	242 1	243 4	244 4	245 5	246 2	246 4	245 4	243 1	240 6	236 4	233.0	231 8	232.0	
30	225.7	227.1	228.3	229.1	229.8	230.2	230.5	230.0	229.7	229.8	230.1	229.3	225.5	221.9	221.0	222.4	224.4	
25	221.6	221.7	223.3	223.2	222.6	221.6	220.7	220.3	219.3	218.9	218.9	218.9	218.4	218.1	218.2	218.8	219.7	
20	224.2	223.8	222.3	219.7	215.3	210.9	207.4	205.6	205.3	205.4	207.3	210.8	215.2	218,2	218.8	217.2	214.6	
15	225.4	225.5	223.4	218.5	212.5	206.4	202.0	199.6	199.3	199.9	202.8	208.6	215.2	218.9	219.4	217.2 217.6 217.6	214.6	
10	224.2	225.9	225.5	224.8	229.0	254.5	258.1	259.2	239.3	230.9	255.7	228.7	254.1	219.0	218.9	237.2	215.8	
ó	233,9	239.0	275.0	281.3	289.7	296.0	299.4	301.0	300.9	300.1	297.0	291.4	284.8	279.0	268.5	256.4	248.2	
RCH	ZON	AL MEA	N PRES	SURE (N m ⁻²)													
IGHT	-80	-70	-60	-50	-40	-30	-20	LATIT	JDE 0	10	20	30	40	50	60	70	80	EXPON
(Km)																		
80	0.953	0.968	1.006	1.040	1.074	1.107	1.135	1.152	1.159	1.145	1.131	1.107	1.051	1.007	0.943	0.880	0.832	E+0
75 70	4 504	4 602	4 903	5 078	5 227	5 350	5 506	5 596	5 606	5 530	5 165	5 141	4 964	2.170	2.019	1.900	1.813	E+0
65																0.844		
60	1.908	1.979	2.099	2.219	2.287	2,297	2,331	2.378	2.393	2.377	2,305	2,198	2.080	1.932	1.804	1.727	1,677	E+1
55	3.722	3.889	4.146	4.390	4.514	4.517	4.555	4.610	4.629	4,612	4.519	4.339	4.130	3.843	3.594	3.414	3,301	E+1
50																6.552		
45	1.351	1.412	1.497	1.572	1,509	1.607	1.611	1.607	1.605	1.604	1.588	1.548	1.485	1.400	1.319	1.254	1.210	E+2
40 35	2.629	2.736	2.883	2.999	5.061	3.056	3.046	5.023	3.008	3.011	2.991	2,935	2.831	2,688	2.559	2.462	2.396	E+2
30	1 107	1 142	1 185	1 217	1 234	1 226	1 212	1 106	1 187	1 188	1 185	1 178	1 155	1 124	1 002	1.060	1.032	E+2
25																2.290		
20	5.084	5,236	5,393	5.546	5,658	5,669	5.647	5.599	5,579	5.593	5.568	5.513	5.420	5,294	5.150	4,993	4.851	E+3
RCH	ZONA	AL MEA	N DENS	ITY (K	g m ⁻³)													
IGHT Km)	-80	-70	-60	-50	-40	-30	-20	-10	O 3OL	10	20	30	40	50	60	70	80	EXPON
80 75	1.635	1.662	1.736	1.778	1.819	1.873	1.926	1.940	1.937	1.912	1.880	1.827	1.742	1,653	1.528	1.433	1.367	E-5
75	7 103	7 160	7 772	9 175	9.407	4,069	9 754	9 010	9.254	4.197	4.055	3.863	3,650	3,408	5.156	3.013 6.256	2.914	E-5
65	1.404	1.463	1.559	1,662	1.710	1.709	1.737	1.778	1.795	1.781	1.717	1.630	1.530	1.422	1.320	1,279	1.248	E-4
60	2,690	2.828	3.027	3.231	3,335	3,319	3.322	3,383	3,398	3.398	3.339	3.202	3,045	2.823	2.639	2,508	2.427	E-4
55	5.059	5,330	5.712	6.032	6.187	6.174	6.199	6.164	6,158	6.161	6.121	5.946	5.707	5.343	5.006	4,690	4,483	E-4
50	0.939	0.983	1.044	1.094	1.118	1.118	1,123	1.116	1.112	1.113	1.106	1.082	1.040	0.982	0.925	0.874	0.839	E-3
45	1.812	1.884	1.980	2.061	2.105	2.104	2.091	2.071	2,058	2,060	2.049	2.015	1.945	1.850	1.766	1.703	1.657	E-3
40 35	7.095	9.006	9.994	4.095	9 667	9.152	4.101	4.037	4.001	4.009	4.006	9.974	3.857	3,709	3.596	3.528	3.474	E-3
30	1.700	1.752	1.800	1.850	1.870	1.855	1.831	1.811	1.800	1.801	1.705	1.780	1.784	1.754	1.721	7.548	1.601	E-3
25	3.730	3.837	3,927	4.022	4.084	4.077	4.049	4.009	4.001	4.015	4.010	3.987	3.955	3.884	3.781	3.647	3.519	E-2
20	7.899	8.149	8.451	8.792	9,155	9,363	9,485	9.487	9.467	9.489	9.357	9.113	8.774	8.452	8.200	8.009	7.874	E-2

		tinued					н	EIGHT (COORDII	MAIES								
APRIL	ZON	AL MEA	N TEMP	ERATUR	E (K)													
HEIGHT (Km)	-80	-70	-60	-50	-40	-30	-20	-10	UDE 0	10	20	30	40	50	60	70	80	
80 75	228.2	224.6	218.3	214.7	211.4	208.2	207.2	210.7	211.3	209.3	208.5	207.5	204.2	201.6	202.0	200.4	199.5	
70	232.9	230.8	228.5	218.4	219.7	218.5	215.9	213.3	212.6	213.9	219.3	222.2	223.9	226.0	227.1	226.9	226.4	
65	241.4	237.9	234.0	228.5	228.3	230.4	228.6	226.1	225.9	226.9	229,6	231.9	233.7	234.9	235.1	234.0	232.8	
60 55	249.9	245.5	241.0	238.5	259.2	240.3	242.0	242.6	243.1	242.1	240.1	241.2	243.1	258 4	244.7	258 8	250 2	
50	258.9	257.2	255.5	257.7	263.4	265.9	267.1	269.2	269.7	269.2	268.2	268.2	269.6	269.5	269.3	269.1	268.7	
45	252.8	252.3	252.2	256.1	260.9	263.8	267.0	269.5	270.2	269.7	269.0	269.2	270.4	270.9	268.7	265.5	263.2	
40 35	237.0	236.2	237.9	243.8	248.6	252.3	257.0	260.4	261.6	261.1	259.5	259.0	260.9	260.0	256.2	252.0	249.2	
30	210.3	211.9	215.0	220.6	225.1	228.4	230.6	231.5	231.0	230.4	231.6	230.7	228.4	226.6	225.8	225.2	225.1	
25	203.6	209.0	216.3	220.6	221.2	221.6	221.5	221.1	220.3	220.1	220,6	220.4	219.4	219.8	221.5	224.3	227.0	
20 15	212.1	214.6	216.9	217.4	214.9	211.3	208.0	206.4	206.0	206.4	208.5	211.6	215.1	218.6	221.1	222.9	224.1	
10	218.3	219.7	220.6	222.0	226.0	231.6	237.0	239.3	239.7	238.9	235.5	229.4	223.5	221.2	221.1	221.5	221.4	
5	233.7	237.8	244.1	252.5	260.7	266.9	271.2	272.4	272.5	272.4	270.2	264.9	257.6	250.8	245.2	240.9	237.9	
0			274.5	280.8	288.9	295.0	298.8	301.0	301.1	300.5	297.8	292.6	286.0	280.5	2/3.1	262.2	255.2	
APRIL	ZON	AL MEA	N PRES	SURE (N m ⁻²)													
HEIGHT	-80	-70	-60	-50	-40	-30	-20	LATIT	UDE	10	20	30	40	50	60	70	80	EXPONEN'
(Km)	-00	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	30	00	70	00	EXPONEN
80	0.798	0.814	0.853	0,915	1,007	1.067	1.097	1,119	1,120	1,109	1,122	1.141	1.148	1,139	1.113	1.072	1.048	E+0
75	1,655	1.704	1.816	1,976	2.201	2.357	2.440	2.473	2.474	2,462	2.484	2,516	2.544	2,532	2.467	2.393	2.349	E+0
70 65				4.216														
60	1.373	1.450	1.592	1.818	2.053	2.194	2.310	2.382	2.392	2.367	2.315	2,290	2.282	2.241	2.173	2.127	2.107	E+1
55	2.673	2.854	3,165	3,621	4.064	4.324	4.519	4.640	4,654	4.619	4.555	4.501	4.465	4.372	4.247	4.149	4.109	E+1
50 45	0.003	1.060	6.186	7.027	1.785	8.226	1.601	1 627	8.752	8.712	8,639	8,536	1 568	1 535	8.023	1 469	1.460	E+1
40	1,979	2,133	2.381	2.646	2.857	2.967	3.039	3.064	3.058	3.050	3.039	3.006	2,953	2.894	2,845	2.820	2.823	E+2
35	4.157	4.489	4.961	5.404	5.741	5.895	5.964	5.955	5.922	5.910	5.922	5.866	5.747	5.653	5.622	5.642	5.695	E+2
30 25	0.916	0.987	2 368	1.149	2 560	2 577	2.570	2 547	2 533	2 537	2 537	2.530	2.507	2.491	2.492	2.515	2.540	E+3
20	4.740	4.956	5.176	5.393	5.563	5.633	5.647	5,610	5.596	5,605	5.579	5.546	5,480	5.404	5,371	5.374	5.388	E+3
APRIL	ZON	AL MEA	N DENS	ITY (K	g m ⁻³)													
								LATIT										
(Km)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80	EXPONENT
80 75	1.219	1.262	1.361	1.484	1.659	1.785	1.845	1.851	1.846	1.845	1.874	1.916	1.958	1.968	1.919	1.865	1.830	E-5
70				6.599														
65	1.001	1.060	1.169	1.351	1.529	1,630	1.729	1,798	1.808	1.782	1.723	1.695	1.684	1,650	1.599	1,569	1.556	E-4
55	1.914	3.057	4.450	2.656 5.073	2.990	5.181	5.325	5.421	5.429	5.406	5.358	5.308	5.271	5.194	5.730	5.026	5.003	E-4
50	0.693	0.749	0.843	0.950	1.030	1.078	1.115	1.131	1.130	1.127	1,122	1.109	1.090	1.067	1.038	1.014	1.006	E-3
45	1.368	1.476	1.655	1.836	1.970	2.044	2.089	2,103	2.099	2.094	2.086	2.059	2.020	1.974	1.941	1.927	1.933	E-3
40 35	2.909	7.126	7.730	3.782	8.500	8.570	8.540	4.099	8.327	8.310	4.080	8.336	8.165	8.086	8.164	8.344	8.504	E-3
30				1.814														
25	3.583	3.706	3.814	3.938	4.032	4.052	4.043	4.014	4.005	4.016	4.007	3.998	3.981	3.948	3.919	3,905	3.898	E-2
20	7.786	8.045	8.314	8.642	9.017	9,286	9.457	9.467	9.464	9.462	9.322	9.133	8.875	8.611	8.463	8.401	8.375	E-2

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HEIGHT COORDINATES
                                      ZONAL MEAN TEMPERATURE (K)
                                                                                                                                                                                          LATITUDE
                                                                                                                          -40
                                                                                                                                                                                                                           0
                                                      -70 -60
                                                                                                   -50
                                                                                                                                                 -30
                                                                                                                                                                       -20
                                                                                                                                                                                                                                               10
                                                                                                                                                                                                                                                                     20
                                                                                                                                                                                                                                                                                                                  40
                                                                                                                                                                                                                                                                                                                                        50
                                                                                                                                                                                                                                                                                                                                                              60
                                                                                                                                                                                                                                                                                                                                                                                      70
 HEIGHT
                                -80
                                                                                                                                                                                             -10
                                                                                                                                                                                                                                                                                            30
                           234,1 229,0 225,3 220,0 214,3 208,0 205,2 207,4 208,2 206,6 203,9 200,7 193,5 187,8 184,9 253,6 231,1 230,0 224,8 218,1 211,3 206,3 204,5 204,5 205,6 207,2 207,1 205,5 206,0 207,3 235,0 235,2 236,6 230,8 223,7 216,9 210,6 206,9 207,4 211,0 215,5 217,5 217,7 220,0 225,1 240,6 241,9 243,7 237,3 231,0 228,9 225,4 222,3 223,4 225,9 228,7 229,9 231,0 233,9 236,7 249,8 250,5 249,3 243,5 238,5 240,1 241,6 243,0 243,5 243,2 242,1 242,8 243,6 247,8 220,9 257,6 257,0 255,2 249,2 238,5 258,5 240,1 241,6 243,0 243,5 243,2 242,1 242,8 243,6 247,8 220,9 257,6 257,0 255,2 249,2 248,1 252,0 256,1 258,5 238,7 266,8 255,2 256,6 259,7 262,8 255,5 256,6 259,7 262,8 255,5 256,0 259,5 254,8 252,3 255,7 261,3 264,8 266,7 266,7 266,5 267,9 269,2 271,2 273,4 275,5 253,6 251,5 246,8 247,1 255,2 261,0 265,3 265,8 266,0 266,4 267,5 269,7 272,9 274,6 275,6 236,7 234,8 231,8 233,7 241,5 249,8 255,5 258,0 258,0 258,0 258,0 259,4 262,9 263,9 263,9 263,9 220,6 217,6 215,0 218,5 228,5 236,2 242,4 246,1 247,3 246,7 245,4 245,7 247,0 247,6 248,0 204,2 202,9 204,7 212,6 220,9 226,9 229,8 231,7 231,4 230,8 251,9 231,9 230,8 230,8 230,8 232,0 204,2 202,2 214,3 213,2 226,1 221,3 220,6 220,8 222,0 221,8 221,3 222,5 224,2 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 248,5 
                                                                                                                                                                                                                                                                                                                                                                            206.1
224.9
238.6
254.7
                                                                                                                                                                                                                                                                                                                                                                                                   205.3
                                                                                                                                                                                                                                                                                                                                                                                                   239.9
                                                                                                                                                                                                                                                                                                                                                                             268.9
277.9
                                                                                                                                                                                                                                                                                                                                                                                                   272.4
                                                                                                                                                                                                                                                                                                                                                                             248.0
                                                                                                                                                                                                                                                                                                                                                                            227.5
226.4
224.8
246.0
           20
15
                                                                                                                                                                                                                                                                                                                                                                                                  230.0
                                     ZONAL MEAN PRESSURE (N m-2)
MAY
                                                                                                                                                                                          LATITUDE
                                -80
                                                      -70
                                                                              -60
                                                                                                    -50
                                                                                                                          -40
                                                                                                                                                 -30
                                                                                                                                                                       -20
                                                                                                                                                                                             -10
                                                                                                                                                                                                                                                                                                                                                                                     70
                            0,674 0,734 0,797 0,846 0,925 0,993 1,377 1,518 1,665 1,792 2,001 2,200 2,815 5,114 3,407 3,733 4,258 4,796 0,570 0,629 0,685 0,763 0,889 1,016 1,132 1,244 1,352 1,532 1,814 2,073
                                                                                                                                                                  1.023 1.034
2.300 2.319
5.129 5.230
1.105 1.141
2.262 2.343
4.429 4.560
8.417 8.617
                                                                                                                                                                                                               1.046
2.343
5.280
                                                                                                                                                                                                                                      1.066
2.390
5.333
                                                                                                                                                                                                                                                            2.462
                                                                                                                                                                                                                                                                                   2.530
                                                                                                                                                                                                                                                                                                          2.596
                                                                                                                                                                                                                                                                                                                                 2.722
                                                                                                                                                                                                                                                                                                                                                      2.863
                                                                                                                                                                                                                                                                                                                                                                              3.014
                                                                                                                                                                                                                                                                                                                                                                                                   3.136
                                                                                                                                                                                                                                                                                                                                                      6.220
                                                                                                                                                                                                               1.149
                                                                                                                                                                                                                                      1.147
                                                                                                                                                                                                                                                            1.152
                                                                                                                                                                                                                                                                                   1.172
                                                                                                                                                                                                                                                                                                          1.204
                                                                                                                                                                                                                                                                                                                                1.246
                                                                                                                                                                                                                                                                                                                                                      1.290
                                                                                                                                                                                                                                                                                                                                                                                                   1.397
          65
60
55
50
                                                                                                                                                                                                                                                                                                                                                                              1.348
                                                                                                                                                                                                                                                                                                                                                                                                                          E+1
                                                                                                                                             2.073
4.097
7.868
                                                                                                                                                                                                                                                            4.596
                             2.195
                                                   2.410
                                                                          2,636
                                                                                                3.026
                                                                                                                       7.031
                                                                                                                                                                                                               4.571
8.634
                                                                                                                                                                                                                                       4.562
                                                                                                                                                                                                                                                                                  4.656
                                                                                                                                                                                                                                                                                                          4.751
                                                                                                                                                                                                                                                                                                                                4.825
                                                                                                                                                                                                                                                                                                                                                      4.920
                                                                                                                                                                                                                                                                                                                                                                             5.062
9.358
                                                                                                                                                                                                                                                                                                                                                                                                   5.177
                                                                                                                                                                                                                                                                                                                                                                                                                          E+1
                                                                                                                                                                  1.584
3.015
5.934
1.213
2.565
5.624
                                                                                                                                                                                                                                     1.620
3.072
5.979
1.212
2.563
5.641
                                                                                                                                             1.494
2.885
5.776
1.200
                                                                                                                                                                                         1.616
3.070
5.984
1.212
           45
                             0.808
                                                   0.892
                                                                         0.999
                                                                                                1.158
                                                                                                                       1.355
                                                                                                                                                                                                                1.620
                                                                                                                                                                                                                                                            1,629
                                                                                                                                                                                                                                                                                   1.640
                                                                                                                                                                                                                                                                                                          1,655
                                                                                                                                                                                                                                                                                                                                1.665
                                                                                                                                                                                                                                                                                                                                                      1,685
                                                                                                                                                                                                                                                                                                                                                                              1.717
                                                                                                                                                                                                                                                                                                                                                                                                   3.237
                                                                                                                                                                                                                                                                                                                                                                              3,202
                                                                                                                                                                                                                                                                                                                                                                                                                          E+2
                                                  3.774 4.309
0.845 0.969
1.993 2.217
4.649 4.993
                                                                                                4.932
1.084
2.399
5.281
                             3.376
                                                                                                                       5.478
                                                                                                                                                                                                                5.970
                                                                                                                                                                                                                                                            6.024
                                                                                                                                                                                                                                                                                   6.036
                                                                                                                                                                                                                                                                                                          6.005
                                                                                                                                                                                                                                                                                                                                6.021
                                                                                                                                                                                                                                                                                                                                                      6.090
                                                                                                                                                                                                                                                                                                                                                                             6.195
                                                                                                                                                                                                                                                                                                                                                                                                   6.276
                                                                                                                                                                                                                                                                                                                                                                                                                         E+2
            35
                             1.793
                                                                                                                      2.512
                                                                                                                                             2.553
                                                                                                                                                                                          2.558
                                                                                                                                                                                                               2.551
                                    ZONAL MEAN DENSITY (Kg m-3)
MAY
                                                                                                                                                                                          LAT! TUDE
                                                                                                                                                                                                                          0
HEIGHT
                                -80
                                                      -70
                                                                            -60
                                                                                                  -50
                                                                                                                       -40
                                                                                                                                                -30
                                                                                                                                                                     -20
                                                                                                                                                                                                                                               10
                                                                                                                                                                                             -10
                                                                                                                                                                                                                                                                    20
                                                                                                                                                                                                                                                                                          30
                                                                                                                                                                                                                                                                                                                 40
                                                                                                                                                                                                                                                                                                                                        50
                                                                                                                                                                                                                                                                                                                                                              60
                                                                                                                                                                                                                                                                                                                                                                                     70
                                                                                                                                                                                                                                                                                                                                                                                                           80 EXPONENT
    (Km)
                          1.003 1.117 1.243 1.340
2.053 2.288 2.522 2.777
0.417 0.461 0.502 0.564
0.826 0.906 0.979 1.120
1.579 1.730 1.889 2.191
2.969 3.267 3.627 4.29
0.562 0.620 0.699 0.816
1.110 1.235 1.410 1.633
                                                                                                                     1.503
3.197
0.663
1.341
2.649
5.077
                                                                                                                                                                  1.737
3.884
0.848
1.709
                                                                                                                                                                                                                                                                                                       2.028 2.164
4.400 4.604
0.914 0.944
1.815 1.857
                                                                                                                                                                                                               1.750
                                                                                                                                            1.664
3.626
0.770
1.547
3.007
5.665
1.049
1.995
4.025
8.519
1.842
4.023
                                                                                                                                                                                                                                                                                   1.939
                                                                                                                                                                                                                                                                                                                                                                                                   2.539
          80
75
70
65
60
55
50
45
40
35
30
25
                                                                                                                                                                                                                                    1.797 1.07.
4.050 4.139
0.881 0.878
1.769 1.754
3.350 3.371
6.187 6.274
                                                                                                                                                                                                                                                                                                                                                     2,303
                                                                                                                                                                                                                                                                                                                                                                                                                         E-5
                                                                                                                                                                                         1.737
3.955
0.881
1.788
3.359
6.145
1.126
2.118
                                                                                                                                                                                                                                                                                   4.255
                                                                                                                                                                                                                                                                                                                                                      4.811
                                                                                                                                                                                                                                                                                 0.890
1.776
3.416
6.323
                                                                                                                                                                                                               0.887
                                                                                                                                                                                                                                                                                                                                                      0.971
                                                                                                                                                                                                                                                                                                                                                                                                    1,049
                                                                                                                                                                                                                                                                                                                                                                                                                         E-4
                                                                                                                                                                                                                                                                                                                                                                                                    2.028
                                                                                                                                                                  3.262
6.025
1.107
2.079
                                                                                                                                                                                                                                     3.350
6.187
1.131
2.119
                                                                                                                                                                                                                                                                                                                               3.515
6.397
1.150
2.112
                                                                                                                                                                                                               3.362
                                                                                                                                                                                                                                                                                                        3.487
6.372
                                                                                                                                                                                                                                                                                                                                                      3.562
6.455
                                                                                                                                                                                                                                                                                                                                                                                                                         E-4
                                                                                                                                                                                                                                                                                                                                                                                                   6.621
                                                  0.620
1.235
2.650
6.042
1.452
3.534
7.929
                                                                        0.699
1.410
3.035
6.982
1.648
3.738
                                                                                               0.816
1.633
3.476
7.863
1.777
3.895
8.559
                                                                                                                     0.958
1.849
3.846
8.351
1.836
3.992
8.875
                                                                                                                                                                                                                                                                                                       1.147
2.112
4.105
8.470
1.842
4.063
9.035
                                                                                                                                                                                                               1.128
                                                                                                                                                                                                                                                            1.132
                                                                                                                                                                                                                                                                                  1.140
                                                                                                                                                                                                                                                                                                                                                      1.158
                                                                                                                                                                                                                                                                                                                                                                              1.173
                                                                                                                                                                                                                                                                                                                                                                            2.167
                                                                                                                                                                                                                                                                                                                                                                                                   2,186
                                                                                                                                                                                                                                                                                                                                                                                                                          E-3
                                                                                                                                                                2.079
4.111
8.528
1.839
4.035
9.366
                            2.368
5.331
1.279
3.332
7.603
                                                                                                                                                                                         4.145
8.471
1.823
4.027
9.447
                                                                                                                                                                                                              4.135
8.411
1.818
4.028
9.479
                                                                                                                                                                                                                                     4.138
8.441
1.830
4.043
9.480
                                                                                                                                                                                                                                                                                                                              4.106
8.471
1.846
4.049
8.818
                                                                                                                                                                                                                                                                                                                                                     4.151
8.555
1.853
4.042
8.639
                                                                                                                                                                                                                                                                                                                                                                            4.211
8.701
1.867
4.038
8.511
                                                                                                                                                                                                                                                                                  4.156
8.559
1.840
4.055
                                                                                                                                                                                                                                                                                                                                                                                                  4.260
8.844
1.884
4.033
                                                                                                                                                                                                                                                            4.166
                                                                                                                                                                                                                                                                                                                                                                                                                          E-3
                                                                                                                                                                                                                                                           1.837
4.042
9.385
```

UNE	ZON	AL MEA	N TEMP	ERATUR	E (K)													
	- 25			-				LATIT						عام ا			22	
EIGHT (Km)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80	
80 75	227.2	223.0	218.9	216.6	211.4	205.1	201.8	203.2	204.1	202.7	201.0	196.8	185.3	178.6	172.6	170.9	170.4	
70	234.6	234.9	236.5	232.5	224.4	215.5	208.2	205.8	206.2	208.0	210.3	211.3	212.6	215.4	220.0	222.7	224.5	
65	243.0	244.3	246.3	241.2	233.9	228.8	224.4	222.0	222.7	223.9	224.4	225.0	229.0	233.4	239.0	242.3	244.7	
60 55	265.0	264.0	258.9	253.2	248.7	251.6	255.1	257.5	257.5	243.3	255.6	257.2	259.7	265.5	269.5	274.7	278.8	
50	267.3	265.1	259.5	254.5	254.7	260.5	264.3	264.8	264.4	264.6 263.1	266.2	267.7	269.8	273.9	277.7	282.2	285.9	
45	257.1	254.9	250.6	247.3	252.8	259.3	263.7	262.5	262.5	263.1	265.2	268.0	271.6	274.3	277.8	281.1	283.4	
40 35	240.1	239.4	235.0	231.4	236.9	247.1	253.4	254.7	255.0	254.7	255.3	257.8	260.8	264.6	267.7	270.7	271.9	
30	199.8	199.9	200.5	206.6	217.1	225.7	228.7	230.7	230.4	230.4	231.5	232.1	233.6	235.1	237.6	239.7	241.1	
25	180.2	188.8	200.4	211.2	218.1	220.7	221.3	220.5	220.3	230.4	221.9	222.5	223.4	225.1	227.8	230.3	232.9	
20	191.3	198.9	206.6	213.3	215.2	212.9	210.2	208.8	208.1	208.6	210.2	212.7	216.7	221.6	225.9	229.6	232.2	
15	198.0	204.0	210.8	215.9	215.6	209.7	203.8	200.8	200.8	201.2	203.3	207.5	213.7	220.1	224.5	227.9	230.7	
5	231.1	235.0	241.7	248.9	255.5	262.7	269.3	272.0	272.2	239.1	272.1	270.2	265.6	260.2	255.9	252.5	249.5	
Ó		237.0	274.2	279.9	286.3	292.0	296.9	300.0	300.7	300.8	299.5	296.2	290.1	283.1	281.3	276.2	271.2	
UNE	ZON	AL MEA	N PRES	SURE (N m ⁻²)													
EIGHT	-80	-70	-60	-50	-40	-30	-20	LATIT	UDE	10	20	30	40	50	es.	70	,	EXPONE
(Km)																		
80 75	0.612	0.690	1.619	0.809	0.879	0.948	0.977	2.236	0.991	1.001	1.028	1.056	1.083	2.843	1.288	1.407	1.501	E+0
70	2,622	2,998	3,333	3,594	4.071	4.664	4.997	5.080	5.090	5,129	5,232	5.440	5.817	6.384	7.049	7.682	8.173	E+0
65	0.529	0.603	0.666	0.728	0.845	0.990	1.084	1.112	1.112	1.114	1.130	1.171	1,243	1.346	1.461	1.580	1.671	E+1
60 55	1.041	2 255	2 505	2 817	3 388	3 000	4 350	4 452	4 440	2.278	4 532	4 689	4 890	5 154	5.454	5.762	5.229	E+1
50	0.373	0.425	0.479	0.546	0.659	0.766	0.830	0.844	0.843	0.844	0.861	0.888	0.922	0.960	1,008	1.054	1.087	E+2
45	0.709	0.812	0.925	1.065	1.276	1.459	1,565	1.594	1,591	1.592	1.617	1,660	1.712	1.772	1.845	1.916	1.963	E+2
40	1.399	1,608	1.855	2.152	2.534	2.833	2.997	3.050	3.046	3.046	3.082	3.145	3.218	3.307	3,420	3.530	3.606	E+2
35	0.645	0.746	0.888	1.039	1.148	1.199	1.218	1.219	1.214	5.987	1.235	1.249	1.265	1.283	1.307	1.333	1.357	E+2
25	1,600	1.810	2.084	2.342	2,499	2,556	2.581	2.579	2.570	2.578	2.601	2.630	2.654	2.682	2.716	2.750	2.782	E+3
20	3,991	4.334	4,783	5.197	5,458	5.579	5,652	5,667	5,658	5,664	5,692	5.726	5.744	5.744	5.749	5.764	5.784	E+3
INE	ZON	AL MEAN	DENS	ITY (K	g m ⁻³)													
EIGHT	-80	-70	-60	-50	-40	-30	-20	LATIT	UDE 0	10	20	30	40	50	60	70	80	EXPONE
(Km)	-00	-10	-00	-30	40	-30		-10		10		,,,	40	,,,	00	70	00	ENT ONE
80	0.938	1.078	1.216	1.301	1.448	1.609	1.687	1.687	1.691	1.721	1.782	1.869	2.036	2.286	2.599	2.867	3.068	E-5
75 70	0.389	0.445	0.491	0.538	0.632	0.754	0.836	0.860	0.860	3.901	0.867	0.897	0.953	1.033	1.116	1.202	1.268	E-4
65	0.758	0.860	0.943	1.052	1.258	1.507	1,682	1.744	1.740	1.734	1.754	1.814	1.890	2.010	2.130	2.271	2.379	E-4
60	1.426	1,612	1.784	2,025	2.464	2.914	3,209	3,278	3,265	3,261	3.331	3.448	3,580	3.740	3,920	4.113	4.255	E-4
55	2.614	2.976	0.647	3.876	4.746	5.512	5.953	6.024	6.006	6.033	6.177	0.352	1 100	1 222	7.049	7.308	7,493	E-4
45	0.960	1,109	1.285	1.501	1.758	1.960	2.067	2.115	2.112	1.111	2.124	2.157	2.196	2.251	2.314	2.375	2.413	E-3
40	2.030	2.340	2.749	3.240	3.726	3.993	4.120	4.172	4.161	4.166	4.206	4.250	4.298	4.354	4.451	4.543	4.620	E-3
35	4.527	5.240	6.335	7.557	8.332	8.581	8.587	8.551	8.498	8.559	8.684	8.752	8.828	8.897	9.039	9.166	9.327	E-3
30 25	3.093	3.341	3.622	3.863	3,992	4.035	4.063	4.074	4.066	1.844	4.084	4.119	4.139	4.151	4.153	4.161	4.161	E-2
20	7.268	7.594	8.065	8.490	8.835	9.127	9.368	9.454	9.469	9.461	9.434	9.381	9.233	9.029	8.866	8.745	8.678	F-2

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TABLE II (confinued)
                                                                                                                                                                                                                                                                                                                                                                                                                                                              HEIGHT COORDINATES
                                                                                              ZONAL MEAN TEMPERATURE (K)
    HEIGHT
                                                                                    -80
                                                                                                                                       -70
                                                                                                                                                                                                  -60
                                                                                                                                                                                                                                                          -50
                                                                                                                                                                                                                                                                                                                    -40
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           40
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            60
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      70
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          -10
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   30
                                                                                                                                                                                   216,8 214,9
222,8 220,5
231,4 227,4
241,1 235,3
251,3 245,5
259,9 252,2
264,0 256,1
258,1 254,5
246,1 240,9
277,5 227,5
206,5 210,4
197,4 211,2
207,8 211,3
206,4 214,2
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210,8 21,3
                                                                       219.9 217.7
224.0 222.6
231.7 250.8
243.6 242.4
258.7 256.1
270.8 267.1
271.9 269.0
261.1 261.0
246.2 249.1
234.0 235.2
209.2 268.5
186.5 194.0
192.2 197.2
192.2 197.2
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            168.3 169.1
195.9 197.9
221.3 224.0
242.9 246.3
260.7 264.6
273.6 278.2
280.4 284.5
278.8 281.1
268.7 269.9
254.2 254.9
254.2 254.9
228.1 230.9
227.9 228.8
228.1 230.9
277.9 228.8
                                                                                                                                                                                                                                                                                                     209.6 204.9
215.0 209.2
219.7 214.2
228.3 224.1
236.6 236.8
247.5 251.1
256.5 262.1
257.0 260.2
226.7 235.6
241.8 248.0
226.7 227.0
219.2 221.0
219.2 221.0
215.1 215.2
215.1 215.2
226.3 229.1
254.7 262.3
264.7 262.3
266.2 291.3
                                                                                                                                                                                                                                                                                                                                                                                                                                                                           201.6 202.1
204.3 204.3
210.1 210.6
224.7 225.8
242.7 244.2
257.9 256.
265.1 264.4
262.0 261.0
252.4 252.5
240.8 241.5
229.1 228.5
220.0 219.4
209.3 206.6
202.1 202.1
237.8 238.1
271.9 271.8
299.5 300.1
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         198.6 189.3

204.6 200.7

210.3 210.9

223.1 224.9

240.8 242.5

254.8 256.9

264.7 267.2

254.2 257.6

242.0 244.5

250.6 234.6

222.1 223.7

212.6 216.3

207.5 212.9

238.6 234.8

298.0 293.1
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205.7
210.7
224.2
239.3
255.2
265.1
262.9
251.5
238.5
221.2
210.9
204.3
235.4
269.2
295.9
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204.8
211.2
225.5
244.5
257.2
264.1
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251.5
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228.8
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209.0
202.5
238.6
271.9
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205.8
210.8
224.3
242.0
255.0
263.9
263.1
251.5
240.8
229.1
220.8
210.5
204.2
239.0
272.1
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            177.7
196.3
213.9
230.6
248.3
262.2
271.1
270.9
261.5
248.4
235.7
225.8
221.6
219.8
230.0
263.6
285.4
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194.6
217.7
237.3
254.8
268.2
275.4
275.3
265.6
251.7
237.7
228.3
226.3
224.6
227.9
                            80
75
70
65
60
55
40
35
30
25
20
15
0
                                                                                          ZONAL MEAN PRESSURE (N m-2)
  JULY
                                                                                                                                                                                                                                                                                                                                                                                                                                                                             LATITUDE
                                                                                                                                          -70
                                                                                                                                                                                                    -60
                                                                                                                                                                                                                                                          -50
                                                                                                                                                                                                                                                                                                                  -40
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 1.003 1.003
2.276 2.271
5.090 5.073
1.096 1.092
2.233 2.222
4.339 4.326
0.822 0.821
1.555 1.554
2.991 2.994
5.910 5.937
1212 1.212
2.578 2.587
5.678 5.689
                                                                                                                                                                                                                                                                                                                                                             0.938 0.982
2.098 2.221
4.613 4.952
0.990 1.070
2.046 2.200
0.701 0.823
1.482 1.552
2.868 2.982
5.784 5.934
1.206 1.223
5.565 2.594
5.591 5.669
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    1,238
3,104
6,979
1,457
2,878
                                                                                                                               0.683
1.460
3.057
                                                                                                                                                                                     0.773
1.653
3.452
                                                                                                                                                                                                                                             0.828 0.881
1.781 1.931
3.756 4.161
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        1.050
2.467
5.556
                                                                                                                                                                                                                                                                                                                                                                                                                                                                           1.000
2.269
5.080
1.097
2.245
4.377
0.829
1.564
3.005
5.949
1.220
2.590
5.689
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   1.006
2.272
5.062
1.093
2.242
4.394
0.838
1.580
3.036
6.018
1.235
2.617
5.732
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            1.126
2.747
6.202
1.317
2.653
5.121
0.960
1.785
3.359
6.515
1.311
2.736
5.848
                            80
75
70
65
60
55
50
45
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35
30
25
20
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5.191
1.124
2.316
4.551
0.867
1.633
3.121
6.164
1.260
2.659
5.796
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              3.457
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            E+0
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    1.198
2.453
4.798
0.910
1.702
                                                                                                                                                                                                                                             0.774
1.559
3.067
0.592
1.140
2.247
4.661
1.022
2.290
5.099
                                                                         0.557
1.087
2.051
0.380
0.716
1.389
2.800
0.601
1.449
3.699
                                                                                                                             0.621
1.218
2.315
0.433
0.817
1.584
3.187
0.686
1.636
3.995
                                                                                                                                                                                     0.702
1.387
2.673
0.508
0.967
1.888
3.845
0.840
1.962
4.577
                                                                                                                                                                                                                                                                                                       0.878
1.804
3.612
0.700
1.341
2.632
5.418
1.156
2.497
5.447
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                1.587
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      1.681
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                3,087
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              E+1
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    2.878
5.470
1.014
1.868
3.482
6.690
1.337
2.773
5.860
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            3.087
5.791
1.062
1.938
3.588
6.849
1.361
2.806
5.874
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    5.242
6.021
1.094
1.983
3.661
6.970
1.383
2.835
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            E+2
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    3.231
6.326
1.265
2.700
5.836
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            E+2
                                                                                          ZONAL MEAN DENSITY (Kg m-3)
  JULY
                                                                                                                                                                                                                                                                                                                    -40
  HEIGHT
                                                                                                                                            -70
                                                                                                                                                                                                                                                          -50
                                                                                                                                                                                                                                                                                                                                                                          -30
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              EXPONENT
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               0 1.783 1.932 2.206 2.541 2.854

7 3.951 4.281 4.873 5.557 6.147

7 0.860 0.918 1.010 1.117 1.213

8 1.756 1.855 1.989 2.139 2.276

7 3.551 3.524 3.723 3.935 4.126

5 6.222 6.507 6.805 7.105 7.373

5 1.141 1.186 1.234 1.282 1.320

5 2.151 2.215 2.295 2.363 2.422

4.278 4.369 4.475 4.367 4.552

8.875 9.013 9.139 9.260 9.387

1.904 1.925 1.937 1.999 1.976

4.171 4.204 4.222 4.232 4.235 4

9.496 9.400 9.193 9.020 8.905 8
                         80
75
70
65
60
55
50
45
40
35
30
25
20
                                                                           0.982
                                                                                                                             1.093
2.284
0.461
0.893
1.657
3.018
0.560
1.090
2.214
4.761
1.147
3.050
7.176
                                                                                                                                                                                   1.242
2.585
0.520
1.014
1.923
3.583
0.670
1.305
2.673
5.887
1.418
3.463
7.863
                                                                                                                                                                                                                                             1.341
2.814
0.575
1.146
2.229
4.237
0.799
1.560
3.250
7.304
1.693
3.778
                                                                                                                                                                                                                                                                                                         1.464
                                                                                                                                                                                                                                                                                                                                                                                                                       1.694
                                                                                                                                                                                                                                                                                                                                                                                                                                                                           1.728
3.869
0.842
1.701
3.223
5.912
1.089
2.079
4.147
8.606
1.855
4.101
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     1.729
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             1.724
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      1.730
                                                                                                                                                                                                                                                                                                                                                                 3,493
                                                                                                                                                                                                                                                                                                                                                               0.750
1.538
3.010
5.647
1.038
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      0.837
1.698
3.227
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0.797
1.464
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1.000
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1.340
2.657
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1.818
3.792
8.325
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3.968
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1.662
3.202
5.915
1.082
2.057
4.131
8.660
1.864
4.085
9.365
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1.691
3.186
5.847
1.083
2.076
4.127
8.525
1.847
4.094
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1.686
3.165
5.859
1.083
2.075
4.147
8.599
1.855
4.093
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E-4
E-4
E-3
E-3
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    2.377
4.269
7.540
1.339
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   6.003
1.106
2.093
4.206
8.705
1.878
4.129
                                                                                                                                                                                                                                                                                                                                                             1.980
4.030
8.626
1.852
4.044
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    2.458
4.725
9.526
1.997
4.233
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            E-3
E-2
E-2
```

(note that 1 N m-2 = 1Pa = 0.01mb = 10dynes cm-2; 1000Kg m-3 = 1g cm-3)

ABLE I							***		COORDII									
NUGUST	ZON	AL MEA	N TEMP	ERATUR	E (K)													
EIGHT	-80	-70	-60	-50	-40	-30	-20	-10	O	10	20	50	40	50	60	70	80	
80	217 8	217 0	218 4	215.4	211 1	207 0	205 4	202 8	20.8 2	204 5	205 %	208.0	106 0	197 7	170 0	177 7	170 0	
75	221 7	221 2	222 6	220 7	216 0	213 3	210 2	207 0	207 0	208 2	200 0	200 7	206 4	202 1	100 2	100 4	202 0	
70 65	227.4	225.9	226.6	224.4 229.2 235.3 245.9 255.9 256.8	220.6	217.3	215.0	213.4	214.8	216.5	217.1	216.4	215.6	216.0	218.8	221.1	224.3	
60	255.4	249.2	241.1	235.3	231.8	234.5	238.2	242.5	244.2	244.7	243.8	241.4	240.7	243.2	248.9	254.8	258.8	
55	270.7	264.1	254.3	245.9	244.2	250.1	255.1	259.0	259.6	258.1	254.1	252.6	253.1	256.5	260.9	265.1	268.7	
50	275.2	270.5	263.4	255.9	256.3	261.3	266.1	267.4	267.1	266.0	263.8	263.1	263.8	267.1	269.2	272.4	275.5	
45	258.9	259.7	255.8	247.8	245.7	249.0	253.3	255.0	254 9	253.5	251.0	252.9	259.9	257.2	259.5	261.6	262.2	
35	244.9	245.7	240.8	233.5	233.0	236.3	240.0	241.3	241.4	240.6	240.4	240.2	241.9	245.1	247.3	248.6	248.7	
30	219.5	221.0	218.9	220.0	224.8	228.1	228.3	228.6	227.9	228.3	228.5	229.6	230.8	233.5	234.7	235.8	236.4	
25 20	183.2	192.8	204.3	215.4	221.0	221.7	220.7	219.2	218.2	218.7	219.5	221.1	222.7	224.5	226.3	227.9	229.4	
15	191.4	196.7	205.8	214.4	215.9	210.5	204.4	202.0	202.0	202.4	204.1	207.2	212.4	219.2	223.9	226.9	229.3	
10	201.0	204.9	210.6	213.4 214.4 217.2 247.9	223.0	229.3	235.3	237.7	237,9	238.5	239.1	238,6	234.8	229.6	227.0	226.4	227.1	
5	229.3	234,4	241.0	247.9	254.5	262.1	269.4	271.8	271.6	271.9	272.4	271.9	268.8	263.2	258.5	254.8	251.5	
0			2/3.0	278.2	285.5	291.0	295.8	544.0	299.9	300.9	300.2	298.9	294.8	287.0	283.8	219.3	2/3.4	
UGUST	ZON	AL MEA	N PRES	SURE (1	w m ⁻²)													
								LATIT	JDE									
EIGHT (Km)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80	EXPONE
80	0.681	0.764	0.843	0.875	0.916	0.980	1.041	1.054	1.061	1.069	1.067	1,060	1.057	1.085	1.147	1.230	1.324	E+0
75	3.074	3.455	3 780	1,881	4.275	2.158	5.073	5 251	2.389	2.396	2.379	2.371	2.418	2.556	2.770	2.989	5.183	E+0
65				0.833														
60	1.246	1.432	1,600	1.714	1.882	2.079	2,237	2.293	2.276	2.254	2,228	2.247	2.329	2.452	2,579	2,692	2.777	E+1
55	2.359	2.756	3.153	3,448	3.812	4.155	4.407	4.465	4.421	4.383	4.363	4.429	4.587	4.801	4.984	5.141	5.250	E+1
45	0.810	0.965	1.142	6.728	1.431	1.518	1.573	1.579	1.564	1.560	1.573	1.603	1.656	1.709	1.752	1.784	1.798	E+1
40	1,535	1.831	2.187	1.295	2.795	2.932	3,003	3.006	2.982	2.985	3.015	3.078	3,160	3.250	3.312	3.356	3.379	E+2
35	3,000	3,567	4.313	5.087	5,656	5,881	5.946	5.931	5,878	5.901	5.982	6,102	6,226	6.367	6.454	6.512	6.551	E+2
30 25				1.074														
20				2.341 5.169														
UGUST	701	U WEAR	n neve	ITY (K	-3,													
00001	2014	IL MEN	UENS	111 101	,													
EIGHT (Km)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	90	60	70	80	EXPONE
80	1.089	1.221	1.344	1.415	1.511	1.641	1.765	1.810	1.818	1.821	1.811	1.811	1.872	2.014	2.222	2.410	2.566	E-5
75	2,288	2.572	2,811	2,969	3,205	3,525	3,838	3,993	4.021	4.010	3,949	3,939	4.081	4.404	4.844	5.223	5,489	E-5
65				0.618														
60				2,537														
55	3.036	3,635	4.319	4.884	5,439	5,788	6.019	6.007	5,932	5,915	5,982	6.109	6.314	6.520	6,655	6,756	6.807	E-4
50 45				0.916														
40				3.543														
35	4.268	5.057	6.240	7,588	8.456	8.670	8.630	8.564	8,482	8.544	8,668	8.852	8,966	9.050	9.091	9.126	9.177	E-3
30	0.986	1.160	1.433	1.700	1.837	1.861	1.868	1.854	1.844	1.850	1.873	1.903	1.923	1.928	1.935	1.939	1.944	E-2
	7 750	5 D4 1	3 444	5 7R7	3.00A	4 057	4.102	4 114	A TOR	A 118	4 140	A 187	4 210	4 708	# 101	4 179	4 161	E-3

								LATIT	UDE									
(Km)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80	
80	212.8	213.6	214.5	211.5	209.7	208.0	206.6	205.5	205.9	206.3	206.0	206.8	205.3	201.8	199.3	200.5	199.1	
75 70	218.6 226.4 236.4 252.6 270.8 277.2 273.5 262.7 237.4 196.6 193.8 201.6 229.5	220.0	223.0	221.6	218.1	214.2	210.5	207.5	207.6	209.1	210.2	211.5	210.7	209.2	208.8	209.8	209.4	
65	236.4	233.4	232.6	231.9	229.6	227.6	226.6	226.5	226.9	228.5	230.1	229.8	226.9	226.2	229.6	232.8	236.3	
60	252.6	245.8	239.8	237.1	236.2	237.3	238.5	241.4	242.4	242.3	242.8	240.2	238.6	238.8	241.1	243.6	247.2	
55	270.8	261.2	250.9	246.9	248.2	252.4	255.5	258.4	258.9	257.9	254.5	253.3	252.1	251.6	252.0	253.7	256.0	
50	278.0	269.4	260.7	256.7	259.0	263.2	266.7	268.1	268.4	267.4	266.0	265.3	264.4	263.5	262.5	262.2	261.7	
45	277.2	270.9	263.5	258.3	259.1	263.2	267.1	268,2	268.2	267.1	265.6	263.5	263.2	262.8	260.9	258.3	256.4	
35	262.7	257.3	246.1	236.6	235.3	238.8	242.3	244.5	244 0	243.1	241.7	240.4	239.6	239.7	238.5	234.8	232.9	
30	237.4	235.0	229.0	225.1	225.7	228.3	229.5	229.7	229.6	229.7	229.7	228.7	228.7	228.4	228.0	226.7	225.5	
25	202.4	208.1	214.1	220,8	222.9	221.8	220.2	219.2	218.2	218.3	219.1	220.1	221.0	221.6	222.0	221.8	221.4	
20	196.6	200.5	208.3	216.7	218.3	214.6	210.8	209.0	208.7	208.8	210.2	212.8	216.0	219.6	222.0	223.0	223.3	
15	193.8	198.7	207.2	215.8	216.7	210.6	204.4	201.7	201.6	201.8	203.2	206.3	212.0	218.2	222.2	224.1	225.2	
5	229.5	234.2	241.2	248 3	255 6	263.4	260 6	271 9	272 0	272 3	272 2	270.8	266 1	250.4	253 8	249.5	246.5	
ó			274.1	278.8	285.3	291.0	295.9	299.1	299.8	300.8	300.3	298.5	293.5	286.1	281.3	275.5	268.6	
SEPTEMB	ER ZON	AL MEA	N PRES	SURE (N m ⁻²)													
EIGHT	-80	-70	-60	-50	-40	-30	-20	LATIT	UDE	10	20	30	40	50	60	70	80	EXPONE
(Km)	-00		-00	20	- 40	-30	-20	-10			20			20	00	,,,	-	En ort
80 75	0.881	0.898	0.931	0.962	1.007	1.052	1,084	1.089	1.087	1.092	1.093	1.077	1.041	1.005	0.989	0.971	0.960	E+0
70	4 - 055	4.106	4.182	4.368	4.664	4.990	5 258	5 381	5.367	5 34 3	5 306	5 191	5 062	A 957	A ROR	4.775	4 739	E+0
65	0.838	0.852	0.866	0.906	0.975	1.053	1.117	1.149	1.145	1.133	1,118	1.094	1.076	1.056	1.034	1.000	0.986	E+1
60	1.00/	1.720	1.703	1.002	2.002	2.100	2.290	2.330	2.334	2.305	2.201	2.228	2.208	2.172	2.107	2.022	1.972	E+1
55	5.849	6 280	5.498	7 227	7 762	9 217	9 579	9 660	9.574	9 506	9.450	4.398 8.388	9.377	4,309	9 007	7.631	7 360	E+1
45	1.072	1.173	1.282	1.387	1.481	1 554	1.606	1.617	1.600	1 501	1 588	1 580	1.580	1 563	1 521	1.456	1.410	E+2
40	1.981	2,193	2.444	2,690	2.877	2,982	3.049	3.058	3.024	3.017	3.027	3.027 5.996	3.030	3.003	2.944	2.844	2.770	E+2
35	3.712	4.167	4.767	5.391	5.782	5,937	5.982	5.973	5.913	5,916	5.964	5,996	6.017	5.970	5.887	5.747	5,633	E+2
30	0.730	0.827	0.972	1.124	1.207	1.225	1.223	1.217	1.206	1.208	1.220	1.233	1.239	1.230	1.217	1.198	1.181	E+3
25 20	3.740	4.121	4.693	5.218	5.535	5,641	5,686	5,692	5.667	5.672	5.709	2.621 5.732	5.721	5.652	5.574	5.499	5.436	E+3
EPTEMB	ER ZON	AL MEA	N DENS	ITY (K	g m ⁻³)													
								LATIT	UDE									
(Km)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80	EXPONE
80 75	1.442	1.464	1.513	1.585	1.673	1.762	1.828	1.846	1.840	1.844	1.848	1.814	1.766	1.734	1.729	1.687	1.679	E-5
70	6.239	6.324	6.387	6.702	7.250	7.895	8.438	8.761	8.723	8.614	8.467	8,272	8.127	7.967	7.777	7.542	7.453	E-5
65	1,235	1,272	1,297	1.362	1.479	1,611	1.717	1.767	1.758	1.728	1,692	1,658	1.652	1,627	1.569	1.497	1.454	E-4
60	2.300	2,438	2,562	2.720	2,953	3.178	3.354	3.391	3.355	3.315	3.252	3,231	3,224	3,169	3.044	2.892	2,780	E-4
55	4.076	4.451	4.857	5,236	5,625	5,928	6.161	6.187	6.119	6,080	6.087	6.048	6.048	5,965	5.767	5.463	5,240	E-4
50 45	0.733	0.813	0.902	0.981	1.044	1.088	1.121	1.126	1.113	1.108	1.108	1.101	1.103	1.092	1.063	1.014	0.981	E-3
40	2.523	2.847	3,292	3.758	4.041	4.120	4.130	4.123	4.077	4.085	4.132	2.088	4.160	4.146	4.108	4.026	3.940	E-3
35	4.923	5.642	6.748	7.937	8,560	8,661	8.579	8,510	8,442	8,478	8,595	8,689	8.749	8,676	8.598	8,525	8,426	E-3
30	1.071	1.226	1.479	1.739	1.863	1.869	1.856	1.846	1.829	1.833	1.851	1.877	1.887	1.876	1.859	1.841	1.824	E-2
25	2.729	2.991	3.411	3.793	4.013	4.078	4.107	4.110	4.093	4.102	4.124	4.149	4.150	4.114	4.066	4.019	3.980	E-2
20	6.627	7.162	7.849	8,388	8,833	9,157	9,397	9,485	9,459	9,466	9.462	9,386	9,226	8,969	8,747	8,592	8,481	E-2

TABLE I	(con	tinued)				н	EIGHT	COORDI	NATES								
OCTOBER	ZON	AL MEA	N TEMP	ERATUR	E (K)													
EIGHT	-80	-70	-60	-50	-40	-30	-20	-10	UDE 0	10	20	30	40	50	60	70	80	
80	200 2	201.0	203.0	202 7	204 7	205.0	206 %	208 %	211 8	211.0	208 4	208 8	210 7	213 4	215 1	220 B	221 8	
75	215.6	217.3	219.1	217.5	215.5	212.7	208.9	207.2	208.4	209.6	210.6	212.5	214.3	216.8	220,6	223,6	225.9	
70	228.2	228.8	229.1	227.6	224.7	221.4	217.9	212.9	211.8	212.9	216.0	218.2	219.0	221.0	225,6	228.0	230.5	
65	250.5	230.4	230.0	235.9	233.9	231.7	240.0	241.6	241 0	225.3	241 2	229.7	230 0	227,4	240.0	244 0	240.4	
55	267.2	261.7	256.5	254.7	254.6	255.1	255.4	257.5	258.6	258.1	256.3	254.4	252.4	249.7	247.8	249.7	253.3	
50	279.3	273.1	267.7	264.9	266.3	267.5	268.1	268.1	268,6	268.0 268.1	266,5	266.0	263.7	259.0	256.5	255,8	256.3	
45	284.0	277.1	269.8	266.2	266.1	267.5	268.3	268.5	268.8	268.1	266,4	263.9	261.3	257,1	252.5	249.2	247.8	
40 35	283.6	274.1	261.6	255.0	254.6	255,7	258.3	260.0	260.3	259.3	256,4	252.3	249.1	245.4	259.2	232.6	228.9	
30	242.8	238.5	232.0	226.7	225.8	228 9	231.1	230.8	231.4	231.5	230.7	239.3	225.1	227.1	218.5	215.6	211.4	
25	216.6	220.2	225.8	224.6	222.9	221.5	220.3	219.6	218.9	219.2	219.9	220.2	219.5	218.2	216.4	213.7	210.6	
20	209.0	212.0	216.4	219.6	218.4	213.9	210.1	208.3	208.1	208.1	209.4	211.7	214.5	217.2	218.4	217.1	215,1	
15	203.1	207.6	214.0	218.5	216.8	210.2	203.9	200.5	200.1	200.4	202.1	206.3	212.0	215.9	220.0	220.6	220.2	
5	205.0	236 0	242 0	249.8	257 4	250.2	255.8	271 0	238.7	238.7	237.5	255.4	262.0	223.2	248 4	220.6	220.5	
ó	233,1	230,7	276.4	280.5	286.4	292.1	296.5	299.3	300.1	300.9	300.1	297.0	291.1	203.5	277.0	268.3	261.6	
TOBER	ZON	AL MEA	N PRES	SURE (N m ⁻²)													
								LATIT										
(IGHT (m)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80	EXPON
80										1.098								
75	2.504	2.511	2.491	2.453	2.479	2.498	2,479	2.437	2.424	2.424	2.418	2.338	2.190	2.014	1.889	1.761	1,680	E+0
65	1.094	1 002	1.078	1.069	1.097	1 126	1 144	1 156	1 156	1,147	1 122	1.072	1 003	0.012	0.998	0.762	0.715	E+0
60	2.182	2,185	2,162	2,152	2.217	2.286	2.336	2.365	2.367	2.351	2.289	2.185	2.055	1.877	1,694	1.533	1.418	E+1
55	4.171	4.222	4.230	4.226	4.359	4,494	4.596	4.624	4.617	4.592	4.487	4.311	4.072	3.733	3.375	3,028	2.768	E+1
50										8,665								
45	2 544	2 689	2 825	2 890	2 970	3 030	3 073	3 076	3.061	1.618	1.596	2 059	2 854	2 702	2 510	2 300	2 119	E+2
35	4.682	5.057	5.489	5.718	5.881	5.973	6.005	5.973	5.943	5.952	5.958	5.875	5.724	5.486	5.210	4.892	4.571	E+2
30	0.908	0.997	1.113	1.183	1,219	1,226	1,220	1.211	1,203	1.206	1.215	1.211	1.193	1,158	1.115	1.069	1.020	E+3
25 20	1.908	2.098 4.600	5.023	2.510 5.379	2.594 5.591	2.599 5.655	2.583 5.669	2.564 5.652	2.549 5.627	2.556 5.641	2.573 5.658	2.577 5.644	2.558 5.585	2.503 5.461	2,438 5,323	2.360 5.194	2.284 5.084	E+3
TOBER	ZON	AL MEA	N DENS	ITY (K	g m ⁻³)													
								LATIT	UDE									
IGHT (m)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80	EXPON
80	1.950	1.954	1.937	1.907	1.907	1.905	1.873	1.828	1.808	1.813	1.823	1.770	1.653	1.515	1,422	1.310	1.244	E-5
75										4.029								
70 65	1.612	1.610	1.587	1.579	1.633	1.692	1.741	1.782	1.701	8.750	1.714	1.625	1.535	1.300	1.251	1 125	1.036	E-5
60	3.025	3.065	3.072	3,080	3,192	3,302	3,390	3,411	3,409	3.391	3,306	3,175	2.995	2.744	2.459	2.189	1,982	E-4
55	5.439	5.619	5.745	5.780	5.964	6.137	6.269	6.257	6,221	6.198	6.099	5,903	5.621	5,207	4.744	4.225	3,807	E-4
50	0.962	1.010	1.045	1.061	1,086	1.111	1,132	1.135	1.130	1.126	1.112	1.073	1.030	0.971	0.892	0.803	0.728	E-3
45	1.721	1.834	1.937	1.984	2.038	2.077	2.110	2.115	2.104	2.102	2.087	2.036	1.966	1.872	1.752	1.601	1.466	E-3
55	6.063	6.774	7.725	2,299	8.564	8,608	8.539	8,420	8.373	8.432	8.544	8.551	8.456	8.245	7,996	7,775	7.479	E-3
30	1.302	1.456	1.67	1.818	1.881	1.866	1.839	1.827	1.811	1.815	1.835	1.850	1.846	1.817	1.778	1.727	1,681	E-2
25	3.069	3.320	3.610	3.892	4.054	4.086	4.085	4.067	4.056	4.063	4.076	4.077	4.059	3.996	3.924	3.847	3.779	E-2
20	7.071	7.561	8.087	8,534	8,917	9,208	9.400	9,451	9.420	9,443	9,413	9.287	9.070	8.758	8,491	8.333	6.234	E-2

(note that 1 N m⁻² = 1Pa = 0.01mb = 10dynes cm⁻²; 1000Kg m⁻³ = 1g cm⁻³)

```
TABLE II (continued)
                                                                                                                                HEIGHT COORDINATES
NOVEMBER ZONAL MEAN TEMPERATURE (K)
                                                                                                                                     LATITUDE
                                                                                                                                        -10
HEIGHT
                        -80
                                        -70
                                                        -60
                                                                        -50
                                                                                       -40
                                                                                                        -30
                                                                                                                       -20
                                                                                                                                                                          10
                                                                                                                                                                                          20
                                                                                                                                                                                                          30
                                                                                                                                                                                                                          40
                                                                                                                                                                                                                                          50
                                                                                                                                                                                                                                                         60
                                                                                                                                                                                                                                                                          70
                                                                                                                                                                                                                                                                                          80
   (Km)
                                   184.7 187.5 190.8 196.4 201.6 205.2 208.7 211.8 211.8 209.8 211.2 215.4 219.9 222.4 226.1 207.9 209.1 208.4 208.3 208.1 208.4 207.8 208.1 208.7 210.5 213.9 218.4 223.0 227.3 227.3 227.3 223.5 223.9 221.9 220.3 218.5 216.6 213.4 210.9 211.0 213.9 218.5 222.9 227.1 231.6 230.4 239.1 236.9 235.3 233.3 231.0 229.7 228.2 226.1 229.4 227.2 229.1 229.7 232.5 237.1 236.8 235.9 251.4 248.7 245.6 244.4 243.2 245.0 244.8 244.2 242.2 240.2 238.3 239.8 245.1 246.0 270.2 266.2 263.5 261.5 258.8 256.8 257.6 258.6 258.3 255.0 253.1 250.3 249.8 250.5 254.3 280.3 276.7 274.2 275.0 271.9 269.8 267.0 266.5 266.4 265.3 263.5 269.2 252.5 249.8 251.4 281.4 278.4 278.4 276.4 275.1 272.6 269.8 267.0 266.5 266.4 265.3 263.3 259.2 252.5 249.8 251.4 274.2 269.5 267.0 265.5 264.3 260.0 259.6 257.6 266.2 263.5 259.2 252.5 249.8 251.4 274.2 269.5 267.0 265.5 264.3 260.0 259.6 257.5 252.5 252.5 249.8 251.4 274.2 269.5 267.0 265.6 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 260.2 
                     182.1 184.7 187.5
206.5 207.9 209.1
226.3 225.6 223.9
240.6 239.1 236.9
259.3 255.9 251.4
273.7 270.2 266.2
                                                                                                                                                                                                                                                                                   227.9
230.0
236.5
                                                                                                                                                                                                                                                                    254.3 256.2 260.2 261.7
        50
                      283.7
                     284.4
277.7
263.3
        40
                                                                                                                                                                                                                                                                                    231.4
        30
                     246.6
                                                                                                                                                                                                                                                                                    201.0
                    233.8 231.8 227.9 222.0
236.1 225.4 223.4 220.4
214.8 216.5 219.0 222.5
235.6 238.7 244.5 252.1
        20
15
                                                                                                                                                                                                                                                                                    208.7
                                                                                                                                                                                                                                                                                   216.9
NOVEMBER ZONAL MEAN PRESSURE (N m-2)
                                                                                                                                    LATITUDE
HEIGHT
                                        -70
                                                        -60
                                                                       -50
                                                                                      -40
                                                                                                      -30
                                                                                                                       -20
                                                                                                                                                                          10
                                                                                                                                                                                          20
                                                                                                                                                                                                          30
                                                                                                                                                                                                                         40
                                                                                                                                                                                                                                         50
                                                                                                                                                                                                                                                         60
                                                                                                                                                                                                                                                                         70
                                                                                                                                                                                                                                                                                          80 EXPONENT
   (Km)
                     1.396
3.303
7.141
                                     1.376
                                                                     1.247
                                                                                     1.198
                                                                                                     1.160
                                                                                                                     1.131
                                                                                                                                     1.101
                                                                                                                                                                                                                                   0.873
                                                                                                                                                                                                                                                   0.827 0.768 0.715 E+0
1.738 1.605 1.486 E+0
                                                     1.312
                                                                                                                                                     1-086
                                                                                                                                                                    1-082
                                                                                                                                                                                    1.066
                                                                                                                                                                                                     1-023 0-947
                                                                                                                                     2.449
                                                                                                                                                                    2.388
                                                                                                                                                                                    2,356
                                                                                                                                                                                                    2,240 2,044
        70
                                     6,961
                                                     6.579
                                                                     6.242
                                                                                     5.953
                                                                                                     5.725
                                                                                                                     5,556
                                                                                                                                    5.419
                                                                                                                                                    5.330
                                                                                                                                                                    5.295
                                                                                                                                                                                    5.175
                                                                                                                                                                                                    4.849
                                                                                                                                                                                                                    4.353
                                                                                                                                                                                                                                    3,898
                                                                                                                                                                                                                                                    3.603
                                                                                                                                                                                                                                                                    3,338
                                                                                                                                                                                                                                                                                    3.092
                                                                                                                                                                                                                                                                                                    E+0
                      1,466
                                     1.432
                                                     1.361
                                                                                                                                                                     1.141
                                                                                                                                                                                     1,105
                                                                                                                                                                                                     1,025
                                                                                                                                                                                                                    0.912
                                                                                                                                                                                                                                    0.808
                                                                                                                                                                                                                                                    0.737
                                                                                                                                                                                                                                                                    0.685
                                                                                                                                                                                                                                                                                    0.635
                                                                                                                                                                                                                                                                                                    E+1
        65
                                                                                                     1,204
                                                                                                    2.433 2.383 2.341 2.332 2.325
4.739 4.556 4.553 4.526 4.521
8.906 8.787 8.617 8.557 8.553
                     2.870
                                                     2.708
                                                                     2,595
                                                                                    2,505
                                                                                                                                                                                    2.255
                                                                                                                                                                                                   2,090
                                                                                                                                                                                                                    1.867
                                                                                                                                                                                                                                    1.643
                                                                                                                                                                                                                                                    1.482
                                                                                                                                                                                                                                                                     1.373
                                                                                                                                                                                                                                                                                    1.273
                                                     5-182
                                                                     4.999
                                                                                                                                                                                                                    3.707
                                                                                                                                                                                                                                    3,263 2,928
                                                                                                                                                                                                                                                                                                    E+1
        55
                                     5.348
                                                                                     4.856
                                                                                                                                                                                   4.416
                                                                                                                                                                                                    4.128
                                                                                                                                                                                                                                                                    2.687
                                                                                                                                                                                                                                                                                    2,480
                                     9.843
                                                                                    9.091
                                                                                                                                                                                    8.392
                                                                                                                                                                                                    7.891
                                                                                                                                                                                                                                    6.327
                                                                                                                                                                                                                                                    5.676
                                                                                                                                                                                                                                                                     5.164
        45
                     1.782
                                     1.792
                                                   1.762
                                                                     1.716
                                                                                     1.676
                                                                                                     1.647
                                                                                                                     1.635
                                                                                                                                    1.612
                                                                                                                                                    1.603
                                                                                                                                                                    1.603
                                                                                                                                                                                    1.574
                                                                                                                                                                                                    1.490
                                                                                                                                                                                                                    1.366
                                                                                                                                                                                                                                   1.223
                                                                                                                                                                                                                                                    1.101
                                                                                                                                                                                                                                                                   0.996
                                                                                                                                                                                                                                                                                   0.911
                                                                                                                                                                                                                                                                                                    F+2
                                                                                                                                                                                                                                                                                                    E+2
        35
                    6.066
                                    6.185 6.207
                                                                     6.118 6.024
                                                                                                     5.987
                                                                                                                    5.970
                                                                                                                                    5.901
                                                                                                                                                    5.881
                                                                                                                                                                    5.895
                                                                                                                                                                                    5.840
                                                                                                                                                                                                    5,676
                                                                                                                                                                                                                    5.401
                                                                                                                                                                                                                                                    4.654 4.272
1.026 0.958
                                                                                                                                                                                                                                                                                   3.942
                                                                                                                                                                                                                                    5.034
                                                                                                                                                                                                                                                                                                    E+2
                                                                                                                                                                                                                                   1.090
                                                                                                                                                                                                                                                                                                   F+3
                                   2.473 2.545 2.583 2.596 2.583 2.570 2.541
5.122 5.345 5.502 5.613 5.644 5.658 5.607
                                                                                                                                                                    2.533
NOVEMBER ZONAL MEAN DENSITY (Kg m-3)
                                                                                                                                  LATITUDE 0
                                                                      -50
                                                                                     -40
                                                                                                                     -20
                                                                                                                                                                          10
                       -80
                                      -70
                                                      -60
                                                                                                     -30
                                                                                                                                                                                         20
                                                                                                                                                                                                          in
                                                                                                                                                                                                                         40
                                                                                                                                                                                                                                                         60
HEIGHT
                                                                                                                                                                                                                                         50
                                                                                                                                                                                                                                                                         70
                                                                                                                                                                                                                                                                                         80 EXPONENT
   (Km)
                                                                                   2,125 2,002 1,920 1,838 1,787 1,780
4,568 4,581 4,232 4,107 4,018 3,986
0,941 0,913 0,994 0,885 0,880 0,874
1,859 1,815 1,782 1,763 1,767 1,764
                    2.671
                                     2.596
                                                     2.438
                                                                    2.276
                                                                                                                                                                                    1.770
                                                                                                                                                                                                    1.687
                                                                                                                                                                                                                    1.532
                                                                                                                                                                                                                                    1.383
                                                                                                                                                                                                                                                                     1.184
                                                                                                                                                                                                   3.648 3.260
0.774 0.680
        75
70
                                                                                                                                                                                   3.899
                                                                                                                                                                                                                                   2.898 2.664 2.461
0.598 0.542 0.505
                                                                    4,805
                                                                                                                                                                                                                                                                                    2.271 E-5
                                     1.075
                                                                    0.980
                     1.099
                                                     1.024
                                                                                                                                                                                                                                                                                   0.468
                                                                                                                                                                                                                                                                                                   E-4
                                                                     1,922
                                                                                                                                                                                    1.695
                                                                                                                                                                                                     1.559
                                                                                                                                                                                                                    1.384
                                                                                                                                                                                                                                    1.210
                                                                                                                                                                                                                                                    1.082
                                                                                                                                                                                                                                                                     1.007
                                                                                                                                                                                                                                                                                    0.936
                                                                   1,922 1,859 1,815 1,782 1,763 1,767 1,764 5,655 3,555 3,546 8,5413 3,330 3,318 3,16 6,608 6,469 6,379 6,317 6,157 6,095 6,096 1,185 1,160 1,141 1,135 1,124 1,119 1,118 2,163 2,123 2,105 2,111 2,098 2,094 2,094 4,159 4,100 4,101 4,106 4,071 4,062 4,071 8,501 8,465 8,458 8,423 8,298 8,262 8,262 8,290 1,847 1,861 1,845 1,830 1,811 1,798 1,803 3,955 4,058 4,072 4,072 4,037 4,019 4,025
                                                                                                                                                                                  3.244
6.009
1.102
2.055
       60
55
50
45
                    3.856
                                                                                                                                                                                                   3.031 2.729
5.682 5.159
                                                                                                                                                                                                                                   2.387 2.123
4.552 4.072
                                                                                                                                                                                                                                                                    1.944
                                                                                                                                                                                                                                                                                   1.794
                                     3.846
                                                     3.753
                                                                                                                                                                                                                                                                                                    E-4
                     1.210
                                     1.223
                                                    1.212
                                                                                                                                                                                                    1.044 0.961
                                                                                                                                                                                                                                   0.858
                                                                                                                                                                                                                                                   0.771
                                                                                                                                                                                                                                                                   0,691
                                     2.218
                     2.183
                                                                                                                                                                                                                                                                                    1.253
                                                                                                                                                                                                                                                                                                   E-3
                    4.073 4.175
8.026 8.289
1.665 1.733
3.542 3.674
7.351 7.696
                                                   4.214
8.476
1.800
3.848
                                                                                                                                                                                   4.030
8.341
1.815
4.027
                                                                                                                                                                                                   3.935 3.774
8.302 8.128
1.816 1.806
4.018 3.986
                                                                                                                                                                                                                                   3.532 3.276
7.832 7.389
1.766 1.704
3.905 3.813
        40
35
30
25
                                                                                                                                                                                                                                                                   2.997
6.921
                                                                                                                                                                                                                                                                                   2.753
                                                                                                                                                                                                                                                                                                   E-3
  (note that 1 N m^{-2} = 1Pa = 0.01mb = 10dynes cm^{-2}; 1000Kg m^{-3} = 1g cm^{-3})
```

TABLE 11							н	CIGHT	COORD II	MIES								
ECEMBER	ZONA	IL MEA	N TEMP	ERATUR	E (K)													
HEIGHT	-80	-70	-60	-50	-40	-30	-20	-10	UDE	10	20	30	40	50	60	70	80	
(Km)				-	-		-				-	-			-			
80	171.6	173.4	1/6.2	182.2	190.7	199.0	203.9	206.2	208.3 207.9 214.0 231.8 250.6 261.5	207.9	206.6	209.9	215.8	220.6	222.8	226.1	229.3	
75 70	200.4	200.8	201.1	201.5	202.9	205.3	207.8	207.6	207.9	207.8	208.7	212.3	219.2	223.9	227.6	228.3	229.8	
65	245 7	243.4	240 3	210.0	210.0	230 1	214.3	214.0	231 0	213.3	213.5	220 5	227 8	221.1	232.9	230.5	233.0	
60	266.3	262 5	257.7	253.5	248 8	246 7	246 8	250.3	250.6	249.2	244 0	230.7	233.0	237.0	244.2	248 6	249 4	
55	281.2	276.8	271.8	267.8	263.7	260.8	259.1	260.8	261.5	260.6	257.0	251.7	246.2	245.6	250.2	256.4	258.5	
50	288.8	284.9	280.6	276.6	273.8	271.0	268.9	266.4	265.7	265.8	265.7	262.9	258.2	253.5	254.2	258.6	260.1	
45	287.2	284.5	281.6	278.3	276.3	272.5	268.7	264.9	263,8	264.1	266.8	264.7	259.6	249.4	246.6	249.1	250.5	
40	277.8	275.7	272.8	269.9	266.7	263.6	260.0	257.3	256.9	257.2	258.6	255.3	247.1	236.9	233.0	233.6	235.6	
35	263.4	261.8	258.4	254.7	251.6	248.9	246.1	244.8	256.9 245.3	245.3	244.4	240.1	233.7	223.8	219.3	217.6	219.5	
30	245.0	244.9	242.7	238.0	234.7	231.7	230.2	228,6	228.6 218.7 205.6 198.9	229.2	228.3	227.5	223.1	217.1	211.3	203,6	201.0	
25	236.2	235.4	232.8	228.4	224.7	222.2	220.4	219.5	218.7	218.8	219.2	218.7	217.4	214.5	209.0	201.1	193.8	
20	236.1	234.0	229.3	222.3	215.7	211.0	208.0	206.5	205.6	206.0	207.8	210.5	214.2	215.9	214.1	209.2	204.3	
15	231.9	230.1	226.8	220.9	213.5	206.9	202.2	199.4	198.9	199.2	201.6	207.2	213.5	217.0	216.7	213.6	210.4	
10	223.1	222.6	222.7	224.0	227.6	232.9	237.3	238.8	238.9	238.3	235.3	228.9	222.2	219.3	217.9	216.1	214.8	
5	240.9	243.0	247.0	253.9	261.7	267.7	271.2	272.1	272.3	272.4	270.1	263.1	254.1	246.5	240.9	236.7	233.4	
0			275.0	281.5	288.6	294.6	298.2	300.2	300.5	300.3	298.1	293.0	286.0	279.1	268.1	257.0	251.6	
ECEMBER	ZONA	L MEA	N PRES	SURE (N m ⁻²)													
								LATIT										
(Km)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80	EXPONE
80	1.563	1.492	1.391	1,285	1.207	1.150	1.121	1.108	1.102	1.086	1.064	1.014	0.924	0.830	0.796	0.736	0.688	E+0
75	3.845	3.650	3,366	3.066	2.815	2,623	2.516	2.478	2.451	2,418	2.372	2,234	1.987	1.758	1.672	1,535	1,425	E+0
70	8.439	8.019	7.417	6.793	6.245	5,812	5,550	5,468	5,416	5.349	5.252	4,864	4.237	3.685	3,455	3.172	2,935	E+0
65	3 310	1.043	1.000	2 900	2.644	2.407	2 101	2 316	1.147	2 205	2 253	2 104	1.046	1.566	0.703	1 204	1 100	EAT
									4.396									
									0.829									
	1 083	1 054	1 802	1 813	1 747	1 681	1 620	1 576	1 561	1 562	1 563	1 506	1 381	1 107	1 058	0.400	0.440	6+2
40	3.603	3.563	3.475	3.349	3.244	3.145	3.058	2.997	1.561	2.975	2.958	2.872	2.680	2.393	2.138	1.871	1.703	E+2
35	6.731	6.684	6.558	6.370	6.213	6.069	5.952	5.857	5.811	5.811	5.782	5.673	5.412	4.989	4.521	3.964	3.585	E+2
30	1.309	1.304	1,291	1.266	1.246	1.226	1,209	1,195	1.184	1.183	1.181	1.169	1,136	1.076	0.994	0.887	0.802	E+3
25	2,662	2,653	2,638	2,624	2,607	2,587	2,565	2.542	2,525	2.520	2.517	2.498	2,452	2.365	2.235	2.065	1.916	E+3
20	5,463	5,472	5,507	5.577	5,630	5,650	5,641	5,616	5,591	5,577	5,557	5,496	5.377	5,205	4,988	4.728	4,500	E+3
ECEMBER	ZONA	L MEA	N DENS	ITY (K	g m ⁻³)													
								LATIT	UDE									
(Km)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80	EXPONEN
80	3.174	2.998	2.750	2.457	2.204	2.014	1.915	1.872	1.843	1.819	1.794	1.684	1.491	1.311	1.245	1.134	1.045	E-5
75	1 307	1 240	1 165	1.002	1.007	0.044	0.000	0 889	4.105	0.074	0.960	0.780	0.666	0.564	0.513	0 474	0.470	E-3
65	2.441	2 350	2 223	2 082	1.007	1 881	1 703	1.740	0.881	1.721	1.601	1.370	1.360	1.151	1.029	0.474	0.436	E-4
60	4.340	4.232	4.062	3.850	3.702	3.527	3.360	3.222	3.185	3.194	3.205	3.057	2.750	2.301	2.011	1.799	1.659	F-4
55	7.587	7.484	7.260	6.947	6.717	6.454	6.198	5.941	5.857	5.877	5.950	5.761	5.256	4.450	3.870	3,392	3,101	E-4
50	1.333	1.322	1,292	1.246	1,207	1.167	1,126	1.097	1.087	1.088	1,091	1.058	0.975	0.845	0.741	0.646	0.589	E-3
45	2,405	2.392	2,341	2,270	2.202	2,150	2,101	2.073	2.061	2,061	2.041	1,981	1.853	1,673	1,495	1,300	1,182	E-3
40	4.518	4.502	4.438	4.323	4.237	4.156	4.097	4.058	4.034	4.029	3.985	3,920	3.778	3,519	3.196	2.791	2.519	E-3
35	8,902	8.894	8.841	8.713	8,603	8.494	8.425	8.333	8.252	8.254	8.241	8,229	8.058	7.764	7.181	6.346	5.689	E-3
30	1.861	1.854	1.852	1.853	1.850	1.843	1.830	1.821	1.805	1.799	1.802	1.790	1.773	1.727	1.639	1.518	1.390	E-2
									4.020									
20	8.061	8,144	8.367	8,739	9.092	9.325	9,448	9,474	9.470	9,433	9.316	9.098	8.744	8.398	8.116	7.874	7,673	F- 2

2.3.1a PLANETARY WAVES

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CLIMATOLOGICAL DISTRIBUTION

Figures 1 and 2 show the mean temperature field at various pressure levels for January and July for both hemispheres. In summer (July in the Northern Hemisphere, January in the Southern Hemisphere) the fields are nearly zonally symmetric, but in winter large longitudinal variations are evident. These are mainly of low wave number, i.e., they may be represented by Fourier analysis around the globe using just a few (one or two) waves. This is the basis for representing the climatology of longitudinal variation in terms of wave components, since the fields may be defined with fewer values than by using a grid in longitude that has a sufficiently small interval to adequately represent the smooth variations.

Figures 3.1-3.24 and Table I give the amplitude and phase of temperature and geopotential height for wave numbers one and two, with ln(pressure) as the vertical coordinate. The fields were calculated and plotted at pressure intervals of 0.2 in ln(pressure) and at latitude intervals of 4 deg, but were interpolated to intervals of 0.5 in ln(pressure) (approximately 3.5 km) and 10 deg latitude for tabulation.

These tables and figures give wave coefficients for the monthly mean temperature fields. Thus they represent the quasi-stationary planetary waves.

The convention used for phase angle is such that the reconstructed temperature is given by:

$$T(\lambda) = T_0 + T_1 \cos(\lambda - \phi_1) + T_2 \cos(2\lambda - \phi_2)$$

where T₀ is the zonal mean, T₁ and T₂ are wave number one and two amplitudes, ϕ_1 and ϕ_2 are wave number one and two phases, and λ is longitude (deg E). T₀, T₁, T₂, ϕ_1 and ϕ_2 all depend on latitude and pressure and are to be found from the tables (T₀ are given in Table I in Section 2.2). Thus for wave number one the maximum occurs at longitude ϕ_1 , and the minimum at ϕ_1 + 180 deg E. For wave number two the maxima are at $\phi_2/2$ and $\phi_2/2+180$ deg E, and the minima at $\phi_2/2+90$ and $\phi_2/2+270$. The same convention applies to geopotential height.

Contour levels for the amplitude figures are: temperature: 0.5, 1, 2, 4, 6, 8, 10, etc. geopotential height: 2, 4, 8, 16, 32, 64, 80, etc. Phase is contoured at 30 deg intervals; however phases are only given in the figures at places where the amplitude exceeds 0.5 K for temperature and 4 dam for geopotential height. This contour is given as a dashed line on the phase figures to mark the edge of the contoured regions. The tables contain phase values at all locations, and amplitudes are plotted over the whole domain irrespective of their size.

For a discussion of the relation between geometric and geopotential height and the extent to which they can be used interchangeably, see Section 2.2.

GENERAL FEATURES OF MEAN PLANETARY WAVE DATA

The following general observations can be made from the amplitude and phase sections of temperature and geopotential height (Figures 3.1-3.24):

- Wave amplitudes are small in the tropics throughout the year, slightly larger in the summer season at mid- and high latitudes and much larger during the winter season.
- 2) Maximum amplitudes occur at about 60-70 deg north or south during winter.
- 3) In the Northern Hemisphere wave number two amplitudes are substantially smaller than wave number one. In the Southern Hemisphere both wave number one and two amplitudes are smaller than in the Northern Hemisphere, but their amplitudes are comparable with each other.
- 4) Amplitudes are generally largest in the stratosphere and lower mesosphere and although they decay above the mid-mesosphere, they remain relatively large up to the top level.
- 5) Where the amplitude is large (midlatitude winter), the phase normally tilts westward with increasing height, and for wave number one with decreasing distance from the equator. Wave number two phase does not exhibit a clear overall latitudinal tendency.

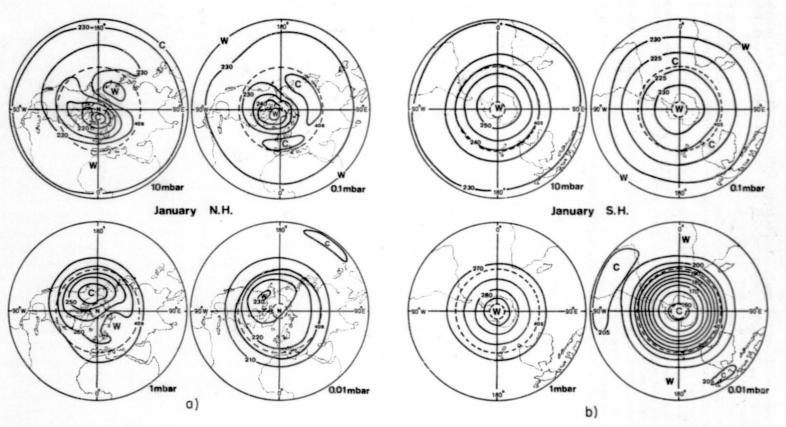


Figure 1.

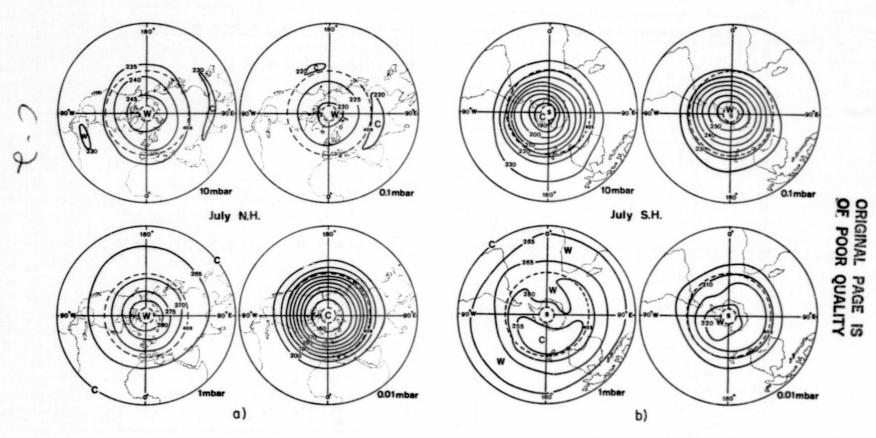


Figure 2.

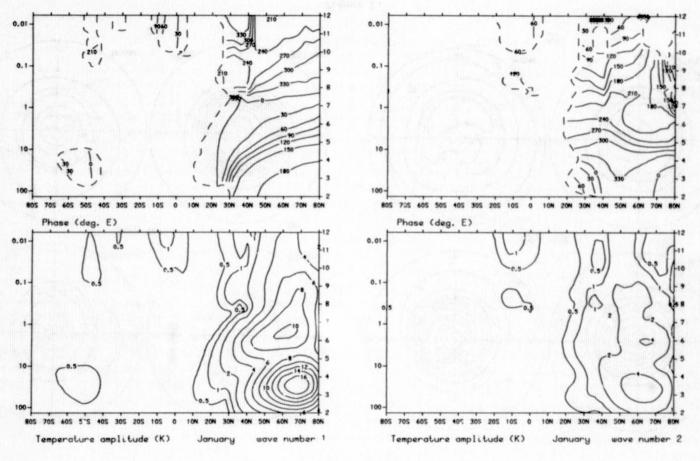


Figure 3.1

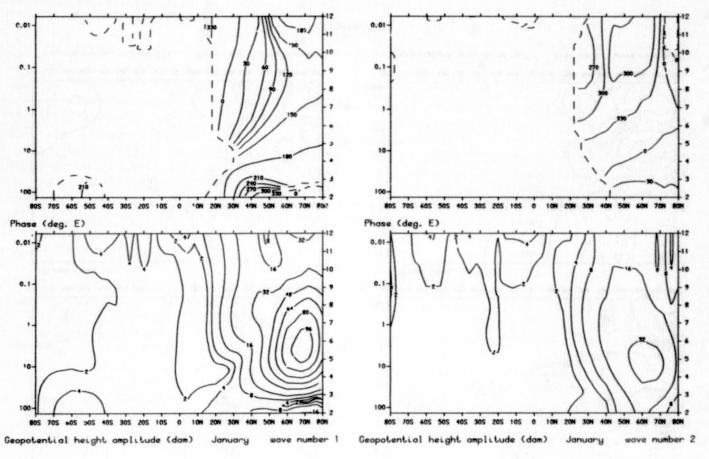


Figure 3.2

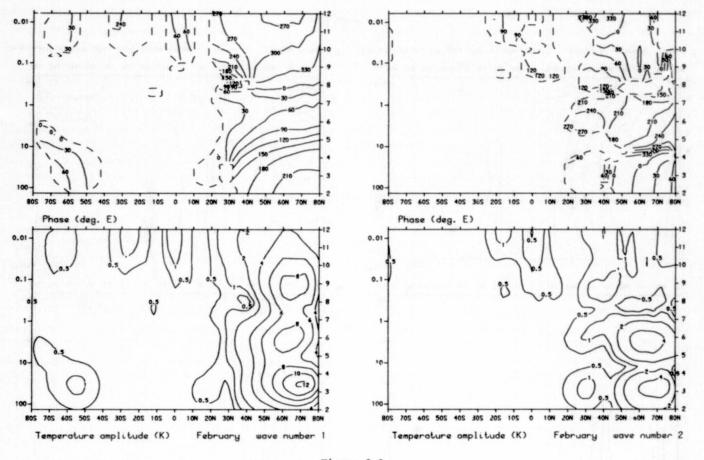


Figure 3.3

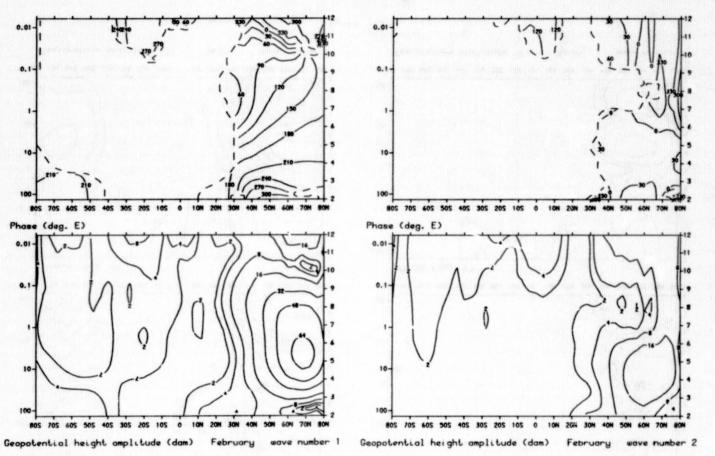


Figure 3.4

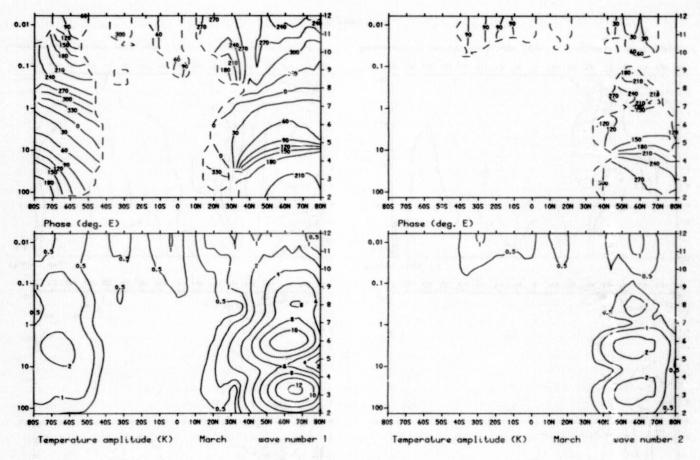


Figure 3.5

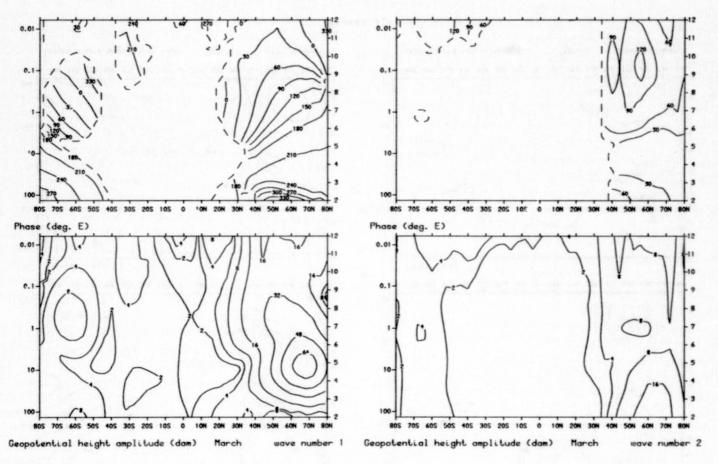


Figure 3.6

167

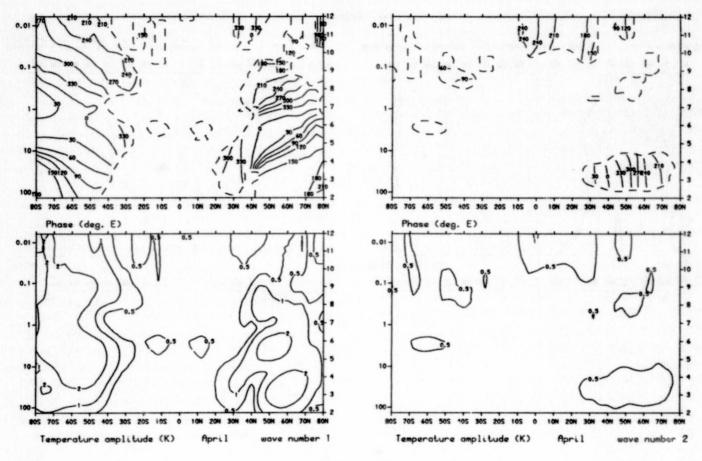


Figure 3.7

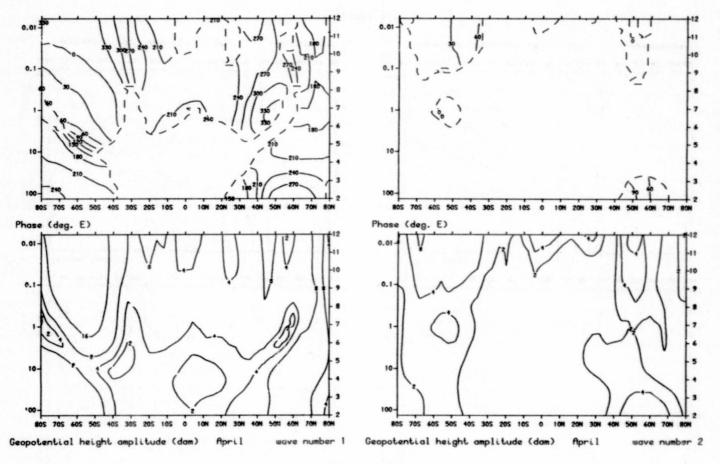


Figure 3.8

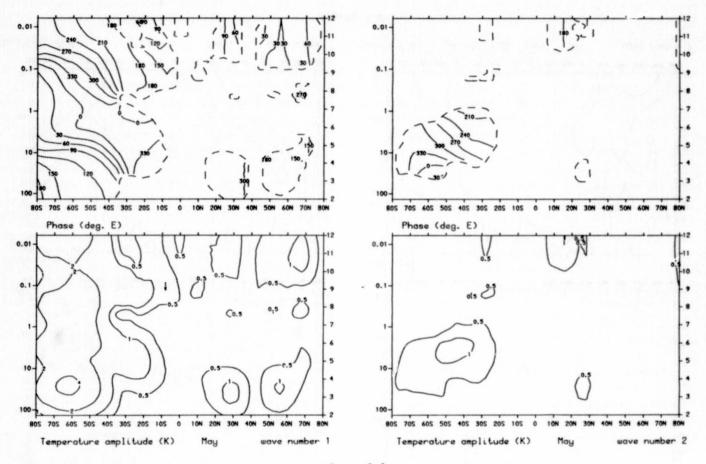


Figure 3.9

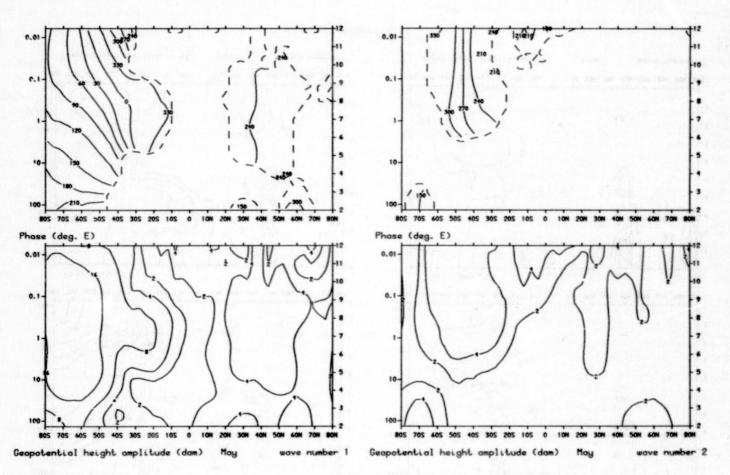


Figure 3.10

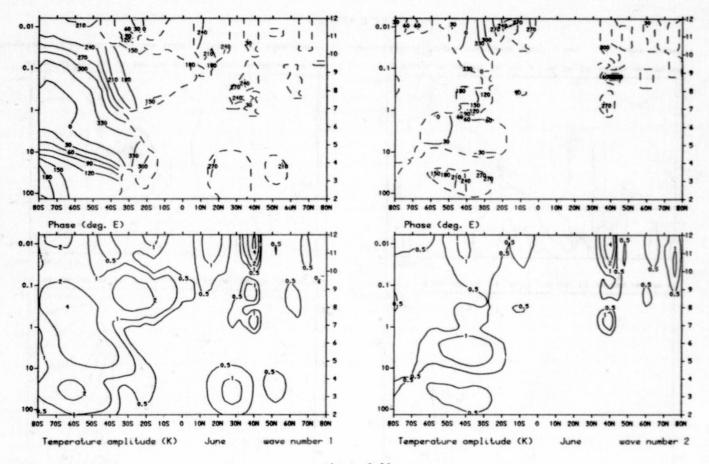


Figure 3.11

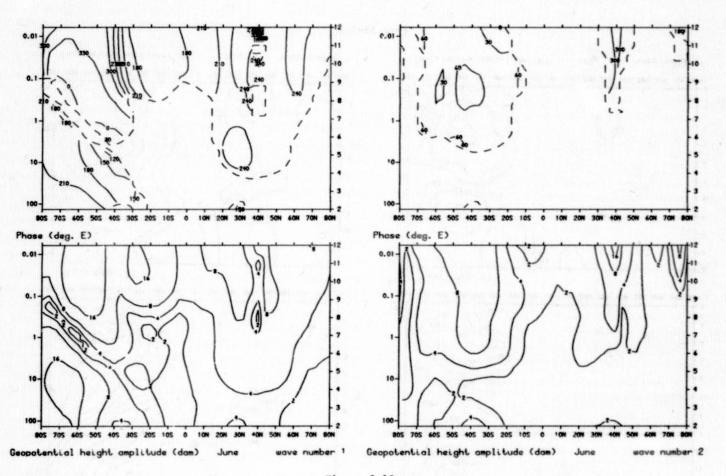


Figure 3.12

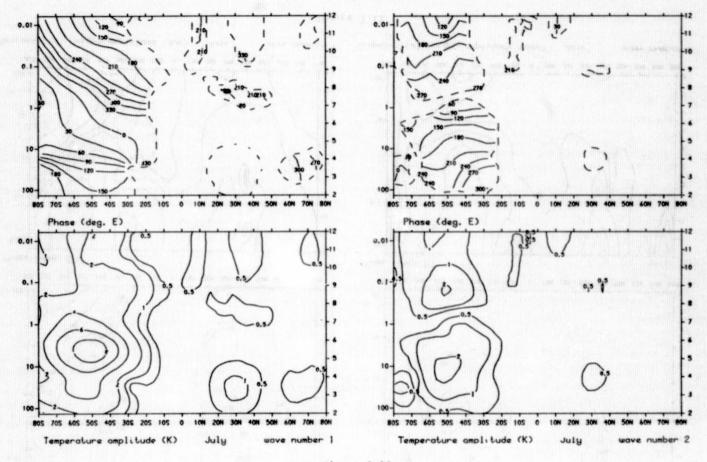


Figure 3.13

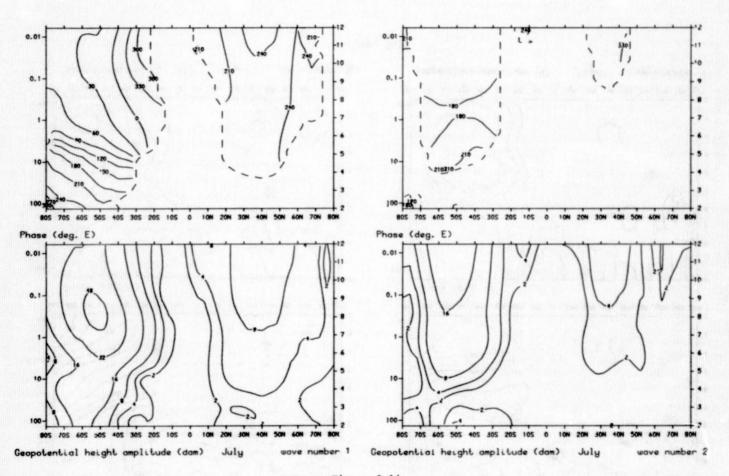


Figure 3.14

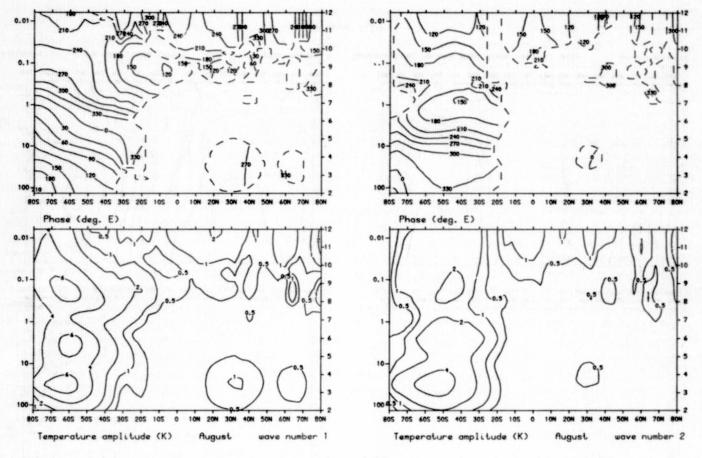


Figure 3.15

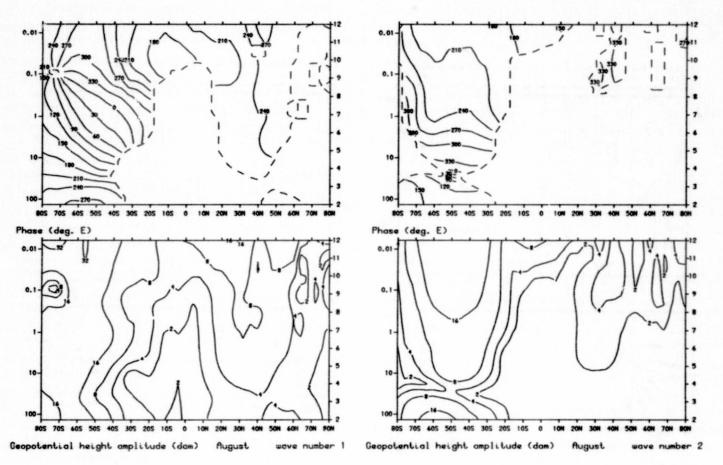


Figure 3.16

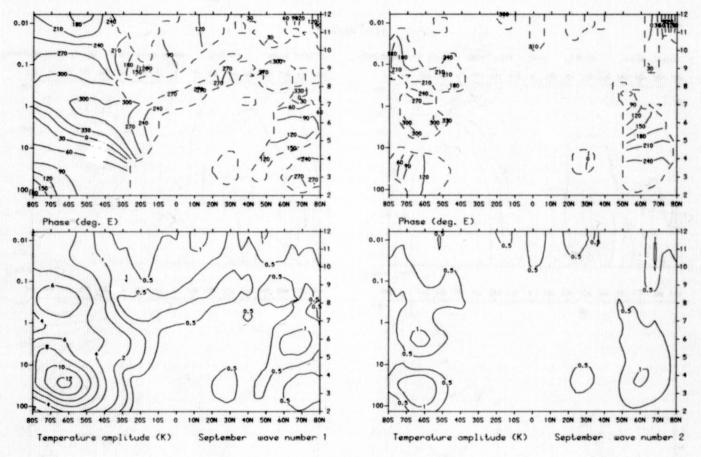


Figure 3.17

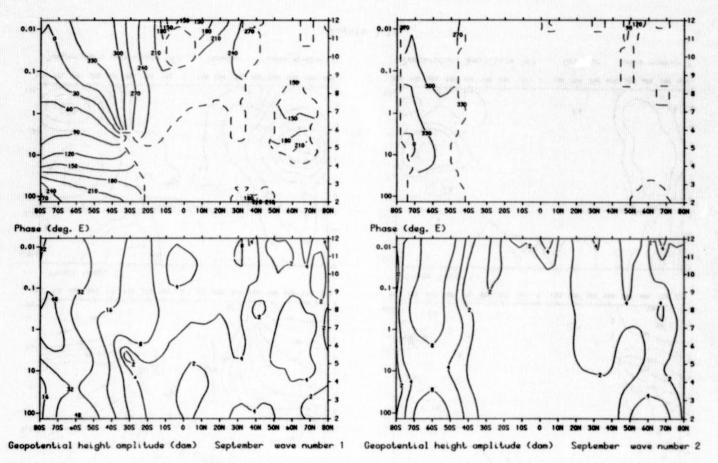


Figure 3.18

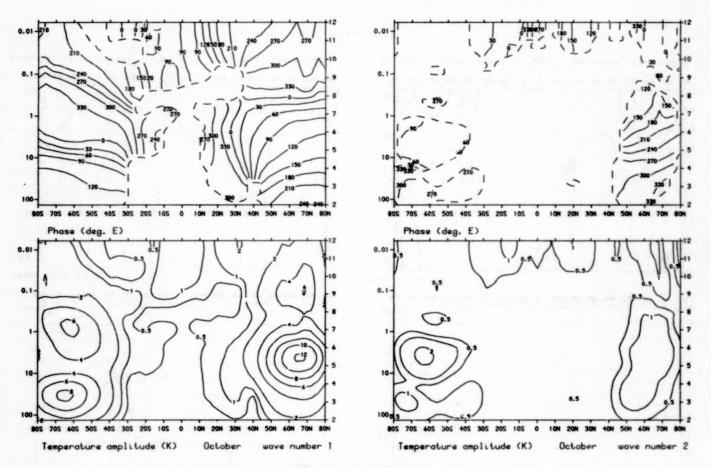


Figure 3.19

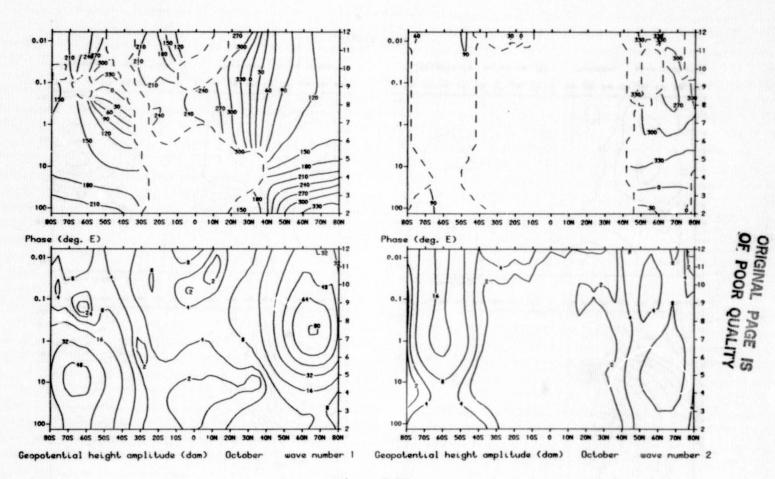


Figure 3.20

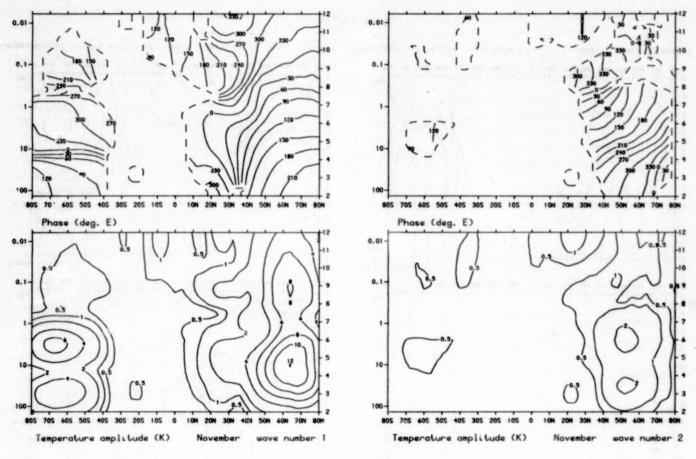


Figure 3.21

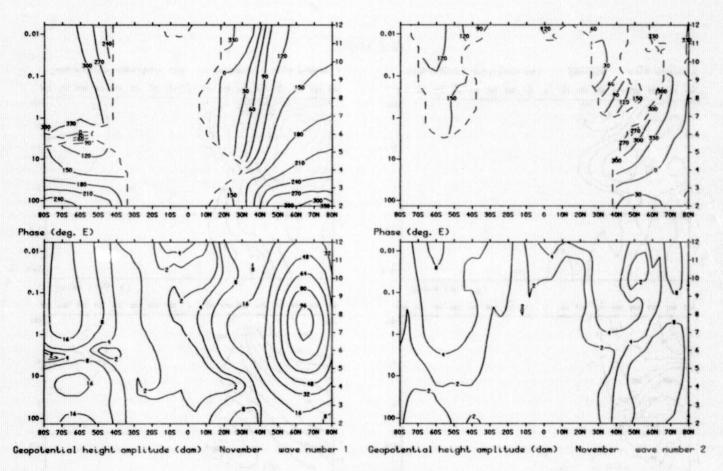


Figure 3.22

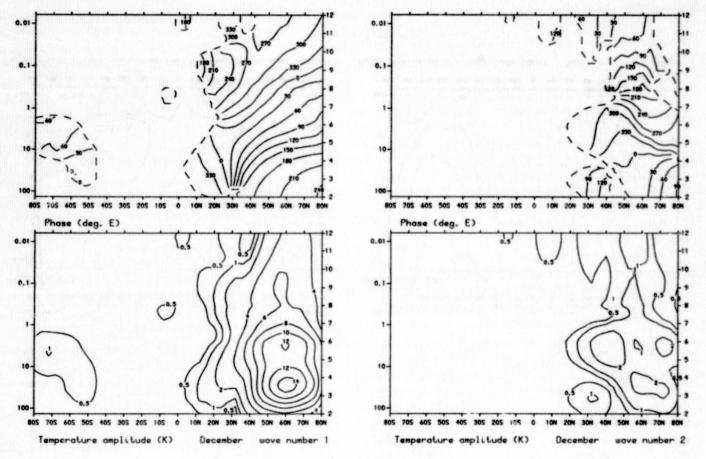


Figure 3.23

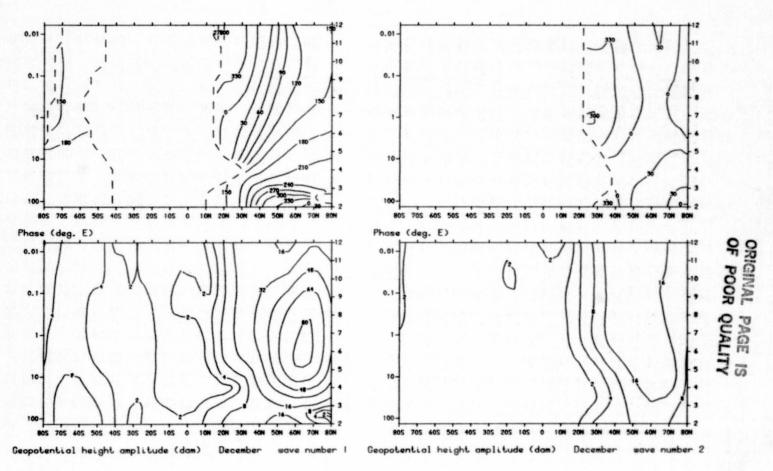


Figure 3.24

	labi			mpr.	vave	s 1	and	2 f	or	12 m	onth	ıs.		- um p				
JANUARY	MEAN T	EMPERA	TURE A	MPLITU	DE (K)	AND P	HASE	WAVE	1									
SCALE	PRESSURE (mb)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	50	40	50	60	70	80
12.0	0.0022	0,28	0,13	0.07	0.40	0.31	0.49	0.16	0.84	0.93	0.35	0.33	0.87	1,10	2,55	4,13	3,32	2.09
11.5	0.0103	0.33	0.14	0.07	0.47	0.35	0.46	0.18	0.79	0.92	0.37	0.31	0.82	1.02	2.84	4.40	3,49	2.00
11.0	0.0169	0.35	0.13	0.06	0.53	0.37	0.39	0.22	0.67	0.84	0.37	0.27	0.70	0.89	3.09	4.58	3,78	2.08
10.5	0.0279	0,34	0.10	0.08	0.55	0,40	0.28	0.24	0.48	0.68	0.38	0.20	0,58	0.86	3,33	4.83	4,41	2,64
10.0	0.0460	0.27	0.05	0.12	0,58	0.44	0.18	0.28	0.30	0.48	0.36	0.13	0,67	1,11	3,62	5,31	5,45	3,63
9.5	0.0758	0,16	0.04	0.17	0,54	0.47	0.23	0.31	0.28	0.27	0.33	0.13	0.97	1,55	3,89	5,96	6,67	4,73
9.0	0,1250	0.10	0.12	0,22	0,43	0.47	186	0.28	0,40	0.10	0,26	0,18	1,25	1,86	4,03	6,61	7,74	5,56
8,5	0.2061	0.20	0.12 179	0.23 250	0.21	0,35	0,41	0.18	0.42	336 0,16 261	329 0.10 356	0.18	1,28 217	1,74	4.01	7.01 318	8,25	5.70 332
8.0	0.3398	0,26	0.09	0,19	0.13	0.23	0.32 136	0,19	0,31	0.21	0.16	0,11	0.93	1,15	4.07	7.30	8,29	5.20
7.5	0,5603	0.18	0,03	0,06	0.25	0.24	0.12	0,28	262	0,13	0.23	0.10	0,40	1,34	5,13	8,30	8,59	346 4,88
7.0	0.9237	0.08	0.10	0.09	0.20	0.20	0.14	310	0.15	0.07	0,17	0.14	0.97	340	6.95	9,45	9.15	5.06
6.5	1.52	0.14	0.17	0.12	0.06	0.08	0.13	0.10	0.07	0.05	0.07	0,26	1.88	5.28	8.74	10.16	9.37	5.26
6.0	2.51	0.26	0.22	28 0.15 360	0.04	0.03	0.10	0.11	0.03	0.06	192	331	359	7.10	9,66	9.75	8.74	5.24
5.5	4.14	0.29	0.32	360	310	342	0.06	0.06	333	261	278	0.55 348 0.83	3.17	6.70	8.02	7.77	7,52	5.43
5.0	6,83	0.28	0.40	0.39	350	328	346	0.09	290	257	303	352	3.05	25	6,00	75	95 8,86	116
4.5	11,25	35	33	0.51	359	327	290	291	287	264	322	352	14	38	80	119	136	146
4.0	18,55	34	33	0.58	0.67	325	275	276	289	284	332	351	1,67	69	127	153	162	166
3.5	30.59	33	33	27	6	326	273	274	291	302	337	350	36	120	157	169	175	179
		0.09	33	30	8	325	272	273	293	311	341	349	61	149	171	178	17,49	188
3.0	50.43	0.04	0.29	33	10	324	272	273	295	317	343	346	0.75 98	161	9.06	184	15.17	195
2.5	83.15	288	0.19	0.35	0.48	325	272	274	296	0.14	0.36	0.53	0,61	3,67	6.92		10.52	6.11
		200	33	36	11	323	212	214	290	321	344	244	125	167	182	188	193	200
JANUARY	MEAN G			HE IGHT						AVE 1	344	344	125	167	162	100	193	200
100000000000000000000000000000000000000	MEAN G PRESSURE (mb)										10	20	30	40	50	60	70	80
SCALE	PRESSURE	ЕОРОТЕ	NTIAL	HE IGHT	AMPLI	TUDE (dam) A	-20 5.2	SE •	AVE 1	10	20	30 15.1	40	50	60	70 35.1	80
SCALE HE I GHT	PRESSURE (mb)	-80 2.8	-70 0.7	HE IGHT	-50	TUDE (dam) A -30 4.1 230 3.9	-20 5.2 211 4.9	-10 0.5 140	0 3.7 10 2.4	10 2.9 337 2.4	20 6.5 338 6.1	30 15.1 349 13.9	40 24.2 20 23.0	7.6 149 6.9	51.2 188 26.1	70 35.1 190 31.0	80 26.8 180 24.6
SCALE HEIGHT 12.0	PRESSURE (mb) 0.0062	-80 2.8 318 2.3 314	-70 0.7 331 0.5	1.8 249 1.8 252	-50 5.0 224 4.4 226 3.7	TUDE (-40 4.7 213 4.3 212 3.7	-30 4.1 230 3.9 221 3.8	-20 5.2 211 4.9 211	-10 0.5 140 1.1 232 2.1	0 3.7 10 2.4 358	10 2.9 337 2.4 335	20 6.5 338 6.1 339 5.7	30 15.1 349 13.9 350 12.9	40 24.2 20 23.0 22 22.2	7.6 149 6.9 118 8.9	51.2 188 26.1 181 22.1	70 35.1 190 31.0 186 28.0	80 26.8 180 24.6 175 23.6
SCALE HEIGHT 12.0	PRESSURE (mb) 0.0062 0.0103	-80 2.8 318 2.3 314	-70 0.7 331 0.5 330 0.3	-60 1.8 249 1.8 252 1.9 254	-50 5.0 224 4.4 226 3.7 228 2.9	TUDE (-40 4.7 213 4.3 212 3.7 211 3.2	-30 4.1 230 3.9 221 3.8 211 3.7	-20 5.2 211 4.9 211 4.6 212 4.3	-10 0.5 140 1.1 232 2.1 244 2.9	3.7 10 2.4 358 1.4 328	10 2.9 337 2.4 335 1.8 332 1.3	20 6.5 338 6.1 339 5.7 340 5.3	30 15.1 349 13.9 350 12.9 352 12.3	40 24.2 20 23.0 22 22.2 25 22.0	7.6 149 6.9 118 8.9 89	51.2 188 26.1 181 22.1 168 21.0	70 35.1 190 31.0 186 28.0 177 27.5	26.8 180 24.6 175 23.6 169 24.4
SCALE HEIGHT 12.0 11.5 11.0	PRESSURE (mb) 0.0062 0.0103 0.0169	-80 2.8 318 2.3 314 1.9 308 1.5 298	0.7 331 0.5 330 0.3 326 0.1 310 0.0	-60 1.8 249 1.8 252 1.9 254 1.9 257	5.0 224 4.4 226 3.7 228 2.9 233 2.2	TUDE (-40 4.7 213 4.3 212 3.7 211 3.2 211	-30 4.1 230 3.9 221 3.8 211 3.7 204 3.6	-20 5.2 211 4.9 211 4.6 212 4.3 213	-10 0.5 140 1.1 232 2.1 244 2.9 245 3.5	3.7 10 2.4 358 1.4 328 1.3 277 1.8	10 2.9 337 2.4 335 1.8 332 1.3 327 0.8	20 6.5 338 6.1 339 5.7 340 5.3 341 5.2	30 15.1 349 13.9 350 12.9 352 12.3 355 12.2	40 24.2 20 23.0 22 22.2 25 22.0 28 22.6	7.6 149 6.9 118 8.9 89 12.8 75	31.2 188 26.1 181 22.1 168 21.0 150 23.9	70 35.1 190 31.0 186 28.0 177 27.5 165 30.5	26.8 180 24.6 175 23.6 169 24.4 161 27.6
SCALE HEIGHT 12.0 11.5 11.0	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279	-80 2.8 518 2.3 514 1.9 308 1.5 298 1.1	0.7 331 0.5 330 0.3 326 0.1 310 0.0 215	HE IGHT -60 1.8 249 1.8 252 1.9 254 1.9 257 1.8 261 1.7	5.0 224 4.4 226 3.7 228 2.9 233 2.2 241	TUDE (-40 4.7 213 4.3 212 3.7 211 3.2 211 2.6 215 2.0	-30 4.1 230 3.9 221 5.8 211 3.7 204 3.6 199 3.3	-20 5.2 211 4.9 211 4.6 212 4.3 213 4.0 215 3.6	-10 0.5 140 1.1 232 2.1 244 2.9 245 3.5 243 3.7	3.7 10 2.4 358 1.4 328 1.3 277 1.8 246 2.2	10 2.9 337 2.4 335 1.8 332 1.3 327 0.8 320 0.3	20 6.5 338 6.1 339 5.7 340 5.3 341 5.2 343 5.2	30 15.1 349 13.9 350 12.9 352 12.3 355 12.2 359	24.2 20 23.0 22 22.2 25 22.0 28 22.6 31 24.2	50 7.6 149 6.9 118 8.9 89 12.8 75 17.6 70 23.1	51.2 188 26.1 181 22.1 168 21.0 150 23.9 133 30.6	70 35.1 190 31.0 186 28.0 177 27.5 165 30.5 152	80 26.8 180 24.6 175 23.6 169 24.4 161 27.6 154
SCALE HEIGHT 12.0 11.5 11.0 10.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460	2.8 318 2.3 314 1.9 308 1.5 298 1.1 284 0.9 271 0.8	0.7 331 0.5 330 0.3 326 0.1 310 0.0 215 0.0 198 0.1	1.8 249 1.9 254 1.9 257 1.8 261 1.7 266 1.5	5.0 224 4.4 226 3.7 228 2.9 233 2.2 241 1.5 257	TUDE (-40 4.7 213 4.3 212 3.7 211 3.2 211 2.6 215 2.0 224	-30 4.1 230 3.9 221 5.8 211 3.7 204 3.6 199 3.3 198 3.0	-20 5.2 211 4.9 211 4.6 212 4.3 213 4.0 215 3.6 219	-10 0.5 140 1.1 232 2.1 244 2.9 245 3.5 243 3.7 238 3.6	3.7 10 2.4 358 1.4 328 1.3 277 1.8 246 2.2 231 2.5	10 2.9 337 2.4 335 1.8 332 1.3 327 0.8 320 0.3 299 0.2	20 6.5 338 6.1 339 5.7 340 5.3 341 5.2 343 5.2 345 5.3	30 15.1 349 13.9 350 12.9 352 12.3 355 12.2 359 12.9 4	24.2 20 23.0 22 22.2 25 22.0 28 22.6 31 24.2 34 26.5	7.6 149 6.9 118 8.9 89 12.8 75 17.6 70 23.1 69 28.8	50 31,2 188 26,1 181 22,1 168 21,0 150 23,9 133 30,6 123 39,6	70 35.1 190 31.0 186 28.0 177 27.5 165 30.5 152 37.5 143 47.5	26.8 180 24.6 175 23.6 161 27.6 154 33.2 149 40.6
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758	-80 2.8 518 2.3 314 1.9 308 1.5 298 1.1 284 0.9 271 0.6	0.7 331 0.5 330 0.3 326 0.1 310 0.0 215 0.0 198 0.1	HE IGHT -60 1.8 249 1.8 252 1.9 254 1.9 257 1.8 261 1.7 266 1.5 272 1.2	5.0 224 4.4 226 3.7 228 2.9 233 2.2 241 1.5 257 1.2 284	TUDE (-40 4.7 213 4.3 212 3.7 211 3.2 211 2.6 215 2.0 224 1.7 243 1.8	-30 4.1 230 3.9 221 3.8 211 3.7 204 3.6 199 3.3 198 3.0 202 2.6	-20 5.2 211 4.9 211 4.6 212 4.3 213 4.0 215 3.6 219 3.3 224 3.0	-10 0.5 140 1.1 232 2.1 244 2.9 245 3.5 243 3.7 238 3.6 231 3.4	3.7 10 2.4 358 1.4 328 1.3 27 1.8 246 2.2 231 2.5 222 2.4	10 2.9 337 2.4 335 1.8 332 1.3 327 0.8 320 0.3 299 0.5	20 6.5 338 6.1 339 5.7 340 5.3 341 5.2 343 5.2 345 5.3	30 15.1 349 13.9 350 12.9 352 12.2 359 12.2 359 12.9 4 14.2 8	40 24.2 20 23.0 22 22.2 25 22.0 28 22.6 31 24.2 34 26.5 36 29.0	7.6 149 6.9 118 8.9 12.8 75 17.6 70 23.1 69 28.8 72	51.2 188 26.1 181 122.1 168 21.0 150 23.9 133 30.6 123 39.6 120 49.4	70 35.1 190 31.0 186 28.0 177 27.5 165 30.5 152 37.5 143.4 47.5 138 59.3	26.8 180 24.6 175 25.6 169 24.4 161 27.6 154 33.2 149 40.6 147 48.9
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250	2.8 518 2.3 514 1.9 308 1.5 298 1.1 284 0.9 271 0.8 266 0.6	0.7 331 0.5 330 0.3 326 0.1 310 0.0 215 0.0 198 0.1 345 0.2	HE IGHT -60 1.8 249 1.8 252 1.9 254 1.9 257 1.8 261 1.7 266 1.5 272 1.2 280 0.9	-50 5.0 224 4.4 226 3.7 228 2.9 233 2.2 241 1.5 257 1.2 284 1.3 305	TUDE (-40 4.7 213 4.3 212 3.7 211 3.2 211 2.6 215 2.0 224 1.7 243 1.8 263 2.1	dam) A -30 4.1 230 3.9 221 3.8 211 3.7 204 3.6 198 3.0 202 2.6 211 2.5	-20 5.2 211 4.9 211 4.6 212 4.3 213 4.0 215 3.6 219 3.3 224 3.0 228 2.8	-10 0.5 140 1.1 232 2.1 244 2.9 245 3.5 243 3.6 231 3.6 231 3.1	3.7 10 2.4 358 1.4 328 1.3 277 1.8 246 2.2 231 2.5 222 2.4 2.5 2.2	10 2.9 337 2.4 335 1.8 332 1.3 327 0.8 320 0.3 299 0.2 187 0.5	20 6.5 338 6.1 339 5.7 340 5.3 341 5.2 343 5.3 347 5.3 347 5.3	30 15.1 349 13.9 350 12.9 355 12.2 359 12.2 359 14.2 8 15.9 15.9	24.2 20 23.0 22 22.2 25 22.0 28 22.6 31 24.2 34 26.5 36 29.0 38 31.0	7.6 149 118 8.99 89 12.8 75 17.6 69 72 34.0 77 38.2	51.2 188 26.1 181 22.1 168 21.0 150 23.9 133 30.6 123 39.6 120 49.4 121 59.0	70 35.1 190 31.0 186 28.0 177 27.5 165 30.5 152 37.5 138 47.5 138 59.3 138 71.1	26.8 180 24.6 175 23.6 169 24.4 161 27.6 154 33.2 149 40.6 147 48.9 147 56.7
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061	-80 2.8 318 2.3 314 1.9 308 1.5 298 0.9 271 0.8 266 0.6 280 0.6 312 0.7	-70 0.7 331 0.5 330 0.3 326 0.1 310 0.0 198 0.1 345 0.2 353 0.4	HEIGHT -60 1.8 249 1.8 252 1.9 254 1.9 257 1.8 261 1.7 266 1.5 272 280 0.9 288 0.8 8	-50 5.0 224 4.4 226 3.7 228 2.9 233 2.2 241 1.5 257 1.2 284 1.3 305 1.4	TUDE (-40 4.7 213 4.3 212 3.7 211 3.2 211 2.6 215 2.0 224 1.7 243 2.6 2.1 270 2.4 2.6 2.1 2.7 2.4 2.6 2.1 2.7 2.4 2.4 2.6 2.1 2.7 2.4 2.4 2.6 2.4 2.4 2.4 2.4 2.4 2.4 2.4 2.4 2.4 2.4	-30 4.1 230 3.9 221 5.6 211 5.7 204 3.6 199 3.3 198 3.0 202 2.6 211 2.5 223 2.6	5.2 211 4.9 211 4.6 212 4.5 213 4.0 215 3.6 219 3.3 3.24 3.0 228 2.8 227 2.8 227	-10 0.5 140 1.1 232 2.1 244 2.9 245 3.5 3.7 238 3.6 6231 3.4 221 3.1 213 2.9 2.9 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1	3.7 10 2.4 358 1.3 227 1.8 2.2 223 1 2.5 222 2.4 215 2.0 2.0 2.0	10 2.9 337 2.4 335 1.8 332 1.3 327 0.8 320 0.3 299 0.2 187 0.5 171 0.5	20 6.5 338 6.1 339 5.7 340 5.3 341 5.2 345 5.3 347 5.5 348 5.7 350 5.8	30 15.1 349 13.9 350 12.9 355 12.3 355 12.2 8 14.2 8 15.9 12 17.4 14 18.0	40 24.2 20 22.2 25 22.0 28 22.6 31 24.2 34 26.5 36 29.0 38 31.0 31.3	7.6 149 6.9 118 8.9 89 12.8 75 17.6 69 28.8 72 34.0 77 38.2 83 40.5	51.2 188 26.1 181 22.1 168 21.0 150 23.9 39.6 123 39.6 120 49.4 121 59.0 126 67.5	70 35.1 190 31.0 28.0 27.5 165 30.5 152 37.5 143 47.5 138 59.3 138 71.1 141 81.7	26.8 180 24.6 175 23.6 169 24.4 161 27.6 154 33.2 149 40.6 147 147 56.7 148
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603	-80 2.8 518 2.3 514 1.9 508 1.5 298 1.1 284 0.9 271 0.8 266 0.6 512 0.7 359 0.7	0.7 331 0.5 330 0.3 326 0.1 310 0.0 215 0.0 0.1 345 0.2 353 0.4 358 0.4	HEIGHT -60 1.8 249 1.8 252 1.9 254 1.9 257 1.8 261 1.7 266 1.5 272 1.2 280 0.9 288 0.8 290 0.7	-50 5.0 224 4.4 226 3.7 228 2.9 233 2.2 241 1.5 257 1.2 284 1.3 305 1.4 309 1.5 299	TUDE (-40 4.7 213 4.3 212 3.7 211 3.2 211 2.6 215 2.0 224 1.7 245 1.8 263 2.1 270 2.4 267 2.6	-30 4.1 230 3.9 221 3.8 211 3.7 204 3.6 199 3.3 3.9 202 2.6 2.1 2.5 2.2 2.2 2.2 2.2 2.2 2.2 2.2	5.2 211 4.9 211 4.6 212 4.3 3.1 3.2 24 3.0 228 227 2.8 220 2.8 220 2.8	0.5 140 0.5 140 1.1 1 232 2.1 244 2.9 245 3.5 245 3.7 238 3.6 231 3.1 213 2.9 210 2.7 210	3.7 10 2.4 4 328 1.3 358 1.4 328 246 2.2 231 2.5 222 2.4 215 2.0 208 1.8 1.8 1.8	10 2.9 337 2.4 335 1.8 335 1.3 352 0.3 320 0.3 329 0.2 187 0.5 171 0.5 182 0.5 192 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	20 6.5 338 6.1 339 5.7 340 5.3 341 5.2 343 5.2 345 5.3 5.3 5.7 350 5.8	30 15.1 349 13.9 350 12.9 355 12.2 359 12.9 4 14.2 8 15.9 12 17.4 14 18.0 16 17.5	40 24.2 20 23.00 22 22.2 25.5 22.00 28 22.6 31 24.2 34 26.5 36 31.0 40 31.3 42 29.1	7.6 149 6.9 89 12.8 75 17.6 70 23.1 169 28.8 72 34.0 34.0 92 41.4	31.2 188 26.1 181 22.1 168 21.0 25.9 133 30.6 120 49.4 121 59.0 126 67.5 133 75.5	70 35.11 190 31.00 186 28.0 177 27.5 165 30.5 143 47.5 143 47.5 138 71.1 141 81.7 145 90.9	26.8 180 24.6 175.6 169 24.4 161 27.6 154 33.2 149 40.6 147 48.9 147 148.9 147 16.7 148 63.1 15.2
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 8.0 7.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603	2.8 318 2.3 314 1.9 308 1.5 298 271 0.8 266 0.66 312 0.7 359 0.7 354 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	-70 0.7 331 0.5 330 0.3 326 0.1 310 0.0 215 0.0 0.1 345 0.2 353 0.4 358 0.5 0.4 0.2 0.2	HE IGHT -60 1.8 249 1.8 252 1.9 254 1.9 254 1.7 266 1.5 272 1.2 280 0.9 288 0.8 0.9 290 0.7 284 0.8 0.8 0.8 0.8	-50 5.0 224 4.4 226 3.7 228 2.9 233 2.241 1.5 257 1.2 284 4.3 0.9 1.4 30.9 1.7 289 1.7 289	TUDE (-40 4.7 213 3.7 211 2.6 215 2.0 2.24 1.7 245 2.1 270 2.6 2.7 245 2.1 270 2.6 2.1 270 2.6 2.1 270 2.6 2.1 270 2.6 2.1 2.7 2.6 2.1 2.7 2.6 2.1 2.7 2.6 2.1 2.7 2.6 2.1 2.7 2.6 2.1 2.8	-30 4.1 230 3.9 221 3.8 211 3.7 204 3.6 3.6 3.9 202 2.6 211 2.5 223 2.7 229 2.7 229 2.9	5.2 211 4.9 211 4.6 212 4.3 3.3 224 5.6 219 5.6 228 2.8 227 2.8 220 2.8 220 2.8 212 2.9 2.9	-10 0.5 140 0.5 140 1.1 232 2.1 244 2.9 245 3.5 5.5 243 3.7 238 3.6 231 3.1 213 3.1 213 2.9 210 2.7 213 2.9 210	3.7 10 2.4 358 1.3 287 1.8 8 246 2.2 231 2.5 222 2.10 2.00 1.8 209 1.7 1.7	10 2.9 337 2.4 335 1.8 327 0.3 299 0.2 187 0.5 171 0.5 182 0.5 182 0.6 6	20 6.5 338 6.1 339 5.7 340 5.3 341 5.2 345 5.3 347 5.5 348 5.7 350 5.8 351 5.8 352 5.8	30 15.1 349 350 12.9 355 12.3 355 12.2 359 12.9 4 14.2 8 15.9 12 17.4 18.0 16 17.5 18	40 24.2 20 23.0 22.2 25 22.0 28 22.6 31 24.2 34 26.5 36 29.0 38 31.0 31.3 42	7.6 149 6.9 1188 8.9 89 12.8 75 17.6 69 28.8 72 34.0 77 38.2 83 40.5 92	51.2 188 26.1 181 22.1 168 21.0 150 23.9 133 30.6 123 39.6 120 49.4 121 59.0 126 67.5 133	70 35.1 190 31.0 186 28.0 177 27.5 165 30.5 152 37.5 138 47.5 138 71.1 141 141 181.7	26.8 180 24.6 175 23.6 169 24.4 161 27.6 154 33.2 147 48.9 147 48.9 147 163.1 152
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 8.0 7.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603 0.9237	-80 2.8 318 2.3 314 1.9 23 308 1.5 298 0.9 271 0.8 266 0.6 312 0.7 339 0.7 339 0.7 339 0.7 339 0.7 339 0.7 339 0.7 339 0.7 339 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7	-70 0.7 331 0.5 330 0.5 330 0.5 326 0.1 310 0.0 215 0.0 198 0.1 345 0.2 353 0.4 6 0.2 352 0.2	HE IGHT -60 1.8 249 1.8 252 2.54 1.9 254 1.7 266 1.5 272 2.80 0.9 288 0.8 290 0.7 284 0.8 272 0.9 0.9	-50 5.0 224 4.4 226 2.9 233 2.2 241 1.5 257 1.2 284 3.05 1.4 3.05 1.5 2.99 1.7 2.89 1.8 2.84 1.5 2.9 1.7 2.80 1.80 1.80 1.80 1.80 1.80 1.80 1.80 1	TUDE (1 -40 4.7 213 4.3 212 3.7 713 4.3 215 2.11 3.2 211 3.2 211 2.6 215 2.0 224 1.7 243 265 2.1 2.0 2.4 267 2.4 267 2.4 267 2.8 258 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.	-30 4.1 230 3.9 221 5.6 199 3.3 198 3.0 202 2.1 2.5 2.6 2.7 2.9 2.9 2.6 3.0 3.0	-20 5.2 211 4.9 211 4.6 4.3 215 3.6 219 3.3 3 224 3.2 28 2.8 220 2.8 220 2.8 220 2.8 3.3 3.3 3.3 3.3 3.3 3.3 3.3 3.3 3.3 3	-10 0.55 140 1.1 232 2.1 244 2.9 245 3.5 243 3.6 231 3.6 231 3.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2	3.7 10 2.4 3598 1.3 328 1.3 277 1.8 246 2.2 231 2.5 222 2.0 208 1.6 2.0 209 1.7 210 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6	10 2.9 337 2.4 335 1.3 3527 0.8 320 0.3 299 0.2 187 0.5 219 0.5 219 0.6 252 0.6 262 0.6 0.5	20 6.5 338 6.1 339 5.7 340 5.3 343 5.2 345 5.3 357 5.8 351 5.8 351 5.8 351 5.8 351 5.8 5.8 5.8 5.8 5.8 5.8 5.8 5.8 5.8 5.8	30 15.1 349 350 12.9 552 12.3 359 12.9 4 14.2 8 8 15.9 12 17.4 18.0 16 17.5 18 11.2 11.2 11.2 11.2 11.2 11.2 11.2 1	40 24.2 20 23.0 22 25 22.0 28 22.6 31 24.2 34 26.5 36 39.0 31.3 42 29.1 47 24.5 61 18.7	50 7.66.9 118 8.99 112.86 77.56 70 23.11 69 28.8 72 34.00 77 73 8.2 83 40.5 92 41.4 42.2 120 44.7	51.2 2.1 181 22.1 185.0 0.6 67.5 141 85.0 0.150	70 35.1 190 31.0 186 20.0 177 27.5 165 30.5 143 47.5 138 71.1 141 181.7 145 90.9 151	80 26.8 180 24.6 179 23.6 169 24.4 119 40.6 147 149 40.6 147 149 40.6 147 149 63.1 152 67.8 156
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 8.0 7.5 7.0	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603 0.9237	-80 2.8 318 2.3 314 1.9 308 1.5 298 1.1 284 0.9 271 0.8 266 0.6 312 0.7 339 0.7 355 0.4 332	NTIAL -70 0.7 331 0.5 330 0.3 326 0.1 310 0.0 215 0.0 198 0.1 345 0.2 353 0.4 358 0.5 3 0.4 358 0.2 352 0.2 352	HE IGHT -60 1.8 249 1.8 252 1.9 254 1.9 257 1.8 261 1.7 266 1.5 252 280 0.9 258 0.8 290 0.7 284 0.8 272 0.9 260	-50 5.0 224 4.4 226 3.7 228 2.9 233 2.2 241 1.5 257 1.2 284 1.3 309 1.5 299 1.7 289 1.8 284 1.8 283 1.8	TUDE (-40 4.7 213 4.3 212 3.7 211 3.2 2211 3.2 2211 3.2 241 1.7 243 1.88 263 2.1 270 2.66 261 2.88 258 2.88	-30 4.1 230 3.9 221 5.6 5.1 5.7 204 3.6 199 3.0 2.2 2.6 223 2.7 229 2.9 2.9 2.7 229 2.9 3.0 3.1	-20 5.2 211 4.9 211 4.9 212 4.3 3.1 3.1 3.1 3.0 215 3.0 228 227 2.8 212 2.9 2.8 212 2.9 2.8 2.1 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0	-10 0.55 140 1.1 232 2.1 244 2.9 245 5.5 245 5.7 238 3.6 231 3.1 210 2.7 210 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7	3.7 10 2.4 3588 1.4 328 1.3 277 1.8 246 2.2 210 2.0 208 1.8 209 1.7 210 1.6 209 1.7 210 1.6 209 1.6	10 2.9 337 2.4 335 1.3 320 0.3 329 0.2 171 0.5 171 0.5 171 0.5 171 0.5 172 0.5 173 0.6 182 0.5 182 0.6 182 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	20 6.5 338 6.1 339 5.7 340 5.3 341 5.2 343 5.3 345 5.3 348 5.5 5.8 350 5.8 350 5.8 350 5.8 350 5.8 350 5.8 350 5.8 350 5.8 5.8 5.8 5.8 5.8 5.8 5.8 5.8 5.8 5.8	30 15.1 349 13.9 3590 12.9 3592 12.2 3599 12.9 4 14.2 17.4 18.0 17.5 18.6 21 12.4 26 8.4	40 24.2 20 23.0 22 25 22.0 28 22.6 31 24.2 34 26.5 36 39.0 31.0 40 31.3 22.9 14.7 24.5 56 18.7 75 15.1	7.6 149 6.9 118 8.9 8.9 12.8 75 17.6 70 23.1 14.0 77 38.2 8.3 40.5 92 41.4 104 42.2 120 44.7 138	51,2 188 26,1 181 22,1 150 21,0 150 22,9 133 30,6 120 49,4 121 59,0 126 137 75,5 141 85,0 150 88,5 158	70 35.1 190 31.0 186 28.0 177 27.5 165 30.5 152 37.5 138 47.5 138 47.5 138 71.1 145 90.9 151 98.3 158 158 159 159 159 159 159 159 159 159	26.8 180 24.6 175 23.6 161 27.6 154 33.2 40.6 147 76.7 148 63.1 156 67.8 156 70.6 162 71.4
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 8.0 7.5 7.0 6.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603 0.9237 1.52 2.51	-80 2.8 318 2.3 314 1.9 308 1.1 284 0.9 271 0.8 266 0.6 280 0.6 312 0.7 359 0.7 359 0.4 264 0.7	0.77 331 0.57 330 0.3 330 0.3 330 0.1 310 0.0 0.1 345 0.1 345 0.2 353 0.4 6 6 0.2 2.5 353 0.4 6 0.2 2.5 353 0.4 6 0.5 353 0.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1	HE IGHT -60 1.8 249 1.8 252 1.9 252 1.9 257 1.8 261 1.7 26 272 280 0.9 288 0.8 290 0.7 284 0.8 272 0.9 260 1.0 0.2 42	-50 5.0 224 4.4 226 3.7 228 2.2 241 1.5 257 1.2 284 1.3 305 1.4 257 288 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7	TUDE (-40 4.7 213 4.3 212 3.7 211 2.6 215 2.2 1.7 243 1.8 263 2.1 270 2.4 267 2.6 261 270 2.8 258 2.8 258 2.8	dam) A 4.1 230 3.9 221 5.8 221 3.7 204 3.6 211 2.5 22 22 2.7 229 2.9 2.6 3.0 2.5 3.1 223 3.1 2.5 3.1 2	-20 5.2 211 4.9 211 4.6 212 4.3 3.1 3.3 3.2 4.0 215 3.3 3.2 228 227 2.8 227 2.8 227 2.8 220 2.8 2.9 2.9 2.8 2.9 2.9 2.9 2.8 2.9 2.9 2.9 2.9 2.9 2.9 2.9 2.9	-10 0.5 140 1.1 232 2.1 244 2.9 245 3.5 243 3.4 221 213 2.9 20 2.7 213 2.6 216 216 217 2.6 215 2.6 216 216 217 2.6	3.7 10 2.4 358 1.4 358 1.5 227 2.5 222 2.4 4.6 2.9 2.0 208 1.6 2.9 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0	10 2.9 337 2.4 335 1.8 332 1.3 320 0.3 329 0.2 187 0.5 171 0.5 182 0.5 219 0.6 252 0.6 262 0.6 262 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	20 6.5 338 6.1 339 5.7 340 5.2 343 5.2 343 5.3 347 5.5 351 5.8 351 5.8 351 5.8 351 5.8 352 5.8 355 5.8 5.8 5.8 5.8 5.8 5.8 5.8 5.8 5.8 5	30 15.1 349 350 12.9 552 12.3 359 12.9 4 14.2 8 8 15.9 12 17.4 18.0 16 17.5 18 11.2 11.2 11.2 11.2 11.2 11.2 11.2 1	40 24.2 20 23.0 22 22.2 25 22.6 31 24.2 34 26.5 36 31.0 31.3 42 29.1 47 24.5 56 18.7 75	50 7.66.9 118 8.99 112.86 77.56 70 23.11 69 28.8 72 34.00 77 73 8.2 83 40.5 92 41.4 42.2 120 44.7	51.2 188 26.1 181 122.1 168 21.0 0 150 23.9 133 30.6 123 39.6 120 120 49.4 121 59.0 67.5 133 75.5 141 85.0 89.5 158	70 35.1 190 31.0 186 28.0 177 27.5 165 152 37.5 143 47.5 143 47.5 143 141 141 141 165 103.4 103.4 103.4 104.4 105.4	80 26.8 180 24.6 169 24.4 161 154 33.2 149 40.6 147 48.9 147 152 67.8 165 70.6 162 71.4 168 88.9 174
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 8.0 7.5 7.0 6.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603 0.9237 1.52 2.51	-80 2.8 318 2.3 314 1.9 308 1.5 298 0.9 271 0.8 266 0.6 280 0.6 352 0.7 354 0.7 354 0.7 238	0.77 331 0.57 330 0.33 330 0.33 326 0.0 215 0.0 215 0.0 215 0.0 215 0.0 235 330 0.3 356 0.3 0 0 0.3 0 0 0 0	HE IGHT -60 1.8 249 1.8 252 1.9 252 1.9 257 1.6 1.5 272 280 0.8 272 0.9 0.7 284 0.8 272 0.9 0.7 284 1.0 260 1.0 242 1.3 226	-50 5.0 224 4.4 226 3.7 228 3.3 227 1.5 257 1.2 284 1.5 257 1.2 284 1.3 305 1.5 299 1.7 289 1.8 284 1.8 283 1.8 2 283 1.8 283 1.8 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	TUDE (-40 4.7 213 4.3 212 3.7 211 3.2 211 2.6 224 1.7 245 1.8 263 2.1 1.8 267 2.6 261 2.7 2.6 2.8 258 2.8 258 2.8 258 2.8 2.7 249 2.6 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8	-30 4.1 230 3.9 221 3.8 211 3.6 211 3.6 199 3.3 198 3.0 202 2.6 211 2.5 223 2.7 229 2.7 229 2.7 229 2.7 229 2.7 229 2.7 229 2.7 229 2.7 2.7 229 2.7 2.7 229 2.7 2.7 229 2.7 2.7 229 2.7 2.7 229 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7	-20 5.2 211 4.9 211 4.6 212 4.13 4.0 215 3.6 219 3.24 3.0 28 2.8 220 2.8 20 2.8 20 2.8 20 2.8 20 2.8 2	-10 0.5 140 1.11 232 2.11 244 3.5 3.7 238 3.7 238 3.7 238 3.7 238 221 3.1 221 3.1 221 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2	3.7 10 2.4 4 328 1.4 328 1.27 1.8 8 246 2.2 2.3 1 2.2 2.4 2.0 208 1.8 2.9 2.9 1.7 210 1.6 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0	2.9 337 2.4 335 1.8 335 1.8 332 1.8 320 0.3 299 0.2 187 0.5 219 0.5 219 0.5 219 0.5 20 0.5 0.5 20 0.5 20 0.5 20 0.5 0.5 20 0.5 0.5 20 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.	20 6.5 338 6.1 339 5.7 340 5.2 343 5.3 347 5.5 5.5 5.3 359 5.6 359 5.6 359 5.6 359 5.7 359 5.7 360 50 50 50 50 50 50 50 50 50 50 50 50 50	30 15.1 349 13.9 350 12.9 355 12.2 8 15.9 12.1 17.4 18.0 16.5 17.1 18.0 16.5 17.1 18.0 16.6 17.6 18.0 19.0 19.0 19.0 19.0 19.0 19.0 19.0 19	40 24.2 20 23.0 22 22.2 25 31 24.2 25,3 36 29.0 31 47 24.5 56 18.7 75 108 11.08 15.8 11.08	7.6 149 6.9 89 89 12.8 75 17.6 70 23.1 6.7 72 34.0 77 38.2 83 40.5 92 41.0 42.2 120 44.7 138 49.3 165	51.2 188 26.1 188 22.1 168 21.0 21.50 25.9 153 30.6 120 49.4 121 59.0 126 67.5 133 75.4 166 89.5 158 89.5 173	70 35.1 190 31.0 186 28.0 177 21.5 152 37.5 138 47.5 138 138 138 141 141 181.7 145 198.3 158 159 151 158 159 159 159 159 159 159 159 159	80 26.8 180 24.6 167 23.6 161 154 33.2 149 40.6 147 76.7 148.9 147 76.7 70.6 67.8 156 70.6 68.9 174 68.9 174 68.9 174 68.9 175 175 175 175 175 175 175 175
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 6.0 5.5 5.0	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603 0.9237 1.52 2.51 4.14 6.83	-80 2.8 318 2.3 318 2.3 314 1.9 308 1.1 284 0.9 271 0.8 266 0.6 0.6 312 0.7 339 0.7 339 0.7 339 0.7 339 0.7 354 0.6 1.1 230 0.4 238	0.77 331 0.57 330 0.33 326 0.33 320 0.00 0.198 0.1 345 0.2 0.3 353 0.4 450 0.5 353 0.5 353 0.6 0.7 353 0.6 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7	HE IGHT -60 1.8 249 1.8 252 252 1.9 254 1.7 266 1.5 272 1.20 0.9 288 0.8 290 0.8 290 0.8 272 0.9 260 0.8 272 1.0 242 1.3 226	-50 5.0 224 4.4 226 3.7 228 233 2.2 241 1.5 257 1.2 284 1.3 305 1.4 309 1.5 299 1.5 299 1.7 289 1.8 1.8 1.8 1.8 1.8 1.8 1.8 1.8	TUDE (-40 4.7 213 4.3 212 3.7 2111 2.6 2.15 2.0 2.4 2.6 2.6 2.6 2.6 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8	dem) A 4.1 230 3.9 221 5.8 221 3.7 204 3.6 222 2.7 229 2.9 2.7 229 2.5 3.1 222 3.0 218	-20 5.2 211 4.9 211 4.6 212 5.2 213 4.0 215 5.6 215 5.6 227 2.8 227 2.8 212 2.9 208 5.0 208	-10 0.5 140 1.1 232 2.1 232 2.1 244 2.5 243 3.6 231 3.1 3.1 3.1 3.1 3.1 3.1 3.1 3.1 3.1 3.1	3.7 10 2.4 328 1.4 328 1.3 277 1.8 246 2.2 231 2.5 222 221 210 2.0 208 209 1.6 209 1.6 206 1.5 201 1.5 201 1.5 193	2.9 337 2.4 335 1.8 335 1.3 352 0.3 320 0.3 29 0.2 187 0.5 21 182 0.5 22 0.5 22 0.6 0.5 22 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	20 6.5 338 6.1 339 5.7 340 5.2 343 347 5.2 348 5.7 350 5.8 352 5.8 352 5.8 352 5.8 352 5.8 352 5.8 352 5.8 352 5.8 352 5.8 352 5.8 5.8 5.8 5.8 5.8 5.8 5.8 5.8 5.8 5.8	30 15.1 349 13.9 350 12.9 352 12.2 359 12.2 17.4 14.2 18.0 16.1 17.5 18.6 21 12.4 4.6 6.6 6.2 3.3 3.5	40 24.2 20 23.0 28 22.2 22.2 24.2 24.2 34 26.5 36 31.0 40 31.3 42 29.1 47 75 75 75 15.1 108 119 16.9 16.9 16.9 17.9 18.9 19.9	7.66 149 6.99 118 8.99 12.88 7.5 7.0 7.7 7.38.2 23.1 6.2 8.3 40.5 9.2 41.4 10.4 42.2 120 44.7 138 48.0 153 165 45.88 174	51.2 188 22.1 181 22.1 168 21.0 150 23.9 163 30.6 120 49.2 115 150 126 67.5 141 08.5 150 89.5 173 78.9 178	70 35.1 190 31.0 186 28.0 177 75 138 47.5 138 47.5 138 71.1 141 81.7 171 90.9 151 103.4 165 103.4 165 105 107 107 107 107 107 107 107 107	26.8 180 24.6 169 23.6 161 27.6 154 33.2 147 76.7 149 65.1 156 67.8 156 68.9 174 174 68.9 174 175 176 177 178 178 178 178 178 178 178 178 178
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 8.0 7.5 7.0 6.5 6.0 5.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603 0.9237 1,52 2,51 4,14 6,83 11,25	-80 2.8 318 2.3 318 1.9 308 1.1 284 0.9 271 0.8 266 0.6 6 312 0.7 339 0.4 332 0.4 264 0.7 359 0.4 264 0.7 359 0.4 264 0.7 359 0.4 264 0.7 359 0.4 264 0.7 359 0.4 264 0.7 359 0.4 264 0.7 359 0.4 264 0.7 359 0.4 264 0.7 359 0.4 264 0.7 359 0.4 264 0.7 359 0.4 264 0.7 359 0.4 264 0.7 359 0.4 264 0.7 359 0.4 264 0.7 359 0.4 264 0.7 359 0.4 264 0.7 359 0.4 264 0.7 359 0.4 265 0.6 0.7 359 0.6 0.7 359 0.6 0.7 359 0.7 359 0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8	0.77 331 0.57 330 0.3 330 0.3 330 0.1 310 0.0 215 0.0 215 0.0 353 0.1 345 0.2 353 0.4 6 6 0.2 253 0.4 6 0.2 253 0.4 6 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2	HE IGHT -60 1.8 249 1.8 252 1.9 254 1.7 266 1.5 272 1.2 280 0.9 288 0.8 290 0.8 290 0.8 272 0.9 260 0.8 272 0.9 260 0.8 272 0.9 260 0.8 272 0.9 260 0.8 272 0.9 260 0.8 272 0.9 260 0.8 272 0.9 260 0.8 272 0.9 260 0.8 272 0.9 260 0.8 272 0.9 260 0.8 272 0.9 260 0.8 272 0.9 260 0.8 272 0.9 260 0.8 272 0.9 260 0.8 272 0.9 260 0.8 272 0.9 260 0.8 272 0.9 260 0.8 272 0.9 260 0.9 272 0.9 260 0.9 272 0.9 260 0.9 272 0	-50 5.0 224 4.4 226 3.7 228 3.3 227 1.5 257 1.2 284 1.5 257 1.2 284 1.3 305 1.5 299 1.7 289 1.8 283 1.8 2 283 1.8 283 1.8 283 1.8 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	TUDE (-40 4.7 213 4.3 212 3.7 211 3.2 211 2.6 224 1.7 245 1.8 263 2.1 270 2.6 261 270 2.6 281 292 282 292 293 293 293 294 295 294 297 294 296 298 298 298 298 298 298 298 298 298 298	dam) A 4.1 230 4.1 230 3.9 221 3.6 3.9 3.9 3.0 202 2.6 229 2.7 229 226 3.0 3.1 222 3.1 222 2.8 2.8 212 2.8 212 2.8 212	5.2 211 4.9 211 4.6 215 3.6 215 3.6 228 227 2.8 212 2.9 208 3.0 208 3.2 207 3.1 3.3 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0	-10 0.5 140 1.1 1232 2.1 232 2.1 242 3.5 3.5 3.6 231 3.6 231 3.1 3.1 3.1 3.1 3.1 3.1 3.1 3.1 3.1 3.1	3.7 10 2.4 3.5 1.4 3.5 8 1.4 3.5 2.7 1.8 2.4 2.5 2.2 2.1 2.5 2.2 2.1 2.1 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0	10 2.9 337 2.4 335 1.8 335 1.3 327 0.8 320 0.3 299 0.2 187 0.5 171 0.5 219 0.6 252 0.6 267 0.7 0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8	20 6.5 338 6.1 339 5.7 343 341 5.2 343 355 5.3 346 5.7 350 5.8 352 352 353 5.8 352 353 5.3 354 5.3 356 5.3 3 5.3 3 5.3 5 5 5 5 5 5 5 5 5 5 5 5	15.1 349 13.9 12.9 12.3 355 12.2 355 12.2 359 12.2 14.2 16.0 16.0 17.5 11.2 26.0	40 24.2 20 22 22.2 25 22.0 28 22.6 31 24.2 34 26.5 56 56 57 56 18.7 75 15.8 141 16.9 16.9 16.9 177	7.6 149 6.99 118 8.99 12.8 75 70 23.1 6.70 77 73 8.2 2 120 44.7 138 49.3 165 49.3 165 47.4 182	51.2 188 26.1 181 22.1 168 21.0 150 23.9 133 30.6 120 120 120 67.5 151 89.5 153 75.5 141 89.6 89.5 173 78.9 178 89.5 173 78.9 178	70 35.1 190 31.0 186 26.0 177 27.5 152 37.5 138 47.5 138 17.1 141 81.7 145 90.9 151 165 165 103.4 177 171 171 171 171 171 171 17	26.8 180 24.6 175 23.6 161 27.6 154 33.2 27.6 149 40.6 147 76.7 148 63.1 156 67.8 156 168 179 174 62.8 179 174 184 184 184 185 186 187 188 188 188 188 188 188 188 188 188
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 8.0 7.5 6.0 5.5 5.0 4.5 4.0 3.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603 0.9237 1.52 2.51 4.14 6.83 11.25 18.55 30.59	-80 2.8 318 2.3 318 2.3 314 1.9 308 1.1 284 0.9 271 0.8 266 0.6 0.6 312 0.7 339 0.7 339 0.7 359 0.4 264 0.7 238 1.1 230 0.4 264 227 1.6 225	0.77 331 0.57 330 0.33 330 0.1 310 0.0 215 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	HE IGHT -60 1.8 249 1.8 252 1.9 257 1.8 261 1.7 266 5.272 1.2 280 0.9 288 0.8 290 0.7 284 0.8 272 0.9 260 1.3 3.6 6.2 213 3.6 6.2 213	-50 5.0 224 4.4 226 3.7 228 2.2 241 1.5 257 1.4 305 1.4 309 1.5 299 1.8 284 1.8 279 1.7 266 1.9 246 2.5 227 3.3 3.1 266	TUDE (-40 4.7 213 4.3 212 3.7 2111 2.6 2.15 2.0 2.24 1.7 243 1.8 263 2.1 27 2.6 2.6 2.7 2.6 2.8 2.8 2.7 2.9 2.6 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8	dem) A 4.1 230 4.1 230 3.9 221 3.8 211 3.6 199 3.3 202 2.6 6 229 2.9 226 3.0 225 3.1 222 3.0 218 8 212 2.7 204	-20 5.2 211 4.9 211 4.6 212 4.0 215 3.0 215 3.0 215 3.2 28 2.8 227 2.8 220 2.8 227 2.8 220 2.8 227 2.8 3.0 3.0 3.0 3.0 3.0 3.0 196 3.0 196 3.0 186	-10 0.5 140 1.1 232 2.1 244 2.5 2.5 245 3.7 238 3.6 231 3.4 21 2.1 213 2.9 210 2.6 212 2.5 215 2.6 212 2.7 218	3.77 10 2.4 4 328 1.4 328 1.4 328 246 2.2 231 2.5 222 2.4 4 2.1 5 2.0 208 1.6 209 1.7 210 1.6 206 1.5 1.9 3 1.7 185 1.9 178	10 2.9 337 2.4 335 1.8 335 1.3 327 0.8 320 0.3 329 0.2 187 0.5 171 0.5 219 0.6 252 0.6 265 0.7 0.5 272 0.5 272 0.5 273 0.5 274 0.5 275 0.6 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7	20 6.5 338 6.1 339 5.7 340 5.2 343 5.2 343 5.2 345 5.3 347 5.5 5.6 351 5.8 3 5.8 3 5.8 3 5.8 3 5.8 3 5.8 3 5.8 3 5.8 3 5.8 3 5.8 3 5.8 3 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	30 15.1 349 13.9 350 12.9 355 12.2 8 15.9 16 16 17.5 18 18.0 16 17.5 18 19.2 10.4 26 4.6 4.6 4.6 4.6 4.6 4.6 4.6 4.	40 24.2 20 23.0 28 22.2 25 36 31.0 31.3 42 24.5 56 18.7 75 56 18.7 75 108 11.08 11.108 11	7.6 149 6.9 89 112.8 7.5 17.6 70 23.1 69 23.1 69 23.1 69 34.0 77 38.2 12 104 42.2 120 44.7 138 49.3 49.3 49.3 49.3 49.3 49.3 49.4 49.4	51.2 188 22.1 188 22.1 188 21.0 23.9 153 30.6 123 39.6 120 126 67.5 158 89.5 158 89.5 173 78.9 178 40.0 187	70 35.1 190 31.0 186 28.0 177 27.5 165 30.5 152 37.5 138 138 137 141 81.7 145 90.9 151 165 165 165 165 165 165 165	80 26.8 180 24.6 169 24.6 161 154 33.2 149 40.6 147 76.7 71.4 189 70.6 68.9 174 68.9 174 186 186 187 186 187 188 188 188 188 188 188 188
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 8.0 7.5 7.0 6.5 6.0 5.5 5.0 4.5 4.0	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603 0.9237 1,52 2,51 4,14 6,83 11,25	-80 2.8 318 2.3 318 1.9 308 1.1 284 0.9 271 0.8 266 0.6 6 312 0.7 339 0.4 332 0.4 264 0.7 359 0.4 264 0.7 359 0.4 264 0.7 359 0.4 264 0.7 359 0.4 264 0.7 359 0.4 264 0.7 359 0.4 264 0.7 359 0.4 264 0.7 359 0.4 264 0.7 359 0.4 264 0.7 359 0.4 264 0.7 359 0.4 264 0.7 359 0.4 264 0.7 359 0.4 264 0.7 359 0.4 264 0.7 359 0.4 264 0.7 359 0.4 264 0.7 359 0.4 264 0.7 359 0.4 265 0.6 0.7 359 0.6 0.7 359 0.6 0.7 359 0.7 359 0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8	0.77 331 0.57 330 0.3 330 0.3 330 0.0 0.0 0.1 345 0.2 0.2 0.3 358 0.5 358 0.5 358 0.5 358 0.5 358 0.5 358 0.6 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7	HE IGHT -60 1.8 249 1.8 252 1.9 254 1.7 266 1.5 272 1.2 280 0.9 288 0.8 290 0.8 290 0.8 272 0.9 260 0.8 272 0.9 260 0.8 272 0.9 260 0.8 272 0.9 260 0.8 272 0.9 260 0.8 272 0.9 260 0.8 272 0.9 260 0.8 272 0.9 260 0.8 272 0.9 260 0.8 272 0.9 260 0.8 272 0.9 260 0.8 272 0.9 260 0.8 272 0.9 260 0.8 272 0.9 260 0.8 272 0.9 260 0.8 272 0.9 260 0.8 272 0.9 260 0.8 272 0.9 260 0.9 272 0.9 260 0.9 272 0.9 260 0.9 272 0	-50 5.0 224 4.4 226 3.7 228 2.2 281 1.5 257 1.2 284 1.3 305 1.4 305 1.5 299 1.8 284 1.8 279 1.2 266 1.9 266 1.9 266 1.9 266 1.9 266 1.9 27 27 28 28 28 28 28 28 28 28 28 28 28 28 28	TUDE (-40 4.7 215 4.3 212 3.7 211 2.6 215 2.0 224 1.7 243 1.27 2.6 2.6 261 2.8 2.8 2.5 2.9 2.4 2.7 2.7 2.4 2.7 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8	dem) A 4.1 230 3.9 221 3.8 211 3.6 211 2.5 23 2.7 229	-20 5.2 211 4.9 211 4.6 212 4.13 213 4.0 215 3.3 224 3.3 224 2.8 220 2.8 212 2.9 208 3.0 228 2.12 2.9 3.0 2.15 3.0 3.0 3.0 3.0 3.	-10 0.5 140 1.1 232 2.1 244 2.5 245 3.7 238 3.6 231 3.1 213 2.9 210 2.6 217 2.6 217 2.6 215 2.5 196 2.6 2.5 196	3.7 10 2.4 4 328 1.4 328 1.5 246 2.2 2 231 2.5 2.2 2 210 2.0 2.0 2.0 1.7 210 1.6 206 1.5 1.9 1.7 185 1.9	2.9 337 2.4 332 1.8 332 1.8 332 0.3 329 0.2 187 0.5 219 0.5 219 0.6 252 0.6 267 0.5 267 0.5 180 0.6 180 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	20 6.5 338 6.1 339 5.7 340 5.2 343 5.3 347 5.5 5.8 352 5.6 352 5.6 352 5.6 352 5.7 359 5.7 10 0.8 10 10 10 10 10 10 10 10 10 10 10 10 10	30 15.1 349 13.9 350 12.9 355 12.2 8 14.2 8 15.9 17.4 18.0 16.5 17.5 18.0 16.6 21 12.4 36 4.6 62 3.3 3.0 4.6 6.6 6.7 6.7 6.7 6.7 6.7 6.7 6	40 24.2 20 22.2 22.2 25 31 24.2 34 26.5 36 31.0 40 31.3 47 24.5 56 18.7 7 108 11.8	7.6 149 6.9 89 89 81 2.8 75 17.6 6.7 77 38.2 34.0 5.9 24.1 104 42.2 120 44.7 182 45.8 165 45.8 165 17.4 182 25.2 25.2	51.2 188 26.1 188 22.1 168 21.0 150 25.9 133 30.6 120 49.4 121 159.0 126 67.5 141 85.0 150 89.5 175 78.9 178 61.7 182 40.0	70 35.1 190 31.0 186 28.0 177 165 30.5 152 37.5 138 47.5 138 138 171 114 181.7 145 198.3 158 158 159 158 159 159 159 159 159 159 159 159	80 26.8 180 24.6 167 23.6 161 152 149 40.6 147 76.7 148.9 149 149 149 150 161 179 174 184 179 174 184 184 184 185 185 185 185 185 185 185 185

JANUARY	MEAN 1	TEMPERA	THE A	MPL ITU	DE (K)	AND P	HASE	WAVE	2									
1 - 2 - 2 - 2	PRESSURE (mb)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
12.0	0.0062	0,32	0.19	0.18	0.15	0,25	0.26	0.52	1,30	0.80	0.36	0.36	0.78	0,58	1.10	0.92	0,33	0.25
11,5	0,0103	0.37	0.21	0.22	0.17	0.27	0.29	0.49	1.24	0.79	0.34	0.35	0.78	0,49	1.10	0.88	0,29	0,42
11.0	0,0169	0.41	0.21	0.24	0.19	0.26	0.29	0.39	1,09	0.72	0.31	0.31	0.73	0.34	1.06	0.85	0.23 257	0.67
10,5	0.0279	0.40	0.20	0.27	0,20	0.26	0.29	0.23	0.82	0,60	0.26	0.27	0.67	0.21	1.11	0.94	0.21	0.98
10.0	0.0460	0.32	0.16	0.26	0.21	0.26	0.27	0.07	0.50	0.44	0.27	0.28	0.67	0,44	1,33	1,28	214 0.39 178	1,30
9,5	0.0758	0.16	0.17	0.23	0.22	0.26	0,23	0,18	0.28	0.24	0.34	0,34	0.75	0.80	1,69	1.77	0.70	1.51 232
9,0	0,1250	0.08	0,22	0.18	0,21	76	0,15	0,34	0.43	0.10	0,39	0,42	0.87	1,08	2,03	2.30	1,11	1,21
8.5	0.2061	0.30	0.21	0.13	0.14	0.16	0.02	0.38	0,60	0.30 191	137	0.46	0.92 146	1.17	2.16	2.68	1,48	0.65
8.0	0.3398	0.50 208	0.16 46	0.07	0.05	0.04	0.20 216	0.32 202	191 0,60 203	0.52	0.30 180	0.44 174	0.90	0.99 140	177 2.10 199	2.85	161 1,70 162	21
7.5	0.5603	0.48	0.14	0.06	0.08	0.14	0.26	0.16	0.33	0.49	0.24	0.47	1.08	1.20	2.04	2,45	1.67	1.11
7.0	0.9237	0.40	0.13	0.08	0.09	0.17	0.21	0.06	0.20	0.32	0,25	0.47	1,19	1,49	2.02	2,49	1,98	1,01
6.5	1,52	0.29	0.07	0.06	0.04	0.09	0.08	0.01	0.17	0.16	0.24	0.52	1,29	1.62	2.09	3.16	2.82	0.53
6.0	2.51	0.24	0.02	0.04	0.02	0.03	0,06	0.03	0.12	0.10	0.23	0.66	1,50	1.73	2.17	3.93	3.73	1.19
5,5	4.14	0.21	0.03	0.07	0.08	0.04	0.11	0.09	0.05	0.05	0.18	0.63	1,45	1.82	1,92	3,22	3,17	1.09
5.0	6.83	0.19	0.06	0.13	0.14	0.05	0,16	87 0.16 94	0.04	0.06	0.10	0.49	1.28	2.03	2.30	2.52	2.18	0.85
4.5	11.25	0.16	0.09	0.18	0.19	0.07	0,21	0.25	0.13 108	0.14 107	0.05	0.27 310	1.00	305 2.17 320	286 3.10 309	3,11 299	2.09	0.76
4.0	18,55	0.14 249	0.11 205	0.21 175	0.23 167	0.07	0.23	0.30	0.20	0.20	0.13	0.24	317 0,85 353	2.10	3,75	4,50	3,47	1.14
3,5	30.59	0,12	0.10	0.22	0.23	0.07	0.22	0.31	0.23	0.22	0.19	0.41	0.89	1.84	3.85	5,29	4,55	1.53
3.0	50.43	0.09	0,49	0.19	0.19	0.06	0.20	0.29	0.23	0.21	0.22	0.51	0.91	1,42	3.36	4.90	4.44	1.48
2.5	93.15	0.07	0.06	0.14	0.14	0.05	0,15	0.23	0.19	0.17	0.18	70 0.45 76	0,75	344 0.94 349	330 2,42 333	3,63 342	3.31	1.07
		287	209	180	170	143	100	**	103	100	00	70	"	349	333	342		
JANUARY		GEOPOTE -80						-		AVE 2	10	20	30	40	50	60	70	80
	PRESSURE (mb)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	60
SCALE HEIGHT 12.0	PRESSURE (mb) 0.0062	-80 2.0 223	-70 1.7 18	-60 4.0 116	-50 2.4 89	-40 3.0 118	-30 3.5 97	-20 2.2 84	-10 5.1 65	0 4.5	1.4	1.6	4.8	13.8	11.6	10.2	8.0 334	5.2
SCALE HEIGHT 12.0 11.5	PRESSURE (mb) 0.0062 0.0103	-80 2.0 223 2.5 216	-70 1.7 16 1.5 27	-60 4.0 116 3.7 116	-50 2.4 89 2.3 94	-40 3.0 118 2.7 116	-30 3.5 97 3.1 98	-20 2.2 84 1.8 101	-10 5.1 65 3.6 79	0 4.5 86 3.5 95	1.4 118 1.5 138	1.6 221 2.1 2.1 218	4.8 289 4.9 275	13.8 311 13.0 311	11.6 307 12.2 300	10.2 287 11.2 283	8.0 334 7.7 337	5.2 296 5.1 301
SCALE HEIGHT 12.0	PRESSURE (mb) 0.0062	-80 223 2.5 216 3.0 211	-70 1.7 16 1.5 27 1.4 38	-60 4.0 116 3.7 116 3.4 117	-50 2.4 89 2.3 94 2.2 100	-40 3.0 118 2.7 116 2.3 116	-30 3.5 97 3.1 98 2.7 100	-20 2.2 84 1.8 101 1.6 122	-10 5.1 65 3.6 79 2.5 105	0 4.5 86 3.5 95 2.7 109	1.4 118 1.5 138 1.7 154	1.6 221 2.1 218 2.6 218	4.8 289 4.9 275 5.5 265	13.8 311 13.0 311 12.4 311	11.6 307 12.2 300 13.2 294	10.2 287 11.2 283 12.4 281	8.0 334 7.7 337 7.6 340	5.2 296 5.1 301 5.0 310
SCALE HEIGHT 12.0 11.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279	-80 223 2.5 216 3.0 211 3.6 208	-70 1.7 18 1.5 27 1.4 38 1.3 50	-60 4.0 116 3.7 116 3.4 117 3.0 118	-50 2.4 89 2.3 94 2.2 100 2.0	-40 3.0 118 2.7 116 2.3 116 1.9	-30 3.5 97 3.1 98 2.7 100 2.3 104	-20 2.2 84 1.8 101 1.6 122 1.7 138	-10 5.1 65 3.6 79 2.5 105 2.2 139	0 4.5 86 3.5 95 2.7 109 2.1 127	1.4 118 1.5 138 1.7 154 1.8 166	1.6 221 2.1 218 2.6 218 3.0 220	4.8 289 4.9 275 5.5 265 6.2 258	13.6 311 13.0 311 12.4 311 12.1 310	11.6 307 12.2 300 13.2 294 14.6 291	10.2 287 11.2 283 12.4 281 13.7 282	8.0 334 7.7 337 7.6 340 7.6 342	5.2 296 5.1 301 5.0 310 4.9 324
SCALE HEIGHT 12.0 11.5 11.0 10.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460	-80 2.0 223 2.5 216 3.0 211 3.6 208 4.1 205	-70 1.7 18 1.5 27 1.4 38 1.3 50 1.1	-60 4.0 116 3.7 116 3.4 117 3.0 118 2.6 119	-50 2.4 89 2.3 94 2.2 100 2.0 107 1.9	-40 3.0 118 2.7 116 2.3 116 1.9 117	-30 3.5 97 3.1 98 2.7 100 2.3 104 2.0 109	-20 2.2 84 1.8 101 1.6 122 1.7 138 1.8 144	-10 5.1 65 3.6 79 2.5 105 2.2 139 2.4 163	0 4.5 86 3.5 95 2.7 109 2.1 127 1.9 148	1.4 118 1.5 138 1.7 154 1.8 166 1.8 178	1.6 221 2.1 218 2.6 218 3.0 220 3.3 223	4.8 289 4.9 275 5.5 265 6.2 258 7.7 256	13.8 311 13.0 311 12.4 311 12.1 310 12.3 308	11.6 307 12.2 300 13.2 294 14.6 291 16.3 291	10.2 287 11.2 283 12.4 281 13.7 282 15.0 285	8.0 334 7.7 337 7.6 340 7.6 342 8.0 343	5.2 296 5.1 301 5.0 310 4.9 324 5.3 343
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758	-80 223 2.5 216 3.0 211 3.6 208 4.1 205 4.4 204	-70 1.7 18 1.5 27 1.4 38 1.3 50 1.1 61 1.0 69	-60 4.0 116 3.7 116 3.4 117 3.0 118 2.6 119 2.3 121	-50 2.4 89 2.3 94 2.2 100 2.0 107 1.9 115 1.7 123	-40 3.0 118 2.7 116 2.3 116 1.9 117 1.5 121 1.3 132	-30 3.5 97 3.1 98 2.7 100 2.3 104 2.0 109 1.7 118	-20 2.2 84 1.8 101 1.6 122 1.7 138 144 1.9 140	-10 5.1 65 3.6 79 2.5 105 2.2 139 2.4 163 2.3 175	0 4.5 86 3.5 95 2.7 109 2.1 127 1.9 148 1.6 163	1.4 118 1.5 138 1.7 154 1.8 166 1.8 178 1.7	1.6 221 2.1 218 2.6 218 3.0 220 3.3 223 3.6 230	4.8 289 4.9 275 5.5 265 6.2 258 7.7 256 8.2 257	13.8 311 13.0 311 12.4 311 12.1 310 12.3 308 13.0 306	11.6 307 12.2 300 13.2 294 14.6 291 16.3 291 18.4 294	10.2 287 11.2 283 12.4 281 13.7 282 15.0 285 16.5 291	8.0 334 7.7 337 7.6 340 7.6 342 8.0 343 8.8 344	5.2 296 5.1 301 5.0 310 4.9 324 5.3 343 6.3
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250	-80 2.0 223 2.5 216 3.0 211 3.6 208 4.1 204 4.5 203	-70 1.7 18 1.5 27 1.4 38 1.3 50 1.1 61 1.0 69 0.7 75	-60 4.0 116 3.7 116 3.4 117 3.0 118 2.6 119 2.3 121 2.0 123	-50 2.4 89 2.3 94 2.2 100 2.0 107 1.9 115 1.7 123 1.6 132	3.0 118 2.7 116 2.3 116 1.9 117 1.5 121 1.3 132	-30 3.5 97 3.1 98 2.7 100 2.3 104 2.0 109 1.7 118 1.5 126	-20 2.2 84 1.8 101 1.6 122 1.7 138 144 1.9 140	-10 5.1 65 3.6 79 2.5 105 2.2 139 2.4 163 2.3 175 1.9	0 4.5 86 3.5 95 2.7 109 2.1 127 1.9 148 1.6	1.4 118 1.5 138 1.7 154 1.8 166 1.8 178 1.7 191	1.6 221 2.1 2.8 2.6 218 3.0 220 3.3 223 3.6 230 3.7 238	4.8 289 275 5.5 265 6.2 258 7.7 256 8.2 257 9.2 262	13.8 311 13.0 311 12.4 311 12.1 310 12.3 308 13.0 306	11.6 307 12.2 300 13.2 294 14.6 291 16.3 291 18.4 294 20.7 298	10.2 287 11.2 283 12.4 281 13.7 282 15.0 285 16.5 291 18.1 299	8.0 334 7.7 337 7.6 340 7.6 342 8.0 343 8.8 344	5.2 296 5.1 301 5.0 310 4.9 324 5.3 343 6.3 1
SCALE HE (GHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061	-80 2.0 223 2.5 216 3.0 211 3.6 208 4.1 205 4.4 204 4.5 203	-70 1.7 18 1.5 27 1.4 38 1.3 50 1.1 61 1.0 69 0.7 75 0.4 82	-60 116 3.7 116 3.4 117 3.0 118 2.6 119 2.3 121 2.0 123 1.7 126	-50 2.4 89 2.3 94 2.2 100 2.0 107 1.9 115 1.7 123 1.6 132 1.4 141	-40 3.0 118 2.7 116 2.3 116 1.9 117 1.5 121 1.3 132 1.1 149	-30 3.5 97 3.1 98 2.7 100 2.3 104 2.0 109 1.7 118 1.5 126 1.5 130	-20 2.2 84 1.8 101 1.6 122 1.7 138 1.8 144 1.9 140 1.9 128 2.0 113	-10 5.1 65 3.6 79 2.5 105 2.2 139 2.4 163 2.3 175 1.9 181	0 4.5 86 3.5 95 2.7 109 2.1 127 1.9 148 1.6 163 172 1.3 173	1.4 118 1.5 138 1.7 154 1.6 166 1.8 17 191 1.6 209	1.6 221 2.1 2.8 2.6 218 3.0 220 3.3 223 3.6 230 3.7 238 3.8 248	4.8 289 4.9 275 5.5 265 6.2 258 7.7 256 8.2 257 9.2 262 10.0 268	13.8 311 13.0 311 12.4 311 12.1 310 12.3 306 13.0 306 14.4 304	11.6 307 12.2 300 13.2 294 14.6 291 16.3 291 18.4 294 20.7 298 22.8 304	10.2 287 11.2 283 12.4 281 13.7 282 15.0 285 16.5 291 18.1 299 19.8 309	8.0 334 7.7 337 7.6 340 7.6 342 8.0 343 8.8 344 10.1 344 12.0 343	5.2 296 5.1 301 5.0 310 4.9 324 5.3 343 6.3 1 7.9 13
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398	-80 2.0 223 2.5 216 3.0 211 3.6 208 4.1 205 4.4 204 4.5 203 4.2 202 3.6 201	-70 1.7 18 1.5 27 1.4 38 1.3 50 1.1 61 1.0 69 0.7 75 0.4 82 0.2 117	-60 4.0 116 3.7 116 3.4 117 3.0 118 2.6 119 2.3 121 2.0 123 1.7 126 126 127	-50 2.4 89 2.3 94 2.2 100 2.0 107 1.9 115 1.7 123 1.6 132 1.4 141	-40 3.0 118 2.7 116 2.3 116 1.9 117 1.5 121 1.3 132 1.1 149 1.2 164	-30 3.5 97 3.1 98 2.7 100 2.3 104 2.0 109 1.7 118 1.5 126 1.5 130 1.5 124	-20 2.2 84 1.8 101 1.6 122 1.7 138 144 1.9 140 1.9 120 113 2.1	-10 5.1 65 3.6 79 2.5 105 2.2 139 2.4 163 2.3 175 1.9 181 1.2 180 0.4 141	0 4.5 86 3.5 95 2.7 109 2.1 127 148 163 1.6 173 173 0.8 162	1.4 118 1.5 138 1.7 154 1.8 166 1.8 178 1.7 191 1.6 209 1.4 230	1.6 221 2.1 2.8 2.6 218 3.0 223 3.3 223 3.6 230 3.7 238 3.8 248 3.8 258	4.8 289 4.9 275 5.5 268 7.7 256 8.2 257 9.2 262 10.0 268 10.5 274	13.8 311 13.0 311 12.4 311 12.3 308 13.0 306 14.4 304	11.6 307 12.2 300 13.2 294 14.6 291 16.3 291 18.4 294 20.7 298 22.8 304 24.3 311	10.2 287 11.2 283 12.4 281 13.7 282 15.0 285 16.5 291 18.1 299 19.8 309 21.5 319	8.0 334 7.7 337 7.6 340 7.6 342 8.0 343 8.8 344 10.1 344 12.0 343 14.3 343	5.2 296 5.1 301 5.0 310 4.9 324 5.3 343 6.3 1 7.9 13 18
SCALE HE (GHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603	-80 2.0 223 2.5 216 3.0 211 3.6 208 4.1 205 4.4 204 4.5 202 3.6 202 3.6 202	-70 1.7 18 1.5 27 1.4 38 1.3 50 1.1 61 1.0 69 0.7 75 0.4 82 0.2 117 0.3 161	-60 4.0 116 3.7 116 3.4 117 3.0 118 2.5 119 2.3 121 2.0 123 1.7 126 1.6 126 1.6 121	-50 2.4 89 2.3 94 2.2 100 1.9 115 1.7 123 1.4 141 1.4 146	-40 3.0 118 2.7 116 2.3 116 2.3 116 1.9 1.7 1.5 121 1.3 132 164 1.2 164 1.2 164 1.1 167	-30 3.5 97 3.1 98 2.7 100 2.3 104 2.0 109 1.7 118 1.5 130 1.5 130 1.5 111	-20 2.2 84 1.8 101 1.6 122 1.7 138 1.6 144 1.9 128 2.0 113 2.1 13 2.1 98 2.2 90	-10 5.1 65 3.6 79 2.5 105 2.2 139 2.4 163 2.3 175 180 0.4 14 10.7 69	0 4.5 86 3.5 95 2.7 109 2.1 127 1.9 148 1.6 1.6 172 1.3 173 0.8 162 0.4	1.4 118 1.5 138 1.7 154 1.8 166 1.8 178 1.7 191 1.6 209 1.4 230 1.3 250 1.1 264	1.6 221 2.1 2.18 2.6 2.18 3.0 220 3.3 223 3.6 230 3.7 238 3.8 248 3.8 248 3.7 269	4.8 289 4.9 275 5.55 6.2 258 7.7 256 8.2 257 9.2 262 10.0 268 10.5 274 10.6 282	13.8 311 13.0 311 12.1 310 12.3 308 13.0 14.4 304 16.0 303 17.6 304 18.8 307	11.6 307 12.2 300 13.2 294 14.6 291 16.3 291 18.4 294 20.7 298 22.8 304 24.3 311 25.2 317	10.2 287 11.2 283 12.4 281 13.7 282 15.0 285 16.5 291 18.1 299 19.8 309 21.5 319 23.1 328	8.0 334 7.7 337 7.6 340 7.6 343 8.0 343 8.4 10.1 344 12.0 343 14.3 343 16.7 343	5.2 296 5.1 301 5.0 310 4.9 324 5.3 343 6.3 17.9 13 18 10.0 18
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603	-80 2.0 223 2.5 216 3.0 211 3.6 208 4.1 205 4.4 204 4.5 203 4.2 202 3.6 201	-70 1.7 18 1.5 27 1.4 38 1.3 50 1.1 61 1.0 69 0.7 75 0.4 82 0.2 117 0.3	-60 4.0 116 5.7 116 5.7 117 5.0 118 2.5 121 123 1.7 126 1.6 129 1.6 1.7 121 1.7 126 1.7 127 127 128 129 121 121 121 121 121 121 121 121 121	-50 2.4 89 2.3 94 2.2 100 107 1.9 115 1.7 123 1.6 132 1.4 141 1.4	-40 3.0 118 2.7 116 2.3 116 1.9 117 1.5 121 1.3 1149 1.2 164 1.2 170 1.1 167 10.9	-30 3.5 97 5.1 98 2.7 100 2.3 104 2.0 109 1.7 118 1.5 124 1.5 111 1.6 98	-20 2.2 84 1.8 101 1.6 122 1.7 138 1.8 144 1.9 140 1.9 128 2.1 98 2.2 90 2.1 86	-10 5.1 65 3.6 79 2.5 105 2.2 139 163 2.3 175 2.3 175 1.9 181 1.2 180 0.4 141 0.7 69 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	0 4.5 86 3.5 95 2.7 109 148 1.6 163 3 1.6 172 1.3 1.6 162 0.4 113 0.7 7,73	1.4 118 1.5 138 1.7 154 1.8 166 1.8 178 1.7 191 1.6 209 1.3 250 1.1 250 0.8 277	1.6 221 2.1 2.8 2.18 3.0 220 3.3 3.23 3.6 230 3.7 238 3.8 258 3.8 258 3.7 279	4.8 289 4.9 275 5.55 6.2 258 7.7 2.56 8.2 257 9.2 262 10.5 274 10.6 282 10.4 291	13.8 311 15.0 311 12.4 310 12.3 306 13.0 306 14.4 304 16.0 303 17.6 304 18.8 307 17.6 307 18.8 30 18.8 30 30 18.8 18.8 18.8 18.8 18.8 18.8 18.8 18.	11.6 307 12.2 300 15.2 294 14.6 291 16.3 291 18.4 294 20.7 298 22.8 304 24.3 311 25.2 317 26.0 324	10.2 287 11.2 283 12.4 281 13.7 282 15.0 285 16.5 291 18.1 299 19.6 309 21.5 319 23.1 326 25.2 335	8.0 334 7.7 337 7.6 340 7.6 342 8.0 343 8.8 344 10.1 1344 12.0 343 14.3 343 16.7 343 19.3 344	5.2 296 5.1 301 5.0 5.0 4.9 324 5.3 343 6.3 1 7.99 15 9.3 18 10.0 18 9.7 11
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 8.0 7.5 7.0	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603	-80 2.0 223 2.5 216 3.0 211 3.6 208 4.1 205 4.4 204 4.5 202 3.6 202 3.6 202	-70 1.7 16 1.5 27 1.4 38 1.3 50 1.1 61 1.0 69 0.7 75 0.4 82 0.2 117 0.3 161 0.5 162 0.5 162 0.6	-60 4.0 116 3.7 116 3.4 117 3.0 118 2.6 119 2.3 121 121 122 123 1.6 1.7 124 1.7 134 1.7 134 1.7 134 1.7 134 137 137 137 138 138 138 138 138 138 138 138 138 138	-50 2.4 89 2.3 94 2.2 100 2.00 107 1.9 115 1.7 123 1.6 132 1.4 141 1.4 146 1.5 145 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6	-40 3.0 118 2.7 116 2.3 116 2.3 116 1.9 117 1.5 121 1.3 132 1.1 149 1.2 170 0.9 160 0.7 152	-30 3.5 97 3.1 98 2.7 100 2.3 104 2.0 109 1.7 118 1.5 126 1.5 124 1.5 126 1.5 126 1.7 1.1 1.6 98 1.7 1.1 1.6 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7	-20 2.2 84 1.8 101 1.6 102 1.7 138 1.8 144 1.9 128 2.0 90 2.1 85	-10 5.1 65 3.6 79 2.5 105 2.2 2.3 139 2.4 163 2.3 175 180 0.4 141 10.7 69 1.0 67 74	0 4.5 86 3.5 95 2.7 109 2.1 127 1.9 148 1.6 1.6 172 1.3 173 0.8 162 0.4	1.4 118 1.5 138 1.7 154 1.8 1.6 1.6 1.8 1.7 191 1.6 209 1.3 250 1.3 250 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.	1.6 221 2.1 2.18 3.0 3.2 3.3 223 3.5 230 3.7 238 3.8 258 3.8 258 3.7 269 3.5 279 3.3 3.5 290 3.5 3.7 290 3.8 3.8 3.8 3.8 3.8 3.7 3.8 3.8 3.8 3.8 3.8 3.8 3.8 3.8 3.8 3.8	4.8 289 4.9 275 265 6.2 256 8.2 257 9.2 262 10.0 268 10.5 274 10.6 282 10.4 291 10.4 291 9.9 301	13.8 311 13.0 311 12.4 311 12.1 310 12.3 308 13.0 303 17.6 303 17.6 307 19.5 313 19.5 313 19.5 313 19.6 307 19.5 313 19.5 313 19.6 313 313 313 313 313 313 313 31	11.6 307 12.2 294 14.6 291 16.3 291 18.4 294 20.7 20.7 317 26.0 324 330 324 3330	10.2 287 11.2 283 12.4 281 13.7 282 15.0 285 16.5 291 18.1 299 19.6 309 21.5 319 21.5 319 25.2 335 25.2 335 26.3	6.0 334 7.7 7.6 340 7.6 343 8.0 343 10.1 343 14.3 343 14.3 343 16.7 343 19.3 344 22.6 347	5.2 296 5.1 301 5.0 310 4.9 324 5.3 343 6.3 1 1 7.9 13 18 10.0 18 9.7 11 11 9.5 2 9.9 9.9 9.9
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 8.0 7.5 7.0 6.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603 0.9237 1.52 2.51	-80 2.0 223 2.5 2.5 2.6 3.0 211 3.6 208 4.1 205 4.4 204 4.5 202 202 202 2.5 202 3.6 201 3.6 201 3.6 203 4.1 205 3.6 205 3.6 205 3.6 205 3.6 205 3.6 205 3.6 205 3.6 205 3.6 205 3.6 205 3.6 205 3.6 205 3.6 205 3.6 205 3.6 205 3.6 205 3.6 205 3.6 205 3.6 3.6 3.6 3.6 3.6 3.6 3.6 3.6 3.6 3.6	-70 1.7 16 1.5 27 1.4 38 1.3 50 1.1 61 1.0 69 0.7 75 0.4 82 0.2 117 0.3 161 0.5 162 0.6 159	-60 4.0 116 5.7 117 3.0 118 2.6 119 2.3 121 122 123 1.7 126 128 1.6 128 1.6 128 1.7 121 127 127 127 127 127 127 127 127 12	-50 2.4 89 2.3 94 2.2 100 2.0 1.7 1.2 1.6 1.4 1.4 1.4 1.4 1.4 1.6 1.5 1.6 1.7 1.7 1.4	-40 3.0 118 2.7 116 2.3 116 1.9 1.7 1.5 121 1.1 1.3 132 1.1 1.4 1.2 164 1.2 160 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.	-30 3.5 97 5.1 98 2.7 100 2.3 104 2.0 109 1.7 118 1.5 126 1.5 126 1.5 121 1.5 121 1.5 121 1.5 1.1 1.5 1.1 1.5 1.1 1.5 1.1 1.5 1.1 1.5 1.5	-20 2.2 84 1.8 101 1.6 102 1.7 138 1.6 144 1.9 140 1.9 128 2.0 113 2.1 86 2.1 86	-10 5.1 65 3.6 79 2.5 105 2.2 2.3 175 1.9 181 1.2 180 0.4 141 0.7 69 1.0 67	0 4.5 86 3.5 95 2.7 109 2.1 127 1.9 1.6 163 1.6 172 1.3 173 0.8 162 0.4 113 0.7 73 0.9 67	1.4 1188 1.5 138 1.7 154 1.6 1.8 1.7 191 1.6 209 1.4 230 1.3 250 1.1 264 0.6 300 0.5 338	1.6 221 2.1 2.18 2.6 2.18 3.0 2.20 3.3 2.23 3.6 2.30 3.7 2.6 2.30 3.8 2.48 3.8 2.6 2.8 3.7 2.6 2.9 3.7 2.6 2.9 3.7 2.6 2.9 3.7 2.9 3.7 2.9 3.7 2.9 3.7 2.9 3.7 2.9 3.7 2.9 3.7 2.9 3.7 2.9 3.9 3.7 2.9 3.9 3.9 3.9 3.9 3.9 3.9 3.9 3.9 3.9 3	4.8 289 4.9 275 5.5 265 6.2 257 7.2 256 8.2 257 9.2 268 10.5 274 10.6 282 10.6 282 10.9 9.9 9.3 10.9 9.9 9.3 10.9 9.9 9.9 9.9 9.9 9.9 9.9 9.9 9.9 9.9	13.8 311 13.0 311 12.4 311 12.3 310 12.3 306 14.4 304 16.0 303 17.6 304 18.8 307 19.5 313 19.6 319 19.5	11,6 307 12,2 300 13,2 294 14,6 291 16,3 291 16,3 291 18,4 294 20,7 27,2 304 24,3 31 25,2 317 26,0 324 27,3 350 28,8 355	10,2 287 11,2 283 12,4 281 15,0 282 15,0 291 18,1 299 19,8 309 21,5 319 23,1 328 25,2 26,5 340 35,0 35,0 35,0 35,0 35,0 35,0 35,0 35,	8.0 334 7.7 7.6 340 343 8.0 343 10.1 344 12.0 343 14.3 343 16.7 343 19.3 19.3 19.3 19.3 19.3 19.3 19.3 19.	5.2 296 5.1 301 5.0 310 4.9 324 5.3 343 6.3 17.9 15 10.0 18 9.7 11 19.5 2 9.9 9.9 9.5 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 7.0 6.5 6.0 5.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603 0.9237	-80 2.0 2.23 2.5 2.6 2.5 2.6 2.6 2.0 4.1 2.0 4.2 2.0 4.2 2.0 3.6 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0	-70 1.7 16 1.5 27 1.4 38 1.3 50 1.1 61 1.0 69 0.7 75 0.4 82 0.2 117 0.3 161 0.5 1.6 159 0.7	-60 4.0 116 5.7 116 5.4 117 3.0 118 2.5 121 2.0 123 126 126 127 127 127 127 127 127 127 127 127 127	-50 2.4 89 2.3 94 2.2 100 2.0 1.7 123 1.6 132 1.4 141 146 1.4 146 1.4 1.4 1.4 1.4 1.4 1.4 1.4 1.4	-40 3.0 118 2.7 116 2.3 116 1.9 117 1.5 121 1.1 1.3 132 1.1 1.49 1.2 164 1.2 160 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.	-30 3.5 97 3.1 98 2.7 100 2.3 104 2.0 109 1.7 118 1.5 130 1.5 111 1.6 98 1.7 91 1.6	-20 2.2 84 1.8 84 101 1.6 122 1.7 138 1.4 14 1.9 140 1.9 128 2.0 113 2.1 86 2.1 86 2.1 86 2.0 86	-10 5.1 65 3.6 79 2.5 105 2.2 2.3 139 2.4 163 2.3 175 180 0.4 141 10.7 69 1.0 67 74	0 4.5 86 5.95 2.7 109 2.1 127 148 1.6 163 1.7 173 0.8 162 0.4 113 0.7 73 0.9 67 1.1 68 1.2 68	1.4 1188 1.5 1.7 154 1.8 166 1.8 166 1.8 17 191 1.6 209 1.4 250 0.6 277 0.6 300 0.5 338 0.6 7	1.6 221 2.1 2.6 2.6 2.20 3.3 3.2 3.3 3.6 2.30 3.7 2.38 2.58 3.6 2.58 3.6 2.7 2.6 3.0 2.7 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8	4.8 289 4.9 275 5.5 5.6 258 7.7 256 8.2 257 10.0 268 10.4 291 9.9 9.9 301 9.0 312 7.3	13.8 311 13.0 311 12.4 310 12.1 310 12.3 308 13.0 306 14.4 304 16.0 303 17.6 304 18.6 307 19.5 313 19.5 313 19.5 313	11.6 307 12.2 300 13.2 294 14.6 291 16.3 291 18.4 294 22.8 331 25.2 27.3 317 26.0 324 27.3 350 28.8 350 29.8 29.8 29.8 29.8 29.8 29.8 29.8 29.8	10.2 287 11.2 283 12.4 281 15.0 285 16.5 291 18.1 309 19.6 309 23.1 536 25.2 335 28.5 340 340 35.0 340 35.0 35.0 35.0 35.0	8.0 334 7.7 7.7 7.6 342 8.0 343 8.8 344 12.0 343 343 16.7 343 344 22.6 352 347 26.8 352 352 353 353	5.2 296 5.11 5.00 5.00 4.9 324 5.3 343 6.3 1 7.9 9.3 11 10.0 9.5 2 9.5 2 9.5 11 11 9.5 2 9.5 11 11 9.5 10 10 10 10 10 10 10 10 10 10 10 10 10
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 8.0 7.5 7.0 6.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603 0.9237 1.52 2.51	-80 2.0 223 2.5 216 5.0 211 3.6 208 4.1 203 4.2 203 3.6 203 2.3 2.0 2.3 2.0 2.1 2.9 2.0 2.3 2.0 2.1 2.9 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0	-70 1.7 16 1.5 27 1.4 38 1.3 50 0.7 7 0.4 82 0.2 0.2 117 0.3 161 10 0.5 162 0.6 0.7 7 156 0.7 156	-60 4.0 116 3.7 116 3.7 117 3.0 118 2.6 119 2.3 121 1.7 126 1.6 1.7 126 1.7 126 1.7 127 127 128 1.7 129 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7	-50 2.4 89 2.3 94 2.2 100 2.0 107 1.7 1.6 1.32 1.4 141 1.4 146 1.4 1.5 1.6 1.7 1.6 1.7 1.6 1.7 1.6 1.7 1.6 1.7 1.6 1.7 1.6 1.7 1.6 1.7 1.6 1.7 1.6 1.7 1.7 1.6 1.7 1.7 1.6 1.7 1.7 1.6 1.7 1.6 1.7 1.7 1.6 1.7 1.7 1.6 1.7 1.7 1.6 1.7 1.7 1.6 1.7 1.7 1.6 1.7 1.7 1.6 1.7 1.7 1.6 1.7 1.7 1.6 1.7 1.7 1.6 1.7 1.7 1.6 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7	-40 3.0 118 2.7 116 2.3 116 1.9 117 1.5 121 1.3 132 1.1 1.4 19 164 1.2 164 1.2 160 0.7 17 0.9 160 0.7 17 19 10 0.9 10 0.9 10 0.9 10 0.9 10 10 0.9 10 10 10 10 10 10 10 10 10 10 10 10 10	-30 3.5 97 5.1 98 2.7 100 2.3 104 1.5 126 1.5 130 1.5 124 1.5 124 1.5 124 1.5 124 1.5 124 1.5 125 126 127 128 128 129 129 129 129 129 129 129 129	-20 2.2 84 1.8 101 1.6 61 1.7 138 1.44 1.9 128 2.0 113 2.11 86 2.1 86 2.1 86 1.9 86	-10 5.1 65 79 2.5 105 2.2 139 163 2.3 175 1.9 181 1.2 180 0.4 141 0.7 67 1.2 74 1.4 1.5 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6	0 4.5 86 95 2.7 109 148 1.6 163 1.3 173 0.8 162 0.4 113 0.7 73 0.9 67 1.1 68 1.3 66	1.4 1.8 1.5 138 1.7 154 1.8 178 1.7 1.1 1.6 209 1.4 230 1.3 250 1.1 250 0.6 277 0.6 0 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0	1.6 221 218 2.6 2218 3.0 220 3.3 223 3.6 230 3.7 238 3.8 248 3.7 269 3.5 279 3.3 290 290 290 290 290 290 290 290 290 290	4.8 289 4.9 275 5.5 5.5 5.5 6.2 258 8.2 257 9.2 262 10.0 268 10.5 274 10.4 291 9.0 10.4 291 9.0 10.4 291 9.0 10.4 291 291 291 291 291 291 291 291 291 291	13.8 311 15.0 311 12.4 310 12.1 308 13.0 306 14.4 307 19.5 313 17.6 307 19.5 313 19.6 313 19.5 313 19.5 315 19.5 316 317 317 19.5 317 318 318 318 318 318 318 318 318 318 318	11.6 307 12.2 300 15.2 294 14.6 291 16.3 291 16.3 291 16.4 294 20.7 298 22.6 304 24.3 317 26.0 324 25.2 335 28.6 355 29.6 341 28.9 346 346	10.2 287 11.2 283 12.4 15.0 285 16.5 291 18.1 299 21.5 319 22.5 319 25.1 35.0 35.0 35.0 35.0 35.0 35.0 35.0 35.5 35.5	8.0 354 7.7 7.3 7.6 342 8.0 343 8.8 8.4 12.0 343 14.3 343 19.3 343 19.3 344 26.8 347 26.8 352 352 31.1 358 33.9 33.9 33.9 33.9 34.9 35.9 35.9 35.9 35.9 35.9 35.9 35.9 35	5.2 296 5.1 301 5.0 310 4.9 324 5.3 343 6.3 1 1 9.5 1 1 9.5 1 1 9.5 1 1 9.5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 8.0 7.5 7.0 6.5 6.0 5.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603 0.9237 1.52 2.51 4.14 6.83 11.25	-80 2.0 223 2.5 216 3.0 211 3.6 4.1 205 4.4 203 4.5 202 202 202 200 1.8 203 200 1.2 200 2.3 200 2.3 200 2.3 200 2.3 200 2.3 200 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3	-70 1.7 16 1.5 27 1.4 38 1.3 36 1.1 61 1.0 69 0.7 7 0.4 82 0.7 1.6 1.6 0.5 162 0.7 156 0.7 158 0.7 158 0.7 158 0.7 158 0.7 158	-60 4.0 116 3.7 116 3.4 117 3.0 123 121 123 1.7 126 1.6 1.7 134 1.7 137 140 1.7 140 1.7 140 1.7 140 1.7 140 1.7 140 1.7 140 140 140 140 140 140 140 140 140 140	-50 2.4 89 2.3 94 2.2 100 2.0 107 1.9 115 1.7 1.7 1.3 1.6 1.5 1.5 1.7 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.7 1.6 1.6 1.7 1.6 1.6 1.7 1.6 1.6 1.7 1.6 1.6 1.7 1.6 1.7 1.6 1.6 1.7 1.7 1.6 1.6 1.7 1.7 1.6 1.7 1.7 1.6 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7	-40 3.0 118 2.7 116 2.3 116 1.9 117 1.5 121 1.3 1.1 1.3 1.1 1.5 1.2 1.6 1.9 1.9 1.9 1.9 1.9 1.9 1.9 1.9 1.9 1.9	-30 3.5 97 3.1 98 2.7 100 2.3 104 2.0 118 1.5 126 1.5 111 1.6 98 1.7 118 1.5 124 1.5 1.5 1.7 1.6 1.5 1.7 1.7 1.6 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7	-20 2.2 84 1.8 101 1.6 61 122 1.7 138 144 1.9 140 1.9 121 1.8 62 2.0 66 2.0 66 1.6 64	-10 5.1 65 3.6 79 2.5 105 2.2 139 2.4 163 2.3 175 1.9 181 1.2 180 0.4 141 0.7 67 74 1.9 1.0 67 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	0 4.55 5.5 95 2.7 109 148 1.66 1.72 1.3 173 0.4 1.62 0.4 1.63 1.64 1.62 1.63 1.64 1.63 1.64 1.65 1.65 1.65 1.65 1.65 1.65 1.65 1.65	1.4 1.5 138 1.7 154 1.8 166 178 1.7 191 1.6 209 1.4 250 0.5 277 0.6 300 0.5 7 7 7 9 0.6 19 19 19 19 19 19 19 19 19 19 19 19 19	1.6 221 218 2.6 218 3.0 220 3.3 3.23 3.6 248 3.5 279 3.5 279 3.5 279 3.5 290 2.8 3.6 24 2.7 3.7 3.7 3.7 3.7 3.7 3.7 3.7 3.7 3.7 3	4.8 4.9 4.9 275 5.5 5.2 265 6.2 258 7.7 256 8.2 257 10.0 268 274 10.6 291 9.0 10.4 291 9.0 10.4 291 9.0 312 7.9 310 7.9 310 7.9 310 7.9 310 7.9 310 7.9 310 7.9 310 7.9 310 7.9 310 7.9 310 7.9 310 7.9 310 7.9 310 7.9 310 7.9 310 7.9 310 7.9 310 7.9 310 7.9 310 7.9 310 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	13.8 311 13.0 311 12.1 310 12.3 306 13.0 13.0 13.0 14.4 16.0 303 17.6 304 18.6 307 19.5 319 319 319 319 319 319 319 319	11.6 307 12.2 300 13.2 294 14.6 291 16.3 294 20.7 298 22.8 304 25.2 27.3 330 26.8 352 28.8 352 29.8 352 29.8 352 29.8 352 352 352 352 352 352 352 352 352 352	10.2 287 11.2 283 12.4 281 13.7 282 15.0 285 16.5 291 18.1 299 23.15 319 23.15 328 25.2 335 25.2 335 35.0 345 37.3 355 36.7 355 36.7 355	6.0 7.7 337 7.6 340 7.6 343 8.0 343 344 10.1 344 12.0 343 14.3 344 19.3 343 19.3 347 26.8 352 352 352 352 352 353 353 354 355 357 357 357 357 357 357 357	5.2 296 5.1 301 5.0 4.9 324 5.3 343 6.3 1 7.9 13 18 10.0 18 89.7 11 9.3 5.5 12 18 10 10 10 10 11 11 12 16 16 16 16 16 16 16 16 16 16 16 16 16
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 7.0 6.5 5.0 4.5 4.0	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603 0.9237 1.52 2.51 4.14 6.83 11.25	-80 2.0 2.0 2.23 2.5 2.6 2.6 3.0 2.11 3.6 2.08 4.1 2.05 4.2 2.02 3.6 2.01 2.9 2.00 1.8 2.03 1.4 2.06 2.1 2.9 0.8 2.08 0.	-70 1.7 16 1.5 27 1.4 38 1.3 38 1.3 30 1.1 61 0.6 9 0.7 7 7 7 7 0.3 161 0.5 0.6 159 0.7 156 0.7 158 0.	-60 4.0 116 5.7 116 5.7 117 3.0 118 2.6 119 2.3 121 2.0 123 1.7 126 128 1.7 1.7 1.6 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7	-50 2.4 89 2.3 94 2.2 100 2.0 107 1.9 115 1.6 132 1.4 146 1.5 1.6 1.6 1.6 1.6 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7	-40 3.0 118 2.7 116 2.3 116 1.9 117 1.5 121 1.1 1.3 132 1.1 1.49 1.2 170 0.6 150 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.	-30 3.5 97 3.1 98 2.7 100 109 109 1.7 118 1.5 124 1.5 124 1.5 124 1.5 124 1.7 91 1.7 91 1.7 91 1.7 98 99 1.7 1.1 1.5 1.5 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	-20 2.2 84 1.8 101 1.6 122 1.7 138 1.8 144 1.9 129 2.1 90 2.1 85 2.1 85 2.1 86 1.9 86 1.9 86 1.9 86	-10 5.1 65 3.6 79 2.5 105 2.2 139 2.4 163 2.3 175 1.9 181 1.2 180 0.4 141 0.7 76 9 1.5 1.9 1.9 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	0 4.55 86 3.55 95 2.7 109 148 163 1.66 162 0.4 113 0.7 7 0.9 67 1.1 168 1.2 1.3 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6	1.4 1.5 1.5 1.8 1.7 1.6 1.8 1.6 1.6 1.6 1.6 1.6 1.7 1.7 1.7 1.7 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6	1.6 221 218 2.6 3.0 3.2 3.3 223 3.7 238 3.8 248 258 3.7 269 3.3 290 3.3 3.3 3.3 3.3 3.3 3.3 3.3 3.3 3.3 3.	4.8 289 4.9 275 5.55 6.2 256 7.7 256 8.2 257 9.2 262 10.0 274 10.4 10.4 10.4 10.4 10.4 10.4 10.4 10.	13.8 311 15.0 311 12.4 311 12.1 300 12.3 306 14.4 304 16.0 303 17.6 304 18.8 307 19.5 313 19.6 313 313 313 313 313 313 313 313 313 31	11.6 307 12.2 300 13.2 294 14.6 291 16.3 291 16.3 291 20.7 298 22.8 351 21 25.2 22.8 351 27.3 350 28.8 353 29.3 351 29.3 29.3 351 29.3 29.3 29.3 29.3 29.3 29.3 29.3 29.3	102 287 11.2 283 12.4 281 13.7 282 15.0 285 5291 18.1 299 19.8 309 23.1 328 25.2 28.5 340 35.0 35.0 35.0 35.0 35.5 35.5 35.5 35.5	6.0 3.34 7.7 3.37 7.6 3.42 8.0 3.43 8.0 3.43 10.1 13.44 12.0 3.43 16.7 3.43 16.7 3.43 19.3 3.43 19.3 3.43 3.43 19.3 3.44 22.6 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5	5.2 5.1 5.0 5.1 5.0 4.9 5.3 343 6.3 7.9 13 9.3 11 9.5 12 9.9 12.8 10 12.8 15 15 10 12.8 15 15 16 17 18 19 19 19 19 19 19 19 19 19 19
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 6.0 7.5 6.0 5.5 5.0 4.5 4.0 3.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.1250 0.2061 0.3398 0.5603 0.9257 1.52 2.51 4.14 6.83 11.25 18.55 30.59	-80 2.0 2.23 2.5 216 3.0 211 3.6 208 4.1 205 4.4 204 4.5 203 3.6 201 1.8 205 1.4 206 0.6 201 0	-70 1.7 16 1.5 27 1.4 38 1.3 38 1.3 1.0 69 0.7 75 0.4 82 0.2 117 0.5 161 0.5 162 0.6 159 0.7 158 0.7 1	-60 4.0 116 3.7 116 3.7 117 3.0 118 2.6 119 121 2.0 123 127 126 128 129 121 127 126 128 129 129 129 129 129 129 129 129	-50 2.4 89 2.3 94 2.0 2.0 100 107 1.7 123 1.6 131 1.4 146 1.5 1.6 145 1.6 145 1.7 146 1.6 1.5 1.7 146 1.6 1.5 1.7 146 1.7 146 1.7 146 1.7 146 1.7 146 1.7 147 147 147 147 148 149 149 149 149 149 149 149 149 149 149	-40 3.0 118 2.7 116 2.3 116 1.9 117 1.5 121 1.1 1.3 132 1.1 149 1.2 170 0.9 160 0.7 152 0.9 0.6 150 0.6 150 0.5 150	-30 3.5 97 3.1 98 2.7 100 2.3 104 1.7 118 1.5 124 1.5 124 1.5 111 1.6 89 1.7 91 1.7 91 1.7 91 1.7 91 1.7 91 1.7 91 1.7 91 1.7 91 1.7 91 1.7 91 1.7 91 91 91 91 91 91 91 91 91 91	-20 2.2 84 1.8 101 122 1.7 138 1.6 140 1.9 100 113 2.1 98 2.0 2.1 86 2.0 86 1.6 84 1.2 80 0.7 70	-10 5.11 65 3.6 79 2.5 105 2.2 139 2.4 163 175 1.9 181 1.2 180 0.4 175 1.9 1.9 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	0 4.55 86 3.5 95 2.7 109 1127 1.9 148 163 1.6 162 0.4 113 0.7 73 0.9 67 71 1.1 68 1.2 68 1.2 62 62 62 62 62 63 64 64 64 64 64 64 64 64 64 64 64 64 64	1.4 118 1.5 138 1.54 1.66 1.66 1.7 191 1.6 209 1.3 250 0.6 300 0.6 7 7 0.6 7 7 0.6 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	1.6 2211 2.18 2.6 3.0 3.3 223 3.3 223 3.6 230 3.6 230 3.6 258 3.6 258 3.6 259 3.5 279 3.3 290 2.7 200 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7	4.8 289 4.9 275 5.255 6.2 258 7.7 2.56 8.2 257 9.2 262 10.6 10.5 274 10.6 282 10.4 291 9.9 301 10.5 312 7.9 324 6.3 7.3 5.3 5.3 5.3 5.3 5.3 5.3 5.3 5.3 5.3 5	13.68 311 12.4 311 12.1 310 12.3 306 14.4 16.0 307 19.5 307 19.6 313 19.6 313 19.6 313 19.6 313 19.6 313 313 326 337 347 358 358 358 358 358 358 358 358	11.6 307 12.2 300 13.2 294 14.6 291 16.3 291 16.3 298 22.8 304 24.3 311 25.2 27.3 350 29.6 355 29.6 355 29.6 355 29.6 355 29.6 355 29.6 355 29.6 355 29.6 355 366 367 367 367 367 367 367 367 367 367	10.2 287 11.2 283 12.4 281 15.7 282 15.0 285 5 291 18.1 299 19.6 309 21.5 319 25.2 25.1 355 345 355 367 37.3 355 38.7 1 355,7 29.99 16	6.0 334 7.7 337 7.6 340 7.6 342 8.0 343 10.1 343 14.3 343 14.3 343 14.3 343 19.3 344 22.6 352 358 359 359 359 359 359 359 359 359	5.2 296 5.1 301 5.0 4.9 5.3 343 6.1 7.9 13 9.3 11 9.3 10.0 18 9.3 11 9.3 5.5 11 9.3 15 10 10 10 10 10 10 10 10 10 10 10 10 10
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 7.0 6.5 5.0 4.5 4.0	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603 0.9237 1.52 2.51 4.14 6.83 11.25	-80 2.0 2.23 2.5 2.6 2.11 3.6 2.08 4.1 2.03 4.2 2.03 2.03 2.03 2.03 2.03 2.03 2.03 2.	-70 1.7 16 1.5 27 1.4 38 1.3 50 1.1 1.0 69 0.7 75 0.4 82 0.2 117 0.5 162 0.6 0.7 158 0.7 156 0	-60 4.0 116 3.7 116 5.4 117 5.0 118 2.5 119 2.3 121 2.0 1.6 1.7 1.6 1.7 1.7 1.6 1.7 1.7 1.6 1.7 1.7 1.6 1.7 1.7 1.6 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7	-50 2.4 89 2.3 94 2.0 100 2.00 107 1.9 11.7 123 1.4 146 1.5 1.7 146 1.5 1.7 146 1.5 1.7 146 1.6 145 1.7 146 1	-40 3.0 118 2.7 116 2.3 116 1.9 117 1.5 113 132 1.1 1.1 1.2 1.0 1.2 1.0 0.7 1.0 0.7 1.0 0.7 1.0 0.0 0.7 1.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	-30 3.5 97 3.1 98 2.7 100 2.3 104 2.0 117 118 1.5 1.5 130 1.5 111 1.6 89 1.7 1.0 84 0.7 76 84	-20 2.2 84 1.8 101 1.2 1.7 138 1.6 140 1.9 140 1.9 2.0 2.1 86 1.9 2.1 86 1.9 86 1.9 86 1.9 86 1.9 86 84 1.2	-10 5.11 65 3.6 79 2.5 105 2.2 139 2.4 139 2.4 110 1.2 180 0.4 141 1.4 79 80 1.6 80 1.5 80 1.	0 3.5 95 2.7 1.9 1.48 163 1.66 1.72 1.3 0.8 1.73 0.8 1.6 1.72 1.3 0.9 7 1.1 68 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2	1.4 118 1.5 138 1.7 154 1.8 1166 1.8 11.7 191 1.4 230 1.3 250 0.6 277 0.6 0.7 0.5 338 0.6 0.7 0.9 0.9 1.3	1.6 221 221 2.18 2.18 3.0 220 3.3 223 3.6 230 3.7 238 3.8 258 3.8 258 3.7 269 3.5 279 3.3 3.2 23 3.3 23 3.3 23 3.3 3.6 25 3.7 26 3.7 27 3.7 27 3.7 27 3.7 3.7 3.7 3.7 3.7 3.7 3.7 3.7 3.7 3.	4.8 289 4.9 275 5265 6.2 258 7.7 256 8.2 257 9.2 262 10.6 282 10.4 291 9.0 312 7.3 337 4.1 357 4.1 3 57 4.1 3 57 4.1 3 57 4.1 3 57 4.1 3 57 4.1 3 57 4.1 3 57 4.1 3 5 4 5 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	13.8 311 15.0 311 12.4 311 12.1 310 12.5 308 16.0 303 17.6 304 307 19.5 313 19.6 307 19.5 313 19.6 307 19.5 313 15.9 31 15.9 31	11.6 307 12.2 2300 14.6 291 16.3 22.8 22.8 304 24.3 311 25.2 317 26.0 324 27.3 330 28.8 353 341 28.9 346 341 28.9 346 347 348 359 348 359 348 349 349 349 349 349 349 349 349 349 349	10.2 287 11.2 283 12.4 281 13.7 282 15.0 285 16.5 291 18.1 299 19.6 309 21.5 309 21.5 309 33.0 349 33.0 39.5 350 39.5 350 39.5 350 39.5 37 29.9 9.9	8.0 334 7.7 337 7.6 340 342 8.0 343 10.1 344 12.0 343 14.3 343 14.3 343 14.3 344 22.6 8.8 352 358 358 358 358 358 358 358 358 358 358	5.2 296 5.1 301 5.0 4.9 324 5.3 343 6.3 18 10.0 18 9.7 7.7 11 9.5 2 9.5 2 9.5 12.6 10.0 12.8 10.0 12.8 10.0 12.8 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10

	nt menut i	EMPERA	TURE A	MPLITU	DE (K)	AND P	HASE	MAVE	1									
ALE		-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	50	40	50	60	70	8
12.0	0.0062	0.24	0.48	0.65	0.14	0.21	1.10	0.96	0.04	1.46	0.36	0,62	1.57	1,95	2,65	3,96	3.30 265	2,
11.5	0.0103	0.27	0.54	0.70	0.13	0.25	1.10	0.95	0.03	1.46	0.38	0,62	1.60	2.09	3.06	4.47	3,88	3,
11.0	0.0169	0.29	0.59	0.71	0.12	0.29	1.03	0.86	0.01	1.37	0.38	0,60	1,54	2.13	3.49	5.05	4.63	3,
10.5	0.0279	0.28	0.58	0.66	0.10	0.35	0.87	0.70	0.03	1.23	0.40	0.56	1.40	2,11	4,00	5.82	5,65	3,
10.0	0.0460	0.27	0.52	0.56	0.09	0,40	0.68	0.49	0.06	1.05	0.42	0.54	1,28	2.03	4,59	6,83	6.87	4
9,5	0.0758	0.25	0.41	0.40	0.08	0.41	0.45	0.28	0.06	0.83	0.44	0.52	1.16	1.85	5,09	7.84	7.96	4
9.0	0,1250	C.30	0.25	0.25	0.06	0.35	0.24	0.14	0.01	0.60	0,41	0,45	1,00	1,49	5,20	8.50	8,50	4
8,5	0.2061	0.40	0.16	0.2	0.08	0.17	0.09	0.17	0.18	0.43	0.28	0.29	0.74	0.86	4,53	8,32	8.10	4
8.0	0.3398	0.50	0.29	0.29	0.21	0.12	0.11	0.31	0.41	0.41	0.16	0.28	0.74	0.04	3,23	7.37	7.10	3
7.5	0,5603	0.34	0.35	0.27	0.34	0.29	0.13	0.35	0.45	0.37	0.34	0.47	0.98	1.03	3.00	6.26	6.37	2
7.0	0.9237	0.09	0.24	0.20	0.31	0.28	0.12	0.24	0.31	0.26	0.37	0.48	1.23	2.05	4.02	6.57	7.07	3
6.5	1,52	0.20	0.19	0,24	0.24	0.17	0.10	0.03	0.07	0.14	0.26	0.28	1.26	2.90	5,37	7.88	8.13	3
6.0	2.51	0.41	0.42	0.40	0.28	0.15	0.13	0.12	0.11	0.11	0.29	0.07	1.26	3.50	6,38	8.95	8.45	4
5,5	4.14	0.45	0.53	0.41	0.18	0.10	0.09	0.11	0.10	0.13	0.27	0.09	1.27	3.35	6.39	8.57	7.20	3
5.0	6.83	0.43	0.57	0.47	0.24	0.07	0.05	0.08	0.10	0.13	0.18	0.23	1.16	2.96	6.05	7,69	6.08	3
4.5	11.25	0.39	0.56 38	0.66	0.54	0.19	0.11	0.15	0.18	0.11	0.15	0.44	0.92	2.65	5.94	7.75	7.32	5
4.0	18,55	0,42	0.55	0.89	0.83	0,30	0.20	0.25	0.28	0,13	0.30	0,61	0.63	2.72	6,29	9,12	10.23	7
3.5	30,59	0.49 125	0.53	1.01	0.99	0,37	0.25	0.34	0,34	0.16	0.45	349 0,73 347	0.40	2,91	6.47	9.90	195	8
3.0	50.43	0.47	0.47	0.93	0.95	0.37	0.26	0.36	0.35	0.18	0.51	0.74	0.26	2.73	180	9.07	10,92	7
2.5	85,15	0.38	0,35	0.71	0.74	0.30	0.22	0.30	0.29	0.16	0.42	0.56	0.19	2.09	191	6.74	7,65	4
		145	104	61	31	341	266	266	291	307	347	345	145	175	198	215	219	
BRUA	PRESSURE	EOPOTE -80	-70	-60	-50	TUDE (-30	ND PHA	-10	AVE 1	10	20	30	40	50	60	70	
IGHT	(mb)																	
12.0		182	13	3.5	1.6	225	8.7 243	9.0 265	287	5.4 46	2.0	255	309	5.7 359	8.2 308	21.7	22.7	1
11.5		178	15	31	1.6	224	7.1 242	7.5 266	287	4.0	1.6	2.3	332	5.2 30	5.7 537	16.7 304	293	
11.0	0.0169	173	1.4	36	1.6	222	5.5 241	6.2 267	3.4 286	2.7	83	242	2.0 36	6.5	5.5	323	11.8	
10.5	0.0279	167	0.6 32	0.5 56	1.7	2.9	4.1 238	5.1 269	287	1.8	0.8 110	0.6	3.6 65	8.9 73	8.7	7.4	310	
10.0	0.0460	163	159	0.5 178	1.8	2.5	3.1 233	4.2 272	3.5 287	1.5 325	0.6 160	0.2	5.6 70	11.6	13.9 83	9.9 69	4.8 116	1
9.5	0.0758	4.4 159	1.0	1.1	1.9	2.1	2.4	3.7 274	3.6 288	1.8	0.9 203	0.9	7.3 68	14.4	20.1	18.2	15.6	1
9.0	0.1250	4.1 156	1.5	1.5	2.0	1.8	2.1	3.4 275	3.6	2.1	1.4	1.6	8.7 63	16.9 84	26.9	28.7	27.5	1
8.5	0.2061	3.6	1.6	1.6	2.0 193	1.6	2.1	3.2 274	3.5	2.2	1.9	2.0	9.5	18 _* 6 84	33.2	39.6 123	39.2	1
8.0	0.3398	3.0 163	1.5	1.6	2.0 199	1.6	2.2	2.9 270	3.2	2.0 265	2.2	2.1	9.5	19.3	37.7	49.0	49.2	3
7.5	0.5603	2.6 172	1.2	1.6	1.9	1.6	2.3	2.5 266	2.7	1.8	2.2	1.6	8.4	18.7	39.6 121	55.4 140	55.7 153	4
7.0	0.9237	2.4 177	0.9	1.5	1.9	1.7	2.2	2.1 261	2.3 265	1.6	2.1	0.9	6.8	17.4	39.6 128	58.7 148	59.6 162	4
6.5	1,52	2.5	0.7	1.3	1.7	1.8	2.2	1.9	2.1	1.5	2.0	0.4	5.3	15.7	38.7	60.0	62.4	4
6.0	2,51	2.9	0.7	0.9	1.5	1.8	2.3	1.9	2.1	1.3	1.8	0.5	4.2	14.5	38.2	61.0	66.0	4
5.5	4.14	3.6	1.4	0.4	1.1	1.8	2.3	2.1	2.1	1.1	1.4	0.5	3.4	14.0	37.4	61.4	68.6	4
5.0	6.83	4.2	2.2	0.8	1.0	1.9	2.3	2.2	2.0	0.9	1.2	0.6	3.3	13.6	165 35.7	182	68.0	
4,5	11.25	4.6	3.0	1.6	1.4	2.0	2.2	256	1.8	0.8	1.2	1.0	136	12.8	179 31.8	193	62.0	
4.0	18.55	186	3.6	2.7 199	2.4	2.3	2.0	1.9	1.5	0.6	1.5	1.7	4.2	11.1	192	44.6	206 50.4	3
	10 50	193	4.2	4.0	3.7	214	1.8	1.6	1.1	0.7	2.1	152	176	8.7	206 18.8	31.6	34.1	1
3,5	30.59										4.00							
3.0		201 4.4 209	209 4.6 217	209 5.3 216	5.2 208	3.1 199	1.5 213	1.2 226	262 0.7 242	0.9 171	157 2.8 159	158 3.8 160	185 4.5 191	6.9	12.6	18.4	17.0	1

SCALE	PRESSURE	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
HEIGHT 12.0	(mb) 0,0062	0.37	0.04	0.28	0.07	0.38	0.39	1.04	0.86	0.51	0.43	0.10	0.54	1.03	0.93	0.53	0.16	0.23
11.5	0,0103	153	188	314	297	30	59	97	79	36	114	343	293	333	354	14	79	247
		0.46	160	0,29 316 0,29	0.06	0.38	0.39	0.99	0.82	0.50	113	360	298	337	359	10	0.18	270
10.5	0.0169	139	0.05	316	325	0.34	0.36	0.85	0.72	0.48	0.51	0.13	308	346	1.01	0.73	26	0.10
		0.61	103	320	342	0.27	0.30	100	0.56	63	112	0.15	345	0.76	1.00	0.82	0.36	0.30
10.0	0,0460	146	0.11	331	0.07	0.18	62	0.35	0.37 95	0.48	110	0.22 68	60	0.70	0.99	357	0.49	0.50
9,5	0.0758	0.63 152	0.13	353	0.10	98	0.10	164	0.18	98	110	0.29	0.57	0.83	0.97	0.96 357	0,58	0.69
9.0	0.1250	165	63	0.13	0.13	152	180	252	198	113	110	95	0.81	1.07	0.93	0,90 358	0.59	0.76
8.5	0.2061	0.28	0.11	0.18	0.13	164	0.07 226	262	219	127	0.57	0.38	0.89	1,17	0.77	0.71	0.45	0.65
8.0	0.3398	270	0.12 340	0.21 67	0.12 70	161	0,10	0.28 262	0.31	0.38	0.44 124	130	0.75	1.03	0.50	0.41	0.22	0.36
7,5	0.5603	0.37 288	0.15	0.15	0.10	0.14	0.05	0.08	0.19	0.18	0.21	0.39	0.42	0.61	0.57	0.36	0,65	0,12
7.0	0.9237	0.26	0.12	0.13	0.09	0.12	0.03	0.03	0.11	0.19	0.19	203	0.69	0.98	1.41	1.72	1,58	0,65
6,5	1,52	0.13	0.07	0.12	0.08	0.11	0.06	0.03	0.10	0.18	0.24	0.46	0.95	1,12	2,11	3,56	3,13	1.46
6.0	2,51	0.16	0.11	0.11	0.06	0.06	0.07	0.01	0.08	0.11	0.26	0.60	1.06	0.88	2.58	5.11	4.73	2.36
5.5	4.14	0.11	0.16	0.16	0.03	0.03	0.10	0.07	0.02	0.02	0.20	0.50	0.78	0.46	2.33	4.72	4,46	2,48
5.0	6,83	0.06	0.22	0.22	0.09	0.11	0.16	0.15	0.13	0.09	0.09	0.35	0,34	0.04	1,54	3,23	3.15	2,06
4.5	11,25	0.11	0.28	0.29	0.16	0.21	0.22	0.23	0.24	0.21	0.06	0.27	0.33	0.38	0.46	1.23	1.44	1.09
4.0	18,55	0.17	0.30	0.32	0.22	0.29	0.28	0.28	0.32	0.30	0.21	0.44	0.78	0.60	0.79	2.17	2.73	0.33
3,5	30,59	0.21	0.30	0.32	0.24	0.32	0.30	0.29	0.35	0.34	0.31	0.62	1.16	0.68	1,50	3.71	4.62	1.65
3.0	50,43	0.20	0.25	0.27	0.22	0.29	0.28	0.27	0.33	0.33	0.35	0.67	1.17	0,61	1.73	4.03	4.73	2.03
2,5	83,15	0.15	0.17	0.19	0.16	0.23	0.22	0.21	0.26	0.25	0.28	0.55	0.93	0.45	1.46	3.21	3.50 3.50	72 1.54 73
FEBRUAR	Y MEAN	GEOPOTE	NTIAL	HEIGHT	AMPLI	TUDE	(dam) A	ND PHA	SE W	AVE 2								
SCALE HE IGHT	PRESSURE (mb)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
12.0	0.0062	5.2	2.3	3.4	2.2	3.0	3.6	5.3	4.5	6.1	6.6	0.8	1.9	8.7	11.4	12.9	13.0	7.4 316
11,5	0.0103	4.7	2.4	3.4	2.3	2.8	3.1	3.9	3.5	5.7	5.9	0.8	2.0	7.9	10.1	12.1	13.0	7.2 318
11.0	0.0169	4.2	2.4	3.4	2.4	2.7	2.7	2.6	2.6	5.2	5.2	0.8	2.2	7.2	8.8	11.1	12.9	7.1 318
10.5	0.0279	3.6	2.3	3.5	2,4	2.6	2.3	1.7	2.1	4.7	4.4	0.7	2.2	6.5	7.4	10.0	12.5	7.1 316
10.0	0.0460	3.0	2.2	3.6	2.4	2.5	2.0	1.2	1.8	4.0	3.6	0.5	2.0	5.7	6.0	8.7	12.0	7.1
9.5	0.0758	2.5	2.1	3.6	2.3	2.4	1.9	0.9	1.7	3.2	2.7	0.4	1.4	4.6	4,5	7.4	11.3	7.2
9.0	0,1250	2.3	1.9	3.5	2.2	2.3	1.8	0.9	1.5	2.4	1.9	0.6	0.5	3.3	3.2	550 6.0 348	10.5	7.5
8.5	0.2061	2.1	1.7	3,3	2.0	2.0	1.9	1.1	1.1	1.5	1.1	1.0	1.0	2.3	2.2	4.9	9.9	7.9
8.0	0.3398	1.7	1.6	3.0	1.8	1,8	1.9	1.4	0.9	0.9	0.6	1.4	291	2.5	2.1	4.1	9.6	8.2
7.5	0.5603	1.3	1,6	2.7 76	1.7	1.5	2.0	1.7	0.9	0.5	0.4	1.8	284	347	346	4.2	10.1	8.4
7.0	0.9237	1.0	1.6	2.6	1.6	1,4	1.9	112	1.1	0.6	0.4	1.9	3.0	4,3	346	5.5	11.4	8.3
6.5	1,52	0.8	1.6	2.6	1.5	1.3	106	112	117	0.8	0.2	1.9	304	5.2	6.0	9,1	13.8	7.5
6.0	2.51	0.6	1.5	2.6	1.4	1.2	1.8	112	114	1.0	0.4	1.8	328	6.2	9.5	354 15.1	338 17.6	295 6.1
5.5	4.14	0.5	1.3	2.4	103	135	109	113	112	105	36	1.8	357	7.0	17	3 22.2	354	315 5.6
5.0	6.83	0.5	1.1	2.1	104	138	1.7	112	111	102	52 0.9	1.8	3.7	7.3	16.0	9 28.0	7 26.8	351 7.0
4.5	11.25	255	67	90	102	135	111	111	112	101	58	1.6	34	7.1	17.5	12	16	20
4.0	18.55	254	68	1.3	94	0.9	109	108	0.6	102	58	1.2	37	6.6	17.3	15	22 26.6	33
3.5	30.59	245	74	0.8	1.3	1.0	100	101	126	106	0.4	44	31	18	17	18	25	37
3.0	50.43	236	227	78	66	1.3	0.6 75 0.5	80	184	177	35	0.4	2.0	12	20	25.8 22 20.4	21.0	7.6
2.5	83,15	228	236	57	53	58	31	6	247	262	313	275	315	5.4	25	27	23	13
4.2	93,13	224	237		45	47	3	327	260	0.9	0.7	1.6	292	356	12.1	15.6	8.1	345

MARCH		EMPERA		MPLITU	DE (K)	AND P	HASE	WAVE	1									
SCALE HE I GHT	PRESSURE (mb)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
12.0	0.0062	0,25 313	0.34	0.89	0.45 58	0.37 313	0.65 320	0.46	0.72	0.81	0.51	1.10	0.97	1,06	1.01	1,67	1,31	0.80
11.5	0.0103	296	0.37	0.88	0.43	310	0,63	0.40	0.72	0.82	0.47	1,07	1.01	1,23	1.33	1,89	1.49	0.73
11.0	0.0169	0.36	0.46	0.80	0.37	0.29	0.56	0.31	0.69	0.80	0.38	0.95	1.02	1.35	1.74	2.24	1,90	0.83
10.5	0.0279	0,50	0.63	0.70	0.31	0.19	0.47	0.16	0.62	0.76	0,26	0.76	1.00	1,49	2,27	2.87	2.70	1.30
10,0	0.0460	0.68	0.89	0.71	0.30	0.13	0.38	0.04	0.54	0.72	0.14	0.55	1.01	1.61	2,91	3,82	3,85	2.08
9,5	0.0758	0.87	1.16	0.91	0.43	0.22	0.37	0.23	0.41	0.70	0.16	0.43	1,05	1.73	3,57	5.03	5.20	3.05
9.0	0.1250	0.98	1.34	1,19	0.62	0.32	0.42	0.40	0.25	0.67	0.26	0.43	1.00	1.73	4,11	6.26	6.51	4.00
8.5	0,2061	0.92	1.35	1,34	0.76	0.37	0.45	0.44	0.05	0.53	0.30	0.40	0.75	1,59	4,39	7,22	7,44	4,65
8.0	0,3398	0,66 265	1,23	1,38	0.81	0.33	0.39	0.37	0.14	0.31	0.22	0.25	0.27	1,32	4,45	7,69	7,88	4.83
7,5	0.5603	0.45	1.32 314	1.34	0,73	0.20	0.24	0.19	0.25	0.07	0,14	0.24	0.36	1.28	4,43	7.26	7.32	4.14
7.0	0,9237	0.88	1.62	1,50	0.71	0.09	0.14	0.12	0.23	0.26	0.32	0.42 306	0,88	2.03	5,62	8, 16	8.18	4.60
6,5	1,52	1.31	1.95	1,74	0,86	0.17	0.12	0.15	0.17	0.29	0.34	0.44	1,36	3,49	7.62 48	10.14	9.85	5.67 45
6.0	2,51	1.56	2.25	2.04	1.14	0.33	0.16	0,17	0,13	0.22	0.27	0.51	1.96	5.10	9,44	11.80	10.93	6.29
5.5	4,14	1.49	2,32	2.19	1,29	0.39	0.17	0.16	0.15	0,19	0,26	0.67	2.32	5.23	8.79	10.23	8,71	4.67
5.0	6,83	1.22	2.07	2.15	1.34	0.39	0,18	0.16	0.17	0.18	0.26	0.80	2.31	4.48	6.77	7.24	5.23	2.00
4,5	11,25	1.02	1,61	1.94	1,30	0.30	0,21	0,19	0.21	0.17	0,29	0,88	1.89	3.11	4.91	6.18	5.08	2.25
4.0	18,55	1.14	1,28	1.68	1.21	0,17	0.25	0.24	0,26	0.15	0.33	0.90	1.23	2.17	5.86	9.13	8.98	5.32
3,5	30.59	1,29	1,17	1.41	1.07	0,04	0,26 258	0.28	0,28	0.14	0.36	0,89	0.59	2.55	7,49	11,42	11,68	7.32
3.0	50.43	1.22	1.07	1.11	0.87	0.06	0.23	0.28	0.28	0.12	0.36	0.81	0.30	2.89	7,59	11,10	11.51	7.41
2,5	83,15	0.94	0.84	0.78	0,62	0.08	0.18	0.22	0.23	0.09	0.29	0,59	0.34	2.49	6.05	8.58	8,76	5,61
			***	120	00	133	264	287	295	277	333	214	260	192	209	216	214	
MARCH	MEAN C	EOPOTE									333	,,,	200	192	209	216	214	
	MEAN G	EOPOTE			AMPLI					277 AVE 1	10	20	30	40	50	60	70	80
SCALE HE I GHT	PRESSURE (mb)	-80	NTIAL -70	HEIGHT	AMPLI -50	TUDE (dam) A -30	ND PHA	SE ¥	AVE 1	10	20	30	40	50	60	70	80
SCALE HEIGHT 12.0	PRESSURE (mb) 0.0062	-80 5.3 253	-70 0.2 284	-60 5.4 39	-50 2.4 338	TUDE (dam) A -30 5.6 232	-20 3.5 216	SE W -10	0 4.4 62	10 3.5 259	20 7.4 284	30 5.5 347	40 21.1 13	50 16.1 25	60	70 18.5 345	80 16.4 324
SCALE HEIGHT 12.0	PRESSURE (mb) 0.0062 0.0103	-80 5.3 253 5.0 249	0.2 284 0.7 302	+EIGHT -60 5.4 39 4.4 29	-50 2,4 338 2,5 323	TUDE (-40 3.6 235 3.5 227	dam) A -30 5.6 232 5.7 223	ND PHA -20 3.5 216 3.7 225	SE W -10 2.1 72 1.2 88	0 4.4 62 3.4 66	10 3.5 259 2.8 254	20 7.4 284 5.8 288	30 5.5 347 5.6 2	40 21.1 13 20.9 18	50 16.1 25 17.3 29	60 15.2 5 16.9	70 18.5 345 19.1 351	80 16.4 324 16.6 327
SCALE HEIGHT 12.0 11.5	PRESSURE (mb) 0.0062 0.0103 0.0169	-80 5.3 253 5.0 249 4.7 246	-70 0.2 284 0.7 302 1.3 315	+E1GHT -60 5.4 39 4.4 29 3.8 14	-50 2,4 338 2,5 323 2,7 310	7u0£ (-40 3.6 235 3.5 227 3.5 219	-30 5.6 232 5.7 223 5.7 214	-20 3.5 216 3.7 225 3.9 233	-10 2.1 72 1.2 88 0.6 150	AVE 1 0 4.4 62 3.4 66 2.4 73	3.5 259 2.8 254 2.2 248	20 7.4 284 5.8 288 4.5 295	30 5.5 347 5.6 2 6.2 16	21.1 13 20.9 18 20.8 23	50 16.1 25 17.3 29 18.8 34	60 15.2 5 16.9 12 18.6 20	70 18.5 345 19.1 351 19.2 358	16.4 324 16.6 327 16.3 331
SCALE HEIGHT 12.0	PRESSURE (mb) 0.0062 0.0103	-80 5.3 253 5.0 249 4.7	-70 0.2 284 0.7 302	-60 5.4 39 4.4 29 3.8	2.4 338 2.5 323 2.7 310 3.0 304	7UDE (-40 3.6 235 3.5 227 3.5 219 3.4 214	5.6 232 5.7 223 5.7 214 5.8 207	-20 3.5 216 3.7 225 3.9	-10 2.1 72 1.2 88 0.6	AVE 1 0 4.4 62 3.4 66 2.4	10 3.5 259 2.8 254 2.2 248 1.8 243	7.4 284 5.8 288 4.5 295 3.5 306	5.5 347 5.6 2 6.2 16 7.2 24	21.1 13 20.9 18 20.8 23 21.0 28	16.1 25 17.3 29 18.8 34 20.7 40	60 15.2 5 16.9 12 18.6 20 20.0 30	70 18.5 345 19.1 351 19.2 358 18.5 8	80 16.4 324 16.6 327 16.3 331 15.2 335
SCALE HEIGHT 12.0 11.5 11.0	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460	-80 5.3 253 5.0 249 4.7 246 4.1 242 3.3 239	0.2 284 0.7 302 1.3 315 1.9 329	+EIGHT -60 5.4 39 4.4 29 3.8 14 3.8 358 4.5 347	-50 2,4 338 2,5 323 2,7 310 3,0 304 3,5 303	3.6 235 3.5 227 3.5 219 3.4 214 3.3 210	5.6 232 5.7 223 5.7 214 5.8 207 5.7 200	3.5 216 3.7 225 3.9 233 4.0 237 4.1 239	2.1 72 1.2 88 0.6 150 1.2 205 1.9 218	4.4 62 3.4 66 2.4 73 1.5 86 0.8	3.5 259 2.8 254 2.2 248 1.8 243 1.5 241	20 7.4 284 5.8 288 4.5 295 3.5 306 3.0 321	30 5.5 347 5.6 2 6.2 16 7.2 24 8.6 29	21.1 13 20.9 18 20.8 23 21.0 28 21.5 36	50 16.1 25 17.3 29 18.8 34 20.7 40 23.1 48	15.2 5 16.9 12 18.6 20 20.0 30 21.5 43	70 18.5 345 19.1 351 19.2 358 18.5 8 17.3	16.4 324 16.6 327 16.3 331 15.2 335 13.0 339
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758	-80 5.3 253 5.0 249 4.7 246 4.1 242 3.3 239 2.2 234	0.2 284 0.7 302 1.3 315 1.9 329 2.9 344 4.1 357	HEIGHT -60 5.4 39 4.4 29 3.8 14 3.8 358 4.5 347 5.6 345	2.4 338 2.5 323 2.7 310 3.0 3.0 3.5 303 3.9 307	7UDE (-40 3.6 235 3.5 227 3.5 219 3.4 214 3.3 210 3.1 210	-30 5.6 232 5.7 223 5.7 214 5.8 207 5.7 200 5.5 196	ND PHA -20 3.5 216 3.7 225 3.9 233 4.0 237 4.1 239 3.9 237	2.1 72 1.2 88 0.6 150 1.2 205 1.9 218 2.6 223	4.4 62 3.4 66 2.4 73 1.5 86 0.8 119 0.8 186	10 3.5 259 2.8 254 2.2 248 1.8 243 1.5 241 1.4 247	20 7.4 284 5.8 288 4.5 295 3.5 306 321 3.1 334	30 5.5 347 5.6 2 6.2 16 7.2 24 8.6 29	21.1 13 20.9 18 20.8 23 21.0 28 21.5 34 22.3	50 16.1 25 17.3 29 18.8 34 20.7 40 23.1 48 26.1 57	15.2 5 16.9 12 18.6 20 20.0 30 21.5 43 23.4 59	70 18.5 345 19.1 351 19.2 358 18.5 8 17.3 22 16.1 45	80 16.4 16.6 327 16.3 331 15.2 339 13.0 339 9.3 343
SCALE HEIGHT 12.0 11.5 11.0 10.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250	-80 5.3 253 5.0 249 4.7 246 4.1 242 3.3 239 2.2 234 0.9 215	0.2 284 0.7 302 1.3 315 1.9 329 2.9 344 4.1 357 5.7	+EIGHT -60 5.4 39 4.4 29 3.8 14 3.8 358 4.5 347 5.6	2.4 338 2.5 325 327 310 3.0 304 3.5 303 3.9 307 4.4 316	7UDE (-40 3.6 235 3.5 227 3.5 219 3.4 214 3.3 210 2.7 214	5.6 232 5.7 223 5.7 214 5.8 207 5.7 200 5.5	ND PHA -20 3.5 216 3.7 225 3.9 233 4.0 237 4.1 239 3.9	SE W -10 2.1 72 1.2 88 0.6 150 1.2 205 1.9 218 2.6	4.4 62 3.4 66 2.4 73 1.5 86 0.8 119 0.8 186	10 3.5 259 2.8 254 2.2 248 1.8 243 1.5 241 1.4 247 1.5 257	20 7.4 284 5.8 288 4.5 295 3.5 306 3.0 321 3.1 3.4 3.6 340	5.5 347 5.6 2 6.2 16 7.2 24 8.6 29	21.1 13 20.9 18 20.8 23 21.0 28 21.5 34 22.3	50 16.1 25 17.3 29 18.8 34 20.7 40 23.1 48 26.1 57 29.6 66	15.2 5 16.9 12 18.6 20 20.0 30 21.5 43 23.4 59 26.5 76	70 18.5 345 19.1 351 19.2 358 18.5 8 17.3 22 16.1 45 16.9 75	16.4 324 16.6 327 16.3 331 15.2 335 13.0 339 9.3 343 4.3 353
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061	-80 5.3 253 5.0 249 4.7 246 4.1 242 3.3 239 2.2 234 0.9 215 0.8 100	0.2 284 0.7 302 1.3 315 1.9 329 344 4.1 357 5.7 9	HEIGHT -60 5.4 39 4.4 29 3.8 14 3.8 358 4.5 347 5.6 345 7.1 350 8.6 357	AMPLI -50 2.4 338 2.5 325 2.7 310 3.0 3.5 303 3.5 303 4.4 316 4.9 327	TUDE (-40 3.6 235 3.5 227 3.5 219 3.4 214 210 2.7 210 2.7 214 2.3 222	5.6 232 5.7 223 5.7 214 5.8 207 5.7 200 5.5 196 5.9 192 4.4	ND PHA -20 3.5 216 3.7 225 3.9 233 4.0 237 4.1 239 3.9 237 3.6 231 3.4 222	2.1 72 1.2 88 0.6 150 1.2 205 1.9 218 2.6 223 3.1 225 3.3 226	4.4 62 3.4 66 2.4 73 1.5 86 0.8 119 0.8 184 219 1.9 232	10 3.5 259 2.8 254 2.2 248 1.8 243 1.5 241 1.4 247 1.5 257	20 7.4 284 5.8 288 4.5 295 3.0 321 3.1 3.34 3.6 340 4.2 341	30 5.5 347 5.6 2 6.2 16 7.2 24 8.6 29 10.1 30 11.6 29 12.8 28	21.1 13 20.9 18 20.8 23 21.5 34 22.3 46 24.3 52	50 16.1 25 17.3 29 18.8 34 20.7 40 23.1 48 26.1 57 29.6 66 33.1	60 15.2 5 16.9 12 18.6 20 20.0 30 21.5 43 23.4 59 26.5 76 30.8	70 18.5 345 19.1 351 19.2 358 18.5 8 17.3 22 16.1 45 16.9 75 20.8	16.4 324 16.6 327 16.3 331 15.2 335 13.0 9.3 343 4.3 353 2.3 148
SCALE HE I GHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398	-80 5.3 253 5.0 249 4.7 246 4.1 242 3.3 239 2.2 234 0.9 215 0.8 100 2.0 86	0.2 284 0.7 302 1.3 315 1.9 329 2.9 344 4.1 357 5.7 9 7.3 1	-60 5.4 39 4.4 29 3.8 3.5 4.5 7.1 3.5 8.6 6.5 7.1 3.5 9.9 6	AMPL1 -50 2.4 338 2.5 323 2.7 310 304 3.5 303 3.9 307 4.4 316 4.9 327 5.4 338	3.6 235 3.5 227 3.5 219 3.4 214 3.3 210 2.7 214 2.3 22 2.0 234	5.6 232 5.7 223 5.7 214 207 5.7 200 5.5 5.0 192 4.4 191 3.7 191	-20 3.5 216 3.7 225 3.9 237 4.1 239 3.9 237 3.6 231 3.4 231 3.9 237	2.1 72 1.2 88 0.6 6 150 1.2 205 1.9 218 2.6 2.3 3.1 225 3.2 225	4.4 66 62 3.4 66 2.4 77 75 86 0.8 119 0.8 129 1.9 29 2.2 238	10 3.5 259 2.8 254 2.2 248 243 1.5 241 1.4 247 1.5 257 1.9 267 2.2 2.71	20 7.4 284 5.8 288 4.5 295 3.5 300 321 3.1 33.6 340 4.2 341	30 5.5 347 5.6 2 6.2 24 8.6 29 10.1 30 11.6 29 12.8 8.1 3.5 5.6 29	40 21.1 13 20.9 18 20.8 23 21.5 34 22.3 40 23.3 46 24.9 56	50 16.1 25 17.3 29 18.8 34 20.7 40 23.1 48 26.1 57 29.6 66 53.1 57 57 53.6 0 85	60 15.2 5 16.9 12 18.6 6 20.0 30 21.5 43 23.4 59 26.5 76 30.8 8 94	70 18.5 345 19.1 351 19.2 358 18.5 8 17.3 22 16.1 45 16.9 75 20.8 18.5 18.5 22 20.8 20.8 21.8 21.8 21.8 21.8 21.8 21.8 21.8 21	16.4 324 16.6 327 16.3 331 15.2 339 9.3 343 353 2.3 148 9.1
SCALE HE1GHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 8.0 7.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.1250 0.2061 0.3398 0.5603	-80 5.3 5.0 249 4.7 246 4.1 242 3.3 239 2.2 234 0.9 2.15 0.8 100 2.0 66 93	0.2 284 0.7 302 1.3 315 1.9 329 2.9 344 4.1 357 5.7 9 7.3 19 8.5 29 8.9	-60 5.4 39 4.4 29 3.8 14 3.8 3.5 3.5 7.1 3.5 9.9 6.6 3.5 7.1 3.5 9.9 6.6	AMPLI -50 2.4 338 2.5 323 2.7 310 3.0 304 3.5 303 3.5 307 4.4 4.9 327 5.4 338 5.7 349	TUDE (-40 3.6 235 3.5 227 3.5 227 3.4 214 3.3 3.1 210 2.7 214 2.3 222 2.0 0 234	5.6 232 5.7 214 5.8 207 5.7 200 5.5 5.0 192 4.4 190 3.7 191 3.3 193	-20 3.5 216 3.7 225 3.9 237 4.0 237 4.1 3.9 237 3.9 237 3.9 237 3.9 237 3.9 237 3.9 237 3.9 237 3.9 237 3.9 237 3.9 3.9 3.9 3.9 3.9 3.9 3.9 3.9 3.9 3.9	2.1 72 1.2 88 80 0.6 150 1.2 205 1.9 218 2.6 223 3.1 225 3.3 226 3.2 225 3.0 222	4.4 62 3.4 66 62.4 73 1.5 86 0.8 186 1.9 1.9 232 2.2 238	10 3.5 259 2.8 254 1.8 243 1.5 241 1.4 247 1.9 267 2.2 2.2 2.2 2.3 2.3 2.3 2.3 2.4 2.4 2.4 2.4 2.4 2.4 2.4 2.4 2.4 2.4	20 7.4 284 5.8 288 4.5 295 3.0 3.0 3.1 3.4 3.6 3.4 4.7 3.4 1 4.7 3.4 1 4.8	5.5 347 5.6 2 6.2 16 7.2 24 8.6 29 10.1 30 11.6 29 12.8 28 13.5 26 13.5 26 13.5 26 13.5 26 27	21.1 13 20.9 18 20.8 23 21.0 28 21.5 34 22.3 40 24.3 52 24.9 56 24.9 61	50 16.1 25 17.3 29 18.8 34 20.7 40 23.1 57 29.6 66 66 53.1 75 36.0 85 37.1 94	60 15.2 5 16.9 12 18.6 20 20.0 30 21.5 76 30.8 94 36.1 11 111 40.7 125	70 18.5 345 19.1 19.2 358 18.5 8 17.3 22 16.1 45 16.9 75 20.8 104 27.2 126 33.4	80 16.4 16.6 327 16.3 331 15.2 335 13.0 339 9.3 343 353 2.3 148 9.1 167 15.2 176
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 8.0 7.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.1250 0.2061 0.3398 0.5603 0.9237	-80 5.3 253 5.0 249 4.7 246 4.1 242 234 4.0 90 90 90 90 90 90 90 90 90 9	0.2 284 0.7 302 1.5 315 1.9 329 2.9 344 4.1 357 5.7 9 7.3 19 8.5 29 40 8.3 40 8.3 8.3 8.3 8.3 8.3 8.3 8.3 8.3 8.3 8.3	5.4 39 3.8 14 3.8 3.5 3.5 3.5 3.5 3.5 3.7 3.7 3.6 3.7 3.7 3.7 3.7 3.7 3.7 3.7 3.7 3.7 3.7	AMPLI -50 2.4 338 2.5 323 2.7 310 304 3.5 3.0 307 4.4 4.9 327 5.4 3.8 5.7 3.8 5.7 3.9 5.7 3.9 5.7 3.9 5.7 3.9 5.7 3.9 5.7 5.7 5.7 5.7 5.7 5.7 5.7 5.7 5.7 5.7	TUDE (-40 3.6 235 5.5 227 3.5 219 3.4 214 2.3 220 234 1.9 244 1.7 249	5.6 232 5.7 213 5.7 214 5.8 207 5.7 196 5.0 192 4.4 190 3.7 191 3.5 193 3.1 195	-20 3.5 216 3.7 225 3.9 237 4.1 239 237 3.9 3.9 237 3.9 3.9 3.9 3.9 3.9 3.9 3.9 3.9 3.9 3.9	2.1 72 1.2 88 0.6 150 1.9 225 3.3 226 3.2 225 3.0 222 2.8 216	4.4 62 3.4 66 62.4 73 1.5 86 186 1.4 1.9 232 2.2 239 2.1 233	10 3.5 259 2.2 248 243 1.5 241 1.4 247 1.5 257 2.2 271 2.3 269 2.1 2.3	20 7.4 284 4.5 288 4.5 3.0 3.0 3.1 3.1 3.3 4.2 3.4 4.7 3.4 4.7 3.4 4.8 3.4 4.5 3.4 4.5 3.6 4.5 3.6 3.6 3.6 3.6 3.6 3.6 3.6 3.6 3.6 3.6	30 5.5 347 5.6 2 6.2 16 8.6 29 10.1 30 11.6 29 12.8 28 13.5 26 13.5 26 12.7 29 12.7 29 13.6	21.1 133 20.9 18 20.8 23 21.5 34 22.3 40 22.3 40 24.3 52 24.9 61 23.8 65	50 16.1 25 17.3 29 18.8 34 20.7 40 25.1 48 26.1 57 36.0 85 37.1 94 35.9 36.0 37 36.0 37 37 39 40 30 40 40 40 40 40 40 40 40 40 4	60 15.2 5 16.9 12 18.6 20.0 30 30 21.5 76 30.8 94 36.1 11 40.7 125 43,4 94 43,5 11 14 40,7	70 18.5 345 19.1 351 19.2 358 8 18.5 8 17.3 22 16.1 45 10.4 27.2 20.8 104 27.2 126 33.4 143 38.7 159	80 16.4 324 16.6 327 16.3 331 15.2 339 9.3 343 4.3 323 148 9.1 167 15.2 20.7 176 20.7 186
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 8.0 7.5 7.0	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.1250 0.2061 0.3398 0.5603 0.9237 1.52	-80 5.3 253 5.0 249 4.7 246 4.1 242 3.3 259 215 0.8 6.0 86 2.0 86 2.7 112 2.9 145 2.9	0.2 284 0.7 302 1.3 302 1.3 35 1.9 329 2.9 344 4.1 357 5.7 9 9.9 8.5 29 8.5 46 6.9 71	HEIGHT -60 5.4 39 4.4 29 3.8 3.58 4.5 3.6 3.50 8.6 6.7 11 3.50 8.6 8.6 8.6 8.6 8.6 8.6 8.6 8.6 8.6 8.6	AMPLI -50 2.4 338 2.5 303 304 3.5 3.0 304 3.5 3.0 304 4.4 338 5.7 3.6 3.6 3.6 3.6 3.6 3.6 3.6 3.6 3.6 3.6	TUDE (-40 3.6 235 3.5 227 3.5 219 3.4 214 3.3 3.1 210 3.1 210 2.7 224 1.9 244 1.7 249 1.6 246	dem) A -30 5.6 232 5.7 223 5.7 220 5.5 196 6.0 192 4.4 190 3.7 191 3.3 193 3.1 195	3.5 216 3.7 225 3.9 237 4.1 239 237 3.6 221 3.2 211 3.1 2.05 3.0 201 2.8 201	2.1 72 1.2 88 0.6 6 150 1.2 205 1.9 218 2.6 223 3.1 225 3.0 222 2.8 216 2.6 2.1 211	4.4 62 3.4 666 62.4 7.1 866 0.8 86 186 1.4 219 232 2.2 238 2.2 239 2.1 233 2.2 239 223	10 3.5 259 2.8 2.54 2.2 248 1.8 243 1.5 241 1.4 247 1.9 267 2.2 271 2.3 269 2.1 262 2.1 262 2.3	20 7.4 284 4.5 3.6 3.0 3.0 3.1 3.1 3.3 4.2 2.3 4.7 3.4 4.7 3.4 4.5 3.4 4.7 3.4 4.5 3.4 4.5 3.6 3.6 3.6 3.6 3.6 3.6 3.6 3.6 3.6 3.6	5.5 5.47 5.6 2 24 8.6 6.2 24 8.6 29 10.1 30 11.6 28 13.5 26 13.5 26 12.7 29 11.3 30	40 21.1 133 20.9 16 23 21.0 28 21.5 34 22.3 40 24.3 52 24.9 56 61 23.8 65 20.8 67 20.8	50 16.1 25 17.3 29 18.8 34 20.7 40 23.1 57 29.6 66 65 35.1 75 36.0 85 37.1 94 35.9 105 96 97 105 105 105 105 105 105 105 105	60 15.2 5 16.9 12 18.6 20.0 30 21.5 43 25.4 59 94 36.1 111 40.7 125 43,5 140 45.7 157	70 18.5 345 19.1 351 19.2 358 8 17.3 22 16.1 45 20.8 10.4 27.2 126 33.4 143 38.7 159 143 38.7 159 144.9 175	80 16.4 324 16.6 327 16.3 331 15.2 13.0 339 9.3 353 353 148 9.1 167 15.2 20.7 186 27.0 196
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 8.0 7.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.9237 1.52 2.51	-80 5.3 253 5.49 4.7 246 4.1 242 2.3 2.4 2.9 2.2 2.5 4 100 2.0 86 8.0 2.6 93 2.7 1.7 2.9 9.1 9.1 9.1 9.1 9.1 9.1 9.1 9.1 9.1 9	0.2 284 0.7 302 1.3 315 1.9 329 2.9 344 1.3 57 5.7 9 7.3 29 8.9 40 8.3 4 6.9 71 5.2 95	HEIGHT60 5.4 29 4.4 29 3.8 14 3.8 3.5 3.5 3.5 3.5 6.6 3.5 7.1 10.1 2.1 2.6 8.8 8.8 4.0 7.0 7.0 5.5	AMPLI -50 2.4 338 2.5 323 3.0 3.0 3.0 3.5 3.0 3.5 3.5 3.0 3.7 4.4 3.8 3.7 5.4 3.8 5.7 7.4 9.6 9.6 9.6 9.6 9.6 9.6 9.6 9.6 9.6 9.6	TUDE (-40 3.6 235 3.5 227 3.5 5.5 227 3.4 214 213 3.1 2.0 2.7 214 2.3 2.0 2.4 1.7 249 1.6 246 1.5 234	dam) A -30 5.6 232 5.7 214 5.8 207 5.7 210 5.9 192 4.4 13.5 193 3.1 193 3.1 193 2.9 196	ND PHAME NO	2.1 1.2 88 0.6 6.150 1.2 205 3.3 1.2 225 3.3 226 222 2.8 8.2 16 2.6 211 2.5 207	4.4 62 3.4 66 2.4 73 1.5 86 6 1.4 219 1.9 232 2.2 239 2.1 1.8 8 1.9 223 1.8 8 1.9 223 1.8 8 213	10 3.5 259 2.8 254 2.2 248 1.8 243 1.4 247 1.5 257 2.2 271 1.9 269 2.1 262 2.1 263 2.2 2.2 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.	20 7.4 5.8 284 5.8 295 3.5 3.0 3.0 3.1 3.3 4.2 3.4 4.2 3.4 4.7 3.4 4.3 4.5 3.4 4.5 3.4 4.5 3.4 4.5 3.6 3.6 3.6 3.6 3.6 3.6 3.6 3.6 3.6 3.6	30 5.5 347 5.6 2 6.2 16 7.2 24 8.6 29 10.1 30 11.6 29 12.8 26 13.5 26 13.5 26 12.7 29 11.3 30 30 30 30 30 30 30 30 30 3	40 21.1 15 20.9 18 20.8 21.0 28 21.5 34 22.3 46 22.3 46 24.9 52 24.9 61 23.8 65 20.8 72 16.3 65	50 16.1 25 17.3 29 18.8 34 20.7 40 25.1 57 29.6 66 55.1 75 36.0 35.9 105 35.9 105 35.1 35.9 105 105 105 105 105 105 105 105	60 15.2 16.9 12 18.6 20 20.0 30 21.5 43 25.4 43.5 94 36.1 111 40.7 125 43.5 140 45.7 157 59 59 59 59 59 59 59 59 59 59	70 18.5 345 19.1 358 18.5 8 17.3 20.6 16.1 45 16.9 75 20.8 145 33.4 27.2 126 33.4 44.9 175 54.1 189	80 16.4 324 16.6 327 16.3 331 15.2 339 9.3 343 4.3 331 148 9.1 1167 127 127 128 20.7 186 20.7
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 8.0 7.5 7.0 6.5 6.0	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.1250 0.2061 0.3398 0.5603 0.9237 1.52 2.51 4.14	-80 5.3 253 253 249 4.7 246 4.1 242 234 0.9 215 0.8 6 2.6 93 2.7 2.7 2.9 2.9 2.9 2.9 2.9 2.9 2.9 2.9 2.9 2.9	NTIAL -70 0.2 284 0.7 302 1.3 315 1.9 344 4.1 357 5.7 9 4.0 8.3 34 6.9 9 4.0 6.9 9 4.1 135	HEIGHT60 5.4 39 4.4 29 3.8 14 3.58 4.5 3.47 5.6 3.47 7.1 3.50 8.6 6.6 10.4 17 10.1 28 8.8 8.8 8.4 6 7 7 4.6 7 7 10.1 4.7 10.1 4.7 10.1 4.7 10.1 4.7 10.1 4.7 10.1 4.7 10.1 4.7 10.1 4.8 8.8 8.8 8.7 7 10.1 4.8 8.7	AMPLI -50 2.4 3.58 2.5 3.23 3.00 3.5 3.9 3.07 4.4 3.38 5.7 3.49 5.6 6.0 10 2.3 2.6 4.4	TUDE (-40 3.6 3.5 5.5 227 3.5 5.9 219 3.4 214 3.1 210 2.7 214 2.0 2.4 1.9 244 1.6 246 1.5 234 1.5 234	dam) A -30 5.6 232 5.7 214 5.8 5.8 207 5.7 214 5.8 192 4.4 191 3.7 191 3.1 195 2.9 196 2.7 196	-20 3.5 216 3.7 225 3.9 237 4.0 237 4.1 237 3.9 237 3.9 237 3.6 222 211 205 3.0 201 2.6 200 2.3 2.6 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7	2.1 72 88 0.6 150 0.6 150 1.2 255 3.3 3.2 222 2.8 8 216 2.6 211 2.5 207 2.3 3.0 202 2.8 8 216 2.6 217 2.5 3.0 202 2.8 8 216 2.6 2.6 2.6 2.7 2.7 2.3 3.0 204	4.4 62 3.4 66 62.4 73 1.5 86 0.8 119 0.8 8186 1.4 219 232 2.2 239 1.9 233 1.9 223 1.8 213 1.8 213	10 3.5 259 2.8 254 1.8 241 1.5 247 1.5 257 7 2.2 271 2.3 262 1.7 2.3 262 1.7 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3	20 7.4 5.8 5.8 288 3.5 3.0 3.0 3.1 3.1 3.4 4.7 3.4 4.7 3.4 4.5 3.4 4.5 3.5 3.6 3.6 3.6 3.6 3.6 3.6 3.6 3.6 3.6 3.6	30 5.5 347 5.6 6.2 16 7.2 24 8.6 6.9 10.1 30 11.6 29 12.8 13.5 26 13.5 26 13.5 27 29 13.5 20 20 20 20 20 20 20 20 20 20	40 21.1 13 20.9 18 20.8 23 21.0 28 21.5 34 22.3 40 23.3 46 24.9 56 50 24.9 61 23.8 65 20.8 72 21.9 21.9 22.3 23.9 24.9 24.9 24.9 24.9 24.9 24.9 24.9 24.9 25.9 26.9 27	50 16.1 25 17.3 29 18.8 34 20.7 40 23.1 48 26.1 57 29.6 65.1 75 36.0 85 37.1 94 94 105 37.1 94 105 37.1 94 105 105 105 105 105 105 105 105	60 15.2 5 16.9 12 20.0 30 21.5 43 23.4 59 94 36.1 111 1125 43.5 140 45.7 175 175 175 175 175 175 175 17	70 18.5 345 19.1 358 18.5 8 17.3 22 16.1 45 20.8 21.2 16.9 17.5 20.8 27.2 126 43.3 38.7 159 175 20.8 44.9 45.9 46.9 46.9 46.9 46.9 46.9 46.9 46.9 46	80 16.4 324 16.6 327 16.3 331 15.2 335 13.0 9.3 343 353 148 9.1 167 20.7 186 27.0 203 203 42.6 207
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 8.0 7.5 7.0 6.5 6.0	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.1250 0.2061 0.3398 0.9237 1.52 2.51 4.14 6.83	-80 5.3 253 5.0 249 4.7 246 4.1 242 234 0.9 215 0.8 100 2.0 86 2.7 112 2.9 145 3.9 145 3.9 145 3.9 145 3.9 145 3.9 145 145 145 145 145 145 145 145 145 145	NTIAL -70 0.2 284 0.7 302 1.3 315 1.9 329 2.9 344 4.1 357 7.9 7.3 319 8.5 29 8.9 40 8.3 40 6.9 71 5.2 95 4.1 1357 7.1 717	HEIGHT -60 5.4 39 4.4 29 3.8 14 358 4.5 357 5.6 345 7.1 350 8.6 6.6 77 10.1 28 8.8 40 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.	AMPLI -50 2.4 338 2.5 523 2.7 310 304 316 4.9 327 348 5.7 349 5.6 360 10 4.0 236 444 1.7 91	TUDE (-40 3.6 235 3.5 219 3.5 219 3.1 210 3.1 210 2.7 214 2.3 2.0 2.4 1.9 244 1.6 2.5 214 1.5 234 1.5 214 1.8 8	dam) A -30 5.6 232 5.7 214 207 5.7 200 192 4.4 190 3.7 191 3.3 193 3.7 195 2.9 196 2.7 194 2.2 2.4 194	-20 3.5 216 3.7 225 3.9 233 4.1 239 3.6 237 4.1 239 237 4.1 259 257 261 262 201 2.6 201 2.6 201 2.6 201 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7	-10 2.1 72 1.2 88 0.6 150 1.9 218 2.6 223 3.3 3.1 225 3.2 25 3.0 222 2.2 25 2.0 202 2.2 200	4.4 66 2.4 73 1.5 66 119 0.8 119 232 2.2 239 1.233 1.8 213 1.7 203 1.6 194	10 3.5 259 2.8 2.2 248 243 1.5 241 1.4 247 7.5 257 2.2 271 2.3 269 2.3 262 1.7 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3	20 7.4 284 5.8 288 4.5 295 3.0 3.0 3.1 3.1 3.4 4.7 341 4.8 344 4.0 353 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5	30 5.5 347 5.6 2 6.2 16 29 10.1 29 11.6 29 12.8 28 13.5 26 15.5 26 15.5 26 16.5 26 16.5 26 16.5 26 16.5 26 16.5 26 26 26 26 26 26 26 26 26 26	40 21.1 13 20.9 18 20.8 23 21.5 34 22.3 46 23.3 46 24.3 52 24.9 61 82.6 72 16.3 86 72 16.3 86 17.0 18.3 19.6 19	50 16.1 25 17.3 29 18.8 34 20.7 40 23.1 48 26.1 75 36.0 85 37.1 94 95 105 32.7 121 30.4 143 34.7 155 168 168 175 175 175 175 175 175 175 175	60 15.2 5 16.9 12 18.6 20.0 20.0 30 21.5 43 25.4 50.8 94 36.1 111 40.7 125 43,4 111 40.7 125 140 157 157 157 157 157 157 157 157	70 18.5 345 19.1 19.2 358 18.5 8 17.3 22 16.1 16.9 75 20.8 104 14.3 33.4 14.3 33.4 14.3 159 175 54.1 175 175 175 175 175 175 175 175 175 17	80 16.4 324 16.6 327 16.3 331 15.2 339 9.3 343 353 2.3 343 353 2.3 148 9.1 167 178 186 27.0 196 27.0 196 27.0 196 27.0 27.
SCALE HE1GHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 8.0 7.5 7.0 6.5 6.0 5.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603 0.9237 1.52 2.51 4.14 6.83	-80 5.3 5.0 249 4.7 246 4.1 242 3.3 3.2 234 0.8 6.8 100 2.0 86 2.6 93 7.112 2.9 145 3.9 17 5.5 197 7.5 222	0.2 284 0.7 302 1.3 315 1.3 315 2.9 329 2.9 344 4.1 337 5.7 9 7 9 8.5 29 8.9 40 40 6.9 9 71 5.2 9 4.1 135 6.9 40 6.9 71 77 6.0 00	-60 5.4 39 4.4 29 3.8 14 358 4.5 358 4.5 357 7.1 350 6.6 357 10.4 7.0 10.1 28 8.8 8.8 8.8 10.9 10.9 10.9 10.9 10.9 10.9 10.9 10.9	AMPLI -50 2.4 338 2.5 323 2.7 310 304 3.5 303 3.9 307 4.4 316 368 5.7 349 327 5.4 4.6 368 6.6 464 4.7 91 2.1 152	TUDE (-40 3.6 235 3.5 217 3.5 217 3.1 210 2.7 214 3.3 222 2.0 234 1.9 246 1.5 246 1.5 214 1.5 214 1.7 249 1.5 214 1.7 249 1.7 249 1.5 214 1.7 249 1.	dam) A -30 5.6 232 5.7 223 5.7 214 8 207 5.5 5 192 4 190 3.7 191 3.3 3.1 195 2.7 196 2.4 194 2.2 192 2.0 186	-20 3.5 216 3.7 225 3.9 233 4.1 239 3.9 237 4.1 239 3.9 237 3.6 231 3.1 3.1 3.1 3.1 3.1 3.1 3.1 3.1 3.1 3.1	-10 2.1 72 1.2 88 0.6 150 0.5 1.9 2.18 2.6 223 3.1 225 3.22 2.8 216 2.6 2.11 2.5 207 2.3 204 2.1 13	4.4 62 3.4 66 62.4 73 5 86 60.8 819 0.8 82 2.2 239 2.1 233 1.8 2.2 2.1 233 1.6 194 1.6 61 1.4	10 3.5 259 2.8 8 254 2.2 248 243 1.5 241 1.4 257 7 1.5 257 2.2 271 2.3 269 2.1 262 1.1 262 1.1 253 1.4 20.9 212 0.9 212	20 7.4 284 5.8 288 4.5 306 3.0 3.1 3.1 3.1 3.1 3.1 3.1 3.1 3.1 4.8 3.1 4.7 3.1 4.7 3.1 4.7 3.1 4.7 3.1 4.7 3.1 4.7 3.1 4.7 3.1 4.7 3.1 4.7 3.1 4.7 3.7 4.7 3.7 4.7 3.7 4.7 4.7 4.7 4.7 4.7 4.7 4.7 4.7 4.7 4	30 5.5 347 5.6 2 6.2 24 8.6 29 10.1 28 13.5 26 12.7 29 10.3 11.6 29 11.6 29 11.6 29 10.1 36 29 10.1 36 29 10.1 36 36 36 36 36 36 36 36 36 36	40 21.1 20.9 18 20.8 21.0 28 21.5 34 46 22.3 46 65 24.9 56 24.9 56 24.9 61 23.8 65 20.8 65 10.6 11.0	50 16.1 25 17.3 29 18.8 34 23.1 48 26.1 75 36.0 85 37.1 121 30.4 43 35.9 105 37.1 121 30.4 48 35.9 105 105 105 105 105 105 105 105	15.2 5 16.9 12 18.6 20 20.0 30 21.5 76 43 25.4 40.7 71.25 140 45.7 1.57 50.5 57.5 57.5 191 62.5 202 61.2 210	70 18.5 345 19.1 19.2 358 18.5 18.5 16.1 4.7 27.2 126 104 27.2 126 33.4 143 38.7 159 44.9 175 54.1 189 64.0 200 69.9 207 68.5 212	80 16.4 324 16.6 327 16.3 331 15.2 339 9.3 343 4.3 393 148 9.1 167 17 186 20.7 186 21.0 21.0 21.0 21.0 42.6 21.0 42.6 21.0 46.7 47.0
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 7.0 6.5 6.0 5.5 5.0 4.5 4.0	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.1250 0.2061 0.3398 0.5603 0.9237 1.52 2.51 4.14 6.83 11.25 18.55	-80 5.3 253 5.0 249 4.7 246 4.1 242 3.3 239 0.9 2.7 215 0.8 6.8 2.6 2.6 3 2.7 1.7 6.8 211 7.5 222 7.5 234	0.2 284 0.7 302 1.5 315 1.5 315 2.9 329 2.9 344 4.1 35 5.7 9 8.5 29 8.9 71 5.2 95 4.1 15 15.2 95 4.1 17 7.7 177 6.8 6.8 6.20	-60 5.4 39 4.4 29 3.8 144 39 3.8 144 358 358 6.6 357 7.1 350 6.6 357 7.1 10.1 28 8.8 40 7.0 3.5 119 19 19 19 19 19	AMPLI -50 2.4 338 2.5 323 2.7 310 30.4 3.5 3.9 30.7 4.4 316 4.9 327 5.4 4.9 5.6 360 10 4.0 23 2.6 4.4 1.7 91 1152 3.3	TUDE (-40 3.6 235 3.5 227 3.5 227 3.5 219 3.1 210 2.7 214 3.3 222 2.0 0 2.4 1.7 249 1.6 246 2.5 24 1.7 249 1.6 1.5 214 1.8 1.9 2.2 2187 2.7 2.9 2.9 2.9 2.9 2.9 2.9 2.9 2.9 2.9 2.9	dam) A -30 5.6 232 5.7 223 5.7 223 5.7 214 8 207 5.5 5.7 210 190 3.7 191 3.3 3.1 195 3.1 195 2.7 196 2.7 196 2.2 192 2.2 192 2.2 192 2.2 192 2.2 192	-20 3.5 216 3.7 225 3.9 233 4.1 239 3.9 237 3.6 231 3.1 222 3.2 211 3.1 201 2.6 200 2.3 3.9 2.1 196 2.0 199 1.9 181	-10 2.1 72 1.2 88 0.6 150 0.6 150 1.2 205 1.9 218 2.6 3.3 3.1 225 3.0 222 2.8 216 2.6 211 2.5 207 2.3 304 2.2 200 2.1 193 2.0 183	4.4 62 3.4 66 6.8 1.5 86 6.8 1.9 2.32 2.2 2.38 2.2 2.31 1.6 1.8 1.6 1.4 1.6 1.6 1.4 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6	10 3.5 259 2.8 8 254 2.2 248 243 1.4 247 1.5 257 2.2 271 2.3 269 2.1 262 2.1 262 2.1 262 2.1 262 2.1 271 2.2 271 2.2 271 2.3 3.6 272 2.1 262 2.1 272 2.1 272 2	20 7.4 5.6 5.6 288 4.5 295 3.5 3.6 3.0 3.0 3.1 3.4 4.2 3.4 4.5 3.4 4.5 3.5 3.5 4.0 3.5 3.5 3.6 3.6 3.6 3.6 3.6 3.6 3.6 3.6 3.6 3.6	5.5 3.47 5.66 2 6.2 24 8.66 29 10.11 30 11.66 28 13.5 26 13.5 26 12.7 29 9.0 36 11.3 5.2 9.0 11.3	40 21.1 13 20.9 18 20.8 21.5 34 21.5 34 22.3 36 24.3 52 24.9 61 12.0 61 12.0 61 12.0 11	50 16.1 25 17.3 29 18.8 34.7 40 25.1 48 26.1 75 56.0 85 37.1 54 35.9 105 30.4 1188 34.7 120 130 148 35 36 37 105 105 105 105 105 105 105 105	15.2 5 16.9 12 20.0 30 21.5 43 25.4 111 40.7 125 43.5 140 65.7 157 57.5 191 62.5 20.2 210 52.7 217	70 18.5 345 19.1 19.2 358 8 17.3 22 16.1 16.9 75 20.8 104 27.2 20.8 133.4 143 38.7 159 149 175 54.1 189 64.0 69.9 207 69.9 207 208 208 208 208 208 208 208 208 208 208	80 16.4 324 16.6 327 16.3 331 15.2 339 339 339 343 4.3 353 148 9.1 1167 127 120 127 120 127 120 120 121 121 121 121 121 121
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 7.0 6.5 5.0 4.5 4.0 3.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.1250 0.2061 0.3398 0.5603 0.9237 1.52 2.51 4.14 6.83 11.25 18.55 30.59	-80 5.3 5.0 249 7.246 4.1 242 3.3 239 0.9 86 6.9 86 6.9 7.1 12 2.9 176 6.8 2.1 7.5 2.2 2.4 7.1 7.5 2.3 7.1 247	NTIAL -70 0.2 284 0.7 302 1.3 315 1.9 329 2.9 34 4.1 357 5.7 9 7.3 19 8.5 52 9.9 40 8.3 35 4.7 17 6.0 0 203 6.8 8 220 7.0 0	HEIGHT60 5.4 39 4.4 29 3.8 14 3.58 4.5 3.57 5.6 3.57 7.1 3.50 8.6 6.6 7.7 10.11 28 8.8 4.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7	AMPLI -50 2.4 338 2.5 338 2.7 310 3.0 3.9 307 4.4 316 4.9 327 5.4 358 5.7 349 5.6 6.0 10 4.0 23 2.6 4.4 1.7 91 2.1 1.52 2.1 1.52 2.3 3.83 4.52 2.00	TUDE (-40 3.6 235 3.5 227 3.5 219 3.1 210 3.1 210 2.7 214 2.3 2.0 2.4 1.7 249 1.6 2.4 1.7 249 1.6 1.5 234 1.8 1.8 1.8 1.8 1.8 1.8 1.8 1.8 1.8 1.8	dam) A -30 5.6 232 5.7 214 5.8 207 5.5 196 6.9 192 4.4 190 3.7 191 3.3 193 3.11 195 2.9 196 2.7 196 192 2.0 186 1.9 1.8	-20 3.5 216 3.7 225 3.9 233 4.0 237 4.1 237 3.9 237 3.6 231 3.4 202 211 205 3.0 201 2.6 200 2.3 199 2.1 190 190 190 191 191 191 190 190 190 19	-10 2.1 72 1.2 8 0.6 150 0.5 1.9 2.5 205 1.9 2.6 223 3.3 3.1 225 3.2 225 2.8 8 2.1 225 2.0 222 2.8 8 2.1 211 2.5 207 2.1 1933 2.0 183 2.1 173	4.4 66 62.4 73 1.5 86 119 0.8 119 1.9 232 2.2 239 223 1.9 223 1.6 12 13 1.6 184 1.6 175 1.6 175 1.7 167	10 3.59 2.88 2.54 2.2 2.48 1.5 2.57 1.5 2.57 2.2 2.71 2.3 2.69 2.1 2.7 2.62 2.7 2.7 2.2 2.7 2.2 2.2 2.3 2.6 2.2 2.1 2.3 2.6 2.3 2.6 2.6 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7	20 7.4 4.5 5.8 8.285 3.5 5.5 3.0 3.1 3.1 3.4 4.2 3.4 4.2 3.4 4.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5	30 5.5 6.2 16.2 24 8.6 6.2 91 10.1 30 12.8 13.5 26 15.5	40 21.1 13 20.9 18 21.0 28 21.5 34 40 22.3 40 23.3 46 24.9 61 25.8 65 24.9 61 25.8 72 16.3 86 67 11.2 10.6 11.2 10.6 11.2 10.6 11.2 10.6	50 16.1 25 17.3 29 18.8 34 20.7 40 23.1 57 56.0 66 53.1 54 55.9 105 30.4 143 31.5 168 34.1 35.1 36.0 30.4 143 36.0 36	60 15.2 5 16.9 12 18.6 20 20.0 30 21.5 43 23.4 59 94 36.1 111 111 140.7 125 140.7 157 157 157 157 157 157 157 15	70 18.5 345 19.1 358 18.5 8 17.3 22 16.1 45 20.8 16.9 17.5 20.8 16.9 17.5 20.8 16.9 17.5 20.8 16.9 17.5 20.8 16.9 17.5 20.8 27.2 16.9 17.5 20.8 27.2 16.9 17.5 20.8 27.2 16.9 17.5 20.8 27.2 16.9 17.5 20.8	80 16.4 324 16.5 327 16.3 331 15.2 339 9.3 343 353 2.3 343 363 20.7 186 20.7 186 20.7 186 20.7 186 20.7 47.1 210 46.7 214 32.1 41.4 214 32.1 41.4 214
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 7.0 6.5 6.0 5.5 5.0 4.5 4.0	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.1250 0.2061 0.3398 0.5603 0.9237 1.52 2.51 4.14 6.83 11.25 18.55	-80 5.3 5.0 249 246 4.1 242 3.3 2.2 234 0.8 100 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2	NTIAL -70 0.2 284 0.7 302 1.3 315 1.9 329 2.9 344 4.1 357 7.9 7.3 319 8.5 29 8.9 40 8.9 40 6.9 71 5.2 95 4.1 135 6.8 220 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0	HEIGHT -60 5.4 39 4.4 29 3.8 14 358 4.5 357 5.6 345 7.1 350 8.6 6.7 10.1 28 8.8 40 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.	AMPLI -50 2.4 338 2.5 323 2.7 310 304 3.5 3.9 307 3.4 316 4.9 327 3.4 36 360 300 10 4.0 2.1 1.7 91 2.1 1.52 3.3	TUDE (-40 3.6 235 3.5 219 3.5 217 3.7 214 2.1 3.3 2.7 214 2.5 2.0 2.4 1.9 2.4 1.6 2.5 2.1 1.9 2.7 2.1 2.9 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0	dam) A -30 5.6 232 5.7 214 5.7 214 5.7 200 5.5 196 6.7 191 3.5 193 3.7 191 3.5 193 2.9 196 2.4 194 2.2 2.0 186 1.9 177 1.8	-20 3.5 216 3.7 225 3.9 233 4.1 239 2.37 4.1 239 2.37 4.1 239 2.37 2.1 205 2.1 2.6 200 2.1 1.6 200 2.1 1.6 200 2.1 1.6 200 2.1 1.6 200 2.1 1.6 200 2.1 1.6 200 2.1 1.6 200 2.1 1.6 200 2.1 1.6 200 2.1 1.6 200 2.1 1.6 200 2.1 1.6 200 2.1 1.6 200 2.1 1.6 200 2.1 1.6 200 2.1 1.6 200 2.1 1.6 200 2.1 1.6 200 2.1 1.6 200 2.1 2.6 200 2.0	-10 2.1 72 1.2 88 0.6 150 1.9 218 2.6 225 3.2 25 3.2 26 2.2 25 3.0 222 2.2 25 2.0 4 2.1 2.5 7 2.0 4 2.1 2.5 7 2.3 204 2.1 1 2.5 7 2.3 204 2.1 1 2.5 7 2.3 204 2.2 200 2.1 1 2.3 204 2.2 200 2.1 1 2.3 204 2.2 200 2.1 1 2.3 204 2.2 200 2.1 1 2.3 204 2.2 200 2.1 1 2.3 204 2.2 200 2.1 1 2.3 204 2.2 200 2.1 1 2.3 204 2.2 200 2.1 1 2.3 204 2.2 200 2.1 1 2.3 204 2.2 200 2.1 1 2.3 204 2.2 200 2.3	AVE 1 0 4.4 62 3.4 66 2.4 73 1.8 66 0.8 119 0.8 119 0.8 22 2.2 239 1.4 219 2.2 238 2.2 238 2.3 1.9 233 1.9 233 1.9 1.6 1.7 203 1.6 1.8 1.7 203 1.6 1.8 1.7 203 1.6 1.8 1.7 1.7 203	10 3.5 259 2.8 254 2.2 248 243 1.5 241 1.4 247 7.57 2.2 271 2.3 269 2.6 27 2.7 2.3 269 2.1 27 2.2 27 2.3 269 2.1 27 2.2 27 2.2 27 2.3 269 2.4 242 2.7 253 2.6 27 2.7 253 2.7 253 2.7 253 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7	20 7.44 5.88 4.5 295 3.06 3.0 3.1 3.1 3.4 3.4 4.7 3.4 1 4.8 3.4 4.0 3.5 3.5 3.6 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0	30 5.5 347 5.6 2 6.2 16.2 24 8.6 6.2 9 10.1 13.5 26 16 16 16 16 16 16 16 16 16 1	40 21.1 20.9 18 20.8 23 21.5 34 22.3 46 23.3 46 24.3 52 24.9 61 12.0 11.2 10.6 12.0 11.2 11.4 196 9.6	50 16.1 25 17.3 29 18.8 34 20.7 40 23.1 48 26.1 75 36.0 85 37.1 94 35.9 105 31.5 168 34.7 20	60 15.2 5 16.9 12 18.6 20.0 30 30 21.5 43 25.4 30.8 94 36.1 111 40.7 125 43 45.7 157 50.7 50	70 18.5 345 19.1 19.2 358 18.5 8 17.3 22 16.1 16.9 75 20.8 104 143 33.4 143 33.4 143 344.9 175 54.1 175 55 54.1 175 54.1	80 16.4 324 16.6 327 16.3 331 15.2 339 9.3 339 9.3 353 323 343 353 323 343 353 321 166 176 176 176 176 176 176 17

SMALE PRESENTAL	MARCH	MEAN	TEMPERA	THE !	AMDI (TII	ne (x)	AND D	WASE	WAVE	,	OF	P	OR	Q	UAL	IT)	1		
1. 1. 1. 1. 1. 1. 1. 1.	SCALE										0	10	20	30	40	50	60	70	80
11.5			0.02	0.20	0.09	0.36	0.49	1.02	0.66	0.60	0.67	0.51	0.50	0.14	0.38	0.67	1.09	0.46	0.23
11.0			63	159	117	123	101	76	93	98	118	141	145	90	30	30	31	24	187
10.5 0.0279 0.18 0.19 0.219			107	161	131	123	98	76	92	96	118	139	142	102	32	33	33	22	178
154 159 159 159 157 158 159 159 158 159			124	163	145	125	99	76	90	93	119	137	139	113	35	39	37	20	172
1.5			134	169	165	127	98	76	87	87	118	135	135	127	42	50	44	18	159
1. 1. 1. 1. 1. 1. 1. 1.				185		128	97	75					128		55	75	58	16	
18			139	224	187	130	95	68	21	32	119	106	120	142			91	19	136
150 287 298 298 298 298 298 297 298 509 10 69 145 176 215 206 196 112 197 198 198 297 298 298 627 74 279 290 295 235 315 552 42 56 199 225 225 181 101 177			138	268	197	130	92	276	313	323	124	57	108	146	133	183	166	34	124
7.5 0.5603 0.12 0.17 0.25 0.17 0.07 0.18 0.06 0.25 0.21 0.15 0.35 0.35 0.22 0.18 10 10 74 255 255 234 307 315 527 319 223 256 229 165 69 70 70 0.9237 0.12 0.11 0.15 0.15 0.15 0.15 0.15 0.15 0.15			135	287	214	123	86	271	297	281	309	10	89	143	176	215	206	156	112
7.0 0,9237 0,12 0,11 0,15 0,21 0,02 0,06 0,06 0,11 0,10 0,10 0,10 0,10 0,10			97	293	288	62	74	275	290	250	315	352	42	56	199	235	223	181	101
1,50			355	318	8	10	74	285	285	234	307	315	327	319	223	256	229	165	89
160 98 41 24 118 99 202 266 279 267 274 249 155 126 150 150 99			340	3	27	14	99	56	280	240	294	279	291	301	198	200	174	138	90
5.5 6.15 0.29 0.11 0.17 0.05 0.05 0.13 0.10 100 103 129 210 270 270 170 118 123 129 129 98 5.7 6.85 0.16 0.16 0.17 0.07 0.04 0.11 0.17 0.07 0.08 0.07 0.08 0.07 0.09 0.08 0.07 0.08 0.08			196	58	41	24	118	98	202	266	279	267	274	249	135	124	130	130	98
Second S				108	60	33	108	108	143	276	277		270		118		129	132	98
## ## ## ## ## ## ## ## ## ## ## ## ##						17	84	104		145	267		269	124			143		
18.59 197 209 227 313 592 114 116 117 166 81 59 118 195 204 200 171			180	180	201	242	346	98	122	121	162	233	270	83	119	145	165	168	127
3.5 30.59 0.60 0.77 0.65 0.51 0.15 0.15 0.50 0.60 110 113 109 116 68 44 299 277 240 230 210 320 30.5 30.59 0.61 0.77 0.65 0.55 27 0.55 0.56 2.78 2.75 0.56 3.0 315 215 215 220 300 68 106 112 107 101 87 55 288 274 259 230 228 3.0 50.43 30.03 0.14 0.38 0.29 0.14 0.36 0.25 0.35 0.25 0.26 0.27 0.26 0.41 0.35 1.27 0.26 22 22 2.2 3 3.0 50.43 30.03 0.04 0.28 0.25 0.25 0.26 0.27 0.26 0.27 0.26 0.26 0.27 0.26 0.26 0.27 0.26 0.26 0.27 0.26 0.26 0.27 0.26 0.26 0.27 0.26 0.26 0.27 0.26 0.26 0.27 0.26 0.26 0.27 0.26 0.26 0.27 0.26 0.26 0.27 0.26 0.26 0.27 0.26 0.26 0.27 0.26 0.26 0.26 0.27 0.26 0.26 0.27 0.26 0.26 0.26 0.26 0.26 0.27 0.26 0.26 0.26 0.26 0.26 0.26 0.27 0.26 0.26 0.26 0.26 0.26 0.26 0.26 0.26			185	197	209	227	313	92	114	116	117	166	81	59	118	195	204	200	171
3.0 50.43 0.03 0.14 0.38 0.29 0.14 0.00 0.28 0.25 0.26 0.20 0.27 0.26 0.41 0.35 1.42 2.78 2.29 1.04 0.62 2.25 0.30 0.00 0.28 0.28 0.27 0.26 0.20 0.27 0.26 0.41 0.35 1.42 2.78 2.27 1.64 0.62 2.25 0.35 0.20 0.00 0.28 0.21 0.10 0.00 0.28 0.21 0.10 0.00 0.28 0.21 0.10 0.00 0.28 0.21 0.10 0.00 0.28 0.21 0.10 0.00 0.28 0.21 0.10 0.00 0.28 0.21 0.10 0.00 0.28 0.25 0.25 0.25 0.25 0.25 0.25 0.25 0.25			194	208	211	224	306	80	110	113	109	116	85	44	299	257	240	230	210
2.5 83.15 0.06 0.09 0.28 0.25 0.210 0.20 0.37 0.22 0.22 0.22 0.22 0.34 0.28 0.28 0.28 0.29 1.90 1.77 1.20 0.50 0.20 0.35 0.28 0.28 0.27 1.26 0.50 0.20 0.35 0.28 0.28 0.27 1.26 0.50 0.20 0.35 0.28 0.28 0.27 1.26 0.50 0.20 0.35 0.28 0.28 0.27 1.26 0.50 0.20 0.20 0.35 0.28 0.28 0.27 1.26 0.50 0.20 0.20 0.20 0.20 0.20 0.20 0.20			315	215	213	220	302	68	106	112	107	101	87	35	298	274	259	250	228
MARCH MEAN GEOPOTENTIAL HEIGHT AMPLITUDE (dam) AND PHASE WAVE 2 SCALE PRESSURE -80 -70 -60 -50 -40 -30 -20 -10 0 10 20 30 40 50 60 70 80 12.0 0.0062 4.2 3.9 4.6 5.2 6.1 4.9 2.8 2.2 2.5 1.9 5.2 3.6 7.0 8.0 9.9 10.2 8.0 12.0 0.0062 4.2 3.9 4.6 5.2 6.1 4.9 2.8 2.2 2.5 1.9 5.2 3.6 7.0 8.0 9.9 10.2 8.0 11.5 0.0103 4.2 5.6 4.6 4.7 5.3 5.5 1.9 1.4 1.6 1.1 2.6 3.4 6.6 7.6 8.8 9.6 8.0 5.7 7.9 11.0 0.0169 4.1 5.5 4.6 4.6 4.7 5.3 5.5 1.9 1.4 1.6 1.1 2.6 3.4 6.6 7.6 7.6 8.8 9.6 8.0 5.7 7.9 11.0 0.0169 4.1 5.3 4.6 4.1 4.5 2.1 1.1 0.6 0.6 0.9 0.4 1.9 3.1 6.1 6. 8 6 8 0 0 5.7 7.9 11.0 0.0169 4.1 5.3 4.6 4.1 4.5 2.1 1.1 0.0 0.7 0.0 0.4 0.2 1.3 2.9 6 0.0 6.8 6.8 6.6 7.6 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0			342	218	213	220	300	68	103	112	107	97	86	29	298	111	269	262	237
SCALE PRESSURE -80 -70 -60 -50 -40 -30 -20 -10 0 10 20 30 40 50 60 70 80 12.0 0.0062 4.2 3.9 4.8 5.2 6.1 4.9 2.8 2.2 2.3 1.9 3.2 3.6 7.0 8.0 9.9 10.2 8.0 11.5 0.0103 4.2 3.6 4.6 4.7 7.3 3.5 1.9 1.4 1.6 1.1 2.6 3.4 6.5 7.6 8.8 9.9 6.0 135 151 144 122 91 68 68 91 123 135 116 18 68 68 98 60 57 70 11.0 0.0169 4.1 3.3 4.4 4.1 4.6 2.1 1.1 0.6 0.0 0.4 1.9 3.1 6.3 7.2 7.7 9.0 8.1 10.5 0.0279 5.9 3.0 4.2 3.5 8.4 4.1 120 88 47 13 329 157 333 90 74 94 111 97 66 73 10.6 0.0460 3.5 2.9 4.0 2.9 3.2 0.5 0.7 0.5 0.3 0.6 0.9 2.7 1.5 6.6 6.6 6.9 9.5 10.0 0.0460 3.5 2.9 4.0 2.9 3.2 0.5 0.7 0.5 0.3 0.6 0.9 2.7 1.5 6.6 5.6 6.1 8.0 6.0 9.9 9.5 0.0758 3.0 2.2 8 3.7 2.3 2.5 0.5 0.7 0.5 0.3 0.6 0.9 2.7 1.5 6.6 5.4 6.1 1.0 7.0 6.6 6.9 9.5 136 144 135 13 117 62 312 312 255 277 311 21 57 100 116 110 70 6.0 6.6 6.9 9.0 0.1 136 144 138 117 62 312 312 255 277 311 21 57 100 116 110 70 6.5 136 144 135 115 79 0.9 0.3 0.4 0.8 0.7 0.6 0.9 0.9 0.6 0.9 0.9 0.6 0.5 0.8 0.9 0.7 0.6 6.6 6.9 9.5 0.0 0.4 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.1 100 70 6.0 6.6 6.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0	2.5	83,15	353			219							87			284	275		
HEIGHT (mb) 12.0 0,0062	MARCH	MEAN	GEOPOTE	NTIAL	HEIGHT	AMPLI	TUDE (dam) A	ND PHA	SE W	AVE 2								
11,5 0,0103			-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
11,5 0,0103	12.0	0.0062							2.8						7.0		9.9		
11,0 0,0169	11,5	0,0103	4.2	3,6	4,6	4.7	5.3	3,5	1.9	1.4	1.6	1.1	2.6	3.4	6.6	7,6	8.8	9,6	8.0
10.5 0.0279	11,0	0.0169	4.1	3.3	4.4	4.1	4.6	2.1	1.1	0.6	0.9	0.4	1.9		6.3	7.2	7.7	9.0	8.1
10.0 0.0460	10,5	0.0279	3.9	3.0	4.2	3.5	3.9	1.0	0.7	0.0	0.4	0.2	1.3		6.0	6.8	6.8	8.4	8.1
9.5 0.0758	10.0	0.0460	3.5	2.9	4.0	2.9	3.2	0.5	0.7	0.5	0.3	0.6	0.9	2.7	5.6	6.5	6.1	8.0	8.0
9.0 0.1250	9,5	0.0758	3.0	2.8	3.7	2.3	2.5	0.6	0.8	0.7	0.6	0.9	0.9	2.6	5.4	6.1	5.5	7.6	7.9
8.5 0.2061	9.0	0.1250	2.5	2.8	3,5	1.9		0.5	0.6	0.8	0.8	1.0	1.0	2.6	5,1	5.8	5.1		7.6
6.0 0.3398	8,5	0.2061	2.0	3.0	3,4	1.5	1.4	0.3	0.1	0.6	0.8	1.0	1.2	2.7	4,9	5.9	5.1		7.2
7.5 0.5603	8.0	0.3398	1.7	3,3	3.4	1.3		0.5	0.4	0.5	0.7	1.0	1.3	2.7	5.0	6.5	6.0	7.4	6.8
7.0 0.9237	7,5	0,5603									0.6			-	5.4			7.6	6.4
6.5 1.52 2.0 3.8 5.8 1.5 0.8 0.8 0.8 1.3 0.6 0.1 0.4 0.7 2.8 5.7 7.8 7.9 7.3 5.8 1.3 138 139 138 68 75 106 93 349 262 342 47 76 85 61 49 43 43 65 6.0 2.51 1.9 3.7 3.8 1.6 0.7 0.6 1.2 0.7 0.2 0.0 0.7 2.9 5.0 5.9 7.3 7.3 5.4 6.0 2.51 1.9 3.7 3.6 3.8 1.6 0.6 66 105 93 61 254 24 46 66 70 40 32 36 5.5 1.1 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2	7.0	0.9237	1.9	3.8	3.7	1.4		0.9	1.2	0.4	0.3	0.7	0.9	2.7	5.8	8.4			6.1
6.0 2.51 1,9 3.7 3.8 1.6 0.7 0.6 1.2 0.7 0.2 0.0 0.7 2.9 5.0 5.9 7.3 7.3 5.4 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	6.5	1,52		3.8	3.8	1.5	0.8		1.5	0.6	0.1	0.4	0.7	2.8		7.8	7.9	7.3	5.8
5.5 4.14 1.7 3.6 3.8 1.7 0.6 0.5 1.1 0.7 0.4 0.3 1.0 3.0 4.2 5.0 8.4 8.5 5.1 134 140 145 150 54 51 98 92 71 75 49 43 47 35 16 15 26 5.0 6.83 1.5 3.4 3.7 1.7 0.6 0.4 0.9 0.7 0.5 0.5 1.2 2.9 4.0 6.2 10.9 10.5 5.2 126 139 144 149 55 33 91 87 68 70 58 59 26 6.2 10.9 10.5 5.2 126 139 144 149 55 33 91 87 68 70 58 59 26 6.2 10.9 10.5 5.2 120 136 139 143 65 15 77 72 55 61 59 35 14 2 4 6 12 4 6 12 136 131 130 131 78 357 42 22 23 48 54 31 15 10 10 10 12 3.5 3.5 3.5 1.7 0.6 0.9 0.9 0.9 0.8 0.5 0.7 1.6 0.9 0.9 1.7 1.6 3.7 1.0 10 10 12 3.5 3.5 3.1 1.5 3.1 1.5 110 10 10 10 12 3.5 3.5 3.1 1.5 3.1 3.1 1.5 3.1 1.5 3.1 3.1 1.5 3.1 3.1 1.5 3.1 3.1 1.5 3.1 3.1 1.5 3.1 3.1 1.5 3.1 3.1 1.5 3.1 3.1 1.5 3.1 3.1 1.5 3.1 3.1 1.5 3.1 3.1 1.5 3.1 3.1 1.5 3.1 3.1 1.5 3.1 3.1 3.1 3.1 3.1 3.1 3.1 3.1 3.1 3.1	6.0	2,51	1.9	3.7	3.8	1.6	0.7	0.6	1.2	0.7	0.2	0.0	0.7	2.9	5.0		7.3		5.4
5.0 6.83 1.5 3.4 3.7 1.7 0.6 0.4 0.9 0.7 0.5 0.5 1.2 2.9 4.0 6.2 10.9 10.5 5.2 14.5 11.25 1.4 3.3 3.5 1.7 0.6 0.4 0.6 0.6 0.6 0.6 1.2 2.9 4.0 6.2 10.9 10.5 5.2 14.5 11.25 1.3 120 136 139 143 65 13 77 72 55 61 59 35 14 2 4.1 7.9 13.3 12.6 5.6 12 12.0 136 139 143 65 13 77 72 55 61 59 35 14 2 4 6 12 12.0 136 139 130 131 78 357 42 22 23 48 54 31 15 10 10 10 10 12 13.5 13.5 13.6 13.6 13.6 13.6 13.6 13.6 13.6 13.6	5,5	4.14		3,6	3.8	1.7	0.6	0.5	1.1				1.0	3.0		5.0	8.4	8.5	5.1
4.5 11.25 1.4 3.3 3.5 1.7 0.6 0.4 0.6 0.5 0.4 0.6 1.2 2.5 4.1 7.9 13.3 12.6 5.6 12 120 136 139 143 65 15 77 72 55 61 59 35 14 2 4 6 12 4.0 18.55 1.3 3.2 3.4 1.7 0.7 0.4 0.4 0.3 0.4 0.6 1.0 2.1 4.1 9.0 15.4 14.6 6.2 15 151 130 131 78 357 42 22 23 48 54 31 15 10 10 10 10 12 3.5 30.59 1.3 3.1 3.4 1.8 0.9 0.3 0.4 0.5 0.5 0.5 0.7 1.6 4.0 9.9 17.1 16.3 7.0 114 126 119 117 88 345 342 329 342 20 32 29 29 25 20 17 15 3.0 50.43 1.4 3.1 3.5 1.9 1.0 0.3 0.7 0.9 0.8 0.6 0.6 1.0 4.2 11.3 18.8 17.7 7.7 15.0 15.1 15.1 122 109 104 95 337 316 312 319 343 338 27 48 42 29 24 20	5.0	6,83		3.4	3.7	1.7	0.6	0.4	0.9	0.7	0.5	0.5	1.2	2.9	4.0	6.2	10.9	10.5	
4.0 18.55 1.3 3.2 3.4 1.7 0.7 0.4 0.4 0.3 0.4 0.6 1.0 2.1 4.1 9.0 15.4 14.6 6.2 15.5 10.1 10.1 10.1 10.1 10.1 10.1 10.1	4,5	11.25	1.4	3.3	3.5	1.7	0.6	0.4	0.6	0.5	0.4	0.6	1,2	2.5	4.1	7.9	13.3	12.6	5.6
3.5 30.59 1.3 3.1 3.4 1.8 0.9 0.3 0.4 0.5 0.5 0.5 0.7 1.6 4.0 9.9 17.1 16.3 7.0 114 126 119 117 88 345 342 329 342 20 32 29 29 29 20 17 15 3.0 50.43 1.4 3.1 3.5 1.9 1.0 0.3 0.7 0.9 0.8 0.6 0.6 0.6 1.0 4.2 11.3 18.8 17.7 7.7 115 122 109 104 95 337 316 312 319 343 338 27 48 42 29 24 20	4.0	18,55				1.7		0.4	0.4	0.3	0.4	0.6	1.0			9.0	15.4	14.6	
3.0 50.43 1.4 3.1 3.5 1.9 1.0 0.3 0.7 0.9 0.8 0.6 0.6 1.0 4.2 11.3 18.8 17.7 7.7 115 122 109 104 95 337 316 312 319 343 338 27 48 42 29 24 20	3,5	30,59	1.3	3.1	3.4	1.8	0.9	0.3	0.4	0.5	0.5	0.5	0.7	1,6	4.0	9.9			7.0
	3.0	50.43		3,1	3,5	1.9		0.3	0.7	0.9		0,6	0,6		4.2	11.3			
	2,5	83,15	1.4	3.2	3.6			0.3	0.9	1.3		0.8	0.9	0.5	4.9	13.2	20.3	18.8	

APRIL		TEMPERA						MAVE										
HEIGHT	PRESSURE (mb)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
12.0	0.0062	2.21	1,92	1.20	0.85	0.59	0,18	0.85	0.37	0.48	0.21	0.13	0,58	0.72 358	0.44	0.45	0,61	0.52
11,5	0.0103	2,19	1,99	1.21	0,94	0,67	0.19	0.83	0.40	0,47	0.19	0.13	0.58	0.69	0.40	0.49	0.66	0.57
11.0	0.0169	2,03	1,99	1.26	1,09	0.77	0.23	0,73	0.41	0.43	0.15	0.13	0,53	0,59	0.30	0.51	0.65	0,57
10.5	0,0279	1.77	1,99	1,45	1,35	0.95	0.32	0.58	0.42	0.57	0.08	0.11	0.45	0.38	0.15	0.55	0.59	0.53
10.0	0.0460	1.56	2.06	1,86	1,71	1,18	0,47	0.38	0,43	0.50	0.02	0.10	0.34	0.09	0.25	0.57	0.49	0.44
9.5	0,0758	1,44	2.23	2,36	2.07	1.39	0,62	0.23	0.40	0.24	0.08	0.07	0.23	0.27	0.54	0.57	0.33	0.40
9.0	0.1250	1,49	2,42	2.84	2,29	1.51	0.74	0.29	0.30	0.18	0.13	0.04	0.17	0.62	0.84	0.57	0.24	0.43
8.5	0.2061	1,69	2.58		2,21	1.36	0.77	0.43	0.11	0.18	0.15	0.10	0.13	0.88	1.12	0.76	0.46	0.52
8.0	0.3398	1,95	2.75	3,02	1.92	0.97	0,67	0.46	0.20	0.25	0.20	0.17	0.10	0.96	1.37	1.19	0.77	0,60
7.5	0.5605	1,85	2.51	2,59	1,40	0.45	0.36	0.36	0.27	0.28	0.21	0.13	0.26	0,85	1,26	1.33	1.02	0,43
7.0	0,9237	1.76	2.49	2,22	1,37	0.42	0.20	0.32	0,30	0.30	0.25	0.16	0,35	0.40	0.88	1.43	1,11	0.28
6.5	1,52	1.88	2.82	2,61	1,81	0.77	0.27	0.35	0.43	0.38	0.41	0.32	0.35	0.27	1,53	1.91	1,15	0.47
6.0	2,51	2,23	3,62	3.51	2,75	1,45	0,57	0,49	0.56	0,44	0,56	0,42	0.25	0,92	350	2.36	1.14	0.70
5.5	4,14	1,94	3.59	3.90	3,30	1,82	0.69	0,46	0,52	0,42	0.54	0.41	0.25	1.37	2.61	2.12	1.09	0.75
5.0	6.83	1.24	2.89	3.85	3,47	1.90	0,67	0,41	0.43	0.38	0.45	0.40	0.55	1,53	2.10	1,59	1,35	0.81
4.5	11.25	0.73	1.95	3.31	3.17	1,66	0.50	0.35	0.35	0.32	0.33	0,43	0.86	1,35	1.23	1.68	1,79	0.87
4.0	18,55	1.29	1,68	2,67	2,62	1.25	0.26	0.27	0.29	0.26	0,25	0.49	1.06	0.91	1.33	118	2.10	0.90 181
3.5	30.59	156	111	2.09	2,01	0.86	0.04	0.19	263	0.20	0.26	0,51	1.09	358	124	3,13	155	181
3.0	50.43	1,75	1.80	1,58	1,48	48	328 0.12	253	285	269	0.30	291	317	0.09	151	160	163	196
2.5	83,15	176	156	107	1,00	75	158	252	302	287	334	298	318	78	159	166	169	206
		179	163	120	94	97	157	247	312	299	342	303	318	149	163	169	173	213
APRIL	MEAN (GEOPOTE	NTIAL	HEIGHT	AMPL I	TUDE (dam) A	ND PHA	SE W	AVE 1								
SCALE HE IGHT	PRESSURE (mb)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
12.0	0,0062	14.2	24.3	28.3	23.5	12.8	7.4 253	9.6	7.6 191	2.6	4.6 220	4.2	5.2 283	6.2	8.3	3.4	7.7	2.5
11.5	0.0103	12.6	24.3	29.4	24.2	12.9	7,5	9.0	7,1	2.9	4.9	4.2	4.7	5.9	7.9	3.9	7.6	3.3
11.0	0.0169	11.5	24.4	30.3	24.6	12.9	7.4	8.5	6.7	3.3	5.1	4.3	4.4	5.8	7.5	4.4	7.6	4.1
10.5	0.0279	10.8	24.2	30.7	24.8	12.8	7.2	8.2	6.3	3.7	5.3	4.3	4.2	5.8	7.3	4.8	7.6 187	4.9
10.0	0.0460	10.3	23.7	30.5	24.8	12.6	6.9	7.9	5.9	4.0	5.3	4.5	4.2	5.8	7.1	5.2	7.6	5.6
9.9	0.0758	9.5	22.7	29.5	24.4	321 12.2 329	6.3 268	7.6	5.7 211	4.3 217	218 5.3 218	4.4	4.4	5.8	7.0	5.4	7.4	6.2
9.0	0.1250	8,3	21.1	28.0	23.7	11.8	5.5	7.3	5.5	4.5	5.1	4.4	4.7	5.6	7.0	5.3	7.1	6.5
8.5	0.2061	6,5	18.7	25.8	22.8	11.5	4.5	6.9	5.5	4.6	4.9	4.5	4.9	5.5	6.9	4,6	6.8	198 6.6
8.0	0.3398	4.2	15,6	23.0	21.5	11.1	3.6	6.5	5.7	4.7	218	4.6	5.0	5.4	6.7	3.3	6.6	6.6
7.5	0.5603	1.9	12.1	20.1	19.8	358	288	6.0	5.7	4.7	4.7	4.7	4.8	5.6	6.5	1.5	7.2	6.7
7.0	0.9237	1.9	8.6	17.2	18.0	10.2	2.5	5.6	5.6	4.5	4.5	4.5	4.6	6.0	6,1	1.7	179 8.6	7.1
6.5	1.52	183	5.0	14.2	16.0	9.3	290	5.1	5.1	4.0	4.0	4.2	252	5.9	339	4.1	174	175
6.0	2.51	7.3	3.1	10.7	13.2	7.9	1.8	4.6	209	3.3	3.3	3.7	258	5.2	1.9	7.1	11.7	178
5.5	4.14	10.4	124	7.5	9.5	5.6	274	4.0	208	205	207	220	264	314	315	180	178	183
5.0	6.83	10.4 204 12.7	6.8 175 11.0	6.6	5.9	3.1	1.3	210 3.5	3.6 207 3.0	2.6 203 2.1	2.5 205 1.8	3.1 222 2.5	266	298	217	12.5	185	7.9 191 7.6
4,5	11.25	206 13.7	190	135	73	1,4	204	203	203	198	199	221	262	266 3.9	205	195	192	199
4.0	18.55	13.3	199	172	128	89	185	195	197	188	186	212	247	233	208	204	202	207
3.5	30.59	215	208	193	174	162	178	188	187	174	168	193	218	216	216	217	215	215
3.0	50.43	225	218	208	196	185	176	182	177	163	158	170	189	211	231	237	232	221
	~	234	229	218	209	197	176	177	170	1.8	1.9	155	174	210	9.0	10.7	8.1 251	3.7 228
2.5	83.15	9.5	13.4	14.6	10.7	4.5	2.6	2.8	2.7	2.1	2.4	3.0	5.5	6.1	9.5	11.6	8.0	2.9

										O		00	R (QUA	LIT	Y		
APRIL				MPLITU				WAVE					**		**	**	70	**
SCALE HEIGHT	(mb)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
12.0	0.0062	0.21	0.48	0.38	0.12	0.17	0.22	0.18	0.48 238	1.03	0.95	194	0,69	0,18	0.60	0.30	0.02	0.40
11,5	0.0103	0.20	0.51	0.42	0.17	0.20	0.25	0.19	0.46	1.00	0.91	0.70	0.73	0,18	0.62	0.28	0.01	0.40
11,0	0.0169	0.20	0.52	0.44	0.26	0.23	0.29	0.18	0.39	0.89	0.80	0.66	0.72	0.16	0.57	0.21	0.04	0.32
10.5	0.0279	0.26	0.55	0.46	0.37	0.28	0.34	0.17	0,31	0.72	0,61	0.58	0.68	0.14	0.46	0.11	0.09	0.18
10.0	0,0460	0.36	0.54	0.46	0.50	0.35	0.59	0.19	0.19	0.54	0.40	0.46	0.61	0.11	0.27	0.13	0.15	0.03
9,5	0.0754	0.47	0.51	0.43	0.60	0.43	0.43	0.22	0.09	0.34	0.18	0.32	0.51	0.11	0.11	0.30	0.20	0.22
9.0	0,1240	0.55	0.44	0.35	0.64	0.49	0.41	0.26	0.08	0.14	0.19	0.16	0.34	0.09	0.52	0.45	0.22	0.38
8,5	0.2061	0.52	0.27	0.23	0.55	0.52	0.26	0,29	0.09	0.11	0.32	0.10	0.12	0.04	0.56	0,50	0.21	0.44
8.0	0.3398	0.43	0.03	0.28	0.43	0.54	0.01	0,28	0.05	0.14	0.34	0.18	0.27	0.13	0,69	0.44	0.16	0.38
7.5	0.5603	0.23	0.18	0.21	0.30	0.38	0.15	0,24	0.10	0.04	0.15	0.11	0.40	0.18	0.46	0,28	0.11	0.19
7.0	0.9237	0.11	0.24	0.11	0.21	0.14	0.16	0,19	0.19	0.19	0.11	0.04	0.34	0.16	0.17	0.20	0.11	0.07
6.5	1.52	0.11	0.29	0.35	0.27	0.15	0.13	0.15	0.19	0.22	0.17	0.12	0.23	0.21	0.11	0.18	0.12	0.04
6.0	2.51	0.18	0.46	0,62	0.49	0.38	0,19	0.11	0.13	0.16	0,15	0.14	0.24	0.36	0.28	0.19	0.05	0,11
5.5	4.14	0.13	0.40	0.51	0.49	0.39	0.16	0.07	0.05	0.09	0.13	0.10	0,12	0.30	0.25	0,11	0.14	0,14
5.0	6.83	0.07	0.29	0.33	0.43	0.37 326	0.12	0.04	0.06	0.04	0.09	0.11	0.12	0.20	0.33	0,17	0.35	0.21
4.5	11,25	0.06	0.21	0.14	0.31	0.31	0.05	0.09	0.14	0.10	0.04	0.21	0.31	0.31	0.53	0.44	0.56	0.27
4.0	18,55	0.10	0.25	0.16	0.17	320 0.21 311	0.02	0.13 117	0.20	0.16	0.06	0.31	0.48	329 0.53 349	0.71 309	0,69	0.70	0.31
3,5	30.59	0.12	0.29	90 0.24 112	0.06	0.13	0.06	0.16	0.22	0.20	0.10	0.35	0.56 33	0.67	0.77	0,80	0.72	0.32 197
3.0	50,43	0.11	0.27	0.25	0.03	0.07	0.09	0.15	0.21	0.20	0.12	0.36	0.54	0,66	0.69	0.72	207	0.28
2.5	83,15	0.09	0.20	0.20	0.05	0.04	0.08	0.11	0.16	0.16	0.11	0.28	0.43 36	0.53	0.51	0.55	0,45	0.20
		,	80	122	133	247	103	105	101	341	52	41	,96	1	319	245	211	190
APRIL		SEOPOTE		HEIGHT				IND PHA		AVE 2								
SCALE HE IGHT	PRESSURE (mb)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
12.0	0.0062	174	7.6 26	7.9	7,1 33	5.5 49	3.6 46	334	2.5	5.8 232	3.8	3.2	4.1	0,6	3,5	2.2	0.8	1.9
11.5	0.0103	177	7.0 22	7.3	6.8	5.3 51	3.3	2.1 327	1.9 239	4.5 229	2.5	2.2 175	159	0.9	3.7 15	355	0.8	2.5
11.0	0.0169	3.7 180	6.4	6.7	6.5 32	5.0	3.0	320	1.2 239	3.3	1.2	1.3	2.0 152	1.1	4.0	2.8	0.8	3.0 199
10.5	0.0279	181	5.8 14	6.1	6.1	4.7	2.5	313	0.7 236	2.3	0.2	0.7	1.0	1.3	4.4 354	3.0	0.7	3.4 198
10.0	0.0460	3.0 180	5.2	5.4 12	5.5	4.2 56	2.0	1.9 306	0.3	1.5	0.5	0.8 57	0.4	1.5	4.7	3.1	0.7	3.5 197
9.5	0.0758	175	4.6	4.7	4.8	3.7 56	1.4	1.7	0.2 190	1.0	0.9	1.2	359	1.6	4.7	3.0	0.8	3.3 196
9.0	0.1250	1.8	4.0 358	4.2	4 . 1	3.0 54	0.8	1.4	0.3	0.7 176	1.0	1.5	1.4 346	1.7	4.5 345	2.7	0.9	2.9 196
8.5	0,2061	1.3	3.6	3.8	3,6	2.4 46	0.3	1.0	183	0,6	0.8 346	1.5	1.8	1.7	3.8	2.4	1.2	195
8.0	0.3398	1.0	3.4 352	3.7	3.6	2.1	0.1 349	0.6 274	0.5	0.6	0.7 309	1.4	1.8	1.6	3.0 356	2.2	1.4	1.6
7.5	0.5603	1.0	3,4 354	3.8	4.0 350	2.2	0.2	0.3 264	0.5	0.6	0.7 280	1.1	1.7	1.5	2.3	2.0	1.5	1.2
7.0	0.9237	1.0	3.6 359	4.0	4.3	2.5	0.4	0.1	161	0,5	0,6	1.1	1.8	1.5	2.0	1.8	1.6	1.1
6.5	1,52	1.1	3,6	4.0	355	2.5	0.6	0.3 96	0,5	0.3	0.4 285	1.2	2.0	1.7	2.1	1.6	1.8	1.0
6.0	2,51	1.3	3,4	3.6	4.0	2.1	0.7	0.5	0.7	0.3	0.3	1.4	2.3	2.1	2.3	1.3	1.8	0.9
5.5	4.14	1.4	3,1	3.2	3.4	1.7	0.8	0.6	0.8	108	357	1.5	2.5	2,6	2.7	1.1	1.7	0.9
5.0	6.83	1.5	2.9	3.0	2.9	1.4 36	1.0	0.7	0.8	0,4	0.4	1.5	2.6	2.9	3.0	1.2	1.4	0.8 167
4.5	11.25	1.5	2.7	2.8	2,6	1.3	1.1	0.6	0,6	0.4	0.5	1.3	2.3	2.9	3.1	1.6	1.1	0.6
4.0	18.55	1.4	2.3	2.6	2.4	1.4	1.1	0,5	0.4	0.2	0.4	0.9	1.7	2.7	5.3	2.4	1.2	0.6
3,5	30.59	1.2	2.0	2.5	2.3	1.6	1.0	0.4	0.1 58	0.1 350	0.3	0.5	1.1	2.5	3.7	3,5	2.1	0.8
3.0	50,43	1.1	1.7	2.5	2.3	1.7	0.9	0.4	0.3	0.3	0.2	0.2	0.6	2.5	4.2	4.7	3.0	1.2
2.5												131						
***	83.15	1.0	1.5	2.5	2.3	1.8	0.8	0.4	0.5	0.5	0.1	0.6	0.9	2.7	4.8	5.6	3:7	1.5

MAY	MEAN	TEMPERA	TURE A	MPLITU	DE (K)	AND P	HASE	WAVE	1									
SCALE	PRESSURE (mb)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
12.0	0.0062	2.23	2.90	2,79	2.06	1.18	0.18	0.65	0.50	0.64	0,28	0.46	0.71	0.40	0.62	0.76	0.92	0.25
11.5	0.0103	2.03	2,68	2,66	1.98	1.25	0.20	0,66	0.51	0.61	0.28	0.50	0.75	0.43	0.70	0.90	1.06	0.27
11.0	0.0169	1,62	2.23	2.37	1.80	1,25	0.41	0.64	0.52	0,53	0.28	0.51	0.73	0.42	0,74	0.97	1.12	0,26
10,5	0.0279	1,12	1,66	2,06	1,65	1.26	0.77	0.67	0,58	0.42	0.32	0.52	0,69	0.38	0.75	0.98	1.08	0.23
10.0	0.0460	0,64	1.24	1.98	1.74	1,29	1,21	0,80	0.71	0.34	0.39	0.51	0.61	0.32	0,69	0.90	0.91	0.17
9.5	0.0758	0.66	1.35	2,27	2,09	1.36	1,63	1.00	0.86	0.36	0.49	0.47	0.45	0.24	0.55	0.71	0.62	0.15
9.0	0,1250	1.14	1.91	2.71	2,50	1.41	1.85	1,19	0.92	0,46	0.55	0.36	0.24	0.15	0,51	0.44	0.30	0.23 326
8.5	0,2061	1,59	2.49	3.07 337	2.74	1.41	1,61	1.20	0.76	0.50	0.49	0.16	0.08	0.06	0,14	0,16	0,32	0.34 301
8.0	0,3398	1.89	2.88	3,24 353	2.71 323	1.33	0.88	0.94	0.39	0.39	0.32	0,14 306	0.39	0.02 180	0.41	0.28	0.57	0.43
7.5	0,5603	1.62	2,58	3,06	2,42	1,10	0.14	0.42	0.07	0.11	0.18	0.23	0.50	0.11	0,42	0.37	0.50 270	0.35 258
7.0	0.9237	1.52	2.43	3.05	2.38	1.19	0.77	0.35	0.31	0.13	0,20	0.16	0.30	0.13 261	0.26	0.28	0.26 260	0.28
6.5	1,52	1.73	2.65	3.25	2.50 354	1,41 345	0.96	0.71	0.35 360	0.20	0.13	0.04	0.10	0.07	0.22	0,13 301	0.12	0.22
6.0	2,51	2.13	3,02	3,39	2,59	1,67	1.14	0.97	0.36	0,16 346	0.07	0.06	0.22	0.07	0.21	0.18	0.37	0.22
5.5	4.14	2.09	2.74	2.71	2.22	1,68	1.41	1,24	0.50	0.23	0.19	0.11	0.10	0.06	0.07	0.18	0.51	0.19
5.0	6.83	1.72	2.38	2.46	2.00	1,44	1,45	1,32 336	0.59	0.31	0.30	0.32	0.23	0.09	0.28	0.37	0.59	0.16
4.5	11,25	1.42	2.66	3,32	2.39	1,20	1.23	1.22	0,61	0.35	0.39	0.55	0.59	0.20	0.58	0.66	0.58	0.13
4.0	18,55	1.76	3,49 133	4.27	2.90	1.21	0.88	0.96	0.55	0.36	0.43	0.72	0.91	0.32	0.80	0.88	0.50	0.11
3,5	30.59	2.06	3.76	4.45	2.98	1,31	0.54	0,68	0.45	0.32	0.40	0.79	1.08	0.39	0.87	0.95	0.37	0.11
3.0	50.43	1.78	3.14	3.71 134	2,60	1,25	0.31	0.46	0.35	0,27	0.35	0,77 280	1.09	0.39	0.78	0.84	0.23	0.10
2,5	83.15	1,24	2.14 155	2,58 137	1,89 126	0.99	0.20	0,29	0.22	0.19	0.26	0,60	0.89	0.32 293	0.58 174	0.61	0,12 170	0.08
MAY	MEAN	GEOPOTE	NTIAL	HE I GHT	AMPLI	TUDE (dam) A	IND PHA	ISE .	AVE 1								
SCALE HE IGHT	PRESSURE (mb)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
12.0	0.0062	11.4	11.6	7.8	7.9	6.2	3.4	1.5	3,3	2.7	3.7	2.4	1.1	5.3	2.4	3.3	4.0	2.7
11.5	0.0103	14.0	15.6	11.7	10.4	6.7	3.6	0.9	2.7	2.6	3,6	2.1	1.6	5.0	3.0	2.4	2.5	3.0
11.0	0.0169	16.5	19.2	15.3	12.7	7.5	3.6	1.0	125	2.6	3.4	2.0	2.5	262	3.8	353	0.9	3.3
10.5	0.0279	18.4	22.1	18.2	14.5	8.4	3.3	1.6	136	2.4	3.2	198	3,5	256 4.5	249 4.7	318	0.8	3.6
10.0	0.0460	19.7	23.9	20.3	356 15.7	9.3	3.2	2,3	0.7	165	2.8	218	4.5	4.5	5.7	3.0	255	3.9
9.5	0.0758	20.1	70	21.7	16.3	10.2	285	3.3	0.8	1.7	2.3	3.1	5.2	4.6	6.5	3.9	3.3	265
9.0	0.1250	19.9	24.7	22.5	16.7	11.0	5.9	4.6	283	191	186	3.7	256 5.8	4.7	7.0	4.7	3.9	263 4.0
8.5	0.2061	19.1	24.0	23.0	16.8	11.5	8.1	6.1	3.2	1.1	1.4	4.0	5.9	4.8	7.1	4.9	4.0	259 3.8
8.0	0,3398	17.9	22.9	23.1	16.8	11.7	348 9.8	7.6	4.0	1.4	1.4	250	256 5.7	4.8	6.8	230 4.8	3.6	3.4
7.5	0.5603	16.7	22.0	23.1	16.6	11.3	10.3	8.6	4.1	1.6	1,6	3.9	5.2	4.8	6.1	4.3	3.2	248
7.0	0.9237	15.7	106	93 23.4	16.2	10.3	355 9.6	8.8	328	1.5	259	3.6	4.7	4.6	5.7	3.8	209	244
6.5	1.52	15.2	116	104	16.1	9.0	353 8.4	8.2	3.5	298	256	3.5	4,5	232	5.5	226 3.6	200	244
6.0	2.51	15.1	125	115	16.9	7.8	6.9	7.1	322	1.5	251	3.5	243	231	5.6	223 3.7	197	1.9
5.5	4.14	15.4	135	125	102	7.0	351 5.0	5.6	317	1.3	247	3,5	246	4.3	219	3.9	204	255
5.0		159	145	133	17.7	6.4	354	327	313	1.0	1.8	3.3	249	232	218	4.0	2.5 219 2.5	263
4.5		15.2	153	140 26.6	123	85 5.8	1.4	1.9	307	252	1.6	241	3.9	233	218	3.9	237	272
4.0		177	160	147	131	101	1.2	308	297	0.8	217	232	3.3	3.9	223	238	256 3.0	279
3.5	30.59	184	16.0	154	9.2	116	110	259	212	179	196	214	229	226 3.7	233	255	271	284
3.0		188	178	165	6.3	133	141	164	138	153	177	187	203	219	249 3.6	274	281	286
2.5		192	190	181	176	163	154	143	128	140	165	162	175	210	268	290 5,3	287	287
	= 1	195	205	201	207	213	162	152	123	134	159	146	158	201	283	200	290	287

MAY	MEAN 1	TEMPERA	TURE A	MPLITU	DE (K)	AND P	HASE	WAVE	2		OF	P	OOF	\$ Q	UA	LII	Y	
SCALE HEIGHT	PRESSURE (mb)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
12.0	0,0062	0.21	0.15	0.47	0.08	0.21	0.54	0.42	0.42	0.16	0.74	0.77	0.28	0.39	0.19	0.17	0.28	0.81
11,5	0.0103	0.21	0.13	0.42	0.07	0.18	0.49	0.38	0.41	0.20	0.73	0.76	0.29	0.42	0.21	0.23	0.31	0.92
11.0	0.0169	0.19	0.08	0.35	0.06	0.09	0.39	0.28	0.37	0.23	0.66	0.68	0.29	0.41	0.22	0.28	0.32	0.95
10.5	0.0279	0.17	0.04	0.30	0.08	0.05	0.25	0.14	0.31	0.29	0.56	0.57	0.28	0.41	0.21	0.33	0.30	0.89
10.0	0.0460	0.15	0.06	0.33	0.12	0.18	0.20	0.07	0.27	0.38	0.43	0.40	0.25	0.39	0.23	0.37	0.23	0.75
9,5	0,0758	0.14	0,11	0.41	0.16	0.32	0.33	0.24	0.31	0.45	0.28	0.21	0.20	0.37	0.24	0.38	0.18	0.59
9.0	0.1250	0.13	199	0.47	0,19	0.40	76	0.36	0.39	0.47	0.15	0.10	0.12	0,34	0,21	0.33	0.17	0.49
8,5	0.2061	94 0.12 137	0,13	0.45	0,21	0,38	92	0,39	0.43	193	0.14	0.18	0.02	0,25	0.11	0.18	0,17	0.45
8.0	0.3398	0.17	0.08	312 0,34 323	350	130	0.35	0.35	0.40	0.24	0.14	0.23	0.18	0.14	0.11	0.13	0.14	0.48
7.5	0.5603	0,19	0.05	0.12	357	0.26	0,36	0.30	0.24	0.06	0.06	0.14	0.21	0.13	0,21	0.24	0.03	0.42
7.0	0.9237	0.19	0.11	0.07	0,33	0.51	182	0.31	192	0,05	0.04	0.07	0.13	0.12	0,15	0.22	0.05	0.30
6.5	1,52	0,15	331	0.34	0,65	0.85	203	0.32	0.14	0.09	0.10	0.06	0.06	0.06	0.06	0.10	0.01	0.11
6.0	2.51	0,11	319	283	1.11	1.17	0.80	0.39	0.17	0,15	0.13	198	0.10	0.10	0.05	78	0.13	0.12
5.5	4.14	243	315	293	262	1,09	0.77	212	216	0.14	0.12	0.08	332	343	0.02	156	0.19	0,18
5.0	6.83	0.14 266 0.20	0.72 319 0.83	0.94 302 0.95	1,19 276 1,05	0.90	231	219	203	188	0.10	343	0.18 357 0.29	333	246	187	0.24	214
4.5	11,25	288	323	314	291	259	245	0.32	188	163	0.07	0.32	0.41	326	283	0.20	216	209
4.0	18,55	300	328	332	312	281	260	232	166	136	279	0.42	19	323	290	254	211	203
17	30.59	308	332	353	346	312	276	240	141	117	328	12	0.50	319	293	272	208	201
3.5		311	337	15	21	341	290	254	117	103	354	15	27	316	296	282	203	197
3.0	50.43	315	342	30	43	1	302	270	99	94	0.11	16	29	315	297	287	199	193
2.5	83,15	0.20 317	348	0.32	0.37 54	0.31	312	295	88	0.12	8	18	31	313	298	291	195	191
MAY	MEAN (GEOPOTE	NTIAL	HEIGHT	AMPLI	TUDE (dam) A	ND PHA	SE W	AVE 2								
SCALE HE IGHT	PRESSURE (mb)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
12.0	0.0062	1.2	2.1	7.3	6.2	5.0	4.1	3.4	4.8	183	4.7	2.6	1.2	4.1	3.3	1.5	2.6	4.9 258
11.5	0.0103	1.5	2.1	7.3	6.3	5.1	3.8	3.5	4.6	4.1	3.6	1.7	1.5	3.6	3.0	1.2	2.3	3.8
11.0	0.0169	1.8	2.2	7.2	6.3	5.2	3.8	3.7	4.4	3.8	2.6	1.2	1.9	3.0	2.7	0.8	1.9	2.6
10.5	0.0279	2.0	2.2	7.0	6.3	5.3	3.9	3.9 189	4.2	3.5	1.8	1.4	2.3	332	2.3	0.4	1.6	1.5
10.0	0.0460	2.2	2.3	6.7	6.2	5.3	4.1	4.0	3.9	3.1	1.1	1.9	2.7	1.8	2.1	0.3	1.3	1.0
9,5	0.0758	2.4	2.3 306	6.2	6.1	5.4 232	4.5	4.0	3.6 187	2.6 187	0.7	2.2	3.0	1.3	1.9	0.8	1.1	1.2
9.0	0.1250	2.5	2.4 311	5.5	5.9	5.5	4.9	3.9 198	3,1	2.1	0.4	2.3	3.2	0.9	1.9	1.3	0.9	1.5
8.5	0,2061	2.5	2.4	4.8	5.8	5.6	5.3	3.7	2.5	1.6	0.2	2.1	3,3	0.9	1.9	1.6	0.6	1.6
8.0	0.3398	2.3	2.4 319	4.2	5.6	5.9	5,6	3.4	1.9	1.3	0.2	1.9	3.2	1.1	1.8	1.7	0.5	1.4
7.5	0.5603	2.1	2.3 321	4.0	5.6	6.0	5.5	3.0	1.4	1.1	0.3	1.7	2.9	1.3	1.6	1.5	0.5	1.2
7.0	0.9237	1,8	2.2	3.9 316	5.6	5.7	5.0	2.6	1.2	1.1	0.3	1.7	2.7	1.3	1.4	1.2	0.5	1.0
6.5	1,52	1.6	1.9	3.6	5.3	5.1	4.3	2.1	1.0	1.0	0.2	1.8	2.6	1.3	1.2	1.0	0.6	1.0
6.0	2,51	1,4	1.4	3.0 326	4.5	4.1	3.5	1.6	0.9	0.9	0.1	1.8	2,5	1.2	1.2	0.9	0.5	1.0
5.5	4,14	1.4	0.4	1.9	3.4 327	3.0	2.5	1.0	0.7	0.8	0.2	1.8	2,4	1.0	1.2	1.0	0.5	0.8
5.0	6.83	1.4	0.7	1.2	2.4	2.3	1.7	0.5	0.5	0.7	0.4	1.6	2.1	0.9	1.2	1.2	0.6	0.5
4.5	11,25	1,6	1.9	1.4	2.0	1.9	1.1	0.1	0.4	0.6	0.5	1.3	1.6	0.8	1.3	1.4	0.8	0.3
4.0	18,55	2.0	3.1	91 2.0 122	1.7	356 1.7 22	0.9	0.5	0.3	0.4	0.6 75	0.8	1.1	0.9	1.4	1.7	1.1	0.3
3.5	30.59	156	4.0	2.6	1.4	1.4	1.1	0.8	0,1	0.2	0.6	0.5	0.7	1.0	1,8	2.0	1.4	0.6
3.0	50,43	3.1 147	4.6	3.0	1.0	1.2	1.4	0.9	0,1	0.1	0 6	0.8	0.9	1.2	67 2.2 79	2.3	1.7	0.8
2.5	83.15	147 3.4 146	5.0 150	153 3.3 162	0.9 145	1.0	1.6	1.1	357 0.2 248	0.1 234	0,6	1.3	1.4	1.3	2,6	2.6 73	1.9	0.9
		146	150	162	145	97	80	67	21/8	234	120	173	179	99	86	73	44	31

JUNE	MEAN 1	EMPERA	TURE A	MPLITU	DE (K)	AND P	HASE	WAVE	,									
SCALE HEIGHT	PRESSURE (mb)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
12.0	0.0062	1.16	2.33	1.82	0.72	0.47	0.93	1.18	0.68	0.17	0.86	1.15	0.17	4.20	0.41	0.35	0.43	0.21
11,5	0.0103	1.02	2.10	1.76	0.78	0.30	0.75	0.97	0.54	0.16	0.87	1.13	0.15	4.70	0.45	0.36	0,49	0,25
11.0	0.0169	0.85	1.71	1,59	0.83	0.21	0,59	0.57	0.26	0.16	0.83	1.03	0.11	3.77	0.45	0.28	0.53	0.28
10,5	0,0279	0.83	1.35	1,45	0.90	0.58	0.86	0.10	0.17	0.25	0.74	0.85	0.07	2.17	0.39	0.18	0.51	0.27
10.0	0.0460	1.05	1.37	1.44	1.01	1.08	1,55	0.84	0.69	0.39	0.64	0,63	0.13	0.71	0.28	0.25	0.42	0,24
9,5	0.0758	1.38	1.87	1.72	1,16	1,52	2,34	1.70	1.24	0.53	0,55	0.37	0.24	0.56	0.10	0.48	0.31	0.17
9,0	0.1250	1.70	2,55	2.25	1,43	1,80	2.94	2.38	1,67	0.64	0.50	0.18	0.37	1.33	0.10	0.69	0.23	0.11
8.5	0.2061	1.85	3,15	2.98	1.88	1,69	2.97	2.56	1.72	0.57	0.48	0.13	0.49	1,19	0.29	0.74	0.20	0.13
8.0	0.3398	1,83	3.52	3,73	2.48	1.28	2.32	2.10	1.34	0.35	0.42	0.19	0,60	0.15	0.41	0.62	0,22	0.34
7.5	0,5603	1.40	2.92	3,48	2.39	1.10	1.31	1.08	0.57	0.03	0.26	0,30	0.58	1,40	0.38	0.30	0.28	0.58
7.0	0.9237	1.05	2.29	3.09	2.33	1.11	0,55	0.39	C.20 83	0.15	0.18	0.29	0.46	1.47	0.27	0.18	0.28	0.26
6,5	1.52	0.89	1.91	2.87	2,54	1.45	0.36	0.23	0.12	0.12	0.13	0.21	0.35	0.43	0.15	0.15	0.22	0.19
6.0	2.51	0.91	1.82	2.97	3,11	2.14	0.66	0.14	0.11	0.11	0.14	0.18	0.29	0.20	0,14	0.10	0.25	0,30
5.5	4.14	0.82	1.64	356	3.24	2,59	1,12	0.23	0.14	0.12	0.13	0.10	0.15	0.24	0.21	0.15	0.27	0,35
5.0	6.83	0.66	1.35	2.14	2,65	2.43	1,33	0.48	0.24	0.18	0.21	0.32	0,31	0,28	0.33	0.23	0,28	0.34
4,5	11,25	0.51	1,24	1.51	1.66	1.69	1.18	0,67	0,32	0.24	0.28	0.59	0.67	0.36	0.48	0.32	0.28	0.30
4.0	18,55	0.82	1,62	1,90	1.33	0.96	0.82	306 0.75	0,36	0.27	0,33	0.80	0.98	0,44	0,59	0.39	0.28	0,22
3.5	30,59	1,11	136	2,40	1,63	0.85	0,41	0.73	0.33	0.26	0,32	0,88	1,12	0.46	0.61	0,40	0.27	0.14
3.0	50,43	0.95	1,59	129	116	1.05	0.07	0,66	0,29	0,22	0.29	0.85	1,11	0,43	199	0,35	0,23	0.09
2.5	85,15	0,62	1.06	1,60	1.37	0.97	0.10	0,49	0.20	0.17	0.22	0,70	0,92	0.35	0.41	0.26	0.17	0.07
		207	169	142	137	139	169	272	288	273	274	274	284	266	194	230	287	155
		201	103				-							-				
JUNE		БЕОРОТЕ	NTIAL	HEIGHT	AMPLI					AVE 1								
	MEAN (PRESSURE (mb)								SE W		10	20	30	40	50	60	70	80
SCALE	PRESSURE	БЕОРОТЕ	NTIAL	HEIGHT	AMPLI	TUDE (dam) A	ND PHA		AVE 1								
SCALE HE IGHT	PRESSURE (mb)	-80 10.9	-70 13.7	HEIGHT -60	-50 21.2	TUDE (dam) A -30	-20	-10 9.9	0 6,2	10	20	30	40	50	60	70	80 5.2 218 4.8
SCALE HEIGHT 12.0	PRESSURE (mb) 0.0062	-80 10.9 279 10.3	13.7 310	-60 21.4 314 22.2	-50 21.2 315 21.5	7UDE (-40 9.1 263 9.6	dam) A -30 16.3 172 17.1	-20 12.7 164 14.3	-10 9.9 170 10.8	0 6,2 189 6.4	10 9.9 210 8.9	20 12.9 225 11.2	30 9.1 245 9.3	40 14.3 35 7.9	50 5.8 216 6.3	60 6.6 259 7.2	70 8.1 235 7.5	60 5.2 218
SCALE HEIGHT 12.0	PRESSURE (mb) 0.0062 0.0103	-80 10.9 279 10.3 287 9.6	13.7 310 14.0 323 14.5	HEIGHT -60 21.4 314 22.2 320 22.7	-50 21.2 315 21.5 318 21.8	7UDE (-40 9.1 263 9.6 262 9.9	16.3 172 17.1 176 17.5	-20 12.7 164 14.3 164 15.5	-10 9.9 170 10.8 169	0 6,2 189 6,4 185 6,6	9.9 210 8.9 206 7.9	20 12.9 225 11.2 225 9.7	30 9.1 245 9.3 245 9.5	40 14.3 35 7.9 29 2.3	5.8 214 6.3 218 6.9	60 6.6 259 7.2 258 7.6	70 8.1 235 7.5 233 6.8	5.2 218 4.8 218
SCALE HEIGHT 12.0 11.5	PRESSURE (mb) 0.0062 0.0103 0.0169	-80 10.9 279 10.3 287 9.6 294 8.6	13.7 310 14.0 323 14.5 334	HEIGHT -60 21.4 314 22.2 320 22.7 327 22.9	21.2 315 21.5 318 21.8 321 21.8	7uDE (-40 9.1 263 9.6 262 9.9 262 9.9	16.3 172 17.1 176 17.5 178	-20 12.7 164 14.3 164 15.5 164 15.8	-10 9.9 170 10.8 769 11.4 168	6,2 189 6,4 185 6,6 182 6,4	9.9 210 8.9 206 7.9 200 7.0	20 12.9 225 11.2 225 9.7 224 8.3	30 9.1 245 9.3 245 9.5 246 9.6	40 14.3 35 7.9 29 2.3 343 3.7	5.8 216 6.3 218 6.9 221 7.4	6.6 259 7.2 258 7.6 258 7.9	70 8.1 235 7.5 233 6.8 231 6.1	5.2 218 4.8 218 4.4 219
SCALE HEIGHT 12.0 11.5 11.0	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279	-80 10.9 279 10.3 287 9.6 294 8.6 298 7.3	13.7 310 14.0 523 14.5 334 14.6 343 13.8	HEIGHT -60 21.4 314 22.2 320 22.7 327 22.9 332 22.5	21.2 315 21.5 518 21.8 321 21.8 325 21.7	9.1 263 9.6 262 9.9 262 9.9 265 9.6	16.3 172 17.1 176 17.5 178 17.0 181	-20 12.7 164 14.3 164 15.5 164 15.8 164 15.2	9.9 170 10.8 169 11.4 168 11.4 168	6,2 189 6,4 185 6,6 182 6,4 180	9.9 210 8.9 206 7.9 200 7.0 195 6.2	20 12.9 225 11.2 225 9.7 224 8.3 224 7.2	9.1 245 9.3 245 9.5 246 9.6 246 9.6	40 14.3 35 7.9 29 2.3 343 3.7 254 5.6	5.8 216 6.3 218 6.9 221 7.4 225 7.9	60 6.6 259 7.2 258 7.6 258 7.9 257	70 8.1 235 7.5 233 6.8 231 6.1 228 5.4 226	5.2 218 4.8 218 4.4 219 4.0 218 3.7 217
SCALE HEIGHT 12.0 11.5 11.0 10.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460	10.9 279 10.3 287 9.6 294 8.6 294 8.7 300 5.6	13.7 310 14.0 523 14.5 334 14.6 343 13.8 350 12.0	HEIGHT -60 21.4 314 22.2 320 22.7 327 22.9 332 22.5 337 21.1	21.2 315 21.5 518 21.8 321 21.8 325 21.7 328 21.1	TUDE (1) -40 9.1 263 9.6 262 9.9 262 9.9 265 9.6 272 9.2	dam) A -30 16.3 172 17.1 176 17.5 178 17.0 181 15.6 184 12.9	12.7 164 14.3 164 15.5 164 15.8 164 15.2 165 13.4	-10 9.9 170 10.8 169 11.4 168 11.4 168 10.8 168 9.4	6,2 189 6,4 185 6,6 182 6,4 180 6,0 180	10 9.9 210 8.9 206 7.9 200 7.0 195 6.2 190 5.5	20 12.9 225 11.2 225 9.7 224 8.3 224 7.2 224 6.5	9.1 245 9.3 245 9.5 246 9.6 246 9.6 245 9.6	40 14.3 35 7.9 29 2.3 343 3.7 254 5.6 241 5.5	5.8 216 6.3 218 6.9 221 7.4 223 7.9 224 8.1	60 6.6 259 7.2 258 7.6 258 7.9 257 7.9 259	70 8.1 235 7.5 233 6.8 231 6.1 228 5.4 226	5.2 218 4.8 218 4.4 219 4.0 218 3.7 217 3.4 215
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758	-80 10.9 279 10.3 287 9.6 294 8.6 298 7.3 300 5.6 295	13.7 310 14.0 523 14.5 334 14.6 343 13.8 350 12.0 356 9.0	HEIGHT -60 21.4 314 22.2 320 22.7 327 22.9 332 22.5 337 21.1 342 18.8	21.2 315 21.5 518 21.8 321 21.8 325 21.7 328 21.7 328 21.1 332	TUDE (-40 9.1 263 9.6 262 9.9 262 9.9 265 9.6 272 9.9 283 9.1	dam) A -30 16.3 172 17.1 176 17.5 178 17.0 181 15.6 184 12.9 9.3	12.7 164 14.3 164 15.5 164 15.8 164 15.8 165 15.8 165 10.4	-10 9.9 170 10.8 169 11.4 168 10.8 168 9.4 168 7.3	6.2 189 6.4 185 6.6 182 6.4 180 6.0 180	9.9 210 8.9 206 7.9 200 7.0 195 6.2 190 5.5 186 4.7	20 12.9 225 11.2 225 9.7 224 8.3 224 7.2 224 6.5 224	9.1 245 9.3 245 9.5 246 9.6 246 9.6 245 9.6 245	40 14.3 35 7.9 29 2.3 343 3.7 254 5.6 241 5.5 239 4.1	5.8 214 6.3 218 6.9 221 7.4 223 7.9 224 8.1 225 8.2	6.6 259 7.2 258 7.6 258 7.9 257 7.9 255 7.6 252	70 8.1 235 7.5 235 6.8 231 6.1 228 5.4 226 4.9 225	5.2 218 4.8 218 4.4 219 4.0 218 3.7 217 3.4 215
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250	-80 10.9 279 10.3 287 9.6 294 8.6 298 7.3 300 5.6 295 4.0 276 3.8	13.7 310 14.0 323 14.5 334 14.6 343 13.8 350 12.0 356 9.0 3	HEIGHT -60 21.4 314 22.2 320 22.7 327 22.9 332 22.5 337 21.1 342 18.8 347 15.2	21.2 315 21.5 318 21.8 321 21.8 321 21.8 321 21.8 321 21.7 328 21.7 332 20.1 336 18.2	TUDE (-40 9.1 263 9.6 262 9.9 265 9.6 272 9.2 283 9.1 299 9.2	dam) A -30 16.3 172 17.1 176 17.5 178 17.0 181 15.6 184 12.9 189 9.3 196 5.4	-20 12.7 164 14.3 164 15.5 164 15.8 165 15.8 165 165 165 165 166 166 166 168	9.9 170 10.8 169 11.4 168 10.8 168 168 9.4 168 7.3 170 4.8	6,2 189 6,4 185 6,6 182 6,6 180 180 5,2 181 4,1 184 2,9	9.9 210 8.9 206 7.9 200 7.0 195 6.2 190 5.5 186 4.7 184	20 12.9 225 11.2 225 9.7 224 8.3 224 6.5 224 6.5 225 5.9	9.1 245 9.3 245 9.5 246 9.6 245 9.6 244 9.3 242 8.9	40 14.3 35 7.9 29 2.3 343 3.7 254 5.6 241 5.5 239 4.1 241 2.3	5.8 216 6.3 218 6.9 221 7.4 223 7.9 224 8.1 225 8.2 224 7.9	60 6.6 259 7.2 258 7.6 258 7.9 257 7.9 259 7.6 252 6.9 247	70 8.1 235 7.5 233 6.8 231 6.1 228 5.4 226 4.9 225 4.2	5.2 218 4.8 218 4.4 219 4.0 216 3.7 217 3.4 215 3.2 213
SCALE HE IGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061	10.9 279 10.3 287 9.6 294 8.6 298 7.3 300 5.6 295 4.0 276 3.8 237	13.7 310 14.0 323 14.6 343 13.8 350 12.0 356 9.0 3 5.0 14	HEIGHT -60 21.4 314 22.2 320 22.7 327 22.9 332 22.5 337 21.1 342 18.8 347 15.2 351 10.4 355 5.1	21.2 315 21.5 518 21.6 325 21.7 328 21.1 332 20.1 336 341 15.3 345 11.9	TUDE (-40 9.1 263 9.6 262 9.9 262 9.9 265 9.6 272 283 9.1 299 9.2 315 9.5	dam) A -30 16.3 172 17.1 176 17.5 178 17.0 181 15.6 184 12.9 189 9.3 196 5.4 213 3.0	-20 12.7 164 14.3 164 15.5 164 15.8 165 165 13.4 166 6.8 173 3.5 186	-10 9.9 170 10.8 169 11.4 168 10.8 168 9.4 168 7.3 170 4.8 174 2.6 187 1.7	6.2 189 6.4 185 6.6 6.4 180 6.0 180 5.2 181 4.1 184 2.9 191 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1	9.9 210 8.9 200 7.0 195 6.2 190 5.5 186 4.7 184 4.0 186 3.5 191	20 12.9 225 11.2 225 9.7 224 8.3 224 6.5 225 5.9 227 5.8 227 5.8 228	30 9.1 245 9.3 245 9.6 246 9.6 245 9.6 8.6 9.6 9.6 9.6 9.6 9.6 9.6 9.6 9	40 14,3 35 7,9 29 2,3 343 3,7 254 5,6 241 5,5 239 4,1 1,2 251 1,3 251 1,3 251	50 5.8 216 6.3 218 6.9 221 7.4 223 7.9 224 8.1 225 8.2 224 7.9 224 7.4 6.8 6.9 6.9 6.9 6.9 6.9 6.9 6.9 6.9	60 6.6 259 7.2 258 7.6 258 7.9 257 7.9 255 7.6 6.9 247 6.0 242 235	70 8.1 235 7.5 233 6.8 231 228 5.4 226 4.9 225 4.5 226 4.2 228 3.9 229	5.2 218 4.8 218 4.4 219 216 3.7 217 3.4 215 3.2 213 3.1 214
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 8.0 7.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398	10.9 279 10.3 287 9.6 294 8.6 298 7.3 300 5.6 295 4.0 275 4.0 275 5.6 287 5.6 297 5.6 297 5.6 297 5.6 297 5.6	NTIAL -70 13.7 310 14.0 323 14.5 334 14.6 343 13.8 9.0 3 5.0 14 1.2 91 4.7	HEIGHT -60 21.4 314 22.2 22.7 320 22.7 327 322 21.1 342 18.8 347 15.2 351 10.4 355 5.1 358 0.4	AMPLI -50 21.2 315 21.5 318 21.8 325 21.7 328 21.1 336 18.2 2 341 15.3 345	TUDE (-40 9.1 263 9.6 262 9.9 265 9.6 272 9.2 283 9.1 1299 9.2 315 9.5 9.3	dem) A -30 16.3 172 17.1 17.6 17.5 17.9 181 15.6 184 12.9 189 9.3 196 5.4 213 3.0 3.0 3.0 3.4 4.0	12.7 164 14.3 164 15.5 164 15.6 165 166 10.4 168 6.8 173 186 1.8 1.8 1.8 1.8 1.8 1.8 1.8 1.8 1.8 1.8	9.9 170 10.8 169 11.4 168 10.8 10.8 168 7.3 170 4.8 174 2.6 187 1.7 2.1 3	6.2 189 6.4 185 6.6 182 6.4 180 6.9 180 6.9 181 6.9 181 6.9 191 6.9 191 6.9 191 6.9 191 6.9 191 6.9 191 6.9 191	9.9 210 8.9 206 7.9 206 7.9 55 5.186 4.7 184 4.0 186 3.5 191	20 12.9 225 11.2 225 9.7 224 8.3 224 7.2 224 6.5 5.9 227 5.8 228 5.4 230 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.	9.1 245 9.3 245 9.5 246 9.6 245 9.6 245 9.3 242 239 239 239 239 6.6 6.6	40 14.3 35 7.99 2.3 343 3.7 254 5.6 241 5.5 239 4.1 241 2.3 251 1.3 263 2.3 263 2.3 264 244 244 245 256 267 267 267 267 267 267 267 267 267 26	50 5.8 216 6.3 218 6.9 221 7.4 223 8.1 125 8.2 224 7.9 224 8.1 225 6.2 24 6.3 7.9 24 6.9 6.9 6.9 6.9 6.9 6.9 6.9 6.9	60 6.6 259 7.2 258 7.6 258 7.9 255 7.6 252 247 6.0 242 235 4.7 231 4.4	70 8.1 235 7.5 233 6.8 231 6.1 226 4.9 225 226 4.5 226 4.5 228 3.9 229 3.6	5.2 218 4.8 219 4.0 218 4.2 217 3.7 217 3.4 215 3.2 213 3.1 214 2.2 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 8.0 7.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603	-80 10.9 279 10.3 287 9.6 294 8.6 298 7.3 300 5.6 295 3.0 276 3.8 237 5.6 212 7.8 206 9.6 209 9.6	13.7 310 14.0 323 14.5 334 14.6 350 350 12.0 356 9.0 12.0 12.0 14.7 17.4 8.4 18.2	HEIGHT -60 21.4 314 22.2 320 22.7 327 22.9 332 22.5 537 21.1 342 351 10.4 355 5.1 358 0.4 325 4.0	21.2 21.5 315 21.5 316 21.8 325 21.7 328 21.1 336 18.2 20.1 341 15.3 345 11.9 350 8.7 357 359	TUDE (-40	dam) A -30 16.3 172 17.1 176 17.5 178 17.0 181 15.6 4 12.9 9.3 196 5.4 4 3.0 259 4.0 326 4.0 4.0 4.0	12.7 164 14.3 164 15.5 164 15.2 165 166 10.4 168 173 3.5 188 223 1.8 223 1.8	9.9 170 10.8 168 11.4 168 10.8 168 17.4 2.6 187 1.7 2.1 2.1 2.1 2.2 2.2 2.2 2.2 2.2 2.2 2.2	6.2 189 6.4 185 6.6 6.0 180 180 5.2 181 184 2.9 191 2.1 202 2.2 2.2 2.2 2.2 2.2 2.2 2.2 2.2 2.2	9.9 200 8.9 200 7.9 206 7.9 206 190 5.5 186 4.7 184 4.0 186 3.5 191 3.2 204 3.3 3.3	20 12.9 225 11.2 225 9.7 7.224 6.3 224 6.5 224 6.5 225 5.9 227 5.8 228 228 228 230 5.0 6.2 24 4.3 4.4 4.6 5.8 5.8 5.8 5.8 5.8 5.8 5.8 5.8 5.8 5.8	30 9.11 9.3 245 9.5 246 9.6 246 9.6 245 9.6 242 8.9 8.2 236 6.2 6.2 6.3 6.6 6.2 6.3 6.3 6.3 6.3 6.3 6.3 6.3 6.3	40 14.3 35 7.9 29 2.3 3.3 3.7 254 4.1 241 2.3 263 2.5 251 1.3 263 2.5 259 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5	5.8 214 6.3 218 6.9 221 7.4 223 7.9 224 8.1 225 6.2 224 7.4 224 6.8 224 6.8 224 6.8	60 6.6 259 7.2 258 7.9 257 7.6 252 7.6 252 4.7 6.0 242 235 4.7 4.7 4.4 4.2 4.4	70 8.1 235 7.5 233 6.8 231 6.1 228 4.9 226 4.9 226 4.9 228 3.9 229 3.9 229 3.9 227 3.2 224 228 228	5.2 218 4.8 218 4.4 215 4.0 218 3.7 3.4 215 3.1 217 3.1 3.1 2.8 3.2 213 3.0 219 2.8 230 2.7 239
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 8.0 7.5 7.0	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603	-80 10.9 279 10.3 287 9.66 298 8.66 298 4.0 276 330 5.66 295 4.0 276 276 277 278 278 278 278 278 278 278 278 278	13.7 510 14.0 523 14.5 334 14.6 350 12.0 356 9.0 3 1.2 9.0 14.0 1.2 9.0 14.0 1.2 9.0 14.0 1.2 9.0 14.0 14.0 14.0 14.0 14.0 14.0 14.0 14	HEIGHT -60 21.4 314 22.2 320 22.7 327 22.9 332 22.5 337 21.1 342 18.8 347 15.2 5.1 358 0.4 359 6.0 185 6.3	21.2 315 21.8 315 321 21.8 325 21.1 332 20.1 332 20.1 334 115,3 345 11.9 350 8.7 357 559 2.8	TUDE (-40	dam) A -30 16.3 172 17.1 176 17.5 178 17.0 181 12.9 9.3 196 213 3.0 8 4.0 0 334 4.0 0 334 3.4 3.4 3.4	-20 12.7 164 14.3 164 15.5 164 15.8 165 165 10.4 168 6.8 6.8 1.73 5.5 186 1.8 223 1.8 225 2.1 265 265 265 265 265 265 265 265 265 265	9.9 170 10.8 689 11.4 168 11.4 168 10.8 168 9.4 168 9.4 168 17.3 170 4.8 187 1.7 2.6 187 1.7 2.2 2.0 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3	6.2 189 6.4 185 6.6 6.4 180 180 180 181 4.1 184 2.9 1.9 1.9 2.0 2.0 2.2 2.2	10 9.9 210 8.9 206 7.0 195 5.5 186 4.7 184 4.0 186 3.5 191 3.2 198 3.2 198 3.3 208 3.3 3.3 3.3 3.3 3.3 3.3 3.3 3.	20 12.9 225 11.2 225 9.7 224 6.5 224 6.5 224 6.1 225 5.9 5.2 4.8 235 4.8 235 4.8	30 9.11 245 9.3 245 9.6 246 9.6 245 9.6 244 9.3 242 8.2 239 8.2 239 6.6 6.2 6.6 6.2 6.6 6.6 6.6 6.6	40 14.3 35 7.9 29 2.3 343 3.7 254 15.5 239 4.1 241 1.3 251 1.3 263 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.	50 5.8 214 6.3 218 6.9 221 7.4 225 7.9 224 7.9 224 7.9 224 6.8 224 6.8 224 6.1 226 6.1 5.9	60 6.6 259 7.2 258 7.9 257 7.9 257 7.6 6.9 242 5.2 242 4.7 231 4.2 4.3 4.0	70 8.1 235 7.5 233 6.8 231 6.1 226 4.9 225 4.5 226 4.5 227 3.6 227 3.6 227 2.2 2.2 2.2 2.2 2.2 2.2 2.2 2.2 2.2	5.2 218 4.8 218 4.0 216 4.0 216 3.7 217 3.4 3.0 215 3.2 213 3.2 214 3.0 2.8 230 2.7 239 2.5 244
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 8.0 7.5 7.0	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603 0.9257	-80 10.9 279 10.3 287 9.6 294 8.6 6.9 7.3 300 5.6 295 4.0 276 5.6 212 7.8 28 7.8 295 10.9 205 10.9 205	13.7 310 14.0 523 14.5 334 14.6 343 13.8 9.0 0 12.0 3 5.0 14.0 12.0 14.0 14.0 14.0 14.0 14.0 14.0 14.0 14	HEIGHT -60 21.4 314 22.2 23.7 320 22.7 327 22.9 332 22.5 337 21.1 342 347 15.2 4.0 0.4 355 6.3 181 12.5	21.2 315 21.5 315 21.6 325 21.6 325 21.7 328 21.1 332 20.1 332 341 115.3 345 11.9 350 8.7 357 5.5 9	TUDE (-40	dam) A -30 16.3 172 17.1 17.6 17.5 178 17.18 15.6 184 12.9 189 3.196 5.4 3.08 4.0 3.56 4.0 3.34 3.4 3.4 3.4 3.4	-20 12.7 164 14.3 164 15.5 166 15.6 166 15.2 166 10.4 168 173 3.5 186 1.8 223 1.8 223 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1	9.9 170 10.8 169 11.4 168 10.8 10.8 168 9.4 168 7.3 170 4.8 174 1.7 2.9 2.0 2.3 1.9	6.2 189 6.4 185 6.6 182 6.8 180 6.9 180 6.9 180 6.9 180 6.9 180 6.9 19	10 9.9 210 8.9 200 7.0 195 6.2 190 186 4.7 184 4.0 186 3.5 191 3.2 204 3.3 3.3 211 3.2 3.3 3.3 3.3 3.3 3.3 3.3 3.3	20 12.9 225 11.2 225 9.7 224 6.5 224 6.1 225 5.9 227 5.8 228 4.8 238 4.8 238 4.8	30 9.1 245 9.3 245 9.6 246 9.6 245 9.6 247 9.3 249 239 8.2 236 6.2 6.6 246 6.1 246 6.1	40 14.3 35 7.9 29 29 3.43 3.7 254 15.5 239 4.1 241 1.3 251 1.3 253 253 253 253 253 253 253 253 253 25	50 5.8 21e 6.3 218 6.9 221 7.4 225 8.2 224 6.8 224 6.8 224 6.8 224 6.9 224 6.9 224 6.9 225 6.9 226 6.9 227 7.9 226 6.9 227 7.9 227 7.9 228 6.9 229 229 6.9 229 229 229 229 229 229 229 2	60 6.6 259 7.2 258 7.9 255 7.9 255 7.9 255 6.9 247 231 4.4 231 4.0 234 4.0 234	70 8.1 235 7.5 233 6.3 231 6.1 226 4.9 225 4.5 226 4.2 228 3.9 3.6 227 3.6 227 228 3.2 229 3.6 227 228 3.6 227 228 3.6 227 228 3.6 229 229 229 229 229 229 229 229 229 22	5.2 218 4.8 219 4.0 216 3.7 217 3.2 215 3.1 214 3.0 2.9 2.8 2.7 2.3 2.7 2.3 2.7 2.3 2.7 2.3 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 8.0 7.5 7.0 6.5 6.0	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603 0.9237 1.52 2.51	-80 10.9 279 10.3 287 9.6 294 8.297 9.6 298 7.3 300 5.6 6 295 5.6 6 212 7.8 205 11.0 205 12.3 206	NTIAL -70 13.7 310 14.0 523 14.5 534 13.8 550 12.0 356 5.0 14 1.2 91 4.7 174 4.8 182 11.4 186 14.1 16.5 189 18.4	HEIGHT -60 21.4 314 22.2 320 22.7 327 22.5 337 21.1 358 347 15.2 15.5 10.4 325 6.3 381 112.5 180 16.2	21.2 315 21.5 318 21.8 321 21.8 325 21.7 328 21.1 336 341 11.9 350 8.7 357 9.2 2.8 367 367 368 367 368 368 368 368 368 368 368 368 368 368	TUDE (-40 9.1 263 9.6 262 9.9 265 9.6 272 283 9.1 299 9.2 315 328 9.3 348 359 6.1 48 4.1	dam) A -30 16.3 172 17.1 176 17.5 178 178 181 15.66 184 12.9 9.3 196 5.4 213 3.0 326 4.0 326 4.0 326 334 3.4 2.2 351	-20 12.7 164 14.3 164 15.8 166 15.8 166 15.2 166 168 173 3.5 1.8 223 1.8 223 1.8 225 2.1 2.6 2.1 2.6 2.2 2.5 2.6 2.2 2.6 2.6 2.6 2.6 2.6 2.6 2.6 2.6	9.9 170 10.8 169 11.4 168 11.4 168 11.4 168 170 4.8 170 4.8 174 2.6 187 2.1 2.0 231 2.0 231 2.0 233 1.7	6.2 189 6.4 185 6.6 182 189 189 189 189 189 189 189 189 189 189	9.9 210 8.9 206 7.9 206 7.9 206 190 5.5 190 186 4.7 184 4.7 184 5.5 191 3.2 204 5.3 5.3 208 5.3 211 3.2 213	20 12.9 225 11.2 225 9,7 224 6.5 224 6.5 224 6.1 225 5.8 227 5.8 228 5.4 230 232 4.8 240 4 240 4 240 4 240 4 240 4 240 4 240 4 240 4 240 4 240 4 240 4 240 4 240 4 240 4 240 4 240 4 4 4 4	9.11 245 9.3 245 9.5 246 9.6 246 9.6 247 9.6 249 9.3 242 259 8.2 236 6.2 36 6.1 247 6.1 247 6.1 247 6.1 247 6.1 247 6.1 247 6.1 6.1 6.1 6.1 6.1 6.1 6.1 6.1 6.1 6.1	40 14.3 35 7.9 29 2.3 343 5.6 241 5.5 241 241 241 251 1.3 253 263 2.3 253 259 268 27 288 288 288 288 288 288 288 288 288	5.8 214 6.3 218 6.9 221 7.4 225 7.9 224 8.2 224 7.9 224 6.8 224 6.3 226 6.1 226 5.9 5.6 6.2 225 5.6 6.9	60 6.6 259 7.2 258 7.6 258 7.6 257 7.9 257 7.6 252 25, 22 25, 24, 231 4.2 233 4.0 234 4.3 3.9 235 3.6 3.6	70 8.11 235 7.5 233 6.8 231 1 228 4.9 225 226 4.9 227 228 3.9 229 3.6 227 224 2.8 2.2 224 2.8 2.2 2.2 2.2 2.2 2.2 2.2 2.2 2.2 2.2	5.2 218 4.8 219 4.0 219 4.0 218 3.7 3.4 215 3.1 2213 3.0 219 2.3 230 2.7 239 2.5 244 1.7 238
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 7.0 6.5 6.0 5.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603 0.9257 1.52 2.51	-80 10.9 279 10.3 287 9.6 298 6.6 298 6.6 298 6.7 3.0 5.6 6.7 5.6 6.7 6.6 209 11.0 205 12.3 205 13.6 206 14.5 208	NTIAL -70 13.7 310 14.0 323 14.5 334 6 343 15.0 350 12.0 0 14 1.2 91 4.7 174 8.4 186 14.1 187 16.5 189 18.4 193 18.4	HEIGHT -60 21.4 314 22.2 320 22.7 327 21.1 342 22.5 337 21.1 10.4 325 5.1 10.4 325 6.3 181 12.5 180 16.2 183 181 12.5 180	21.2 315 21.8 518 21.8 521 21.8 325 21.7 328 21.1 336 341 15.3 345 11.9 350 8.7 357 9 2.8 11.8 15.9 350 8.7 357 9 11.9 11.9 11.9 11.9 11.9 11.9 11.9 1	TUDE (-40 9.1 263 9.6 262 9.9 262 9.9 265 9.6 272 283 3.9 9.1 328 9.3 339 8.8 8.3 359 8.8 359 8.8 4.1 103 5.6	dam) A -30 16.3 172 17.1 176 17.5 178 181 15.6 184 12.9 9.3 196 5.4 213 3.0 0 326 4.0 334 3.4 341 2.2 351 0.7 40	ND PHA -20 12.7 164 14.3 164 15.5 164 15.5 165 166 10.4 168 173 3.5 186 2.1 263 2.1 264 2.5 2.3 249 2.3 249 2.1	9.9 170 10.8 169 11.4 168 11.4 168 11.4 168 17.3 170 2.6 17.7 2.13 1.7 2.9 2.0 2.3 1.9 2.3 1.9 2.3 1.9 2.3 1.9 2.3 1.9 2.3 1.9 2.9 2.9 2.9 2.9 2.9 2.9 2.9 2.9 2.9 2	6.2 189 6.4 185 6.6 6.6 180 5.2 189 191 2.1 202 208 2.2 208 2.2 211 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1	9.9 210 8.9 206 7.9 206 7.9 206 6.2 1190 186 4.7 184 4.0 186 5.5 191 3.2 204 8.3 3.2 211 3.2 2.2 2.2 2.2 2.2 2.2 2.2 2.2 2.2 2.2	20 12.9 225 11.2 225 9.7 224 6.5 224 6.1 225 5.9 227 5.8 8.3 228 5.4 6.1 225 5.9 227 5.8 8.3 8.3 8.3 8.3 8.3 8.3 8.3 8.3 8.3 8	9.1 245 9.3 245 9.5 246 9.6 246 9.6 247 9.3 242 8.2 236 7.3 239 6.6 236 6.6 246 6.1 244 6.1 244 6.1 245 8.2 245	40 14.3 3.5 7.9 2.3 3.4 3.7 2.5 4.1 2.3 2.5 1.1 2.3 2.5 2.5 2.3 4.5 2.5 2.5 2.5 2.5 2.5 2.5 2.5 2.5 2.5 2	50 5.8 214 6.3 218 6.9 221 7.9 224 7.9 224 7.9 224 7.9 224 7.9 224 7.9 224 7.9 224 7.9 224 7.9 224 7.9 224 7.9 224 7.9 224 7.9 224 7.9 224 7.9 224 7.9 224 7.9 225 7.9 226 7.9 227 7.9 228 7.9 229 7.9 7.9 7.9 7.9 7.9 7.9 7.9 7.	60 6.6 259 7.2 258 7.6 258 7.9 257 7.9 257 7.6 252 6.9 247 6.0 242 5.2 235 4.7 231 4.4 2313 4.0 234 5.2 235 5.3 3.6 237	70 8.1 235 7.5 233 6.8 231 1228 4.9 225 4.5 226 4.9 229 3.6 227 3.2 228 229 3.6 227 3.2 228 229 229 3.6 227 3.2 228 229 3.2 229 3.6 227 3.6 3.6 3.6 3.6 3.6 3.6 3.6 3.6 3.6 3.6	5.2 218 4.4 4.2 19 4.0 218 4.0 218 3.0 217 3.4 2.17 3.4 2.19 2.8 230 2.7 239 2.2 1.7 2.4 2.1 1.7 2.2 231 1.7 2.0 8 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 7.0 6.5 6.0 5.5 5.0	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603 0.9237 1.52 2.51 4.14 6.83	-80 10.9 279 10.3 287 9.6 294 8.6 8.6 298 7.3 3 3 207 5.6 297 5.6 298 298 298 298 298 298 298 298 298 298	NTIAL -70 13.7 310 14.0 523 14.5 534 14.6 5350 12.0 556 9.0 12.0 15.0 14.7 174 8.4 182 11.4 186 14.1 187 16.5 189 18.4 197 19.1	HEIGHT -60 21.4 314 22.2 22.7 320 22.7 327 22.9 332 22.5 337 21.1 342 22.5 357 15.2 4.0 0.4 355 5.1 358 0.4 185 180 16.2 183 181 12.5 180 16.2 183 181 18.3	AMPLI -50 21.2 315 315 21.6 325 316 327 326 21.1 332 20.1 336 18.2 20.1 350 8.7 357 4.6 130 8.3 152 10.8 163 152 10.8 163 152 10.8 163 152 10.8 163 11.6	TUDE (-40 9.1 263 9.6 262 9.9 262 9.9 265 9.6 272 9.2 283 339 9.1 299 9.2 283 339 8.8 839 6.1 15 4.1 48 4.1 103 5.6 6.1 134	dam) A -30 16.3 172 17.1 176 17.5 178 17.1 176 181 15.6 184 12.9 9.3 196 5.4 308 4.0 0 334 341 2 2 351 0.7 7 40 1.6 137	-20 12.7 164 14.3 164 15.5 164 15.2 165 13.4 166 6.8 8.7 173 1.8 223 1.8 223 1.8 266 2.1 266 2.1 266 2.1 266 2.2 2.2 2.2 2.2 2.2 2.2 2.2 2.2 2.2	9.9 170 10.8 169 11.4 168 10.8 168 7.3 170 125 125 127 229 2.0 233 1.9 25 1.7 211 1.4 219 1.2 1.4 219 1.2 1.4 219 1.2 1.4 219 1.2 1.4 219 1.2 1.4 219 1.2 1.4 219 1.2 1.4 219 1.2 1.4 219 1.2 1.4 219 1.2 1.4 219 1.2 1.4 219 1.2 1.2 1.4 219 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2	6.2 189 6.4 185 6.6 182 6.4 180 180 180 180 180 2.2 181 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.	9.9 210 8.9 206 7.9 200 7.9 200 5.5 186 4.7 184 4.0 186 3.5 191 3.2 198 3.2 204 3.3 211 3.2 212 2.2 22 22 22 22 22 22 22 22 22 22 22 22	20 12.9 225 11.2 225 9.7 224 6.5 224 6.5 227 5.8 228 6.1 225 5.9 227 5.8 230 5.0 6.1 235 4.8 235 235 235 235 235 235 235 235	9.11 245 9.3 245 9.5 246 9.6 246 9.6 244 8.9 9.6 242 236 6.1 247 5.8 8.2 242 6.1 244 6.1 245 6.1 246 7 8 7 8 7 8 7 8 7 8 7 8 8 7 8 7 8 7 8	40 14,3 35 7,9 2,3 343 35,5 5,6 241 241 2,3 251 1,3 253 259 4,5 250 259 260 27 27 27 27 27 27 27 27 27 27 27 27 27	50 5.8 216 6.3 218 6.9 221 7.9 224 8.1 225 224 7.4 224 6.3 226 6.1 225 5.9 225 5.9 225 5.9 224 4.7 225 5.9 226 6.9 227 6.9 6.9 6.9 6.9 6.9 6.9 6.9 6.9	60 6.6 259 7.2 258 7.6 258 7.9 257 7.6 252 4.7 231 4.2 4.3 4.0 234 4.0 235 3.6 3.7 3.7 3.7 3.7 3.7 3.7 3.7 3.7	70 8.1 235 7.5 233 6.8 231 1.28 5.4 4.9 226 4.9 227 3.6 227 3.6 227 3.6 227 3.6 227 3.6 227 3.6 228 229 229 220 221 221 221 222 231 231 241 251 261 271 272 273 274 275 275 275 275 275 275 275 275	5.2 218 4.8 4.8 218 4.4 219 4.16 216 5.7 217 3.4 215 3.14 3.00 2.19 2.8 230 2.5 244 2.1 242 2.1 242 2.1 242 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 8.0 7.5 6.0 5.5 5.0 4.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603 0.9237 1.52 2.51 4.14 6.83	-80 10.9 279 10.3 287 9.6 294 6 298 7.3 3.0 276 3.8 297 5.6 297 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	NTIAL -70 13.7 310 14.0 523 14.5 534 14.5 334 15.8 350 12.0 3 550 14 1.2 91 1.4 186 14.1 186 14.1 187 189 19.4 191 19.1 203	HEIGHT -60 21.4 314 22.2 320 22.7 327 337 21.1 342 15.2 357 15.2 357 16.8 347 15.2 16.8 355 181 10.4 12.5 180 16.2 183 18.7 194 18.7	AMPLI -50 21.2 315 518 21.8 321 21.8 325 21.7 328 21.1 336 18.2 20.1 336 18.2 20.1 536 18.2 11.9 350 6.7 357 6.5 5 9 9 2.8 6.5 10.8 8 163 311.6 173 11.6 173	TUDE (1 -40 -40 -40 -40 -40 -40 -40 -40 -40 -40	dam) A -30 16.3 172 17.1 17.6 17.5 178 17.8 181 15.6 184 12.9 3.1 96 5.4 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0	-20 12.7 164 14.3 164 15.5 164 15.5 165 166 168 6.8 173 3.5 186 1.8 223 1.8 226 2.1 265 2.4 264 261 27 2.0 198	9.9 170 10.8 169 11.4 168 10.8 168 170 4.8 170 2.6 187 1.7 213 1.7 229 2.0 231 1.4 2.6 187 221 1.7 211 2.0 2.1 1.7 211 2.0 2.1 1.7 211 2.0 2.1 1.7 211 2.0 2.1 1.7 211 2.0 2.1 1.7 2.1	6.2 189 6.4 185 6.6 182 6.4 180 6.0 180 180 180 2.9 208 2.2 211 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1	9.9 210 8.9 200 7.9 200 7.9 200 195 6.2 190 5.5 186 4.7 184 4.0 186 3.5 191 3.2 204 3.3 3211 3.2 213 2.2 223 2.2 223 2	20 12.9 225 11.2 225 9.7 224 6.5 224 6.5 227 5.8 228 5.4 230 232 4.8 238 240 4.5 239 4.8 240 4.2 255 5.4 255 5.5 5.5 5.5 5.5	9.11 245 9.3 245 9.5 246 9.6 246 9.6 247 9.3 242 8.9 9.3 233 6.2 236 6.1 246 6.1 247 7.3 248 6.1 248 748 748 748 748 748 748 748 748 748 7	40 14,3 35 7,9 29 2,3 343 35,5 5,6 241 241 2,5 2,5 2,5 2,3 2,3 2,3 2,3 2,3 2,3 2,3 2,3 2,3 2,3	50 5.8 21e 6.3 21e 6.9 221 7.9 224 8.1 225 7.9 224 7.4 24 26.8 224 7.4 24 25 5.9 225 5.9 225 5.9 225 5.9 226 5.9 227 5.9 6.9 6.9 6.9 6.9 6.9 6.9 6.9 6	60 6.6 259 7.2 258 7.6 258 7.9 257 7.9 247 6.0 242 235 4.7 231 4.2 233 4.0 234 4.7 233 4.0 234 235 235 235 237 237 237 237 237 237 237 237 237 237	70 8.1 235 7.5 233 6.8 231 1.228 5.4 4.9 225 226 4.9 227 228 3.9 229 3.6 227 224 228 228 229 229 3.6 227 228 228 229 3.6 227 228 228 229 3.6 227 228 228 229 3.6 229 3.7 3.7 3.7 3.7 3.7 3.7 3.7 3.7	5.2 218 4.4 219 218 4.0 218 3.0 218 3.0 218 3.0 218 3.0 219 2.8 229 2.7 239 2.7 239 2.7 231 0.5 244 2.1 1.7 2231 0.5 218 218 218 218 218 218 218 218 218 218
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 7.0 6.5 6.0 5.5 5.0 4.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603 0.9237 1.52 2.51 4.14 6.83 11.25	-80 10.9 279 10.3 287 9.6 298 8.6 298 8.6 298 8.6 298 8.7 3 300 5.6 29 205 10.3 205 11.0 205 12.3 205 11.0 12.3 205 11.0 12.3 205 11.0 12.3 205 11.0 12.3 205 11.0 12.3 205 11.0 12.3 205 12.3 205 12.3 206 14.5 208	NTIAL -70 13.7 310 14.0 523 14.5 334 6343 13.6 343 13.6 9.0 14 1.2 91 14.7 174 6.4 186 14.1 187 16.5 189 18.4 193 19,4 197 19.1 203	HEIGHT -60 21.4 314 22.2 23.2 22.7 327 21.1 342 353 22.5 357 21.1 10.4 325 5.1 10.4 325 6.3 181 12.5 180 16.2 183 187 18.7 194	21.2 315 21.8 521 518 21.8 521 21.8 325 21.7 328 21.1 336 341 15.3 345 11.9 2.8 341 15.3 355 8.7 357 8.7 8 8.7 8 8 8 8 8 8 8 8 8 8 8 8 8 8	TUDE (-40 9.11 263 9.66 262 9.99 265 9.69 272 9.22 315 9.51 328 9.33 8.8 359 6.11 15 4.11 103 6.7 149	dam) A -30 16.3 172 17.1 176 17.5 178 181 15.6 184 12.9 9.3 196 5.4 213 3.0 326 4.0 334 3.4 341 2.2 259 1.6 137 3.1 149	ND PHA -20 12.7 164 14.3 164 15.5 164 15.5 165 166 10.4 168 173 3.5 186 2.1 263 2.1 264 2.5 2.2 2.3 2.4 2.5 2.6 2.7 2.7 2.9 2.9 2.9 2.9 2.9 2.9 2.9 2.9	-10 9.9 170 10.8 169 11.4 168 10.8 168 10.8 168 17.4 1.7 1.7 2.7 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1	6.2 189 6.4 185 6.6 6.180 6.2 189 6.4 180 6.2 180 180 180 180 180 180 180 180 180 180	9.9 210 8.9 206 7.9 206 7.9 206 6.2 1190 186 4.7 184 4.0 186 5.5 122 204 3.3 208 3.3 208 2.1 2.9 212 2.9 212 2.9 212 2.9 208 2.4 4.0 200	20 12.9 225 11.2 225 9.7 224 6.5 224 6.5 224 6.1 225 5.9 227 5.8 235 4.8 235 4.8 235 4.8 239 5.8 239 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	9.1 245 9.3 245 9.5 246 9.6 246 9.3 242 9.3 242 8.2 236 6.6 6.1 244 6.1 244 6.1 244 6.1 244 6.1 244 6.1 244 6.1 245 245 246 6.1 245 245 245 245 245 245 245 245 245 245	40 14.3 7.9 29 2.3 3.7 254 5.5 6.6 6.2 239 4.1 241 251 1.3 251 1.3 253 4.5 253 4.5 253 4.5 253 4.5 253 253 253 253 253 253 253 25	50 5.8 214 6.3 218 6.9 221 7.9 224 8.1 225 6.2 224 7.4 224 6.3 226 6.3 226 5.9 22 5.6 22 5.2 224 5.2 224 5.2 224 6.3 226 5.9 225 5.0 225	60 6.6 259 7.2 258 7.6 258 7.9 257 7.9 257 7.9 242 252 242 233 4.0 234 4.2 233 4.0 234 235 3.6 237 238 238 238 238 238 238 238 238	70 8.1 2355 7.5 233 6.8 231 1228 4.9 225 4.5 226 4.9 227 3.2 228 3.9 229 3.6 227 3.2 228 229 3.6 227 3.2 228 229 3.6 227 3.7 3.7 3.7 3.7 3.7 3.7 3.7 3.7 3.7 3.	5.2 218 4.8 4.8 218 4.4 219 4.16 216 5.7 217 3.4 215 3.14 3.00 2.19 2.8 230 2.5 244 2.1 242 2.1 242 2.1 242 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1

										O		UU	" "	LON	IL:	1		
JUNE		TEMPERA						WAVE	7.00							-		
SCALE	PRESSURE (mb)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
12.0	0.0062	0.81	0.66	0.57	0,62	1.04	0.82	0.55	0,70	0.42	0.24	0.46	0.30	3,53	0.33	0.58	0.41	0.30
11.5	0,0103	0.71	0.58	0.51	0,61	1.07	0.84	0.54	0.71	0.39	0.23	0.43	0.30	3.99	0.37	0.60	0.47	0.36
11.0	0.0169	0.54	0.44	0.41	0.57	1.05	0.83	0.51	0,65	0.30	0.22	0.36	0.26	3.26 278	0.37	0.54	0.48	0.37
10.5	0,0279	0.32	0.27	0.28	0.49	0.99	0.79	0.45	0.54	0.14	0.23	0.24	0.19	2.04	0.34	0.37	0.43	0.35
10.0	0,0460	0,17	0.17	0.15	0.40	0.88	0.75	0.40	0.39	0.04	0.26	0.17	0.12	0.94	0.27	0.16	0.32	0.27
9.5	0.0758	0.29	0.24	0.11	0.28	0.69	0.70	0.35	0,21	0.23	0.31	0.25	0.08	0.11	0.20	0.37	0.14	0.13
9.0	0,1250	0.48	0.31	0.10	0.15	0.39	0,60	0.31	0.16	0.37	0.35	0.35	0.11	0.53	0.17	0.64	0.07	0.07
8.5	0,2061	0.58	0.27	0.04	0.05	0.22	0.45	0.28	0.34	0.37	0.25	0.33	0.15	0.41	0.18	0.67	0.19	0.24
8.0	0,3398	0.59	0.16	0.10	0.19	0.78	0.53	0.35	0.52	0.25	0.10	0.23	0.24	0.51	0.17	0.44	0.20	0.36
7.5	0.5603	0.41	0.17	0.30	0.14	0.90	0.57	0.32	0.44	0.20	0.16	0.18	283 0.28 297	1.46 274	353 0.12 316	0.05	0.08	0.30
7.0	0.9237	0.25	0.27	0.44	0.20	0.69	0.49	0.28	0.29	0.23	0.21	0.16	0.22	1,42	0.15	0.24	0.02	0.16
6.5	1.52	0.13	0.29	-	0.68	0.88	0.59	0.25	0.13	0.12	0.12	0.03	0.15	0,58	0.16	0.18	0.03	0.03
6.0	2,51	0.23	0.33	0.75	1.26	1,66	1.24	0.56	0.14	0.06	0.05	0.14	0.19	0.16	0.17	0.11	0.08	0.08
5,5	4.14	0.24	0.38	0.71	1.20	1.68	1.34	0,67	0.19	0.10	0.09	0.25	0.27	0.25	0.22	0.12	253 0.12 238	0.10
5.0	6.83	0.14	0,42	0.56	0.84	1.29	1.13	0.64	0.22	0.14	0.14	0.35	0.36	0.34	0,29	0.12	0.16	0.13
4.5	11,25	0.13	0.48	0.41	0.35	0.63	0.68	0.48	0.22	0.17	0.17	0.43	0.43	0.42	0,35	0.11	0.19	0.14
4.0	18,55	0,43	0.48	0.46	0.33	0.19	0.36	0.30	0.19	0.17	0.19	0.46	0.46	0.46	0.38	0.10	0.19	0.15 200
3.5	30.59	0.58 348	0.39	0.53	0.55	0,52	0.49	0,23	0.14	0.17	0.18	0.44	350	334 0,43 335	356 0,35	0.08	0,17	0.13
3.0	50,43	0.50	0.25	0.47	0.60	0,68	0,63	0.28	0.09	0.14	0.16	0.39	352 0.38	0.37	0.30	0.06	0.14	0.11
2.5	83,15	0.34	0.14	0.34	192	0,62	265 0.58	0.27	0.05	0.10	0.12	0.29	0,29	0.27	0.21	0.04	0,09	0.07
		346	49	150	195	241	259	270	18	63	22	360	352	336	5	337	215	200
JUNE		GEOPOTE			-		(dam) A			AVE 2								
HEIGHT	(mb)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
12.0	0.0062	2.3	5.3	8.2	11.0	13.9	10.8	3.6	1.8	1.7	3.5 52	3.2	4.7 327	23.1	3.8	73	2.5	2.2
11.5	0.0103	3.3	4.4	7.4	10.1	12.6	10.8	4.3	1.9	2.1	3.2	3.2	4.3	17.6 284	3.6 322	1.6	1.9	1.9
11.0	0.0169	192	3.6	6.7	9.3	11.4	10.8	4.9	2.4	2.5	2.9	3.2	3.9 326	12.1	3.4 330	1.5	1.2	1.5
10.5	0.0279	4.7	3.1	6.3	8.5	10.5	10.8	5.4 32	3.0	2.8	2.6	3.3	3.6 326	8,4	3.3	1.6	0.6	1.3
10.0	0.0460	4.9	2.9	6.0	8.0 52	9.8	10.6	5.8	3,5	2.9	2.2	3.2	3.3	6.2	3.2	1.6	0.4	1.3
9.5	0.0758	202	3.0	5.9	7,5	9.6	10.3	6.1	3,8	2.8	1.8	2.9	3.2 327	5.5	3.1	1.3	0.5	1.4
9.0	0.1250	4.2	3.3	6.0	7.3	9.6	9.8	6.1	3.8	2.5	1.5	2.5	3.2	5.9	2.9	0.6	0.6	1.4
8.5	0.2061	3.4 206	3.7	6.1	7.1	9.8	9.2	5.9	3.5	2.1	1.3	2.1	3.2	6.6	2.7	0.7	0.4	1.2
8.0	0.3398	2.6	4.0	6.0	7.1	10.1	8,6	5.5	2.9	1.7	1.1	1.9	3.1 338	6.6	2.4 358	1.5	0.2	0.9
7.5	0.5603	1.9	4.0	5.8	7.2	10.4	8.3	5.1	2.3	1.4	1.0	2.1	2.8	5.2 295	2.2	1.7	0.3	0.6
7.0	0,9237	1.7	3.9	5.3	7.1	10.5	8.3	5.0	2.0	1.3	1.0	2.4	2.5	3.2	2.1	1,5	0.4	0.6
6.5	1,52	1.6	3,6	4.7	6.5	9.8	7.9	4.8	1.9	1.3	1.1	2.5	2,4 354	2.2	2.1	1.2	0.3	0.6
6.0	2,51	1.4	3.3	4.0	5.3	8.0	6.6	4.3	1.9	1.3	1.1	2.4	2.2	1.9	2.0	1.1	0.3	0.5
5.5	4.14	1.0	3.0	3.1 58	3.9	5.5	4.7	3,4	1.6	1.1	1.0	2.1	1.9	1.6	1.8	1.1	0.3	0.4
5.0	6,83	0.7	2.7	2.4	2.9	3.3	2.9	2.4	1.3	1.0	0.8	1,7	1.4	1.2	1,6	1.1	0.3	0.3
4.5	11.25	0.7	2.4	1.8	2.4	2.0	1,6	1,6	1.0	0.8	0.6	1.2	0.9	0.7	1.3	1.1	0.5	0.3
4.0	18,55	1.1	2.2	1.2	2.1	1.6	1.0	1.1	0.7	0.5	0.4	0.6	0.5	0.4	1.1	1.1	0.7	98 0.4 63
3.5	30,59	1.9	2.1	1.0	1.9	2.1	1.3	0.9	0.5	0.3	0.4	0.4	0.7	0.8	1.1	1.2	1.0	0.5
3.0	50.43	2.7 173	2.2 145	1.4	2.2	3.0 70	2.1	1.1	0.3	0.2	0.5	0.9 157	132 1.2 151	1.4	1.2	1.2	1.2	0.7
2.5	83.15	3.3 172	2.2 152	1.9	2.8	4.0	3.0	1.4	0.3 82	0.2	0.6 165	1.4	1.7	1.9	1.5	1.2	1.3	0.8
		172	152	334	22	66	81	74	62	203	100	100	157	145	137	84	53	38

	MEAN 1	EMPERA	TURE A	MPLITU	OE (K)	AND P	HASE	MAVE	1									
SCALE	PRESSURE (mb)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
12.0	0.0062	1.04	1,68	2.16	1.98	1.43	0.78	0.55	0.28	0.57	0.54	0.34	0.67	0.64	0.24	0.22	0.49	0.13
11.5	0.0103	0.96	1,61	2.18	1.89	1.30	0.69	0,41	0.22	0.33	0.57	0.34	0.69	0,68	0.25	0.23	0.57	0.14
11.0	0.0169	0.87	1,45	2.11	1.75	1.20	0.67	0.15	0.13	0.31	0.59	0.33	0,65	0,69	0.26	0.23	0.60	0.13
10.5	0.0279	0.93	1.28	2.03	1.80	1,42	0.97	0.24	0.,02	0.29	0.57	0.29	0.56	0.67	0.25	0.22	0.56	0.11
10.0	0.0460	1,18	1,21	1,99	2.16	2.07	1,55	0.73	0.20	0.36	0.55	0.25	0.45	0.59	0.22	0.24	0.46	0.07
9.5	0.0758	1,51	1,28	1,92	2,57	2.84	2.18	1.22	0.39	0,46	0.53	0.22	0.37	0.48	0.20	0,34	0.28	0.08
9.0	0.1250	1.80	1,52	1.85	2.70	3,29	2,61	1.53	0.54	0.50	0.47	0.26	0.37	0.33	0.17	0.43	0.12	0.13
8.5	0.2061	1.96	1.96	2.16	2,44	3,12	2,55	1,47	0.56	0.38	0.38	0.38	0.46	0.29	0.24	0.45	0.16	0.12
8.0	0.3398	1,99	2.59	3,22	2,63	2,52	2.09	1.05	0.43	0.25	0.37	0.53	0.55	0.47	0.41	0.33	0.31	0.06
7.5	0.5603	1.84	3,07	4.11	3,35	2.53	1.81	0.75	0.17	0.32	0.32	0.51	0.55	0,60	0.51	0.11	0.35	0.09
7.0	0.9237	1.95	3.77	5.07	4,46	3,11	1.71	0,60	0.09	0.32	0.25	0.40	0.47	0.55	0,49	0.18	0.30	0.09
6.5	1,52	2,43	4.73	6.28	6.08	4,47	2.23	0.63	0.16	0.19	0.13	0.25	0.34	0.38	0,36	0.27	0.23	0.08
6.0	2,51	3.17	5.79	7.68	8.24	6.52	3,39	1.07	0.23	0.12	0.07	0.14	0.23	0.25	0.27	0.26	0.22	0.20
5.5	4,14	3,04	5.89	8.10	9.11	7.33	3,99	1,42	0.32	0.13	0.08	0.05	0.20	0.23	0.27	0.21	0.26	0.31
5.0	6.83	2.51	5.33	7.49	8.48	6.66	3.75	1,47	0.37	0.15	0.13	0.29	0.43	0.33	0.30	0.27	0.36	0.40
4,5	11,25	1.52	4.06	6.01	6.59	4.79	2.64	1.21	0.38	0.18	0.19	0.56	0.76	0.53	0.34	0.44	0,50	0.46
4.0	18.55	1.13	2.84	4.90	5.02	3.19	1,35	0.80	0.35	0.20	0.23	0.76	1,02	0.71	0.38	0,61	0.60	0,47 263
3.5	30,59	2.46	3.09	4,61	4,52	2.84	0,67	0.48	0.30	0.19	0.24	0.83	1.11	0.78 256	0.37	0.67	0.63	0.43
3.0	50,43	2,34	3.10	4.13	4.20	2.96	1.00	0.39	0.24	0.17	0.22	0.80	1.08	0.75	0.32	0,61	0.55	0.35
		202	102	140	100						0.17	0,65	0.88	0.59		0.45	0.40	0.24
2.5	83,15	207	193	159	3.32 147	146	1.09	239	299	301	279	257	253	257	283	318	287	244
JULY	MEAN (207 EOPOTE	193	159 HEIGHT	147	TUDE (161 dam) A	239 ND PHA	299 SE #	301 AVE 1	279	257	253	257	283	318	287	244
JULY		207	193	159	147	146	161	239	299	301								80
JULY	MEAN (207 EOPOTE	193	159 HEIGHT	147	TUDE (161 dam) A	239 ND PHA	299 SE #	301 AVE 1	279	257	253	257	283	318	287	244
JULY SCALE HEIGHT	MEAN (PRESSURE (mb)	207 EOPOTE -80 22.6	193 NTIAL -70 26.4	159 HEIGHT -60	147 AMPL1 -50 34.5	146 TUDE (-40	161 dem) A -30	239 ND PHA -20 3.3	299 SE + -10	301 AVE 1 0	10	20 7.2	253	40	50	60	70	80
JULY SCALE HEIGHT 12.0	MEAN (PRESSURE (mb) 0.0062	207 EOPOTE -80 22.6 37 23.6	193 NTIAL -70 26.4 39 28.8	159 HEIGHT -60 31.3 32 33.9	147 AMPLI -50 34.5 31 35.1	146 TUDE (-40 21.1 0 21.5	161 dem) A -30 7.8 316 8.4	239 ND PHA -20 3.3 269 3.2	299 SE * -10 0.3 172 0.6	301 AVE 1 0 3.6 197 3.2	10 7.7 203 6.9	257 20 7.2 222 7.1	30 8.8 244 9.2	40 9.7 257 9.6	50 10.2 238 9.8	60 6.9 241 6.9	70 4.8 200 4.5	80 3.5 268 3.4
JULY SCALE HEIGHT 12.0	PRESSURE (mb) 0.0062 0.0103	207 -80 22.6 37 23.6 40 24.2	193 NTIAL -70 26.4 39 28.8 39 31.0	159 HEIGHT -60 31.3 32 33.9 29 36.8	147 AMPLI -50 34.5 31 35.1 27 36.4	146 TUDE (-40 21.1 0 21.5 355 22.4	161 dam) A -30 7.8 316 8.4 309 9.2	239 ND PHA -20 3.3 269 3.2 256 3.3	299 SE * -10 0.3 172 0.6 166 0.9	301 AVE 1 0 3.6 197 3.2 202 2.9	10 7,7 203 6,9 203 6,0	257 20 7,2 222 7,1 218 7,1	30 8.8 244 9.2 238 9.6	257 40 9,7 257 9,6 252 9,5	50 10.2 238 9.8 237 9.5	60 6.9 241 6.9 244 6.9	70 4.8 200 4.5 209 4.3	80 3.5 268 3.4 270 3.2
JULY SCALE HEIGHT 12.0 11.5	MEAN (PRESSURE (mb) 0.0062 0.0103 0.0169	207 SEOPOTE -80 22.6 57 23.6 40 24.2 43 24.3	193 NTIAL -70 26.4 39 28.8 39 31.0 39 32.9	159 HEIGHT -60 31.3 32 33.9 29 36.8 27 39.8	147 AMPLI -50 34.5 31 35.1 27 36.4 23 38.5	146 TUDE (-40 21.1 0 21.5 355 22.4 351 24.2	7.8 316 8.4 309 9.2 306	239 ND PHA -20 3.3 269 3.2 256 3.3 249 3.3	299 SE * -10 0.3 172 0.6 166 0.9 164 1.0	301 0 3.6 197 3.2 202 2.9 208 2.4	10 7.7 203 6.9 203 6.0 203 5.2	20 7.2 222 7.1 218 7.1 214 7.0	30 8.8 244 9.2 238 9.6 233 9.9	257 40 9.7 257 9.6 252 9.5 246 9.6	283 50 10.2 238 9.8 237 9.5 236 9.2	60 6.9 241 6.9 244 6.9 246 6.9	70 4.8 200 4.5 209 4.3 220 4.4	3.5 268 3.4 270 3.2 273 3.1
JULY SCALE HEIGHT 12.0 11.5 11.0	MEAN (PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279	207 207 207 207 206 37 23.6 40 24.2 43 24.3 46 25.7	193 NTIAL -70 26.4 59 28.8 39 31.0 39 32.9 40 34.3	159 HEIGHT -60 31.3 32 33.9 29 36.8 27 39.8 27 42.7	147 AMPLI -50 34.5 31 35.1 27 36.4 23 38.5 21 41.4	146 TUDE (-40 21.1 0 21.5 355 22.4 351 24.2 350 26.6	7.8 316 8.4 309 9.2 306 10.4 308 11.8	239 ND PHA -20 3.3 269 3.2 256 3.3 249 3.3 250 3.4	299 SE * -10 0.3 172 0.6 166 0.9 164 1.0 162 0.8	301 AVE 1 0 3.6 197 3.2 202 2.9 208 2.4 212 1.9	10 7.7 203 6.9 203 6.0 203 5.2 202 4.4	257 20 7.2 222 7.1 218 7.1 214 7.0 210 6.9	30 6.8 244 9.2 238 9.6 233 9.9 228 10.2	257 40 9.7 257 9.6 252 9.5 246 9.6 240 9.7	283 50 10.2 238 9.8 237 9.5 236 9.2 235 8.9	60 6.9 241 6.9 244 6.9 246 6.9 249	70 4.8 200 4.5 209 4.3 220 4.4 231 4.7	3.5 268 3.4 270 3.2 273 3.1 275 3.0
JULY SCALE HEIGHT 12.0 11.5 11.0 10.5	MEAN (PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279	207 207 200°0TE -80 22.6 37 23.6 40 24.2 43 24.3 46 25.7 49 22.5	193 NTIAL -70 26.4 39 28.8 39 31.0 32.9 40 34.3 42 35.1	159 HEIGHT -60 31.3 32 33.9 29 36.8 27 39.8 27 42.7 27 45.2	147 AMPLI -50 34.5 31 35.1 27 36.4 23 38.5 21 41.4 20 44.7	146 TUDE (-40 21.1 0 21.5 355 22.4 351 24.2 350 26.6 351 29.8	7.8 316 8.4 309 9.2 306 10.4 508 11.8 313 13.9	239 ND PHA -20 3.3 269 3.2 256 3.3 249 3.3 250 3.4 262 3.8	299 SE * -10 0.3 172 0.6 166 0.9 164 1.0 162 0.8 159 0.4	3.6 197 3.2 202 2.9 208 2.4 212 1.9 214	7.7 203 6.9 203 6.0 203 5.2 202 4.4 200 3.6	257 20 7.2 222 7.1 218 7.1 214 7.0 210 6.9 207 6.7	30 8.8 244 9.2 238 9.6 233 9.9 228 10.2 224	9.7 257 9.6 252 9.5 246 9.6 240 9.7 234 9.9	283 50 10.2 238 9.8 237 9.5 236 9.2 235 8.9 234 8.7	60 6.9 241 6.9 244 6.9 246 6.9 245 6.7 251 6.3	70 4.8 200 4.5 209 4.3 220 4.4 231 4.7 240 5.0	3.5 268 3.4 270 3.2 273 3.1 275 3.0 276
JULY SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0	MEAN (PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758	207 206 22.6 37 23.6 40 24.2 43 24.3 46 25.7 9 22.5 53 20.7	193 NTIAL -70 26.4 39 28.8 39 31.0 39 32.9 40 34.3 45 35.1 45	159 HEIGHT -60 31.3 32 33.9 29 36.8 27 39.8 27 42.7 45.2 29 46.9	147 AMPLI -50 34.5 31 35.1 27 36.4 23 38.5 21 41.4 20 44.7 22 48.0	146 TUDE (-40 21.1 0 21.5 355 22.4 351 24.2 350 26.6 351 29.8 354 33.5	161 dam) A -30 7.8 316 8.4 309 9.2 306 10.4 308 11.8 313.9 321 16.4	239 ND PHA -20 3.3 269 3.2 256 3.3 249 3.3 250 3.4 262 3.8 284 5.0	299 SE W -10 0.3 172 0.6 166 0.9 164 1.0 162 0.8 159 0.4 149 0.3	301 0 3.6 197 3.2 202 2.9 208 2.4 212 1.9 210 0.5	279 10 7.7 203 6.9 203 6.0 203 5.2 202 4.4 200 3.6 197 2.9	257 20 7.2 222 7.1 218 7.1 214 7.0 210 6.9 205 6.7	30 8.8 244 9.2 238 9.6 233 9.9 228 10.2 221 221 9.8	257 40 9.7 257 9.6 252 9.5 246 9.6 240 9.7 234 9.9 230 9.9	283 50 10.2 238 9.8 237 9.5 236 9.2 235 8.9 234 8.7 232 8.6	518 60 6.9 241 6.9 244 6.9 246 6.9 249 6.7 251 6.3 253 5.7	70 4.8 209 4.3 220 4.4 231 4.7 240 5.0 245 5.3	80 3.5 268 3.4 270 3.2 273 3.1 275 3.0 276 2.9 2.75
JULY SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5	MEAN (PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250	207 22.6 57 23.6 40 24.2 43 24.5 46 25.7 49 22.5 53 20.7 58 18.4	193 NTIAL -70 26.4 59 28.8 59 51.0 59 40 34.3 42 35.1 45 35.1 45 35.8	159 HEIGHT -60 31.3 32 33.9 29 36.8 27 39.8 27 42.7 27 45.2 29 46.9 32 47.1	147 AMPLI -50 34.5 31 35.1 27 36.4 23 38.5 21 41.4 20 44.7 22 48.0 24 50.3	146 TUDE (-40 21.1 0 21.5 355 22.4 351 24.2 350 26.6 351 29.8 354 33.5 359	161 dam) A -30 7.8 316 8.4 309 9.2 306 10.4 308 11.8 313 13.9 321 16.4 331 19.1	239 ND PHA -20 3.3 269 3.2 256 3.3 249 3.3 250 3.4 262 3.8 284 5.0 6.7	299 SE -10 0.3 172 0.6 166 0.9 164 1.0 162 0.8 159 0.4 149 0.3 14	301 0 3.6 197 3.2 202 2.9 208 2.4 212 1.9 214 1.2 210 0.5 189 0.4	279 10 7.7 203 6.9 203 6.0 203 5.2 202 4.4 200 5.6 197 2.9 2.3	257 20 7.2 222 7.1 218 7.1 210 6.9 207 6.7 205 6.4 204 6.0	253 30 8.8 244 9.2 238 9.6 233 9.9 228 10.2 224 10.1 221 9.8 218 9.3	257 40 9.7 257 9.6 252 9.5 246 9.7 234 9.9 230 9.9 226 9.7	283 50 10.2 238 9.8 237 9.5 236 9.2 235 8.9 234 8.7 232 8.6 231 8.3	518 60 6.9 241 6.9 244 6.9 246 6.7 251 6.3 253 5.7 253 5.1	70 4.8 200 4.5 209 4.3 220 4.4 231 4.7 240 5.0 245 5.3	80 3.55 268 3.4 270 3.2 273 3.1 275 3.0 276 2.9 275 2.9 275 2.9 275 2.9 275 2.9 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7
JULY SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5	MEAN (0 PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061	207 22.6 37 23.6 40 24.2 43 24.3 24.3 26.5 3 20.7 58 18.4 62 15.7	193 NTIAL -70 26.4 39 28.8 39 31.0 39 32.9 40 34.3 35.1 45 35.0 48 33.8 33.8 33.8 33.8 34.0 35.1 35.0 46.0 36.0 37.0 38.0 3	159 HEIGHT -60 31.3 32.9 36.8 27 39.8 27 42.7 27 45.2 46.9 32 47.1 35 45.2	147 AMPLI -50 34.5 31.1 27 36.4 23 38.5 21 41.4 20 44.7 22 48.0 24 50.7	146 TUDE (-40 21.1 0 21.5 355 355 22.4 351 24.2 350 26.6 351 354 351 35.5 359 37.0 4 39.2	161 -30 7.8 316 8.4 308 10.4 308 11.8 313 13.9 321 16.4 331 19.1	239 -20 3.3 269 3.2 256 3.3 250 3.4 262 3.8 284 5.0 3.0 6.7 3.0 6.7 3.0 8.1	299 SE * -10 0.3 172 0.6 166 0.9 164 1.0 162 0.8 159 0.4 149 0.3 14 1.1 353 1.8	301 AVE 1 0 3.6 197 3.2 202 2.9 2.4 212 1.9 214 1.2 210 0.5 189 0.4 0.5 189 0.6	279 10 7.7 203 6.9 203 5.2 202 4.4 200 5.6 197 2.9 192 3.1 190	200 7.2 222 7.1 218 7.1 7.0 210 6.9 207 6.4 204 6.0 6.0 5.4	255 30 6.8 244 9.2 238 9.6 233 9.9 228 10.2 224 10.1 221 9.8 218 9.3 217 8.6	257 40 9.7 257 9.6 252 9.5 246 9.6 240 9.7 234 9.9 230 9.9 226 9.5 227 224 9.5 9.5 9.5 9.5 9.5 9.5 9.5 9.5 9.5 9.5	283 50 10.2 238 9.8 237 9.5 235 8.9 235 8.7 232 8.6 231 8.3 230 7.8	60 6.9 241 6.9 246 6.9 249 6.7 251 6.3 5.7 253 5.7 253	70 4.8 209 4.5 209 4.3 220 4.4 231 4.7 240 5.0 245 5.3 246 5.3 246 5.3	80 3.55 268 3.4 270 3.2 273 3.1 275 3.0 276 2.9 275 2.9 272 2.9 272 2.9 272 2.9 273
JULY SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5	MEAN (6 PRESSURE (mb) 0.0062 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398	207 -80 22.6 37 23.6 40 24.2 43 24.3 46 25.7 49 22.5 53 20.7 56 18.4 62 15.7 65 12.9	193 NTIAL -70 26.4 39 28.8 39 31.0 39 32.9 40 34.3 35.1 45 55.0 38.8 52 27.9	159 HEIGHT -60 31.3 32 35.9 29 36.8 27 39.8 27 42.7 27 45.2 29 46.9 32 47.1 35 45.2 39 41.2	147 AMPLII -50 34.5 31 35.1 27 36.4 20 38.5 21 41.4 20 44.7 22 48.0 50.3 28 50.7 32 48.8	TUDE (-40 21.1 0 21.5 355 22.4 351 24.2 350 25.8 354 35.3 354 35.3 359 37.0 4 39.2 9	161 dam) A -30 7.8 316 8.4 309 9.2 2306 10.4 108 11.8 313 13.9 321 16.4 331 340 21.1 340 21.1 348 21.8	239 ND PHA -20 3.3 269 3.2 256 3.3 250 3.4 262 3.3 250 3.4 264 5.0 6.7 320 8.1 330 8.2 8.3 8.3 8.4 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0	299 SE # -10 0.3 172 0.6 166 0.9 164 1.0 162 0.8 159 0.4 149 0.3 14 1.1 353 1.8 8 349 2.2	301 0 3.6 197 3.2 202 2.9 208 2.4 212 210 0.5 1.9 214 1.2 210 0.5 189 0.4 93 0.6 48 0.7	279 10 7.7 203 6.9 203 6.0 203 5.2 202 4.4 20 3.6 197 2.9 192 2.3 190 1.8 193 1.5	207.2227.112187.1121447.00210 6.99207.205 6.44204.99207.49	255 30 6.8 244 9.2 238 9.6 233 9.9 228 10.1 221 9.8 218 9.3 217 8.6 6.218 7.8	257 40 9.7 257 9.6 252 9.5 240 9.7 234 9.9 230 9.9 226 9.7 224 9.2 223	283 50 10.2 238 9.8 237 9.5 236 9.2 235 8.9 234 8.7 232 8.6 6.3 230 7.8 8.3 230 7.7 2	516 60 6.9 241 6.9 244 6.9 249 6.7 251 6.3 253 5.7 253 5.1 252 4.5 254 4.6 4.6 4.6 4.6 4.6 4.6 5.6 5.6 5.6 5.6 5.6 5.6 5.6 5.6 5.6 5	70 4.8 200 4.5 209 4.3 24.4 231 4.7 245 5.3 245 5.1 242 4.6	80 3.5268 3.4 2700 3.2 273 3.1 275 3.0 276 2.9 275 2.9 275 2.9 268 2.9 266 2.8
JULY SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 8.0 7.5	MEAN (6 PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603	207 -80 22.6 37 23.6 40 24.2 43 24.3 46 25.7 59 10.4 25.7 50 10.7 10.9	193 NTIAL -70 26.4 39 28.8 39 31.0 39 32.9 40 34.3 42 35.1 45 35.8 51.2 27.9 60 23.6	159 HEIGHT -60 31.3 32 33.9 29 36.8 27 39.8 27 42.7 27 45.2 29 46.9 32 47.1 35.2 39 41.2 435.8	147 AMPLI -50 34.5 31 35.1 27 36.4 23 38.5 21 41.4 20 44.7 22 48.0 24 8.0 36.5 45.4	146 TUDE (-40 21.1 0 21.5 355 22.4 350 26.6 351 29.8 354 355 359 37.0 4.2 350 351 351 351 351 351 351 351 351	161 dam) A -30 7.8 316 6.4 309 9.2 306 10.4 108 11.8 313 13.9 321 16.4 331 19.1 348 21.8 355 21.4	239 ND PHA -20 3.3 269 3.2 256 3.3 250 3.4 262 3.8 284 5.0 6.7 320 6.7 330 8.7 338 8.5 8.5	299 SE # -10 0.3 172 0.6 166 0.9 164 1.0 0.4 149 0.3 14 1.1 353 14 1.1 353 349 2.2 2.3 347 2.3	301 0 3.6 197 3.2 202 2.9 208 2.4 212 210 0.5 189 0.4 93 0.6 48 0.7 15 0.8 0.8	279 10 7.7 203 6.9 203 6.0 203 5.2 202 4.4 200 3.6 197 2.9 192 2.3 190 1.6 193 1.5 1.6 1.6 1.6	207.2227.11 218 7.01 210 6.9 207 6.7 205 6.4 204 6.00 205 6.4 209 4.9 216 6.4 4.7	253 30 8.8 244 9.2 238 9.6 6 233 9.9 228 10.1 221 9.3 217 8.6 228 7.8 220 7.3 7.3	257 40 9.7 257 9.6 252 9.5 246 9.7 234 9.9 9.9 230 9.7 224 9.7 224 9.7 224 7.7 247 7 247 7 7 247 7 7 247 7 7 247 7 7 7	283 50 10.2 238 9.8 237 9.5 236 8.7 232 8.6 231 8.3 230 7.2 231 6.5 6.5	316 60 6.9 241 6.9 246 6.9 249 6.7 251 6.3 253 5.1 253 5.1 252 4.2 249 4.1	287 70 4.8 200 4.5 209 4.4 231 4.7 240 5.0 245 5.3 246 5.3 246 6.4 4.4 4.1	80 3.55 268 5.4 270 3.2 273 3.1 2.9 275 2.9 272 2.9 268 2.9 266 2.8 266 2.8 269 2.7
JULY SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 6.0 7.5	MEAN (PRESSURE (mb) 0.0062 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603 0.9237	207 -80 -80 -80 -80 -80 -80 -80 -80 -80 -80	193 NNTIAL -70 26.4 39 28.8 39 31.0 34.3 42 35.1 45 35.0 48 33.8 27.9 60 23.6 65 18.6	159 HEIGHT -60 31.3 32.9 29 36.6 27 39.8 27 42.7 27 45.2 29 46.9 32 47.11 35 45.2 39 41.2 44 35.8 50 29.4	147 AMPLI -50 34.5 31 35.1 27 36.4 20 44.7 22 48.0 24 45.4 45.4 40.5	146 TUDE (-40 21.1 0 21.5 355 355 22.4 351 24.2 2350 26.6 351 353 354 35.5 359 37.0 4 39.2 9 39.5 15 38.1 20 34.6 27 28.9 9	161 ddm) A 4 -30 7.8 316 8.4 309 9.2 306 10.4 313 13.9 321 16.4 331 19.1 340 21.1 348 355 21.4 1 19.5	239 ND PHA -20 3.3 269 3.2 256 3.3 250 3.4 252 3.8 250 3.6 6.7 320 8.1 330 8.7 338 8.5 344 7.9 348 6.7	299 SE W -10 0.3 172 0.6 166 0.9 162 0.8 159 0.4 14 1.1 353 1.8 349 2.2 347 2.3 344 2.2 341 1.9	301 0 3.6 197 3.2 202 202 212 212 210 0.5 189 0.4 93 0.6 83 0.7 15 0.8 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9	279 10 7.7 203 6.9 203 6.0 203 6.0 202 4.4 200 3.6 197 2.9 192 2.3 190 1.8 1.5 208 1.6 224 1.7 230 1.9	207 7.2 222 7.1 214 7.0 210 6.9 207 6.4 204 6.0 205 5.4 24 4.6 223 4.6 24 4.7 4.9 4.7	253 50 6.8 244 9.2 236 9.6 233 9.9 228 10.2 224 10.1 221 9.6 216 8.6 220 7.0 228 7.0 226 6.9 6.9 6.9	257 40 9.7 252 9.5 240 9.7 234 9.9 226 9.2 224 9.2 224 7.6 6.8 6.8 6.8	283 50 10.2 238 9.8 237 9.5 236 9.2 235 6.9 234 8.6 231 8.3 230 7.2 231 6.5 5.5 5.5 5.5 5.5 5.5	318 60 6.9 241 6.9 244 6.9 249 6.7 251 6.3 255 3.5 252 249 4.1 252 4.1 252 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0	287 70 4.8 200 4.5 209 4.3 220 4.4 251 4.7 240 5.0 245 5.3 246 241 4.1 242 3.8 245 3.6 3.6	80 3.5 268 3.4 270 3.1 275 3.0 276 2.9 275 2.9 268 2.6 2.8 269 2.7 270 2.9 2.7 2.9 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7
JULY SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 6.0 7.5 7.0	MEAN (6 PRESSURE (mb) 0.0062 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603 0.9237 1.52	207 -80 -80 -80 -80 -80 -80 -80 -80 -80 -80	193 NTIAL -70 26.4 39 38.8 39 31.0 30 32.9 40 34.3 35.1 45 35.0 48 33.8 52 27.9 60 23.6 65 18.6 67 75 18.6	159 HEIGHT -60 31.3 32 33.9 29 36.6 27 42.7 27 45.2 29 46.9 32 47.11 35 45.2 36.8 45.2 29 44.4 35.8 50 20.4	147 AMPLII -50 34.5 31 35.1 27 36.4 20 44.7 22 48.0 24 50.3 28 50.7 28 48.6 40.5 49 34.3	146 TUDE (-40 21.1 0 21.5 355 355 22.4 351 29.8 354 35.5 35.9 37.0 39.5 15 38.1 20.3 34.6 27	161 dem) A A 30 7.8 316 6.4 309 9.2 309 10.4 508 11.8 313 13.9 321 16.4 331 19.1 340 21.1 340 21.1 355 21.4 1 19.5 7 16.6 0	239 ND PHAME -20 3.3 269 3.2 256 3.3 249 3.3 250 3.4 262 284 5.0 6.7 320 8.1 330 8.7 338 8.5 344 7.348	299 SE W -10 0.3 172 0.66 166 0.9 164 1.0 0.8 1162 0.8 1353 14 1.1 353 344 2.2 2.3 347 2.3 341	301 0 3.6 197 3.2 202 202 2.9 208 2.4 2.12 210 0.5 189 0.4 93 0.6 48 0.7 15 0.8 0.9 0.8 0.9 0.9 0.9 0.0 0.0 0.0 0.0 0.0	279 10 7.7 203 6.9 203 6.0 203 5.2 202 4.4 200 2.9 197 2.9 193 1.5 208 1.6 224 1.6 224 1.7 230	207 7.2 222 7.1 214 7.1 214 7.1 210 6.9 207 6.7 205 6.4 209 4.9 216 4.7 223 4.2 29	253 30 6.8 244 9.2 238 9.6 233 9.29 10.1 221 9.8 218 9.3 217 7.8 6.6 218 7.3 224 7.3 224 7.3 224	257 40 9.7 257 9.5 246 240 9.7 234 9.9 230 9.7 224 7.6 226 226 7.1 229	283 50 10.2 238 9.8 236 9.5 236 8.9 234 8.7 232 8.6 230 7.2 231 6.5 233 5.9 235 6.5 233 5.9 235 7.2 235 8.9 236 8 8 236 8 8 8 8 236 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	318 60 6.9 241 6.9 244 6.7 251 3.253 5.7 253 5.1 252 4.2 249 4.1 252 4.2 4.2 4.2 4.2 4.2 4.2 4.2 4.2 4.2 4.	287 70 4.8 200 4.5 209 4.5 220 4.4 231 4.7 240 5.0 245 5.1 242 4.6 4.6 241 4.1 242 3.8 245 3.6 248	80 3.5268 5.4270 3.2273 3.11275 3.0276 2.99275 2.99268 2.8266 2.8266 2.8269 2.7220 2.5269
JULY SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 8.0 7.5 7.0 6.5	MEAN (6 PRESSURE (mb) 0.0062 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603 0.9237 1.52 2.51	207 -80 22.6 37 23.6 40 24.2 43 46 62 25.7 58 40 62 10.2 66 7.0 69 5.5 93	193 NTIAL -70 26.4 39 31.0 32.9 40 34.3 35.1 45 35.0 48 33.6 52 27.9 60 23.6 65 18.6 75 13.6	159 HEIGHT -60 31.3 32 33.9 29 36.8 27 39.8 27 42.7 45.2 29 46.9 32 47.1 35 45.2 29 46.9 32 47.1 35 49.2 29 46.9 30 41.2 44 35.8 50 29.4 67 76	147 AMPLII -50 34.5 31 35.1 27 36.4 20 34.5 21 41.4 20 44.7 7 22 48.0 24 40.5 36.6 40.5 49 34.3 62 49.2	146 TUDE (-40 21.1 021.5 355 22.4 350 26.6 351 29.8 35.5 359 37.0 4 39.2 39.5 15 30.6 27 28.9 34.6 27 21.7	161 dem) A -30 7.8 316 6.4 3309 9.2 306 10.4 108 11.8 3313 13.9 321 16.4 3313 19.1 340 21.8 3553 21.4 1 19.5 7 16.0 3 11.0	239 ND PHA -20 3.3 269 3.2 256 3.3 250 3.4 262 3.8 284 5.0 306 6.7 338 8.7 338 8.7 348 6.7 348 4.9	299 SE ** -10 0.3 172 0.6 166 0.9 164 1.0 162 0.8 159 0.4 14 1.9 338 344 2.2 347 1.9 338 1.6	301 0 3.6 197 3.2 2.9 2.9 2.4 212 210 0.5 189 0.4 8 0.7 15 0.8 3.8 0.9 3.8 0.9 3.8 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9	279 10 7.7 203 6.9 203 6.0 203 5.6 202 4.0 209 192 2.9 1.8 1.5 208 1.7 2.9 2.1 1.7 2.9 1.8 1.5 208 1.7 2.9 2.1 1.7 2.9 2.1 1.8	207 7.2 222 7.1 218 7.1 218 7.0 210 6.9 207 6.7 205 6.4 209 4.9 216 4.7 232 4.6 229 4.7 232	253 30 6.8 244 9.2 238 9.6 233 9.9 228 10.1 121 9.8 218 9.3 217 8.6 218 227 7.0 228 240 258 268 278 278 278 278 278 278 278 27	257 40 9.7 257 9.6 252 9.5 246 9.6 234 9.9 224 9.9 224 9.2 225 8.4 226 7.1 226 6.8 232 6.8 6.8 6.8 6.8 6.8 6.8 6.8 6.8 6.8 6.8	283 50 10.2 236 9.8 237 9.5 235 8.9 235 8.7 232 231 8.3 230 7.8 230 7.8 231 6.5 231 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.	318 60 6.9 241 6.9 244 6.9 249 6.7 251 6.3 253 35.7 253 35.7 253 4.5 252 249 4.1 252 5.1 252 4.1 252 4.1 252 4.1 252 4.1 252 4.1 252 4.1 252 4.1 252 5.1 2 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	70 4.8 200 4.5 209 4.3 241 4.7 240 5.0 245 5.3 245 5.3 245 5.4 4.6 4.1 242 4.6 4.1 242 4.6 243 245 245 245 245 245 245 245 245	244 80 3.5 268 3.4 270 3.2 273 3.1 2.9 275 2.9 275 2.9 266 2.8 266 2.8 269 2.7 270 2.5 2.9 2.7 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0
JULY SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 6.0 7.5 6.0	MEAN (6 PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603 0.9237 1.52 2.51 4.14	207 -80 -22.6 37 -23.6 40 -24.2 43 -24.3 46.2 -7.7 49 -22.5 53 -7.7 65 -7.0 66 -7.0 69 -7.0 69 -7.0 69 -7.0 69 -7.0 69 -7.0 69 -7.0 69 -7.0 69 -7.0 69 -7.0 69 -7.0 66 67 -7.0 66 67 -7.0 66 66 -7.0	193 NTIAL -70 26.4 39 31.0 39 31.0 34.3 42 35.1 45 35.8 52 27.9 60 23.6 65 10.6 66 11.5 13.6	159 HEIGHT -60 31.3 32 33.9 29 36.8 27 39.8 27 45.2 29 46.9 32 47.1 35 45.2 39 41.2 29.4 45.2 39 41.1 107 107 10.7	147 AMPLII -50 34.5 31 35.1 27 36.4 20 44.7 22 48.0 24 49.0 36.3 28.8 36.5 27 32 48.8 36.3 28.8 36.3 24.8	146 TUDE (-40 21.1 21.5 355 22.4 351 24.2 350 351 29.8 354 35.5 359 37.0 4 39.2 9 39.5 15 38.1 20.8 37 21.7 21.7 21.7 21.7 21.7 21.7 21.7 21.	161 dam) A -30 7.8 316 8.4 309 9.2 306 10.4 313 321 16.4 313 348 21.8 21.8 355 21.4 11.0 23 11.0 23 6.1	239 ND PHA -20 3.3 269 3.5 256 3.3 250 3.4 262 3.8 284 5.0 3.6 6.7 320 8.7 330 8.7 340	299 SE N -10 0.3 172 0.6 166 0.9 164 1.0 162 0.8 159 0.4 149 0.3 1.1 353 1.8 349 2.2 347 2.3 344 1.9 336 1.6 334	301 0 3.6 197 3.2 202 2.9 208 2.4 212 210 0.5 1.9 214 1.2 210 0.5 1.9 3.6 1.9 2.9 2.9 2.9 2.9 2.9 2.9 2.9 2	279 10 7.7 203 6.0 203 6.0 203 5.2 202 24.4 200 3.6 197 2.9 1.8 193 1.5 224 1.9 230 1.9 211 1.9 228	257 20 7.2 222 7.1 218 7.0 210 6.9 207 6.4 208 6.4 209 4.9 229 4.7 223 4.7 233 4.7 234 4.7 235 4.7 246 4.7 256 4.7 257 268 269 269 269 269 269 269 269 269	253 30 6.8 244 9.6 238 9.9 232 224 10.1 221 9.8 218 7.8 228 6.9 238 6.9 6.8 236 6.8 236 6.8 236 6.8 236 6.8 236 6.8 236 6.8 6.8 6.8 6.8 6.8 6.8 6.8 6.	257 40 9.7 257 9.6 252 9.6 240 9.7 234 9.9 226 9.7 224 9.7 224 7.6 6.2 6.6 232 6.6 6.6 6.2 6.6 6.6 6.6 6.6 6.	283 50 10,2 238 9.37 9.5 237 9.5 235 8.9 234 8.7 232 8.6 231 6.5 230 7.2 235 5.5 230 7.2 235 5.5 230 7.2 244 8.7 255 8.8 257 7.8 257 8.8 257 7.8 257 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	318 60 6.9 241 6.9 244 6.9 249 7 251 6.3 5.7 253 5.7 253 6.5 6.2 6.0 6.9 6.0 6.9 6.0 6.9 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0	70 4.8 200 4.5 209 4.4 220 4.4 245 5.3 246 5.3 247 5.3 248 5.3 248 5.3 248 5.3 248 5.3 248 5.3 248 5.3 6.3 6.3 6.3 6.3 6.3 6.3 6.3 6	244 80 3.5 268 3.4 270 3.2 273 3.0 275 3.0 275 2.9 275 275 275 275 275 275 275 275 275 275
JULY SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 7.0 6.5 5.0	MEAN (PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603 0.9237 1.52 2.51 4.14 6.83	207 -80 -80 -82.67 -82.67 -83.67 -84.0 -84.22 -83.77 -85 -86.67 -	193 NTIAL -70 26.4 39 31.0 39 31.0 34.3 42 35.1 55.0 23.6 65 18.6 65 11.5 13.6 96 11.5 13.6 14.0 172 17.9 192 20.0	159 HEIGHT -60 31.3 35.9 29 36.6 27 39.8 27 42.7 27 42.7 27 45.2 39 46.9 32 47.1 35.8 50 29.4 44 35.8 50 29.4 10.7 10.7 18.7 144 22.0 170 24.3	147 AMPLI -50 34.51 35.11 27 36.4 23 38.55 21 41.4 20 44.7 22 48.08 50.7 32 48.8 50.7 32 48.8 26 28.2 83 24.8 12 28.2 83 24.8	146 TUDE (-40 21.1 21.5 355 22.4 350 26.6 351 24.2 25.8 354 35.9 37.0 439.2 99.3 38.1 20.3 34.6 27.2 28.9 37.0 38.1 20.3 31.2 21.7 53.1 15.9 15.9 15.9 15.9 17.9 17.9 18.1 19.9 19.9 19.9 19.9 19.9 19.9	161 dam) A -30 7.8 316 6.4 309 9.2 306 10.4 309 11.8 313 13.9 321 16.4 331 19.1 348 21.8 355 21.4 119.5 7 16.0 23 6.1 45 3.6	239 ND PHA -20 3.3 269 3.2 256 3.3 249 3.3 3.0 269 3.3 3.4 262 3.3 3.6 6.7 3.0 6.7 3.3 8.5 3.4 7.9 3.4 8.5 3.4 7.9 3.4 8.5 3.4 7.9 3.4 8.5 3.4 7.9 3.4 8.5 3.4 7.9 3.4 8.5 3.4 7.9 3.4 8.5 3.4 7.9 3.4 8.5 3.4 7.9 3.4 8.5 3.4 7.9 3.4 8.5 3.4 7.9 3.4 8.5 3.4 7.9 3.4 8.5 3.6 7.9 3.6 8.7 8.7 8.7 8.7 8.7 8.7 8.7 8.7 8.7 8.7	299 SE N -10 0.3 172 0.6 166 0.9 164 1.0 162 0.8 159 0.4 149 0.3 14 1.1 353 1.8 349 2.2 347 2.3 344 1.9 336 1.6 334 1.9 336 1.6 334 1.9 336 1.6 334 1.9	301 3.6 197 3.2 202 2.9 208 2.4 212 210 0.5 189 0.4 0.7 15 0.8 308 301 0.8 301 0.9 0.4 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7	279 10 7.7 203 6.9 203 6.0 203 5.2 203 4.4 200 1.8 193 1.6 1.6 224 1.7 230 1.9 231 1.9 248 1.9 217 1.8 1.9	257 20 7.2 2222 7.1 218 7.1 214 7.0 6.9 207 6.7 205 6.4 209 4.9 209 4.9 207 208 4.6 229 4.6 229 4.7 233 4.6 227 237 248 257 257 257 257 257 257 257 257	253 30 6.8 244 9.2 238 9.9 228 10.2 221 9.8 218 220 7.3 224 7.0 228 6.9 230 240 250 260 270 270 270 270 270 270 270 27	257 40 9.7 257 9.6 252 9.6 246 9.7 234 9.7 234 9.7 247 248 247 258 268 278 288 298 298 298 298 298 298 29	263 50 10.2 238 9.8 237 9.5 9.2 234 8.6 6.9 231 6.3 230 7.8 231 6.5 233 5.5 233 5.5 238 5.2 240 4.8 4.8 237 238 239 239 239 239 239 239 239 239 239 239	318 60 6.9 241 6.9 244 6.9 246 6.9 246 6.7 251 5.7 253 5.1 252 249 4.1 256 6.3 253 3.8 3.8 3.8 3.8 3.8 3.8 3.8 3.8 3.8 3.	70 4.8 200 4.5 209 4.4 220 4.4 220 4.4 245 5.3 246 5.3 246 241 4.1 242 3.8 248 3.8 251 293 293 293 294 295 296 297 297 297 297 297 297 297 297	244 80 3.5 268 3.2 270 3.1 275 3.1 275 2.9 275 2.9 268 2.9 266 2.8 269 2.7 2.5 265 1.7 2.6 2.9 2.5 2.6 2.0 2.5 2.6 2.6 2.6 2.6 2.6 2.6 2.6 2.6 2.6 2.6
JULY SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 6.0 5.5 5.0 4.5	MEAN (6 PRESSURE (mb) 0.0062 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603 0.9237 1.52 2.51 4.14 6.83 11.25	207 -80 -80 -80 -80 -80 -80 -80 -80 -80 -80	193 NTIAL -70 26.4 39 31.0 39 31.0 39 32.9 40 34.3 42 35.1 45 35.6 65 37 60 23.6 65 13.6 65 13.6 96 11.5 13.9 17.9 17.9	159 HEIGHT -60 31.3 33.9 29 36.86 27 39.8 27 45.2 29 46.9 32 47.1 35 45.2 29 46.9 30 21.6 6 6 6 16.1 16.7 144 22.0 170	147 AMPLII -50 34.5 31 35.1 27 36.4 20 34.5 21 41.4 20 44.7 22 48.0 24 49.0 34.3 28 48.8 36.3 62 28.2 28.2 28.2 28.3	146 TUDE (-40 21.1 21.5 355 22.4 355 22.4 351 24.2 350 351 29.8 35.5 354 39.2 9 39.5 37.0 4 39.2 28.9 37.5 38.1 28.9 37.5 38.1 28.9 37.5 38.1 38.2 38.1 38.2 38.1 38.2 38.1 38.2 38.1 38.2 38.1 38.2 38.1 38.2 38.1 38.2 38.1 38.2 38.1 38.2 38.2 38.2 38.2 38.2 38.2 38.2 38.2	161 dam) A -30 7.8 8.4 309 9.2 336 10.4 313 11.8 331 11.4 335 21.4 1348 355 21.4 11.1 19.5 7 16.0 13 11.0 25 6.1 11.0 25 6.6 95	239 ND PHA -20 3,3 269 3,2 256 3,3 250 3,4 262 3,8 284 409 3,3 8,7 330 8,7 330 8,7 348 4,9 348	299 SE * -10 0.3 172 0.6 166 0.9 164 1.0 0.8 159 0.4 14 14 1.1 1.3 33 1.8 349 2.2 347 2.3 344 2.2 347 2.3 341 1.9 338 1.6 334 1.1 328 0.5 315 0.2 2299	301 3.6 197 3.2 202 2.9 2.08 2.4 2.12 2.10 0.5 1.9 2.14 2.12 2.10 0.5 1.9 3.8 0.6 48 0.7 15 0.8 3.8 0.9 3.8 3.8 3.9 3.9 3.9 3.9 3.9 3.9 3.9 3.9	279 10 7.7 203 6.0 203 6.0 205 5.2 202 24.4 200 3.6 197 2.9 192 2.3 190 1.8 1.6 224 1.7 230 1.9 231 1.9 241 1.9 221 2.9 224 2.9 224 2.9 224 2.9 227	257 20 7.2 2222 7.1 218 7.0 210 6.9 207 6.7 205 6.4 209 216 4.7 223 4.6 209 4.7 233 4.6 202 4.7 233 4.2 202 218 25 218	253 30 6.8 244 9.2 238 9.9 228 10.1 221 8.6 218 220 7.0 24 7.0 28 29 24 4.3 24 4.3 224 4.3 224 4.3 227 229 229 229 229 229 229 229	257 40 9.7 257 9.6 252 9.6 246 9.7 234 9.9 9.2 230 9.9 246 9.7 234 9.2 226 9.7 234 9.6 246 9.7 234 9.6 246 9.7 254 9.6 256 9.7 9.7 9.7 9.7 9.7 9.7 9.7 9.7	263 50 10.2 236 9.8 237 9.5 236 6.9 234 8.7 232 8.7 231 6.5 231 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	318 60 6.9 241 6.9 244 6.9 6.7 251 6.3 253 5.1 252 6.3 249 6.7 251 6.3 6.2 249 6.7 251 6.3 6.2 249 6.7 6.3 6.2 6.3 6.3 6.3 6.2 6.3 6.3 6.3 6.3 6.3 6.3 6.3 6.3 6.3 6.3	70 4.8 200 4.5 209 4.4 210 240 240 240 240 241 4.7 240 241 242 3.6 241 4.7 242 3.6 241 3.6 241 3.6 241 3.6 241 3.6 241 3.6 241 3.6 241 3.6 241 3.6 241 3.6 241 3.6 241 3.6 241 3.6 241 3.6 241 3.6 241 3.6 3.6 3.6 3.6 3.6 3.6 3.6 3.6	244 80 3.5 268 3.4 273 3.1 275 3.0 276 2.9 266 2.8 266 2.8 269 2.7 270 2.9 2.9 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0
JULY SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 6.0 7.5 7.0 6.5 5.0 4.5	MEAN (6 PRESSURE (mb) 0.0062 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603 0.9237 1.52 2.51 4.14 6.63 11.25 18.55	207 -80 -80 -80 -80 -80 -80 -80 -80 -80 -80	193 NTIAL -70 26.4 39 28.8 39 31.0 39 32.9 40 34.3 45 55.0 48 33.8 27.9 60 23.6 65 18.6 65 11.5 13.6 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11	159 HEIGHT -60 31.3 32.9 29.9 36.6 27 39.8 27 42.7 25.9 46.9 32 47.1 55.8 50 29.4 48 50 29.4 107 1107 18.7 18.7 188 22.0 170 170 24.3 188 25.9	147 AMPLI -50 34.5 51 35.1 27 36.4 23 38.5 21 41.4 23 48.0 24.7 22 48.0 40.5 49 34.3 62 48.8 36 49 34.3 62 83 24.8 81 23.9 111 23.9 137 23.0 157 20.4	146 TUDE (-40 21.1 21.5 355 25.6 351 24.2 29.8 354 359.2 37.0 34.6 27 28.9 39.5 15.2 21.7 53 11.9 11.9 11.9 11.9 13.8	161 dam) A -30 7.88 316 8.4 309 9.2 336 10.4 313 306 11.8 313 311 16.4 355 21.4 11 19.1 19.1 19.1 19.1 19.1 19.1 19.	239 ND PHA -20 3.3 269 3.2 256 3.2 256 3.3 249 3.3 3.5 3.6 250 3.4 262 8.1 330 8.5 3.6 4.7 338 8.5 344 7.9 348 6.7 348	299 SE * -10 0.3 172 0.6 166 0.9 164 1.0 0.6 159 0.4 1.1 353 14 1.1 353 14 2.2 347 2.3 344 2.2 341 1.1 358 3.6 3.34 1.1 328 0.5 315 0.2 229	301 3.6 197 3.2 202 2.9 208 2.4 2.1 2.10 0.5 189 0.4 93 0.6 48 0.7 15 0.8 3.8 0.9 3.14 0.9 3.14 0.5 0.6 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7	279 10 7.7 203 6.9 203 6.0 203 5.2 202 4.4 200 2.9 1.8 193 1.5 208 1.7 230 1.9 224 1.7 1.8 207 1.8 207 1.8 207 1.8	257 20 7.2 212 7.1 218 7.1 214 7.0 210 6.9 207 6.9 205 6.4 209 4.9 209 4.9 216 4.7 232 4.6 227 232 4.6 232 4.7 232 232 232 232 232 232 232 23	253 30 6.8 244 9.6 9.6 10.2 224 10.2 224 10.2 218 9.3 217 8.6 218 7.3 247 7.0 228 6.3 234 6.3 6.3 6.3 6.3 6.3 6.3 6.3 6.3	257 40 9.7 257 9.6 252 9.5 246 9.9 9.9 230 9.7 224 7.6 225 8.4 7.1 229 8.3 8.4 8.6 8.6 8.6 8.6 8.6 8.6 8.6 8.6	283 50 10,2 238 9,8 237 9,2 236 8,6 231 8,3 230 7,2 231 6,5 231 6,5 235 5,9 235 5,2 335 5,2 34 4,8 230 5,8 230 5,8 200 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	318 60 6.9 241 6.9 244 6.9 246 6.9 247 251 6.3 5.7 253 5.1 252 4.1 256 6.3 6.3 6.3 6.3 6.3 6.3 6.3 6.3 6.3 6.	70 4.8 200 4.5 209 4.4 220 4.4 4.7 240 5.3 245 5.3 245 5.3 245 5.3 245 5.3 245 5.3 245 5.3 245 5.3 245 5.1 242 4.4 4.6 245 5.3 245 5.1 245 5.1 245 5.1 246 5.1 247 248 248 249 249 249 249 249 249 249 249	244 80 3.5 268 3.4 270 3.2 273 3.1 275 2.9 275 2.9 266 2.8 266 2.8 269 2.2 270 2.5 2.9 2.6 2.6 2.6 2.6 2.6 2.6 2.6 2.6 2.6 2.6

	MEAN T	EMPERA	TURE A	MPL ITU	DE (K)	AND P	HASE	WAVE	2									
SCALE	PRESSURE (mb)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
12.0	0.0062	0,19	0.62	1.20	0.91	0.59	0.17	0.26	0.48	0.13	0.69	0.48	0.27	0,18	0.13	0.22	0.19	0.33
11.5	0.0103	0.25	0.68	1.14	0.78	0.57	0.17	295 0,26 285	251 0,51 249	0.14	0.65 34	0.46 34	0.27	273 0,20 276	0.14	219 0,25 216	0,22 182	0.37
11.0	0.0169	0.35 237	0.72	1.00	121 0.64 150	0.54	0,17	0.26	0.51	0.14	0.55	0.39	0.27	0,22	0.15	0.28	0.24	0.41
10.5	0.0279	0.42	0.76	0.85	0.76	0,60	0.19	0.27	0.51	0.16	0.40	0.28	0.28	0.24	0.18	0.31	0.23	0.38
10.0	0.0460	0.51	0.80	0.84	1,18	0.81	0.26	0.31	0.49	0.19	0.19	0.20	0.31	0.28	0.23	0.32	0.21	0.30
9,5	0.0758	0.56	0.80	1.00	1.67	1,11	0.37	0.37	0.46	0.23	0.06	0.22	0.39	0.32	0.30	0.30	0.17	0.19
9.0	0.1250	0.52	0.75	1,22	2,00	1.31	0.49	0.39	0.40	0.23	0.23	0.29	0.44	0,33	0.34	0.22	0.12	0.17
8.5	0.2061	0.37	0,62	1,35	1.96	1.27	0,57	0.32	0.27	0.16	0.31	0.26	0.42	0.31	0.31	0.12	0.11	0.21
8.0	0.3398	0.14	0.55	1.53	1.51	0.91	0.55	0.17	0.13	0.05	0.27	0.20	0.35	0.23	0.20	0.02	0,15	0.19
7.5	0,5603	0.02	0.44	0.73	0.23	0.40	0.21	0.11	0.08	0.05	0.17	0.17	0.23	0.15	0.08	0.03	0.14	0.07
7.0	0.9237	0.11	0.19	0.10	0.72	0.95	0.43	0.21	0.05	0.02	0.16	0.14	0.14	0.13	0.09	0.01	0.13	0.04
6,5	1,52	0.25	0.32	0.52	0.94	1.18	0.80	0.30	0.08	0.06	0.10	0.02	0.08	0.15	0.11	0.03	0.08	0.07
6.0	2,51	0.40	0.77	1.26	1.31	1.63	1.25	0.49	0.13	0.09	0.06	0.07	0.21	0.24	0.14	0.05	0.07	0.09
5.5	4,14	0.30	0.75	1.52	1.66	1.81	1.30	0.49	0.12	0.07	0.04	0.16	0.33	0.31	0.18	0.05	0.08	0,07
5.0	6,83	0.14	0.63	1.66	2.06	1.88	1.17	0.41	0.10	0.06	0.04	0.26	0.44	0,39	0.28	0.08	0.08	0.04
4,5	11.25	0.21	0.40	1.67	2.27	1.73	0.92	0.30	0.06	0.09	0.07	0.35	0.54	0.45	0.37	0,12	0.07	0.03
4.0	18,55	0,63	0.37	1.58	2.15	1.48	0.30	0.30	0.03	0.12	0.10	0.40	0.57	0.48	0.44	0.14	0.05	0.07
3,5	30.59	1.03	0.64	1.29	1.76	1.22	0.87	0.38	0.02	0.12	0.11	0.39	0.54	0.45	0.43	0.15	0.03	0.10
3.0	50.43	0.75	0.66	0.89	1.25	0.98	0.91	0,43	0.03	0.12	0.11	0.35	0.47	0.38	0.36	0.14	0.02	0.10
2.5	83.15	0,42	0.45	0.54	0.76	0.70	0.75	0.37	0,04	0.09	0.09	0.27	0.35	0.28	0.26	0.10	0.02	0.08
											-			-	-		10	
JULY	PRESSURE	-80	-70	-60	-50	-40	-30	ND PHA	-10	AVE 2	10	20	30	40	50	60	70	80
HEIGHT	(mb)																	
12.0	-	226	191	189	199	201	7.6	209	247	202	42	348	321	318	351	190	183	82
11.5		4.7	10.8					* *		0.0							2.8	
11.0		226	192	193	202	203	192	201	246	0.2 196	49	338	317	320	3.0 354	186	184	75
		4.3 226	9.8 193	193 21.1 196	202 23.7 204	203 15.6 205	7.2 192	201 2.9 194	246 2.9 245	196 0.2 186	0.3 102	338 2.5 326	517 6.0 314	5.3 322	354 3.0 358	186 2.4 181	184 2.5 184	75 1.2 62
10.5	0.0279	4.3 226 3.7 224	9.8 193 8.7 194	193 21.1 196 20.0 198	202 23.7 204 22.9 206	203 15.6 205 14.8 206	7.2 192 6.9 192	2.9 194 2.8 186	2.9 245 2.2 245	196 0.2 186 0.1 150	0.3 102 0.7 185	338 2.5 326 2.3 315	317 6.0 314 5.7 311	320 5.3 322 5.0 324	354 3.0 358 3.0 3	186 2.4 181 2.0 174	184 2.5 184 2.1 184	75 1.2 62 0.9 36
10.0	0.0279	4.3 226 3.7 224 3.1 219	9.8 193 8.7 194 7.6 194	193 21.1 196 20.0 198 18.8 199	202 23.7 204 22.9 206 21.5 206	203 15.6 205 14.8 206 13.8 205	7.2 192 6.9 192 6.6 191	201 2.9 194 2.8 186 2.7 178	246 2.9 245 2.2 245 1.5 247	196 0.2 186 0.1 150 0.1 75	0.3 102 0.7 185 1.1 193	338 2.5 326 2.3 315 2.0 308	317 6.0 314 5.7 311 5.4 309	5.3 322 5.0 324 4.7 326	354 3.0 358 3.0 3 2.9 8	186 2.4 181 2.0 174 1.7 164	184 2.5 184 2.1 184 1.8 185	75 1.2 62 0.9 36 0.8
10.0	0.0279 0.0460 0.0758	4.3 226 3.7 224 3.1 219 2.5 210	192 9.8 193 8.7 194 7.6 194 6.4 193	193 21.1 196 20.0 198 18.8 199 17.5 198	202 23.7 204 22.9 206 21.5 206 19.5 204	203 15.6 205 14.8 206 13.8 205 12.6 202	7.2 192 6.9 192 6.6 191 6.4 187	2.9 194 2.8 186 2.7 178 2.4 169	246 2.9 245 2.2 245 1.5 247 0.8 254	196 0.2 186 0.1 150 0.1 75 0.3 52	0.3 102 0.7 185 1.1 193 1.2	338 2.5 326 2.3 315 2.0 308 1.8 307	317 6.0 314 5.7 311 5.4 309 4.9 307	5.3 322 5.0 324 4.7 326 4.3 329	354 3.0 358 3.0 3 2.9 8 2.7	186 2.4 181 2.0 174 1.7 164 1.4 150	184 2.5 184 2.1 184 1.8 185 1.5 186	75 1.2 62 0.9 36 0.8 1 0.8 334
9.5	0.0279 0.0460 0.0758 0.1250	4.3 226 3.7 224 3.1 219 2.5 210 1.9 194	9.8 193 8.7 194 7.6 194 6.4 193 5.3	193 21.1 196 20.0 198 18.8 199 17.5 198 16.2 195	202 23.7 204 22.9 206 21.5 206 19.5 204 17.3 199	203 15.6 205 14.8 206 13.8 205 12.6 202 11.4 195	192 7.2 192 6.9 192 6.6 191 6.4 187 6.2 182	201 2.9 194 2.8 186 2.7 178 2.4 169 2.1 157	246 2.9 245 2.2 245 1.5 247 0.8 254 0.2 302	196 0.2 186 0.1 150 0.1 75 0.3 52 0.5 46	49 0.3 102 0.7 185 1.1 193 1.2 192 1.1 184	338 2.5 326 2.3 315 2.0 308 1.8 307 1.5 315	5.7 311 5.7 311 5.4 309 4.9 307 4.3 308	5.3 5.3 322 5.0 324 4.7 326 4.3 329 3.8 331	3.0 3.0 3.58 3.0 3.2.9 8 2.7 15 2.4 24	186 2.4 181 2.0 174 1.7 164 1.4 150 1.3	184 2.5 184 2.1 184 1.8 185 1.5 186 1.3 187	75 1.2 62 0.9 36 0.8 1 0.8 334 0.7 316
10.0 9.5 9.0 8.5	0.0279 0.0460 0.0758 0.1250 0.2061	4.3 226 3.7 224 3.1 219 2.5 210 1.9 194 1.7	192 9.8 193 8.7 194 7.6 194 6.4 193 5.3 190 4.6 182	193 21.1 196 20.0 198 18.8 199 17.5 198 16.2 195 14.9	202 23.7 204 22.9 206 21.5 206 19.5 204 17.3 199 15.1 192	203 15.6 205 14.8 206 13.8 205 12.6 202 11.4 195 10.6 186	192 7.2 192 6.9 192 6.6 191 6.4 187 6.2 182 6.1	201 2.9 194 2.8 186 2.7 178 2.4 169 2.1 157 1.9	246 2.9 245 2.2 245 1.5 247 0.8 254 0.2 302 0.4 31	196 0.2 186 0.1 150 0.1 75 0.3 52 0.5 46 0.7 46	49 0.3 102 0.7 185 1.1 193 1.2 192 1.1 184 0.7 169	338 2.5 326 2.3 315 2.0 308 1.8 307 1.5 315 1.4 331	317 6.0 314 5.7 311 5.4 309 4.9 307 4.3 308 3.7 311	320 5.3 322 5.0 324 4.7 326 4.3 329 3.8 331 3.4 333	354 3.0 358 3.0 3 2.9 8 2.7 15 2.4 24 2.2 34	186 2.4 181 2.0 174 1.7 164 1.50 1.3 134 1.2	184 2.5 184 2.1 184 1.8 185 1.5 186 1.3 187 1.1	75 1.2 62 0.9 36 0.8 1 0.8 334 0.7 316 0.5 299
10.0 9.5 9.0 8.5 8.0	0.0279 0.0460 0.0758 0.1250 0.2061 0.3398	4.3 226 3.7 224 3.1 219 2.5 210 1.9 194	192 9.8 193 8.7 194 7.6 194 6.4 193 5.3 190	193 21.1 196 20.0 198 18.8 199 17.5 198 16.2 195 14.9 190 13.9	202 23.7 204 22.9 206 21.5 206 19.5 204 17.3 199 15.1 192 13.7 183	203 15.6 205 14.8 206 13.8 205 12.6 202 11.4 195 10.6 186 10.3	192 7.2 192 6.9 192 6.6 191 6.4 187 6.2 182	201 2.9 194 2.8 186 2.7 178 2.4 169 2.1 157	246 2.9 245 2.2 245 1.5 247 0.8 254 0.2 302 0.4 31 0.7 48	196 0.2 186 0.1 150 0.1 75 0.3 52 0.5 46 0.7 46 0.9 48	49 0.3 102 0.7 185 1.1 193 1.2 192 1.1 184 0.7 169 0.4 136	338 2.5 326 2.3 315 2.0 308 1.8 307 1.5 315	5.7 311 5.7 311 5.4 309 4.9 307 4.3 308 3.7	320 5.3 322 5.0 324 4.7 326 4.3 329 3.8 331	3.0 3.0 3.58 3.0 3.2.9 8 2.7 15 2.4 24 2.2	186 2.4 181 2.0 174 1.7 164 1.4 150 1.3 134	184 2.5 184 2.1 184 1.8 185 1.5 186 1.3 187 1.1 185 1.0 180	75 1.2 62 0.9 36 0.8 1 0.8 334 0.7 316 0.5 299 0.2 264
10.0 9.5 9.0 8.5 8.0 7.5	0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603	4.3 226 3.7 224 3.1 219 2.5 210 1.9 194 1.7 161 1.8 159	192 9.8 193 8.7 194 7.6 194 6.4 193 5.3 190 4.6 182 4.4 172 4.7 163	193 21.1 196 20.0 198 18.8 199 17.5 198 16.2 195 14.9 190 13.9 183 13.6 177	202 23.7 204 22.9 206 21.5 206 19.5 204 17.3 199 15.1 192 13.7 183 13.4 179	203 15.6 205 14.8 206 13.8 205 12.6 202 11.4 195 10.6 10.3 178	192 7.2 192 6.9 192 6.6 191 6.4 182 6.1 175 6.2 167 6.5 164	201 2.9 194 2.8 186 2.7 178 2.4 169 2.1 157 1.9 143 1.8 131	246 2.9 245 2.2 245 1.5 247 0.8 254 0.2 302 0.4 31 0.7 48 0.7 58	196 0.2 186 0.1 150 0.1 75 0.3 52 0.5 46 0.7 46 0.9 48 0.9 51	49 0.3 102 0.7 185 1.1 193 1.2 192 192 1.1 184 0.7 169 0.4 136 0.2 92	338 2.5 326 2.3 315 2.0 308 1.8 307 1.5 315 1.4 331 1.5 343	317 6.0 314 5.7 311 5.4 309 4.9 307 4.3 308 3.7 311 3.2 318	5.3 5.2 5.0 324 4.7 326 4.3 329 3.8 331 3.4 333 3.0 335 2.8 338	354 3.0 358 3.0 3.2 2.9 8 2.7 15 2.4 24 2.2 34 2.0 43 2.0	186 2.4 181 2.0 174 1.7 164 1.5 1.3 134 1.2 123 1.2 118 1.2	184 2.5 184 2.1 184 1.8 185 1.5 186 1.3 187 1.1 185 1.0 180 0.8 172	75 1.2 62 0.9 36 0.8 1 0.8 334 0.7 316 0.5 299 0.2 264 0.2 212
10.0 9.5 9.0 8.5 8.0 7.5	0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603	4.3 226 3.7 224 3.1 219 2.5 210 1.9 194 1.7 174 1.7 161 1.8 159	9.8 193 8.7 194 7.6 194 6.4 193 5.3 190 4.6 182 4.4 172 4.7 163 5.0 159	193 21.1 196 20.0 198 18.8 199 17.5 198 16.2 195 14.9 190 13.9 18.3 13.6 177	202 23.7 204 22.9 206 21.5 206 19.5 204 17.3 199 15.1 192 13.7 183 13.4 179	203 15.6 205 14.8 206 13.6 202 12.6 202 11.4 195 10.6 186 10.3 178 10.6 175	192 7.2 192 6.9 192 6.6 191 6.4 187 6.2 182 6.1 175 6.5 164 6.7 166	201 2.9 194 2.8 186 2.7 178 2.4 169 2.1 157 1.9 143 1.8 131 1.8 131	246 2.9 245 2.2 245 1.5 247 0.8 254 0.2 302 0.4 31 0.7 48 0.7 58 0.6 63	196 0.2 186 0.1 150 0.3 52 0.5 46 0.7 46 0.9 48 0.9 51	49 0.3 102 0.7 185 1.1 193 1.2 192 1.1 184 0.7 169 0.4 136 0.2 92 0.1	338 2.5 326 2.3 315 2.0 308 1.8 307 1.5 315 1.4 331 1.7 344 1.9 340	317 6.0 314 5.7 317 309 4.9 307 4.3 308 3.7 311 3.2 318 3.2 325 3.3 329	320 5.3 322 5.0 324 4.7 326 4.3 329 3.8 331 3.4 333 3.0 335 2.8 338 2.7 342	354 3.0 358 3.0 3.7 2.9 8 2.7 15 2.4 24 2.2 34 2.0 49 2.0 51	186 2.4 181 2.0 174 1.7 164 1.4 150 1.3 134 1.2 123 1.2 118 1.2 120 1.2	184 2.5 184 2.1 188 185 1.5 186 1.3 187 1.1 185 1.0 180 0.8 172 0.7 162	75 1.2 62 0.9 36 0.8 334 0.7 316 0.5 299 0.2 264 0.2 212 0.1 187
10.0 9.5 9.0 8.5 8.0 7.5 7.0	0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603 0.9237	4.3 226 3.7 224 3.1 219 2.5 210 1.9 194 1.7 161 1.8 159 1.5 159	192 9.8 193 8.7 194 7.6 194 6.4 193 5.3 190 4.6 182 4.4 172 4.7 163 5.0 159 4.8	193 21.1 196 20.0 198 18.8 199 17.5 198 16.2 195 14.9 190 13.9 183 15.6 175 13.4 176	202 25.7 204 22.9 206 21.5 206 19.5 204 17.3 192 13.7 183 13.4 17.9 13.7 180 14.0 185	203 15.6 205 14.8 206 13.8 205 12.6 202 11.4 195 10.6 178 10.6 175 11.1 180	192 7.2 192 6.6 191 6.4 187 6.2 182 167 6.5 167 6.5 166 6.3	201 2.9 194 2.8 186 2.7 178 2.4 169 2.1 157 1.9 143 1.8 131 1.8 131 1.8 138	246 2.9 245 2.45 1.5 247 0.8 254 0.2 302 0.4 31 0.7 48 0.7 58 63 0.6 57	196 0.2 186 0.1 150 0.1 75 0.3 52 0.5 46 0.7 46 0.9 48 0.9 51 0.7 45	49 0.3 102 0.7 185 1.1 193 1.2 192 1.1 184 0.7 169 0.4 136 0.2 92 0.1 0	338 2.5 326 2.3 315 2.0 308 1.8 307 1.5 315 1.4 331 1.5 343 1.7 344 1.9 340 2.0 338	317 6.0 314 5.7 311 5.4 309 4.9 307 4.3 33 33 311 3.2 318 3.2 329 3.3 332	5.3 5.2 5.0 324 4.7 526 4.3 329 3.8 331 3.4 333 3.0 335 2.8 335 2.7 342 2.6 345	354 3.0 358 3.0 3 2.9 8 2.7 15 2.4 24 2.2 34 2.0 43 2.0 43 2.0 51 2.1	186 2.4 181 2.0 174 1.7 164 1.50 1.3 134 1.2 123 1.2 118 1.2 121 1.2 121	184 2.5 184 2.1 184 1.8 185 1.5 186 1.3 187 1.1 185 1.0 180 0.8 172 0.7 162 0.6 153	75 1.2 62 0.9 36 0.8 334 0.7 316 0.5 299 0.2 212 0.1 187 0.0 177
10.0 9.5 9.0 8.5 8.0 7.5 7.0 6.5	0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603 0.9237 1.52 2.51	4.3 226 3.7 229 3.1 219 2.5 210 1.9 194 1.7 174 1.7 161 1.8 159 1.7 160 1.5 159	192 9.8 193 8.7 194 7.6 194 6.4 193 5.3 190 4.6 182 4.7 163 5.0 159 4.8 4.0 158	193 21.1 196 20.0 198 18.8 199 17.5 198 16.2 195 14.9 190 13.9 183 13.6 175 13.4 176 175 13.4 176	202 25.7 204 22.9 206 21.5 204 17.3 199 15.1 192 13.7 183 13.4 179 13.7 180 14.0 185 191	203 15.6 205 14.8 206 13.8 205 12.6 202 11.4 195 10.6 186 10.3 178 11.1 180 10.3 197	7.2 192 6.9 192 6.6 191 6.4 187 6.2 182 6.1 175 6.2 167 6.5 164 6.7 166 6.3 174 166 6.3 174 186 186 186 186 186 186 186 186 186 186	201 2.9 194 2.8 186 2.7 178 2.4 169 143 1.8 131 1.8 131 1.8 131 1.8 131 1.8 131	246 2.9 245 2.2 245 1.5 247 0.8 254 0.2 302 0.4 31 0.7 48 0.6 63 0.6 63 0.7 44	196 0.2 1186 0.1 150 0.1 75 0.5 46 0.9 48 0.9 48 0.9 51 0.8 51 0.8 51 0.8 36	0.3 102 0.7 185 1.1 193 1.2 192 0.4 136 0.2 92 0.1 0.3 339	338 2.5 326 2.3 315 2.0 307 1.5 315 1.5 343 1.7 344 1.9 340 2.0 338 2.0 338	317 6.0 314 5.7 311 5.4 309 4.9 307 4.3 308 3.7 311 3.2 3.2 3.3 3.2 3.3 3.3 3.3 3.3 3.3 3.3	5.0 5.3 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0	354 3.0 358 3.0 3 2.9 8 2.7 15 2.4 24 2.2 34 2.0 49 2.0 51 2.1 2.5 49 2.2 58	186 2.4 181 2.0 174 1.7 164 1.4 150 103 134 1.2 123 1.2 120 1.2 121 1.2 121 1.2 121 1.2	184 2.5 184 1.8 1.8 1.8 1.8 1.8 1.8 1.8 1.8 1.8 1.8	75 1.2 62 0.9 36 0.8 334 0.7 316 0.5 299 0.2 264 0.2 212 0.1 187 0.0 177 0.1 345
10.0 9.5 9.0 8.5 8.0 7.5 7.0 6.5 6.0	0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603 0.9237 1.52 2.51 4.14	4.3 226 5.7 224 2.5 2.5 210 2.5 2.5 210 1.9 1.7 1.7 1.7 1.7 1.6 1.8 1.5 1.5 1.5 1.5 1.5 1.0 1.5 1.5 1.0 1.5 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	192 9.88 8.7 194 7.66 6.4 193 5.3 1.72 4.4 1.72 1.63 5.0 1.59 4.8 1.58 4.0 1.58 4.0 1.58	193 21.1 196 20.0 198 18.8 17.5 198 16.2 190 15.9 190 15.6 177 15.6 175 180 12.5 180 10.9	202 25.7 204 22.9 206 21.5 206 19.5 204 17.3 192 15.7 183 17.9 15.7 183 17.9 15.7 183 17.9 15.7 183 17.9 185 185 185 185 185 185 185 185 185 185	203 15.66 205 14.8 206 13.8 205 12.6 202 11.4 10.6 186 10.3 175 11.1 180 10.3 11.1 188 10.3 19.7 18.8 19.8	192 7.2 6.9 192 6.6 6.6 187 6.2 167 6.5 164 6.7 166 6.3 174 5.4 184	201 2.9 194 2.8 186 2.7 178 169 2.1 1.9 143 1.8 131 1.8 136 148 1.1 158 0.4 175	246 2.9 245 2.2 245 1.5 247 0.8 254 0.2 302 0.4 31 0.7 48 0.6 63 0.6 63 0.6 0.7 0.7 0.8 0.6 0.6 0.6 0.7 0.7 0.8 0.6 0.6 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7	196 0.2 186 1.6 0.1 1.50 0.1 1.50 0.3 52 0.5 46 0.9 48 0.9 51 0.8 51 0.8 6.8 6.8 28	49 0.3 102 0.7 185 1.1 193 1.2 192 1.1 184 0.7 169 0.4 136 0.2 92 0.1 1.0 0.2 311 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3	338 2.5 326 2.3 315 2.0 308 307 1.5 351 1.4 331 1.7 344 1.9 340 2.0 338 2.0 338 2.3	317 6.00 314 5.7 311 5.4 307 4.3 308 3.7 311 3.2 318 3.2 3.3 3.3 3.3 3.3 3.3 3.3 3.3 3.3 3.3	320 5.3 322 5.0 324 4.7 329 3.8 333 3.0 335 338 2.7 342 2.6 345 2.4 349 2.6 345 2.7 345 2.7 345 345 345 345 345 345 345 345	354 3.00 358 3.0 3 2.9 9 8 2.7 15 2.4 2.2 34 2.0 43 2.0 49 2.0 2.0 49 2.1 54 2.2 58 2.7 69 2.1 60 2 5 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	186 2.4 181 2.0 174 1.7 164 150 1.3 1.3 1.2 123 1.2 120 1.2 121 1.2 118 1.2 1.1 1.2 1.1 1.2	184 2.5 184 1.8 185 1.5 186 1.3 187 1.1 180 0.8 172 0.6 153 0.5 146 0.4 135	75 1.2 62 0.9 36 0.8 334 0.7 316 0.7 316 0.5 29 0.2 264 0.2 212 0.1 187 0.0 177 0.1 334
10.0 9.5 9.0 8.5 8.0 7.5 7.0 6.5 6.0 5.5	0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.9603 0.9237 1.52 2.51 4.14 6.83	4.3 226 3.7 224 5.1 219 2.5 2.5 2.5 2.7 1.7 1.7 1.7 1.7 1.6 1.8 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5	192 9.88 193 8.7 194 7.66 6.4 193 5.3 190 4.6 182 4.7 163 5.0 9.0 199 4.8 158 4.9 158 2.9 161 2.0 172	193 21.1 196 20.0 198 18.8 199 17.5 195 14.9 190 13.9 13.6 177 13.6 177 13.6 177 13.6 177 13.6 177 183 199 190 199 190 199 199 199 199 199 199	202 23.7 204 22.9 206 21.5 206 19.5 204 17.3 199 15.1 192 13.7 183 13.4 179 18.5 13.7 180 185 199 11.8 187 187 189 189 189 189 189 189 189 189 189 189	203 15.6 205 14.8 206 13.8 205 12.6 202 11.4 195 10.6 186 175 10.6 175 11.1 188 10.3 11.1 188 10.3 11.1 188 10.3 10.3 11.4 188 10.3 10.3 10.3 10.3 10.3 10.3 10.3 10.3	192 7.2 192 6.9 192 6.6 191 6.4 187 6.2 182 6.1 175 6.5 164 6.7 176 6.3 174 5.9 2.6 2.22	201 2.9 194 2.8 186 2.7 178 2.4 169 2.1 1.57 1.9 143 1.8 131 1.8 131 1.8 138 1.6 148 159 0.4 175 0.3 326	246 2.9 245 2.2 245 1.5 247 0.8 254 0.2 302 0.4 31 0.7 58 0.6 63 0.6 57 0.7 48 0.8 0.6 57 0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8	196 0.2 186 0.1 150 0.1 150 0.3 52 0.5 46 0.7 46 0.9 51 0.8 51 0.7 45 0.8 28 0.8 21	49 0.3 102 0.7 185 1.1 193 1.2 192 1.1 184 0.7 169 0.4 314 0.2 92 0.1 1.0 0.2 311 0.3 0.2 92 0.4 314 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.	338 2.5 326 2.3 315 2.0 308 1.8 307 1.5 315 1.4 331 1.7 343 1.9 340 2.0 338 1.8 339 1.8 339 1.8 339 1.8 341	317 6.00 314 5.7 311 5.4 4.9 307 4.9 307 4.3 308 3.7 311 3.2 325 3.3 3.3 3.3 3.3 3.3 3.3 3.3 3.3 3.3 3.	320 5.3 322 5.0 324 4.7 526 4.3 333 3.4 333 3.0 2.7 342 2.6 343 2.7 342 2.6 343 353 353 353 353 353 353 353	354 3.00 3.58 3.00 3.2.99 8 2.77 15 2.44 2.22 3.44 2.00 4.99 2.00 3.11 5.42 2.58 2.11 6.44 1.86 7.00	186 2.4 181 2.0 174 1.7 1.7 164 1.5 1.2 123 1.2 123 1.2 121 118 1.2 121 1.2 121 1.2 121 1.2 121 1.2 121 1.2 121 1.2 1.2	184 2.5 184 1.84 1.85 1.5 186 1.3 187 1.1 185 1.0 0.8 172 0.7 162 0.6 153 0.5 146 0.4 135 0.4 135 0.4 135 0.4 135 0.4 135 0.4 135 0.5 0.5 135 135 0.5 135 0.5 10 10 10 10 10 10 10 10 10 10 10 10 10	75 1.2 62 0.9 36 0.8 1 0.8 334 0.7 316 0.5 299 0.2 264 0.2 212 0.1 187 0.0 177 0.0 177 0.1 349 0.2 234 0.7 349 0.7 356 0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8 0.8
10.0 9.5 9.0 8.5 8.0 7.5 7.0 6.5 6.0 5.5	0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603 0.9237 1.52 2.51 4.14 6.83	4.3 226 5.1 219 2.5 2.5 2.5 2.10 1.9 1.7 1.7 1.7 1.7 1.7 1.6 1.8 1.9 1.9 1.0 1.9 1.9 1.0 1.9 1.9 1.0 1.9 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	192 9.88 193 8.7 194 7.66 6.4 193 5.3 190 4.6 182 4.7 163 159 4.8 158 4.0 158 2.9 161 2.0 172	193 21-11 196 20.0 198 18-8 199 17-5 198 16-2 195 14-9 190 13-6 177 13-6 175 13-6 175 180 10.9 186 9.0 194 9.0 194 9.0	202 23.7 204 22.9 206 21.5 206 19.5 204 17.3 199 13.7 183 17.8 17.8 17.8 17.8 17.8 17.8 17.8 17.8	203 15.6 205 14.8 206 13.8 205 12.6 202 11.4 195 10.6 175 11.1 180 11.1 188 10.3 197 8.4 206 6.2 220 206 207 207 207 207 207 207 207 207 207 207	192 7.2 6.9 192 6.9 191 6.4 187 6.2 167 6.5 164 6.7 166 6.3 3.9 200 2.6 222 2.553	201 2.9 194 2.8 186 2.7 178 2.4 169 2.1 1.57 1.9 143 1.8 131 1.8 138 1.6 1.8 1.9 1.9 0.3 326 0.7 356	246 2.99 245 2.2 245 1.5 247 0.8 254 0.2 0.4 310 0.7 48 0.7 48 0.6 63 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6 0.6	196 0.2 186 0.1 150 0.1 175 0.3 52 0.5 46 0.7 46 0.9 48 0.9 51 0.8 51 0.7 45 0.8 28 0.8 21 0.7	49 0.3 102 0.7 185 1.1 193 1.2 192 1.1 184 0.7 169 0.4 136 0.2 92 0.1 0.3 331 0.3 331 0.4 321 0.4 321 0.3 331 0.4 0.3 331 0.4 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.5	338 2.5 326 2.3 315 2.0 308 1.8 307 1.5 3315 1.4 3311 1.5 343 1.7 344 1.9 340 2.0 338 2.0 338 1.8 2.0 338 1.9 340 2.0 340 340 340 340 340 340 340 340 340 34	317 6.00 314 5.7 311 5.4 4.9 309 4.9 307 318 3.2 318 3.2 3.2 3.3 3.2 3.3 3.2 3.3 3.3 2.7 3.3 3.3 2.7 3.3 3.3 2.7 3.3 3.3 2.7 3.3 3.7 3.3 3.7 3.7 3.7 3.7 3.7 3.7 3	320 5.3 322 5.0 324 4.7 326 4.5 329 3.8 3.3 3.3 3.3 3.3 3.3 3.3 2.6 3.6 3.7 3.2 2.6 3.6 3.7 3.7 3.7 3.7 3.7 3.7 3.7 3.7	354 3.00 3.00 3.00 3.00 3.00 3.00 2.77 15 2.44 2.22 3.44 2.00 51 2.10 51 2.10 51 2.10 51 2.10 51 2.10 51 2.10 51 51 51 51 51 51 51 51 51 51 51 51 51	186 2.4 181 2.0 174 1.7 1.7 164 1.3 1.3 1.3 1.3 1.2 123 1.2 121 1.2 121 1.2 121 1.2 1.3 1.3 1.2 1.3 1.2 1.3 1.3 1.3 1.3 1.3 1.3 1.3 1.3 1.3 1.3	184 2.5 184 1.84 1.85 185 186 1.5 186 1.3 180 180 0.8 172 0.7 162 0.6 153 0.5 146 0.3 119 0.3 119 0.3	75 1.2 0.9 36 0.8 10.8 334 0.7 516 0.5 299 0.2 264 0.2 212 0.1 187 0.0 177 0.1 187 0.0 177 0.3 345 0.3 0 0.3 0 0.3 0 0.3 0 0.3 0 0.3 0 0.3 0 0.3 0 0 0.3 0 0 0.3 0 0 0 0
10.0 9.5 9.0 8.5 8.0 7.5 7.0 6.5 5.0 4.5	0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603 0.9237 1.52 2.51 4.14 6.83 11.25	4.3 226 5.7 224 5.1 219 2.5 210 1.9 194 1.7 161 1.8 159 1.0 147 0.1 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	192 9.8 193 8.7 194 6.4 193 5.3 190 4.6 182 4.7 163 5.0 158 2.9 158 2.9 161 172 1.6 192 1.9 1.9 1.9 1.9 1.9 1.9 1.9 1.9	193 21.1 196 20.0 198 18.8 199 17.5 198 16.2 199 13.9 13.6 177 13.6 175 13.6 12.5 180 199 183 13.6 175 180 199 183 199 183 183 183 184 199 183 183 184 185 186 186 187 187 187 187 187 187 187 187 187 187	202 23.7 204 22.9 206 19.5 206 17.5 199 15.1 17.5 183 13.4 179 18.0 14.0 18.5 19.7 18.5 19.7 18.5 19.7 18.5 19.7 18.5 19.7 18.5 19.7 19.7 19.7 19.7 19.7 19.7 19.7 19.7	203 15.6 205 14.8 206 13.8 205 12.6 202 10.6 186 10.3 178 10.6 175 11.1 188 10.3 178 11.1 188 10.3 178 11.1 188 206 202 205 205 205 205 205 205 205 205 205	192 7.2 7.2 192 6.9 192 6.6 191 6.4 187 6.2 182 6.5 164 6.5 164 6.3 184 5.4 184 5.9 2.6 2.2 2.5 2.5 3.0 3.0 3.0	201 2.9 194 2.8 186 2.7 178 2.4 169 2.1 157 1.9 1.3 1.8 1.3 1.8 1.3 1.6 1.6 1.7 5 0.7 356 0.7 356 1.0 1.0	246 2.99 245 2.22 245 2.47 0.88 254 0.2 302 0.4 31 0.7 58 0.6 63 0.6 63 0.7 44 0.9 28 1.0 24 1.11 22	196 0.2 186 0.1 150 0.1 75 0.3 3 2 0.5 46 0.9 51 0.8 36 0.8 36 0.8 28 0.8 21 0.7 16 0.7 10	49 0.3 102 0.7 185 1.1 193 1.2 192 1.1 184 0.7 169 0.4 136 0.2 92 0.1 0.2 311 0.3 339 0.4 314 0.3 337	338 2.5 326 2.3 315 326 2.0 308 1.8 8 307 1.5 343 1.7 344 2.0 338 2.0 338 1.5 343 1.1 344 0.5 53 353	317 6.00 314 5.7 311 5.4 309 4.9 307 4.3 308 3.7 311 3.2 325 3.3 3.2 3.2 3.3 3.3 3.3 3.3 3.3 3.3 3.3	320 5.3 322 5.0 324 4.7 326 4.3 329 3.8 331 333 3.0 335 2.8 337 2.8 342 2.6 345 2.4 349 2.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3	354 3.00 3.58 3.00 3.00 8 2.77 15 2.4 2.4 2.00 4.9 2.00 4.9 2.00 4.9 2.00 4.9 2.00 4.9 2.00 4.9 2.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00	186 2.4 181 2.0 174 167 167 168 1.7 168 1.3 154 1.2 123 1.2 120 1.2 121 1.2 1.2	184 2.5 184 1.88 1.5 185 1.5 186 1.3 187 1.1 185 1.0 180 0.8 172 0.7 162 0.7 162 0.7 162 0.7 162 0.7 163 0.8 153 0.8 163 0.0 163 0.0 163 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	75 1.2 0.9 0.9 36 0.8 1 0.8 1334 0.7 316 0.5 299 0.2 264 0.1 187 0.0 177 0.0 177 0.0 1734 0.3 335 0.3 335 0.3 335
10.0 9.5 9.0 8.5 8.0 7.5 7.0 6.5 6.0 5.5 5.0 4.5	0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.9603 0.9237 1.52 2.51 4.14 6.83 11.25 18.55 30.59	4.3 226 5.7 2244 5.1 1219 2.5 2100 1.9 194 1.7 7161 1.8 159 1.0 147 7.7 121 0.5 94 1.7 163 1.9 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6	192 9.8 8.7 193 8.7 194 6.4 193 5.3 193 4.6 182 4.7 163 5.0 159 4.8 4.7 163 159 4.8 4.9 159 161 172 1.9 1.9 1.9 1.9 1.9 1.9 1.9 1.9	193 21.1 196 20.0 198 199 17.5 198 16.2 199 183 183 13.6 175 13.4 175 13.6 175 13.6 175 13.6 175 13.6 175 180 198 198 198 198 198 198 198 198 198 198	202 23.7 204 22.9 206 21.5 206 19.5 204 17.3 1992 13.7 180 14.0 185 191 11.8 197 9.3 202 209 200 6.6 291	203 15.6 205 14.8 205 12.6 202 11.4 195 10.6 186 10.3 178 10.6 175 11.1 188 10.3 197 18.4 206 6.2 220 230 240 250 250 250 250 250 250 250 250 250 25	192 7.2 6.9 192 6.9 192 6.6 191 6.4 187 6.2 182 182 167 6.5 164 6.7 166 6.3 174 5.4 184 3.9 200 2.6 2.5 253 3.0 3.0 3.9 3.8	201 2.9 194 2.8 186 2.7 178 2.1 169 2.1 157 1.9 143 1.8 131 1.8 136 1.6 148 1.1 158 0.4 175 0.3 326 0.7 356 0.7 356 0.7 356 1.0 16 1.2 39	246 2.99 245 2.22 245 5.247 0.88 254 0.2 302 0.4 31 0.7 58 0.6 63 0.6 63 0.6 63 0.6 1.0 28 1.0 28 1.1 22 1.11 20	196 0.2 186 0.1 150 0.1 75 0.3 52 0.5 46 0.9 51 0.8 51 0.8 28 0.8 28 0.8 21 0.7 10 0.6 4	49 0.3 102 0.7 185 1.1 193 1.2 1.1 192 1.1 1.1 192 1.1 1.3 1.2 2.2 1.1 1.3 1.3 1.3 1.3 1.3 1.3 1.3 1.3 1.3	338 2.5 326 2.3 307 308 1.8 307 1.5 331 1.5 343 1.7 344 2.0 338 2.0 338 2.0 338 339 1.5 338 1.9 340 2.0 358 358 358 358 358 358 358 358 358 358	317 6.00 314 5.7 311 5.4 309 4.9 307 4.3 307 4.3 308 3.7 311 3.2 325 5.3 329 3.3 3.3 2.7 3.3 3.3 2.7 3.3 4.9 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0	320 5.3 322 5.0 324 4.7 526 4.3 329 3.8 333 3.0 3.3 3.0 3.3 3.4 3.3 3.5 2.8 3.3 3.5 2.8 3.3 3.5 3.5 3.5 3.5 3.5 3.5 3.5	354 3.00 3.58 3.00 3.00 3.2.9 8.7 15 2.4 2.4 2.4 2.0 51 2.1 64 4.8 8.7 70 1.4 9.6 1.8 9.6 9.6 9.6 9.6 9.6 9.6 9.6 9.6 9.6 9.6	186 2.4 181 2.0 174 1.7 164 1.4 150 1.3 1.4 1.2 123 1.2 120 1.2 121 1.2 121 1.2 121 1.2 1.1 1.5 1.1 1.5 1.1 1.5 1.1 1.5 1.1 1.5 1.1 1.5 1.1 1.5 1.1 1.5 1.6 1.6 1.6 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7	184 2.5 184 1.8 1.8 1.8 1.8 1.8 1.8 1.8 1.8 1.8 1.8	75 1.2 0.9 3.6 0.8 1 0.8 1334 0.7 252 264 0.1 187 0.0 2.2 224 0.1 187 0.0 1.7 0.1 0.5 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3 0.3
10.0 9.5 9.0 8.5 8.0 7.5 7.0 6.5 5.0 4.5	0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603 0.9237 1.52 2.51 4.14 6.83 11.25 18.55 30.59	4.3 226 5.7 224 5.1 219 2.5 210 1.9 1.7 161 1.7 161 1.8 1.9 1.7 160 1.5 1.5 1.9 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7	192 9.8 8.7 194 7.6 7.6 194 6.4 193 190 4.6 182 4.7 163 5.0 158 4.8 158 2.9 161 2.0 172 1.6 192 2.5 2.6	193 21.1 196 20.0 198 199 17.5 198 16.2 195 14.9 190 15.9 1183 15.6 177 13.6 176 12.5 180 10.9 194 6.9 203 4.8 214	202 23.7 204 22.99 206 21.5 206 19.5 204 17.3 199 15.1 192 13.7 180 14.0 185 191 11.8 197 202 6.2 209 3.0 220 0.6	203 15.6 205 14.8 206 13.8 205 12.6 202 11.4 195 10.6 175 11.1 188 10.3 11.1 188 10.3 11.1 188 205 202 202 202 203 203 203 204 205 205 205 205 205 205 205 205 205 205	192 7.2 192 6.9 192 6.9 191 6.4 187 6.2 187 6.2 167 6.5 164 6.7 166 6.3 174 184 3.9 200 2.6 222 1.5 3.0 0.8 3.0 0.9	201 2.9 194 2.8 186 2.7 178 2.4 169 2.1 157 1.9 143 1.8 131 1.8 1.6 148 8 0.4 1.158 0.4 1.5 0.3 326 0.7 356 1.0 16 1.2	246 2.99 245 245 1.247 0.8 254 0.2 302 0.4 31 0.7 48 0.6 63 0.6 657 0.7 44 0.8 34 0.9 28 1.0 24	196 0.2 186 0.1 150 0.1 75 0.3 52 0.5 6 0.7 46 0.9 51 0.8 51 0.8 28 0.8 21 0.7 16 0.7 10 0.6	49 0.3 102 0.7 185 1.1 193 1.2 192 1.1 184 40.7 169 0.4 136 0.2 311 0.3 309 0.4 321 0.3 327 0.2 337 0.1 0.4 321 0.3 327 0.2 337 0.1	338 2.5 326 2.3 315 307 1.5 307 1.5 315 1.4 331 1.7 343 1.7 344 1.9 340 2.0 338 2.0 338 1.8 339 341 1.1 343 1.8 343 1.8 343 1.8 343 1.8 344 1.8 345 1.8 346 1.8 1.8 1.8 1.8 1.8 1.8 1.8 1.8 1.8 1.8	317 6.00 314 5.7 311 5.4 309 4.9 307 4.3 308 3.7 311 3.2 325 3.3 3.2 3.2 3.3 3.3 3.2 3.3 3.3 3.3 3.3	320 5.3 322 5.0 324 4.7 326 4.3 339 3.8 331 3.3 3.0 335 338 2.7 342 2.6 345 349 2.0 357 357 357 357 357 357 357 357	354 3.00 3.03 3.03 3.03 3.03 3.03 2.97 1.52 2.44 2.44 2.00 4.33 2.00 5.11 5.44 2.12 5.66 7.01 1.47 7.91 1.60 1.60 1.60 1.60 1.60 1.60 1.60 1.6	186 2.4 181 2.0 174 1.7 1.6 1.3 1.5 1.2 123 1.2 120 1.2 121 1.2 121 1.2 121 1.2 121 1.3 1.3 1.4 1.2 1.2 1.3 1.3 1.4 1.4 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5	184 2.5 184 1.8 1.8 1.8 1.8 1.8 1.8 1.8 1.8 1.8 1.8	75 1.2 62 0.9 36 0.8 1 1 0.8 534 0.7 316 0.5 22 22 212 0.1 187 0.2 2212 0.1 197 0.2 334 0.2 334 0.3 335 0.3 335 0.3 336 0.3 3 0.3 3 0.3 3 0.3 3 0.3 3 0.3 3 0.3 3 0.3 3 0.3 3 0.3 3 0 0.3 3 0.3 3 0.3 3 0.3 0 0.3 0 0.3 0 0.3 0 0.3 0 0.3 0 0.3 0 0.3 0 0.3 0 0.3 0 0.3 0 0.3 0 0.3 0 0.3 0 0.3 0 0.3 0 0.3 0 0.3 0 0 0.3 0 0 0.3 0 0.3 0 0.3 0 0.3 0 0.3 0 0.3 0 0.3 0 0.3 0 0.3 0 0.3 0 0.3 0 0.3 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0.0 0 0 0.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0

AUGUST MEAN TEMPERATURE AMPLITUDE (K) AND PHASE WAVE I SCALE PRESSURE HEIGHT (mb) 2.43 3.63 2.29 0.55 0.38 1.20 12,0 0,0062 1.08 0.78 1.29 1.54 2.11 1.93 0.97 0.81 274 257 252 237 245 260 302 284 1,60 0,52 11.5 0.0103 2.80 4.00 2,54 0.85 0.50 1.05 0,94 0.70 1,21 235 2,01 259 0.89 0,83 1,70 0.57 2,47 3,19 4.34 2.88 1,28 0.69 0.77 0,54 1,03 231 1.75 1,63 0,70 267 0.59 2.37 10.5 0.0279 4.78 3,47 213 0,60 205 0.35 0.76 1,11 1,32 1,22 339 0.70 1,45 0.55 1,92 4.14 5.34 2,74 1,55 1.01 0.86 0.32 0.51 0.84 0.75 0.44 0.54 1.08 4,35 169 1.12 9.5 0.0758 4.41 5.85 5.36 3,72 2.20 1,71 1,42 0.56 0.48 0,63 0.55 188 0.73 0.35 0.58 166 0.34 4.27 6.07 258 2,32 1,89 0.80 0.52 0.95 8,5 0.2061 3.59 5,75 5,38 3,60 2.58 1.99 0.86 0,67 132 0.66 0.60 0.84 0.11 6.46 0.36 344 5.06 2.47 1.74 0.73 0.47 0.3398 6.00 5,41 3.92 0.14 0.35 0.32 0.38 0.13 0.35 345 2,79 4.06 4,54 4.02 3.20 1.20 0.47 0.18 0.12 0.24 0.17 288 0.02 0.27 4.01 4.16 5 334 7.0 0.9237 2.89 2.92 2.16 1.50 0.82 0.33 0.15 0.15 0.29 0,29 0.53 0.31 267 239 0,17 355 0.02 6.5 1,52 2,64 4.49 5,28 3,82 2.03 1,04 0,38 0.14 0.06 0.17 199 0,31 0,29 0,17 0,02 6.0 2.51 2.38 4.88 6.49 73 41 12 5,21 2,71 1,12 0.25 0.06 0.04 0.08 0.16 0.25 0,16 0.32 0.13 195 0.09 55 6.59 0.23 0.32 5.5 5.42 0.10 0.39 5.0 2,69 4.93 3.01 1,58 0.13 4.83 6.05 0.66 0,20 0.33 0.51 11,25 1.35 0.75 5 328 4.5 122 4.66 5,49 4.31 2.53 96 73 56 36 0.24 0.15 305 258 0.18 0.52 0,76 0,61 0,36 322 310 4.0 3,55 5.31 6.03 4.38 2.15 0.94 0.74 0,25 0,17 0,22 0.68 0.95 0.77 311 0.60 0.54 327 313 3.5 30,59 4.21 6.34 6.75 4.73 2.08 0.57 0,69 299 0.17 0.23 0.72 256 0.63 0.43 0.67 315 3.0 5,11 6,13 4,49 170 143 122 1.97 0.30 0.59 0,21 0.14 0.22 0.68 0.95 0.75 0.38 0,61 0.57 2.5 83.15 1.17 3.07 4.35 3.44 1.58 0.21 0.41 0.15 0.11 0.17 0.54 0.75 0.59 0.29 206 181 151 130 118 103 293 295 265 278 261 259 276 330 AUGUST MEAN GEOPOTENTIAL HEIGHT AMPLITUDE (dam) AND PHASE SCALE PRESSURE HEIGHT (mb) -50 -30 -20 -10 10 20 30 40 50 60 12.0 0.0062 33.3 35.3 30.1 28.9 240 273 277 18.1 12.3 11.1 6.6 8.2 11.7 15.7 16.7 6.2 11.5 13.6 3.9 29.5 17.4 10.8 6.9 6.2 9.6 13.0 14.3 5.1 10.4 11.1 3.4 7.7 10.6 11.0 0.0169 25.1 25.7 29.8 27.9 16.6 206 10.5 5.9 5.8 3.0 20.1 26.6 15.5 10.0 5,1 3.9 5.6 198 8.7 270 2.8 4.9 346 203 10.0 0.0460 219 26.6 24.6 14.0 9.1 170 192 7.3 196 9.2 4.2 2.9 0.0758 9.5 7.3 322 22.0 12.2 8.1 4.6 167 3.7 6.4 5.0 7.0 3.3 3.0 7.7 22.5 10.4 2.9 9.0 0.1250 3.1 6.4 19.6 6,5 5.9 179 3.2 8,1 6.2 6.8 2.9 11.1 12.5 22.8 18.9 9.5 265 4.7 195 186 2.6 5.8 8.2 7.6 6.8 3.2 3.1 5.6 0.3398 15.6 18.9 25.1 20.9 10.8 4.6 2.6 8.5 3.7 6.7 7.5 0.5603 19.2 27.3 27.5 24.2 13.5 7.9 4.8 2.4 2.1 2.6 5.8 8.4 6.4 4.0 21.6 25.5 28.0 106 56 7.0 0.9237 26.0 15.5 1.9 304 1.9 2.5 5.4 8.0 7.8 6.0 3.8 2.7 1.9 26.1 314 1.8 7.7 7.2 2.7 258 6.5 1.52 22.9 26.1 24.7 15.4 8.1 1.6 2.5 5.1 5.6 3.6 258 2.51 23.2 23.6 21.4 13.4 7.1 316 239 1.8 2.5 4.9 7.4 6.9 239 5.2 3.5 2.6 294 5.5 4.14 168 27.0 22.2 10.4 5.2 3.7 1.5 1.8 213 4.7 7.1 6.6 245 3.3 2.6 5.0 21.8 22.4 6.83 27.7 15.1 7.5 3.0 3.0 224 1.7 2.2 225 6.5 6.2 238 243 3.1 2.4 254 4.5 11.25 27.6 12.9 5.4 2.0 5.6 226 5.6 234 3.9 158 0.9 211 3.8 2.1 4.0 18.2 25.9 20.9 10.3 138 1.0 1.3 1.7 1.8 4.9 3.7 1.5 3.1 4.5 2.7 233 18.1 8.1 3.8 1.9 1.0 1.6 1.6 1.7 195 3.7 3.0 2.0 3.0 50.43 233 17.8 17.3 9.2 4.5 2.5 1.8 1.7 1.7 2.2 180 199 1.4 3.9 3.5 2.5 83.15

205 192 2.9

ORIGINAL PAGE IS

AUGUST	MEAN	TEMPERA	TURE I	MPLITU	DE (K)	AND P	HASE	WAVE	, (OF	PO	OR	QU	ALI	TV				
SCALE	PRESSURE	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80	
HEIGHT 12.0	(mb) 0,0062	0.25	0.92	1,17	1,55	1.87	1.23	0.49	1.08	1,51	0.85	0.93	1.32	0.61	0.39	0,91	0.07	1,21	
11.5	0,0103	0,18	141	1,19	1.52	1,83	118	0,48	1.09	1,47	0.83 138	0.91 118	1.29	90	102 0.39 102	1,00	0.09	1.33	
11.0	0.0169	0.06	1.20	1.15	109	1,67	1,23	0.43	1.02	1,33	0.74	0.81	103	0.46	0,37	162	0.12	1,37	
10.5		0,07	155	116	119	117	1.17	152	143	1.10	0,61	0,62	103	0.28	0.31	164	201	315	
10.0	0.0460	219	163	130	137	130	12.	147	146	165	151	121	105	62	0.22	167	187	307	
9,5	0.0758	0,21 215 0,31	1,51	1.08	162	1,63 165 1,98	0.98 140 0.85	138	0.74	0.85	0.47 167 0.37	0.39	0.55	0,20 357 0,41	95	0.87 173 0.66	180	1.07 291 0.85	
9.0	0,1250	0.34	176	169	184	186	156	0.16	160	195	192	0.12	128	314	75	184	0.34 179 0.34	264	
8,5	0,2061	214	185	1,67	196	198	177	233	177	0.29	219	265	258	301	338	210	185	0.77	
8.0	0.3398	217	201	203	203	205	200	263	208 C.26	254 0,13	230	290	271	296	314	266	213	197	
		228	241	214	2.07	209	221	259	239	312	139	0.16 308	0.37 278	291	309	308	281	169	
7,5	0.5603	241	274	199	1,74	1.16	172	0,56	226	62	95	53	285	286	305	329	306	109	
7.0	0,9237	0.18 236	250	1.52	2.17	1,84	1.34	186	0.18	0.18 93	0.23	120	312	287	301	346	308	0.28	
6.5	1,52	237	203	172	2.94 167	170	1.91	170	168	129	0.13	0.05	5.12 321	306	301	345	289	0.14 86	
6.0	2.51	245	208	181	3.77	3.41	182	1.04	170	169	0.10	360	0.22 329	318	317	299	283	172	
5.5	4,14	0.52 262	233	2.24	3.06	2,80	203	188	0.19	0.07	0.07	0.14 354	0.33 342	2.28 556	319	290	288	169	
5.0	6,83	285	271	1.86 242	2,68 246	2,52 250	1.55 234	212	165	0.05	0.05	0.25 355	349	0.32 351	323	285	0.13 296	162	
4.5	11.25	315	1,63 307	2,54	3,45	2.83	1.46 273	0.39 263	108	0.06 76	0.05	0.35 357	0.52 393	0.37	0.18	0.25 284	308	0.09	
4.0	18,55	1.03 340	329	3.93	4.47 307	3,24 305	1,66	0.49 311	0.07	0.08	0.06	0.40 357	356	0.39	0.17	0.28	0.10	0.05	
3,5	30,59	1.56 354	3,45	4,60	4.83	3.33	1.81 318	0,64	0.11	0.09	0.07	0,39	0.52 358	0.37	0.13	0.27	0.09	0.06	
3.0	50,43	0.97	2,75	4.05	4.33 324	2.94 325	1.72	0,68	2.12	0.08	0.07	0.35	359	0.31	0.10	0.22	0.08	0.06	
2.5	83,15	0.47	1,59	2.77 334	3,16	2.18 330	1.33	0.55	0.10	0.06	0.06	0.26 360	0.55	0.23	0.06	0.16	0.05	0.05	
AUGUST	MEAN (GEOPOTE	NTIAL	HEIGHT	AMPLI	TUDE (dam) A	IND PHA	ISE .	AVE 2									
SCALE	PRESSURE (mb)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80	
12.0	0.0062	3.8	15.1	22,4	28.5	26.8	18,1	7.7	9.0	8,6	5.9	3.5	4,6	5,2	2.3	5,4	2,2	7.3	
11.5	0,0103	4,1	14,3	192	198	196	17.3	7.1	7,5 154	6.7	148	2.4	3.2	5.4	2,2	189	256	286	
11.0	0.0169	4,2	13.3	197	28.8	202	16.5	6,6	6.0	5.0	152	1.6	2.7	5,6	18	198	257	4.6	
10.5	0.0279	250	12.2	201	28,5	207	191	6.2	4.6	168	156	1,6	3.2	5.7	2.5	215	1.9	3.7 235	
10.0	0,0460	4.0	10.9	205	27,6	212	197	6.0	3.4	172	159	2.0	343	5.6	351	2.4	1.9	3.4	
9.5	0.0758	3.7 255	9.7	209	214	216	14.5	5.9	165	176	160	2,3	4.3	5.2	342	276	277	3.3	
9.0	0,1250	3,4	8,6	213	217	21,4	13.7	205	169	172	151	345	326	4.5	337	3,1	291	183	
8.5	0,2061	3,1	7.6	216	220	18.4	210	206	170	0.9	128	346	327	327	335	313	303	163	
8.0	0.3398	266	258 6.7	219	17.7	16.1	211	203	162	104	109	352	333	335	336	322	313	141	
7.5		271	266	12.1	15.6	231	212	197	146	96	101	358	340	347	340	327	321	118	
7.0		2.7 273	5.9 267 5.4	223	231	236	213	191	131	96	101	2.1	3.7 345 3.6	356	344	329	326	106	
6.5	1,52	2.6 275 2.3	267	229	241	15.0	220	188	120	1.0 95 0.8	104	2.1 358	347	2.7	348	328	333	0.9	
		282	272	243	256	256	233	192	1.0	89	104	356	348	2.6	354	325	340	132	
6.0	2,51	1.9 295	287	266	276	273	7.6 253	210	87	76	88	356	350	10	1.4	325	348	132	
5.5	4,14	316	338	8.3 291	295	291	6.7 278	262	66	64	61	356	352	16	1.2	329	358	113	
5.0	6.83	3/8	3.7	7.9	311	306	5.9 300	328	1.0	0.7 56	40	1.7 356	353	1.8	1.1	339	0.9	0.4 85	
4.5	11.25	0.7	358	6.0 330	326	9.8 319	319	359	51	0.6	0.2	1.3 356	1.6 354	33	1.0	0.9 356	0.9	60	
4.0	18.55	1.2	1.8	2.8	6.6 350	6.1 337	341	1.1	1.0	0.5	0.1	0.7 355	0.8 353	0.9	0.9	0.9	0.8	0.3	
3.5	30.59	2.8 148	138	5.6 113	65	2.6	1.5	73	0.9	0.4	0.1 324	0.2 346	0.1 276	0.5	63	1.0	0.7	0.3	
3.0	50,43	4.6	9.9	11,5	8.9 113	107	2.7	1.6	0.7 62	0.2	0.1 263	0.4	0.7 184	0.4	0.9 73	1.3	0.7	0.2	
2.5	83,15	5.5 166	12.8	16.3	13.8	7.6 126	4.6	2.2 130	0.6	0.1	0.2	0.8	1.3	0.7	0.9	1.5	0.6	0.1	

	ER MEAN T	- Miles						WAVE										
SCALE HEIGHT	PRESSURE (mb)		-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
12.0	0.0062	210	2.72 197	180	1,29	0,53	249	322	0.41	121	1.08	0.89	0.39	0.53	1.02	0.91	0.57	0.78
11.5	0.0103	2,26	2.79 206	2.25 189	1.27	0.65	234	322	0.47	0.51 116	1.08	0.85 134	0.33	0.46	0.97	0.88	0.57	0.82
11.0	0.0169	2,66	2,79	2.08	202	0.77 228	219	0.14 326	0.54	109	1.02	136	0.25	0.34	0.84	0.75	133	0.79 78
10.5	0.0279	3,23 246	2.94	2,08	231	0.92 232	0,66	0.04	0,64 86	0,66	0.90	0.56	0,21	0.22 329	0.62	0.56	139	0.68
10.0	0.0460	3,95 258	3,53	2.64 263	1.78	1.08	0.85	0.25	0.73	0.76	0.74	0.33	0.37	0.32	0.40	0.37	0.25	0.53
9,5	0.0758	4,73	4.63	3.86 283	2,62	1,23	0.96	0.45	0.81	0.81	0.52 96	0.18	0.58 258	0.55	0.39 309	0.45 310	0.17	0.34
9,0	0.1250	5.34	5.97 294	5.39 294	3,62 288	1,41 265	0.91	0.55	0.77	0.70	0.21	0.35	0.73	0.66	0.58	0.69	0,32	0.10
8,5	0.2061	5.51	7.10	6.77	4.51	1.68	0.54	0.47	0.52	0.35	0.22	0.52	0.69	0.53	0.67	0.79	0.51	0.28
8.0	0.3398	5,21	7.56 312	7,50	5,00	2,10	0,25	0.20	0.10	0.23	0.63	0.56	0,45	0.34	0.54	0.64	C.63	0,60
7.5	0,5603	3,93	6.33	6.41	4,29	2,11	0.62	0.17	0,41	0,62	0.70	0.36	0.09	0.51	0.32	0.34	0.58	0.58
7.0	0.9237	2.86	4.81	5,53	4.08	2,40	1.14	0.51	0,59	0,60	0.52	0.21	0.10	0.51	0.37	0.55	0.69	0.47
6.5	1,52	3.60	4,50	5.30	4,53	3,08	1.86	0.89	0.54	0.36	0.31	0.18	0.10	0.27	0.31	0.85	1.03	0.57
6.0	2,51	5.55	6.40	5.86	5.22	3,93	2,62	1.28	0,51	0.27	0.26	0.17	0.10	0.19	0.22	1,13	1.31	0.73
5.5	4.14	6.73	8.01	6.04	4,65	3,66	2,52	1,29	0.46	0.24	0.24	0.11	0.15	0.17	0.25	1,13	1.17	0.50
5.0	6.83	7.27	9.18	7.21	4.91	3.20	2.02	1.13	0.39	0.23	0.21	0.16	0.29	0.13	0.38	0.93	0.80	0.17
4,5	11,25	7.34	10.02	9.36	6.61	3.28	1.29	0.85	0.31	0.23	0.18	0.30	0.47	0.05	0.49	0.59	0.41	0.19
4.0	18,55	7.28		11.57	8.31	3.88	0.98	0.52	0.25	0.23	0.18	0.43	0,61	0.06	0.55	0.37	0.55	0.48
3,5	30,59	7.04	10.76	12.19	8.87	4.28	1.27	0.28 316	0.23	0.23	0.18	0.50	0,65	0.11	0.52	0.45	0.80	0.64
3.0	50,43	4.79	8.27	10.43	7.95	4.03	1.47	0,25	0.23	0.21	0.19	0.49	0,61	0.14	0.43	0.52	0,84	0,62
2.5	83,15	2.66	4,92	7.27	5.91	3.13	1.28	0.24	0.18	0.16	0.15	0,39	0.47	0.12	0.31	0.46	268	0,47
		169	124	94	84	85	82	51	316	290	309	281	294	76	117	269	273	256
	BER MEAN G									AVE 1								
	PRESSURE (mb)	-80	-70	HEIGHT	AMPLI	TUDE (dam) A	ND PHA	SE #	AVE 1	10	20	30	40	50	60	70	80
SCALE	PRESSURE										10 6.2 156	20 6.6 195	30 7.9 235	40 4.2 278	50 2.1	60 3.3 90	70 4.9 138	5,5
SCALE HE I GHT	PRESSURE (mb)	-80 26.0	-70 35.5	-60 33.0	-50 27.5	-40 21.3	-30 15.5	-20 9.6	-10 4.7	0	6.2	6.6	7.9	4.2	2,1	3.3	4.9	
SCALE HEIGHT 12.0	PRESSURE (mb) 0,0062	-80 26.0 353 28.3	-70 35.5 346 38.9	-60 33.0 321 35.6	-50 27.5 315 28.9	-40 21.3 303 21.1	-30 15.5 257 15.0	-20 9.6 232 9.6 229 9.6	-10 4.7 151 4.4	0 4.8 150 4.1	6.2 156 5.1	6.6 195 6.1 205 5.8	7.9 235 8.0 239 8.1	4.2 278 4.5 270 4.7	2.1 17 1.0 338 1.3	3.3 90 2.3 108	4.9 138 4.1 141 3.3	5.5 52 4.5 46 3.5
SCALE HEIGHT 12.0	PRESSURE (mb) 0.0062 0.0103	-80 26.0 353 28.3 358 30.8	-70 35.5 346 38.9 350 41.9	-60 33.0 321 35.6 325 37.6 329 38.7	-50 27.5 315 28.9 317 30.0 320 30.4	-40 21.3 303 21.1 305 21.0 308 20.6	-30 15.5 257 15.0 257 14.5 259 13.9	9.6 232 9.6 229 9.6 227 9.7	-10 4.7 151 4.4 158 4.1 168 4.1	0 4.8 150 4.1 157 3.5 168 3.2	6.2 156 5.1 168 4.4 184 4.3	6.6 195 6.1 205 5.8 216 5.7	7.9 235 8.0 239	4.2 278 4.5 270	2.1 17 1.0 338	3.3 90 2.3 108	4.9 138 4.1 141	5.5 52 4.5 46 3.5 3.7 2.8
SCALE HEIGHT 12.0 11.5	PRESSURE (mb) 0.0062 0.0103 0.0169	-80 26.0 353 28.3 358 30.8 3	-70 35.5 346 38.9 350 41.9 353 44.3	-60 33.0 321 35.6 325 37.6 329	-50 27.5 315 28.9 317 30.0 320	-40 21.3 303 21.1 305 21.0 308	-30 15.5 257 15.0 257 14.5 259	9.6 232 9.6 229 9.6 227 9.7 227	-10 4.7 151 4.4 158 4.1 168	0 4.8 150 4.1 157 3.5 168	6.2 156 5.1 168 4.4 184	6.6 195 6.1 205 5.8 216	7.9 235 8.0 239 8.1 242 8.0	4.2 278 4.5 270 4.7 263 4.7	2.1 17 1.0 338 1.3 267 2.1	3.3 90 2.3 108 1.9 139 2.1	4.9 138 4.1 141 3.3 143 2.7	5.5 52 4.5 46 3.5 37
SCALE HEIGHT 12.0 11.5 11.0	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279	-80 26.0 353 28.3 358 30.8 3 33.3 9	-70 35.5 346 38.9 350 41.9 353 44.3 358 45.7	-60 33.0 321 35.6 325 37.6 329 38.7 333 38.6	-50 27.5 315 28.9 317 30.0 320 30.4 323 30.0	-40 21.3 303 21.1 305 21.0 308 20.8 311 20.5 315 20.0	-30 15.5 257 15.0 257 14.5 259 13.9 261 13.4 265	-20 9.6 232 9.6 229 9.6 227 9.7 227 9.7 228 9.7	-10 4.7 151 4.4 158 4.1 168 4.1 180 4.3 193	0 4.6 150 4.1 157 3.5 168 3.2 185 3.3 204 3.9	6.2 156 5.1 168 4.4 184 4.3 203 4.6 218	6.6 195 6.1 205 5.8 216 5.7 226 5.7 232	7.9 235 8.0 239 8.1 242 8.0 244 7.6 245	4.2 278 4.5 270 4.7 263 4.7 258 4.5 255	2.1 17 1.0 338 1.3 267 2.1 243 2.7	3.3 90 2.3 108 1.9 139 2.1 166 2.7 175	4.9 138 4.1 141 3.3 143 2.7 145 2.2	5.5 52 4.5 46 3.5 37 2.8 21 2.5
SCALE HEIGHT 12.0 11.5 11.0 10.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460	-80 26.0 353 26.3 358 30.8 3 33.3 9 16 38.8	-70 35.5 346 38.9 350 41.9 353 44.3 358 45.7 3	-60 33.0 321 35.6 325 37.6 329 38.7 333 38.6 338 36.7 344	-50 27.5 315 28.9 317 30.0 320 30.4 323 30.0 527 28.5 333 25.8	21.3 303 21.1 305 21.0 308 20.8 311 20.5 315 20.0 320	-30 15.5 257 15.0 257 14.5 259 13.9 261 13.4 265	-20 9.6 232 9.6 229 9.6 227 9.7 227 9.7 228 9.7 231	-10 4.7 151 4.4 158 4.1 168 4.1 180 4.3 193	0 4.6 150 4.1 157 3.5 168 3.2 185 3.3 204	6.2 156 5.1 168 4.4 184 4.3 203 4.6 218	6.6 195 6.1 205 5.8 216 5.7 226 5.7 232 5.5 235	7.9 235 8.0 239 8.1 242 8.0 244 7.6 245	4.2 278 4.5 270 4.7 263 4.7 258 4.5 255	2.1 17 1.0 338 1.3 267 2.1 243 2.7 232 2.8	3.3 90 2.3 108 1.9 139 2.1 166 2.7 175 3.2 172	4.9 138 4.1 141 3.3 143 2.7 145 2.2 144 2.0 139 2.2	5.5 52 4.5 46 3.5 3.7 2.8 21 2.5 3.49 2.6
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758	-80 26.0 353 28.3 358 30.8 3 33.3 9 35.9 16 38.8 25	-70 35.5 346 38.9 350 41.9 353 44.3 358 45.7 3 46.1 11	-60 33.0 321 35.6 325 37.6 329 38.7 333 38.6 338 36.7 344	-50 27.5 315 28.9 317 30.0 320 30.4 323 30.0 527 28.5 333	21.3 303 21.1 305 21.0 308 20.8 311 20.5 315 20.0 320	-30 15.5 257 15.0 257 14.5 259 13.9 261 13.4 265 13.0 271 12.8 277	-20 9.6 232 9.6 229 9.6 227 9.7 227 9.7 228 9.7 231	-10 4.7 151 4.4 158 4.1 168 4.1 180 4.3 193 4.8 206 5.6 216 6.3	0 4.6 150 4.1 157 3.5 168 3.2 185 3.3 204 3.9 220 4.7 230 5.3	6.2 156 5.1 168 4.4 184 4.3 203 4.6 218 5.1 227 5.5 231	6.6 195 0.1 205 5.8 216 5.7 226 5.7 232 5.5 235 5.1 234	7.9 235 8.0 239 8.1 242 8.0 244 7.6 245 6.9 244 6.0 241 5.1	4.2 278 4.5 270 4.7 263 4.7 258 4.5 255 3.8 254 2.9 253	2.1 17 1.0 338 1.3 267 2.1 243 2.7 232 2.8 222 2.7 207 2.5	3.3 90 2.3 108 1.9 139 2.1 166 2.7 175 3.2 172 3.7 161	4.9 138 4.1 141 3.3 143 2.7 145 2.2 144 2.0 139 2.2 132 2.8	5.5 52 4.5 46 3.5 3.7 2.8 21 2.5 3 2.5 3.49 2.6 341 2.4
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758	-80 26.0 353 28.3 358 30.8 3 35.9 16 38.8 25 42.1 34 45.3	-70 35.5 346 38.9 350 41.9 353 44.3 358 45.7 3 46.1 11 45.8 20 45.4 33 45.3	-60 33.0 321 35.6 329 38.7 333 38.6 338 36.7 344 33.3 354 29.2	-50 27.5 315 28.9 317 30.0 520 30.4 323 30.0 527 28.5 333 25.8 341 22.3 352 18.7	-40 21.3 303 21.1 305 21.0 308 20.8 311 20.5 315 20.0 320 19.2 325 17.8 330 15.6	-30 15.5 257 15.0 257 14.5 259 13.9 261 13.4 265 13.0 271 12.8 277 12.8 282	-20 9.6 232 9.6 227 9.7 227 9.7 228 9.7 231 9.8 235 10.0 240 10.3	-10 4.7 151 4.4 158 4.1 168 4.1 180 4.3 193 4.8 206 5.6 216 6.3 222 6.7	0 4.8 150 4.1 157 3.5 168 3.2 185 3.3 204 3.9 220 4.7 230 5.3 234 5.4	6.2 156 5.1 168 4.4 184 4.3 203 4.6 218 5.1 227 5.5 231 5.5	6.6 195 6.1 205 5.8 216 5.7 226 5.7 232 5.5 235 5.1 234 4.7 229	7.9 235 8.0 239 8.1 242 8.0 244 7.6 245 6.9 241 5.1 235	4.2 278 4.5 270 4.7 263 4.7 258 4.5 255 3.8 254 2.9 253 2.1 249	2.1 17 1.0 338 1.3 267 2.1 243 2.7 232 2.8 222 2.7 207 2.5 187 2.7	3.3 90 2.3 108 1.9 139 2.1 166 2.7 175 3.7 161 4.4 149 5.2	4.9 138 4.1 141 3.3 143 2.7 145 2.2 144 2.0 139 2.2 132 2.8 127 3.6	5.5 52 4.5 46 3.5 3.7 2.8 21 2.5 3 2.5 349 2.6 341 2.4 341 1.8
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061	-80 26.0 353 358 30.8 3 35.3 9 35.9 16 38.8 25 42.1 34 45.3 44.1 53	-70 35.5 346 38.9 350 41.9 353 44.3 358 45.7 3 46.1 45.8 20 45.4 33 45.3 46.2	-60 33.0 321 35.6 325 37.6 329 38.6 338 36.7 344 35.3 354 29.2 9 26.2 30 27.2	-50 27.5 315 28.9 317 30.0 320 30.4 323 30.0 527 28.5 333 25.8 341 22.3 352 18.7 9	21.3 305 21.1 305 21.0 30.8 311 20.5 315 20.0 320 320 19.2 325 17.8 330 15.6 13.1	-30 15.5 257 15.0 257 14.5 259 13.4 265 13.4 265 13.0 271 12.8 282 12.8 282 12.8	-20 9.6 232 9.6 229 9.6 227 9.7 228 9.7 231 9.8 235 10.0 240 10.3	-10 4.7 151 4.4 158 4.1 168 4.1 180 4.3 193 4.8 206 5.6 216 6.3 222 6.7 224	0 4.8 150 4.1 157 3.5 168 3.2 185 3.3 204 3.9 220 4.7 230 5.3 234 5.4 233 4.9	6.2 156 5.1 168 4.4 184 4.3 203 4.6 218 5.1 227 5.5 231 5.5 231 5.5 231 4.4	6.6 195 0.1 205 5.8 216 5.7 226 5.7 232 5.5 235 5.1 234 4.7 229 4.2 220 3.8	7.9 235 8.0 239 8.1 244 7.6 245 6.9 241 5.1 235 4.4 228	4.2 278 4.5 270 4.7 263 4.7 253 4.5 259 3.8 254 2.9 253 2.1 249 253 2.1 249 257 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1	2.1 17 1.0 338 1.3 267 2.1 2.2 2.7 232 2.8 222 2.7 207 2.5 187 2.7 167 3.1	3.3 90 2.3 108 1.9 139 2.1 162 7 175 3.2 172 3.7 161 4.4 149 5.2 140 5.8	4.9 138 4.1 141 3.3 143 2.7 145 2.2 144 2.0 139 2.2 132 2.8 127 3.6 127	5.5 52 4.6 3.5 3.7 2.8 21 2.5 3.4 2.5 3.4 2.6 3.4 3.4 1.0
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398	-80 26.0 353 358 30.8 3 35.3 9 16 38.8 25 42.1 34 45.3 50.0 61 50.4	-70 35.5 346 38.9 350 41.9 353 44.3 353 46.1 11 45.8 20 45.4 45.3 46.3 45.3 46.1 11 45.8 20 45.4 56 57 58 58 58 58 58 58 58 58 58 58 58 58 58	-60 33.0 321 35.6 325 37.6 329 38.7 333 38.6 338 36.7 334 35.5 29.2 9 26.2 30 27.2 52	-50 27.5 315 28.9 317 30.0 30.4 323 30.4 323 50.0 527 28.5 333 25.8 341 22.3 352 18.7 9 17.1 30 18.2	-40 21.3 503 21.1 305 21.0 308 20.8 311 20.5 350 19.2 325 17.8 330 15.6 336 13.1 13.4 10.8	-30 15.5 257 15.0 257 14.5 259 261 13.4 265 13.0 271 12.8 277 12.8 282 12.6 284 12.1 282	9.6 232 9.6 229 9.6 227 9.7 227 9.7 228 9.6 235 0.240 10.3 242 9.9	-10 4.7 151 4.4 158 4.1 168 4.3 193 5.6 6.3 202 6.7 224 6.5 222 5.9	0 4.8 150 4.1 157 3.5 168 3.2 185 3.3 204 4.7 230 5.3 4.9 228 4.1	6.2 156 5.1 168 4.4 184 4.3 203 4.6 218 5.1 227 5.5 231 5.5 231 5.1 226 4.4 218	6.6 195 5.1 205 5.7 226 5.7 226 5.7 232 5.5 235 5.1 234 4.7 229 4.2 220 3.8 215	7.9 235 8.0 239 8.1 242 8.0 244 7.6 245 6.9 244 6.0 241 5.1 235 4.4 228 4.2 244	4.2 278 4.5 270 4.7 263 4.7 258 4.5 255 254 2.9 253 2.1 249 1.6 237 2.0 2.3 2.8	2.1 17 1.0 338 1.3 267 2.1 243 2.7 232 2.8 222 2.7 207 2.5 187 2.7 167 3.6	3.3 90 2.3 108 1.9 2.1 166 2.7 175 3.7 161 4.4 149 5.2 140 5.8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	4.9 138 4.1 141 3.3 143 2.7 145 2.2 144 2.0 139 2.2 132 2.8 127 3.6 127 4.4	5.5 52 4.6 3.5 57 2.1 2.5 3 2.5 3.49 2.6 3.41 2.4 3.41 1.8 3.48 1.0 4
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 8.0 7.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603	-80 26.0 353 30.8 3 35.3 9 16 38.8 25 42.1 34 45.3 44 48.1 50.0 61	-70 35.5 346 38.9 350 41.9 353 44.3 358 45.7 3 46.1 11 45.8 20 45.4 33 46,3 45,3 45,3 45,3 67 52.3	-60 33.0 321 35.6 325 37.6 329 38.7 333 38.6 338 36.7 344 33.3 35.4 29.2 9 26.2 52 30 27.2 52 30 31.3 36.7 36.7 36.7 36.7 37.8 37.8 37.8 37.8 37.8 37.8 37.8 37	-50 27.5 315 28.9 317 30.0 320 30.4 323 30.0 527 28.5 333 25.8 341 30 18.7 9 17.1 30 18.2 21.4	-40 21.3 503 21.1 305 21.0 308 20.6 311 20.5 515 20.0 520 19.2 325 17.8 330 15.6 336 13.1 343 10.8 354 9.2	-50 15.5 257 15.0 257 14.5 259 13.9 261 13.4 263 13.0 12.8 277 12.8 282 12.6 284 12.8 282 10.9 280 8,7	9.6 232 9.6 229 9.6 227 9.7 227 9.7 228 9.7 231 10.0 240 10.3 242 9.9 9.40 6.9	-10 4.7 151 4.4 158 4.1 180 4.3 193 4.8 206 6.3 222 6.7 224 6.5 222 5.9 218 5.1	4.8 150 4.1 157 3.5 168 3.2 185 3.3 204 4.7 230 5.3 234 4.9 228 4.1 1 221 3.9 3	6.2 156 5.1 168 4.4 4.3 203 5.1 227 5.5 231 5.5 231 5.1 226 4.4 218 3.7 209 3.2	6.6 195 6.1 205 5.8 216 5.7 226 5.5 232 5.5 234 4.7 229 4.2 220 3.8 212 3.8 212 3.8 213	7.9 235 8.0 239 8.1 242 8.0 244 6.0 241 5.1 255 4.4 4.2 224 4.2 224 4.3	4.2 278 4.5 270 4.7 265 4.7 255 3.8 254 2.9 2.9 2.1 249 1.6 2.7 2.0 2.2 2.3 2.1 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3	2.1 17 1.0 338 1.3 267 2.1 243 2.2 2.7 207 2.5 187 2.7 160 3.6 164 4.0	3.3 90 2.3 108 1.9 139 2.1 166 2.7 175 3.2 172 3.7 161 4.4 149 5.8 138 6.1 143 5.9	4.9 138 4.1 141 3.3 145 2.7 145 2.2 144 2.0 139 2.2 2.8 127 3.6 127 4.4 152 4.7	5.5 52 4.6 3.5 3.7 2.8 21 2.5 3.49 2.6 3.41 1.8 3.41 1.8 3.41 1.8 3.41 1.8 3.5 3.7 0.5
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 8.0 7.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0798 0.1250 0.2061 0.3398 0.5603 0.9237	-80 26.0 353 28.3 30.8 30.8 35.9 9 55.9 16 38.8 25 42.1 34 45.3 44.1 55 50.0 61 50.4 66 48.1 7 7 7	-70 35.5 346 38.9 350 41.9 353 44.3 358 45.7 358 46.1 11 45.8 20 45.4 33 46.1 50 45.4 50 67 52.3 67	-60 33.0 521 35.6 525 37.6 529 38.7 533 38.6 338 36.7 334 35.3 29.2 9 26.2 52 30 27.2 52 30 27.2 52 52 54 54 54 54 54 54 54 54 54 54 54 54 54	-50 27.5 315 28.9 317 30.0 320 30.4 323 30.0 327 28.5 333 25.8 341 22.3 352 18.7 9 17.1 30.0 20.0 21.4 65 25.0 26.0 26.0 27.0 28.5 28	21.3 303 21.1 305 21.0 308 20.6 311 20.5 315 20.5 320 320 320 320 320 320 330 320 32	-50 15.5 257 15.0 257 14.5 259 13.9 261 13.4 265 271 12.8 282 12.6 284 12.1 282 10.9 8.7 278	9.6 232 9.6 227 9.6 227 9.7 227 9.7 231 9.8 235 10.0 240 10.3 242 9.9 9.2 39 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2 7.2	4.7 151 4.4 158 4.1 168 4.3 193 206 5.6 6.3 222 6.7 224 6.5 222 5.9 9 218	0 4.6 150 4.1 157 3.5 168 5.2 204 4.7 230 5.3 234 4.9 228 4.9 228 4.9 228 4.9 228 4.9 228 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5	6.2 156 5.1 168 4.4 184 4.3 203 4.6 218 5.1 227 5.5 231 5.1 226 4.4 4.8 3.7 209 3.2 204 4.8	6.6 195 6.1 205 5.8 216 5.7 232 5.5 5.1 234 4.7 229 4.2 220 3.8 215 208 3.2 208 3.2 209 3.0	7.9 235 8.0 239 8.1 242 8.0 244 7.6 245 6.9 244 5.1 1.25 4.4 226 4.2 224 4.3 224 4.3 224	4.2 278 4.5 270 4.7 265 4.7 258 255 3.8 254 2.9 253 2.1 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0	2.1 17 1.0 338 1.3 267 2.1 243 2.7 232 2.7 207 2.5 187 2.7 167 3.6 164 4.0 4.0	3.5 90 2.5 108 1.9 139 2.1 166 2.7 175 3.2 172 3.7 161 4.4 149 5.2 140 5.8 8 6.1 143 5.9	4.9 138 4.1 141 3.5 145 2.2 144 2.0 139 2.2 2.8 127 3.6 6 127 4.4 152 4.6 4.6 7 142 4.6 4.6 4.6 4.6 4.6 4.6 4.6 4.6 4.6 4.6	5.5 52 4.5 4.6 3.5 5.7 2.8 21 2.5 3.4 2.5 3.4 2.6 3.4 1.0 4.3 2.7 0.5 2.7 0.5 2.5 1.4
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 8.0 7.5 7.0	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603 0.9237	-80 26.0 353 353 358 3 358 3 358 3 35.3 3 35.3 4 48.1 5 50.0 61 50.4 66 48.1 70 42.9 76 35.4	-70 35.5 346 38.9 350 41.9 353 358 44.3 358 45.7 3 46.1 11 45.8 20 45.4 35,3 46.7 50 45.8 51.3 67 50.4 50.4 50.4	-60 33.0 321 35.6 329 37.6 38.7 333 38.7 344 33.3 35.7 344 29.2 92.2 92.2 92.3 30.7 31.3 67 77 40.6 43.3	-50 27.5 315 28.9 317 30.0 323 30.0 527 28.5 333 25.8 341 22.3 352 18.7 9 17.1 30 18.2 50 21.4 65 26.0 79 29.9 29.9	-40 21.3 503 21.1 305 21.0 308 311 20.5 515 20.0 320 19.2 23.2 17.8 330 13.1 15.6 336 13.1 10.8 354 9.2 15 9.5 11.8	-30 15.5 257 15.0 257 14.5 257 14.5 257 13.9 261 13.0 271 12.8 282 12.1 12.8 282 10.9 280 8.7 278 12.5 12.6 12.6 12.6 12.6 12.6 12.6 12.6 12.6	9.6 232 9.6 229 9.6 227 9.7 227 9.7 231 9.8 235 10.0 240 6.9 240 6.9 239 7.4 237 7.5 7.5 7.5 7.5 7.5 7.5 7.5 7.5 7.5 7.	-10 4.7 151 4.4 158 4.1 168 4.1 180 4.3 193 4.8 206 6.5 216 6.5 222 5.9 218 5.1 5.1 5.2 5.2 5.2 5.2 5.2 5.2 5.2 5.2 5.2 5.2	0 4.6 150 4.1 157 3.5 168 3.2 20 4.7 230 5.3 24 4.7 230 4.3 23 4.9 220 4.7 230 5.3 24 23 3.9 220 5.3 23 4.1 21 21 21 21 21 21 21 21 21 21 21 21 21	6.2 156 5.1 168 4.4 3 203 4.6 6 218 5.1 227 5.5 231 226 4.4 218 3.7 209 3.2 204 2.8 2.5 5.5 2.5 2.5 2.5 2.5 2.5 2.5 2.5 2.5	6.6 195 5.8 216 5.7 226 5.7 232 5.5 235 5.1 234 4.7 229 3.8 3.2 220 3.8 208 3.2 209 3.0 213 2.9	7.9 235 8.0 239 8.1 242 7.6 6.9 244 5.1 255 4.4 226 4.3 224 4.3 224 4.3 224 4.3	4.2 278 4.5 270 4.7 258 4.9 253 3.8 254 2.9 2.9 2.1 249 2.2 2.3 2.1 2.1 2.3 2.1 2.3 2.1 2.3 2.3 2.1 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3	2.1 177 1.0 338 1.5 267 2.1 245 2.2 2.7 2.7 2.7 2.5 187 160 3.6 164 4.0 4.0 4.2 173 4.2	3.5 90 2.3 108 1.9 139 2.1 166 2.7 175 3.2 3.7 161 4.4 149 5.2 140 6.1 143 5.9 155 5.4 4.8 4.8 4.8 4.8 4.8 4.8 4.8 4.8 4.8 4	4.9 138 4.1 141 3.3 145 2.2 144 2.0 139 2.2 2.8 127 4.4 4.7 142 4.7 142 4.7 144 4.1 157	5.5 52 4.5 4.6 3.5 3.7 2.8 2.5 3.4 2.5 3.4 2.6 3.4 3.4 3.4 3.4 3.4 3.4 3.4 3.4 3.4 3.4
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 8.0 7.5 7.0 6.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3598 0.5603 0.9237 1.52 2.51	-80 26.0 3553 28.3 358 30.8 35.9 16 38.8 22.1 34 45.3 44 48.1 50.0 61 70 42.9 76 35.4 83 27.0	-70 35.5 36.9 350 41.9 353 44.3 358 46.1 11 45.8 25.8 45.3 45.3 46.3 37 46.1 11 11 12 45.8 45.7 45.8 45.7 46.7 57 46.8 46.7 47 47 47 48 49 49 49 49 49 49 49 49 49 49	-60 33.0 321 35.6 325 37.6 38.7 333 38.6 338 36.7 344 29.2 29.2 30 27.2 52 31.3 67 40.6 87 43.3 88 43.6 94 43.6 94 43.6 94 43.6 94 44 45 46 47 47 47 47 47 47 47 47 47 47 47 47 47	-50 27.5 315 317 30.0 320 30.0 327 28.5 333 352 28.6 341 22.3 359 18.7 9 17.1 30 18.2 50 79 29.9 19.1 30.0	-40 21.3 503 21.1 305 21.0 308 20.8 511 20.5 515 20.0 520 17.8 336 13.1 343 10.8 554 9.2 15 9.5 76 11.5 11.5	-30 15.5 257 14.5 259 13.9 13.4 265 13.0 271 12.6 282 12.1 12.8 282 10.9 280 12.1 282 10.9 280 15.0 282 12.1 282 10.1 2 10.1 2 10.1 2 10.1 2 10.1 2 10.1 2 10.1 2 10.1 2 10.1 2 10.1 2 10.1 2 10.1 2 10.1 2 10.1 2 10.1 2 10.1 2 10.1 2 10.1 2 10.1 10.1	9.6 232 9.6 229 9.6 227 9.7 227 9.7 231 10.0 240 10.3 242 9.9 240 6.9 237 7.4 4 25 5	4.7 158 4.1 168 4.1 180 4.3 193 4.8 206 5.6 5.6 6.7 224 6.5 5.9 218 222 5.9 218 4.1 215 3.7 215 3.7 215 3.7 3.7 3.7 3.7 3.7 3.7 3.7 3.7 3.7 3.7	0 4.6 150 3.1 157 3.5 168 3.2 204 4.7 230 4.7 230 4.7 233 4.9 228 4.1 221 3.5 228 4.1 221 225 227 225 227 227 227 227 227 227 227	6.2 156 5.1 168 4.4 4.3 203 4.6 4.3 203 5.1 227 231 5.5 231 5.5 231 5.7 226 4.4 2.8 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0	6.6 195 5.0 5.0 5.0 216 5.7 226 5.7 232 5.5 5.1 234 4.7 229 4.2 220 3.0 8.2 220 3.0 212 209 3.0 213 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0	7.9 235 8.0 239 8.1 242 8.0 244 7.6 6.9 244 15.1 5.1 255 4.4 228 4.2 244 4.3 226 4.2 238 4.1 228 3.8 3.8 3.8	4.2 278 4.5 270 4.7 265 4.7 258 4.9 253 3.8 254 2.9 253 2.1 1.6 237 249 253 2.1 249 253 2.1 249 253 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1	2.1 177 1.0 3.38 1.3 267 2.1 243 2.7 207 2.5 187 2.7 167 3.6 4.2 2.7 4.2 4.2 4.2 4.2 4.2 4.2 4.2 4.2 4.2 4.2	3.3 900 2.3 108 1.9 139 2.1 166 2.7 175 3.7 161 4.4 4.9 140 5.8 6.1 1184 4.6 1184 4.6 4.8 184 4.5	4.9 138 4.1 141 3.3 145 2.7 144 2.0 139 2.2 152 2.8 127 3.6 127 4.1 4.1 4.6 157 4.1 179 4.0 4.0 4.2 4.2 4.2 4.2 4.2 4.2 4.2 4.2 4.2 4.2	5.5 52 4.5 4.6 3.5 3.7 2.8 2.1 2.5 3.4 2.5 3.4 2.4 3.4 1.0 4 0.3 2.7 1.4 0.5 2.3 2.5 2.4 2.4 2.4 2.4 2.4 2.4 2.4 2.4 2.4 2.4
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 8.0 7.5 7.0 6.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0798 0.1290 0.2061 0.3398 0.5603 0.9237 1.52 2.51	-80 26.0 353 36.3 358 30.8 63 35.3 9 35.9 16 36.8 62 42.1 34 45.3 35 50.0 61 50.4 66 48.1 76 42.9 76 35.4 83 27.0 94	-70 55.5 546 36.9 350 41.9 353 44.3 358 46.1 11 45.8 20 45.4 33 46.3 45.3 46.3 45.3 46.3 47.3 46.3 47.3 46.3 48.2	-60 33.0 321 35.6 323 37.6 329 38.7 333 38.6 338 36.7 334 33.3 43.3 29.2 92 92 92 92 93 94 97 96.1 97 96.1 97 97 98.	-50 27.5 315 28.9 317 30.0 320 30.4 323 30.0 327 28.5 333 25.8 341 22.3 35.2 18.7 9 17.1 30 18.2 20.9 20.9 91 31.3 10.3	-40 21.3 503 21.0 308 20.6 511 20.0 520 19.2 525 17.8 530 15.6 330 15.6 330 15.6 330 15.6 343 10.8 354 9.2 15 76 11.5 76	-30 15.5 257 14.5 259 13.9 261 13.4 263 13.0 271 12.8 282 12.1 282 12.1 282 12.1 282 12.1 282 12.1 282 12.1 282 12.1 282 12.1 13.4 282 12.1 2 2.1 2.1	9.6 239 9.6 229 9.6 227 227 227 227 227 231 9.8 25 242 10.3 242 9.9 240 6.9 237 5.5 33 3.9 223 2.9	-10 4.7 151 4.4 158 4.1 168 4.1 168 4.3 193 206 6.5 216 6.5 222 5.9 224 6.5 5.1 215 215 215 215 215 215 216 217 217 218 218 218 218 218 218 218 218	0 4.6 4.1 157 3.5 168 3.2 204 4.7 230 5.3 234 4.9 220 4.7 230 228 4.1 228 4.1 228 228 229 220 220 220 220 220 220 220 220 220	6.2 1756 5.1 168 4.4 4.3 203 4.1 184 4.3 203 5.1 127 5.5 231 5.1 227 231 5.1 202 202 2.5 202 2.6 202 2.1 202 2.1 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0	6.6 195 5.8 205 5.7 226 5.7 232 5.5 5.1 234 4.2 229 4.2 220 3.8 212 3.5 208 3.2 213 2.15 2.16 2.16 2.16 2.16 2.16 2.16 2.16 2.16	7.9 235 8.0 239 8.1 242 8.0 244 4.1 235 4.4 224 4.3 226 4.2 228 4.1 238 3.8 225 3.5 3.5 3.5	4.2 278 4.5 270 4.7 263 4.7 258 3.8 4.5 255 3.8 2.1 249 2.0 223 2.1 2.1 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5	2.1 177 1.0 338 1.3 267 2.1 243 222 2.7 207 2.5 187 2.7 1160 3.6 4.2 173 4.2 173 4.1 185 3.6	3.5 900 1.99 139 2.1 166 2.7 175 3.2 172 3.7 161 4.4 4.5 138 5.9 155 4.4 167 4.8 4.5 4.5 4.6 4.5 4.6 4.6 4.6 4.6 4.6 4.6 4.6 4.6 4.6 4.6	4.9 158 4.1 141 3.5 143 2.7 145 2.2 144 2.1 2.8 127 4.4 4.7 132 4.7 142 4.6 157 4.0 179 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	5.5 52 4.5 4.5 4.5 3.5 57 2.8 2.1 2.5 3.4 2.5 3.4 2.4 3.4 1.0 4 4 0.3 27 0.5 21 2.4 2.4 2.4 2.5 2.7 2.7 2.8 2.7 2.7 2.8 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 8.0 7.5 7.0 6.5 6.0	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0798 0.1250 0.2061 0.3398 0.5603 0.9237 1.52 2.51 4.14 6.83	-80 26.0 353 358 30.8 33.3 35.3 35.3 35.3 36.8 25 42.1 53.5 50.0 61 55.4 44.1 53.5 66 48.1 70.7 70.9 42.9 42.9 42.9 42.9 42.9 42.9 42.9 42	-70 55.5 346.9 350 41.9 353 44.3 353 46.1 11 45.8 20 45.4 48.2 58 51.3 36 77 52.3 70.4 82 45.2 45.2 45.2 46.2 47 48.2 48.2 49.2	-60 33.0 321 35.6 529 37.6 529 36.7 344 35.3 35.3 429.2 27.2 9 26.2 30 27.2 9 43.0 43.0 111 39.5 127 25.2	750 27.5 315 28.9 317 30.0 320 30.4 323 30.0 327 28.5 333 28.6 341 22.3 392 18.7 9 17.1 30 18.2 50 79 9 19 19 20 20 21 40 40 40 40 40 40 40 40 40 40	-40 21.3 505 21.1 505 21.0 308 20.8 511 20.5 515 20.0 520 19.2 20.6 336 15.6 336 13.1 13.4 335 10.8 359 47 11.5 76 11.5 97 14.0 115.5	-30 15.5 257 15.0 257 14.5 259 13.9 261 13.4 265 271 12.8 282 12.6 284 11.1 282 12.6 282 162 162 162 162 162 162 162 162 162 16	9.6 229 9.6 229 9.6 229 9.7 227 9.7 228 9.7 227 10.0 240 10.3 242 210.3 242 237 5.5 5.5 233 3.9 9.23 2.9 2.25	-10 4.7 151 4.4 158 4.1 168 4.1 168 4.3 193 206 6.5 6.6 7.224 6.5 7.224 6.5 7.224 7.224 7.224 7.224 7.224 7.225 7.226 7.227	0 4.6 1.50 4.1 1.57 3.5 1.68 3.9 220 4.7 230 5.3 3.9 228 4.1 1.21 2.15 2.15 2.15 2.15 2.15 2.15 2.	6.2 156 5.1 168 4.4 184 4.3 203 4.6 218 5.5 231 5.5 231 5.5 231 5.5 231 226 246 202 2.5 202 2.1 202 2.1 203 203 203 203 203 203 203 203 203 203	6.6 6.6 195 5.8 216 5.7 232 5.7 235 5.1 234 4.7 220 3.8 220 3.1 2.9 20 215 20 215 20 215 216 216 216 216 217 217 218 218 218 218 218 218 218 218 218 218	7.9 235 8.0 239 8.1 242 8.0 244 7.6 245 6.0 241 5.1 226 4.4 226 4.3 224 4.3 228 4.2 228 4.3 228 5.8 5.8 5.8 5.8 5.8 5.8 5.8 5.8 5.8 5.	4.2 278 4.5 270 4.7 263 4.7 255 3.8 4.9 255 254 2.9 253 2.2 2.0 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3	2.1 177 1.0 338 1.3 267 2.1 243 222 2.7 207 2.7 2.7 2.7 167 3.6 164 4.0 173 4.2 177 4.1 183 5.6 8 192 193 193 193 193 193 193 193 193 193 193	3.5 900 1.9 139 2.1 166 2.7 175 3.2 172 3.7 161 14.4 14.9 5.8 138 6.1 14.5 5.9 18.4 4.5 2.7 4.8 4.5 2.7 4.0	4.9 158 4.1 141 3.5 143 2.7 145 2.2 144 2.2 132 2.8 132 2.8 132 4.7 4.6 157 4.1 179 4.0 2.5 4.7 4.6 4.1 179 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0 4.0	5,5 52 4,5 46 5,5 57 2,8 21 2,5 549 2,6 541 1,8 348 1,0 4 0,3 2,7 0,5 2,1 4 2,4 2,4 2,5 3,5 4 1,0 4 2,5 4 2,5 4 2,5 4 4 4 2,5 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 8.0 7.5 7.0 6.5 6.0 5.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603 0.9237 1.52 2.51 4.14 6.83	-80 26.0 353 358 30.8 353 353 353 353 353 34 445.3 445.3 446.1 50.4 466 48.1 50.4 48.1 50.4 48.1 10.4 48.1 48.1 48.1 48.1 48.1 48.1 48.1 48	-70 55.5 546 38.9 350 41.9 353 44.3 353 45.7 358 45.7 367 111 45.8 45.8 45.8 367 50.4 50.4 50.4 50.4 50.4 50.7 109 33.4 50.4 50.2 50.3 50.7 109 33.4 50.7 109 34.7 109 34	-60 33.0 521 35.6 529 37.6 529 38.7 333 36.7 334 35.3 554 29.2 52 52 52 53 67 40.6 87 43.0 98 43.0 111 59.5 127 55.1	-50 27.5 315 28.9 317 30.0 30.4 323 30.0 30.7 28.5 333 25.8 352 18.7 50 18.2 50 21.4 50 21.4 50 22.3 10.2 21.8 22.3 10.2 21.8 22.8 10.2 22.8 22.8 22.8 22.8 22.8 22.8 22.8 2	-40 21.3 303 21.1 305 21.0 308 20.8 311 20.5 351 20.0 320 15.6 336 15.6 336 15.6 336 15.6 336 15.7 15.6 336 15.1 343 354 9.2 17.8 17.8 17.8 17.8 17.8 17.8 17.8 17.8	-50 15.5 257 15.0 257 14.5 261 13.4 261 13.4 277 12.6 282 12.6 282 12.1 282 280 8.7 278 1.8 280 1.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2	-20 9.66 229 9.66 229 9.67 227 9.77 228 9.7 2251 9.89 10.00 10.3 242 240 6.99 6.90 6.90 6.90 6.90 6.90 6.90 6.9	-10 4.7 151 4.4 158 4.1 168 4.5 195 5.6 6.5 222 6.7 224 6.7 224 6.7 225 5.9 105 105 105 105 105 105 105 105	0 4.0 1.50 4.1 1.57 3.5 1.68 3.2 2.04 4.7 2.30 5.3 3.9 2.20 4.7 2.30 5.3 3.9 2.24 4.1 2.21 3.5 2.24 4.1 2.21 2.21 2.25 2.25 2.25 2.25 2.25 2.	6.2 156 5.1 168 4.4 4.3 203 4.6 218 227 5.5 5.5 221 226 202 2.1 200 1.9 158 188 188 203 203 203 203 203 203 203 203 203 203	6.6 195 5.1 205 5.2 216 5.7 226 5.7 235 5.35 5.35 5.35 5.35 5.35 5.35 5.35	7.9 235 8.0 239 8.0 244 7.6 6.9 244 7.6 6.9 241 5.1 224 4.3 224 4.3 224 4.3 228 3.8 8.0 25 25 3.5 25 25 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.	4.2 278 4.5 270 4.7 265 4.7 258 4.5 254 2.9 2.9 2.9 2.1 2.0 2.3 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1	2.1 17 1.0 338 1.5 267 2.1 243 2.7 2.7 2.7 2.7 2.7 160 3.6 4.0 4.2 177 4.1 183 3.6 203 3.6 203 3.6	3.3 90 2.3 108 1.9 1.39 2.1 1166 2.7 1772 3.7 161 4.4 4.5 138 138 143 5.9 1143 5.2 144 4.5 144 4.5 145 145 145 146 147 147 147 148 148 148 148 148 148 148 148 148 148	4.9 138 4.1 141 3.5 2.7 145 2.2 144 2.0 139 2.2 2.8 8.6 127 3.6 127 4.7 4.1 179 4.0 205 4.7 4.7 4.7 4.7 4.7 4.7 4.7 4.7 4.7 4.7	5,5 52 4,5 46 5,5 7 2,8 2,1 2,5 3,4 2,6 3,4 1,8 3,4 1,0 4 0,3 2,7 0,5 1,4 2,4 2,3 2,3 2,5 1,0 2,4 1,0 2,5 1,0 2,5 1,0 1,0 1,0 1,0 1,0 1,0 1,0 1,0 1,0 1,0
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 6.5 6.0 5.5 5.0 4.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603 0.9237 1.52 2.51 4.14 6.83 11.25	-80 26.00 353 358 30.88 3 35.3 35.9 16 38.8 25 42.1 53 44 45.3 45.3 46.1 70 42.9 96 88 81,2 12.4 144 9.9 199 11.6	-70 35.5 346 38.9 350 41.9 353 44.3 353 46.1 11 45.8 20 45.4 33 45.7 5 74 50.4 48.2 45.8 82 45.8 94 39.7 109 33.4 128 28.5 27.1 188	-60 33.0 321 35.6 325 37.6 329 38.7 333 38.6 338.6 338.6 338.6 33.5 429.2 92 92 92 93 93 94 96.1 97 98.	-50 27.5 315 28.9 317 30.0 320 30.4 323 30.0 327 28.5 333 352 28.6 341 22.3 3592 118.7 9 17.1 30 18.2 20.9 91 31.3 103 21.4 65 26.0 79 29.9 91 31.3 103 21.8 25.8 48 140 25.8 140 24.5 169 27.9	-40 21.3 503 21.1 505 21.0 308 20.8 511 20.5 511 20.5 520 17.8 530 18.2 17.8 13.4 10.8 554 47 11.5 9.5 76 11.5 11.5 11.5 11.5 11.5 11.5 11.5 11.	-30 15.5 257 14.5 259 13.9 261 13.4 265 13.0 271 12.8 282 12.1 12.1 282 10.9 280 7.7 278 1.8 282 10.9 280 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5	-20 9.66 232 9.66 229 9.66 229 9.7 227 9.7 228 9.8 235 10.0 240 10.3 242 9.9 239 240 6.9 237 7.4 237 5.5 3.9 223 223 225 2.7 7.8 7.8 7.8 7.8 7.8 7.8 7.8 7.8 7.8 7	-10 4.7 151 4.4 158 4.1 168 4.1 168 4.3 193 4.8 206 5.6 6.3 222 6.5 222 5.9 218 25 5.9 218 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7	4.6 4.1 157 3.5 5.3 204 3.9 220 4.7 230 234 4.1 221 5.5 2.7 221 1.8 204 1.8 194 1.8 194 1.8	6.2 156 156 4.4 4.3 203 4.6 218 5.5 231 5.5 231 5.5 231 226 4.4 2.8 202 2.5 202 2.5 202 2.1 200 1.9 1.9 1.9 1.9 1.9 1.9 1.9 1.9 1.9 1.9	6.6 195 5.0 195 5.0 216 5.7 226 5.5 5.1 229 220 3.0 3.0 2.1 3.5 2.2 209 3.0 2.1 2.7 2.1 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7	7.9 235 8.0 239 8.1 242 8.0 244 7.6 245 6.9 244 4.2 228 4.3 226 4.2 228 4.3 226 4.2 228 4.3 226 3.8 225 3.8 225 3.8 225 3.8 225 3.8 225 3.8 225 3.8 226 3.8 3.8 3.8 3.8 3.8 3.8 3.8 3.8 3.8 3.8	4.2 278 4.5 270 4.7 263 4.7 259 3.8 4.5 254 2.9 255 2.1 249 29 20 20 20 20 20 20 20 20 20 20 20 20 20	2.1 177 1.0 338 1.3 267 2.1 245 2.7 232 2.7 2.7 2.7 167 3.1 169 4.2 173 4.2 173 4.2 173 4.2 173 3.6 4.2 173 3.6 4.2 173 3.6 4.2 173 3.6 4.2 173 4 173 4 173 173 173 173 173 173 173 173 173 173	3.5 108 1.99 2.1 139 2.1 166 2.7 172 3.7 161 4.4 149 153 6.1 1143 5.8 163 164 165 173 167 167 167 167 167 167 167 167 167 167	4.9 158 4.1 141 3.5 143 2.7 145 2.2 144 2.0 2.0 2.2 152 2.8 127 4.4 1.5 1.7 4.1 4.6 1.5 1.7 4.0 2.5 4.7 2.2 2.2 4.7 2.2 2.2 4.6 4.1 2.7 2.7 2.7 2.7 2.7 4.7 4.7 4.7 4.7 4.7 4.7 4.7 4.7 4.7 4	5.5 52 4.5 4.5 4.5 3.5 5.7 2.8 2.1 2.5 3.4 2.4 3.4 1.0 4 4 0.3 2.7 0.5 2.3 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8
SCALE HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 6.5 6.0 5.5 5.0 4.5 4.0 3.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603 0.9237 1.52 2.51 4.14 6.83 11.25 18.55	-80 26.0 353 358 30.8 33.3 35.3 35.3 36.8 25 42.1 53 50.0 61 53.4 44.3 48.1 53 76 42.9 76 42.9 94 18.8 112.4 12.4 12.4 12.4 12.4 12.4 12.4 12.	-70 55.5 346 38.9 350 41.9 353 44.3 353 45.7 11 45.8 20 45.4 48.2 45.3 46 48.2 45.3 47 50.4 82 45.8 94 33 33 46.1 118	-60 33.0 35.6 525 37.6 529 36.7 344 35.5 26.2 30 27.2 30 27.2 30 31.3 36.7 34.4 35.5 44.0 35.6 87 40.6 87 43.0 111 39.5 127 129.2 139.2 149.2 159.2 169.2 179.	750 27.5 315 28.9 317 30.0 320 30.4 323 30.0 327 28.5 333 32.8 341 22.3 392 18.7 9 17.3 10.0 21.4 50.0 79.9 10.0 21.4 50.0 79.9 10.0 21.4 50.0 50.0	-40 21.3 505 21.1 505 21.0 308 20.6 511 20.5 515 21.0 520 19.2 20.6 536 15.6 536 13.1 13.4 330 15.6 6 336 15.6 13.1 13.1 13.1 13.2 15.5 47 11.5 76 11.5 97 14.0 115.5 137 13.2	-30 15.5 257 15.0 257 14.5 259 13.9 261 13.4 265 271 12.8 282 12.6 284 11.2 282 10.9 280 8.7 278 12.8 280 8.7 278 12.8 280 8.7 278 12.8 280 8.7 278 12.8 280 8.7 278 1.8 280 8.7 278 1.8 280 8.7 278 8.7 280 80 80 80 80 80 80 80 80 80 80 80 80 8	-20 9.66 229 9.66 229 9.67 227 9.77 228 9.79 235 10.00 10.3 242 10.3 242 10.3 242 2.37 2.57 2.57 2.58 2.99 2.79 2.71 2.71 2.71 2.72 2.72 2.72 2.73 2.73 2.73 2.73 2.73	-10 4.7 151 4.4 158 4.1 168 4.1 168 4.3 193 206 6.3 222 6.7 224 6.5 6.5 6.5 6.7 224 215 225 235 246 217 218 219 219 219 219 219 219 219 219	0 4.6 150 4.1 157 3.5 168 3.2 204 4.7 230 5.3 3.9 228 4.1 215 2.1 25 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1	6.2 156 5.1 168 4.4 4.3 203 4.6 218 5.5 231 5.5 231 5.5 231 5.5 231 226 24 202 2.5 202 2.1 202 2.1 203 203 203 203 203 203 203 203 203 203	6.6 195 5.8 216 5.7 226 5.7 232 5.1 234 4.7 220 3.8 220 3.8 220 213 2.9 2.9 2.1 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7	7.9 235 8.0 239 8.1 242 8.0 244 7.6 245 6.0 241 5.1 228 4.4 228 4.3 226 4.2 224 4.3 228 8.3 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0	4.2 278 4.5 270 4.7 263 4.7 258 4.5 254 2.9 3.5 2.1 2.1 2.2 3.5 2.1 3.5 2.1 3.5 2.1 3.5 2.1 3.5 2.1 3.5 2.1 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5	2.1 1.0 338 1.5 267 2.1 243 222 2.7 207 2.5 167 3.6 4.0 169 4.2 173 4.1 173 4 173 4 173 4 173 4 173 173 173 173 173 173 173 173 173 173	3.5 90 2.3 108 2.1 1.9 2.1 172 3.7 161 4.4 4.5 138 6.1 143 5.9 155.4 4.6 4.5 2.7 4.8 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5 4.5	4.9 158 4.1 141 3.5 145 2.7 145 2.2 144 2.2 132 2.8 132 4.7 4.4 132 4.6 157 4.1 179 4.6 157 4.1 179 4.2 2.2 4.7 4.1 179 4.2 4.6 4.1 5.5 5.7 4.1 4.1 4.1 4.1 4.1 4.1 4.1 4.1 4.1 4.1	5,5 52 4,5 46 5,5 57 2,8 21 2,5 341 2,4 4 0,3 2,7 0,5 1,4 2,8 2,5 1,4 2,8 2,5 1,4 2,8 2,5 2,5 2,5 1,0 2,5 2,6 2,7 2,7 2,8 2,7 2,7 2,8 2,7 2,7 2,8 2,8 2,8 2,8 2,8 2,8 2,8 2,8 2,8 2,8

	PRESSURE		-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
HEIGHT	(mb)																	
12.0	0.0062	145	0.20	303	301	275	240	0.52 318	270	187	149	108	100	175	39	358	36	0.75
11.5	0.0103	0.37	173	0.14 290	296	0.28 268	240	320	0.36 266	190	152	107	101	172	0.13	360	0.73	0.77
11.0	0,0169	158	172	260	0.46 288	0.30 261	0.18	322	0.34 256	194	158	107	104	0.19	0.11	0.31	0.75	0.72
10.5	0.0279	0.49	0.49	0.12	0,45	0.36	0.15	0.17	0.32	0.62	0.21	103	0.39	0.18	0.09	0.34	0.73	0.56
10.0	0.0460	0.55	0.60	0.23	0.45	0.41	0.09	0.09	0.34	0,54	0.18	0.18	0.31	0.17	0.05 96	0.35	0.68	0,40
9.5	0.0758	0,57	0.68	0.35	0.48	0.45	0.03	0,27	0.35	0.46	0.17	0.10	0.23	0.18	0.07	0.36	0.60	0.2
9.0	0.1250	0.51	0.69	0.48	0.56	0.50	0.06	0.37	0,35	0.40	0.17	0.26	0.15	0.20	0.16	0.35	0.49	0.16
8.5	0.2061	0.34	0.58	0.59	0.64	0.56	0.12	0.28	0.28	0.27	0.18	0.31	0.11	0.16	0.28	0.32	0.30	0.27
8.0	0,5398	0.15	0.50	0.72	0.68	0.64	0.15	0.14	0.15	0.11	0.16	0.20	0.10	0.08	0.45	0.33	0.07	0.35
7.5	0,5603	0.15	0.68	0.70	0.30	0.43	0.18	0.31	0.05	0.15	0,09	0.03	0.11	0.03	0.51	0.42	0.23	0.22
7.0	0,9237	0.31	0.82	0.77	0.16	0.35	0.19	0.27	0.04	0.17	0.07	0.14	0.10	0.05	0.51	0.50	0.41	0.14
6.5	1.52	0.35	0.84	0.95	0.46	0.37	0.16	0.09	0.06	0.10	0.07	0.09	0.06	0,11	0.49	0,62	0.53	0.16
6.0	2,51	0.29	0.81	1.16	0.60	0.32	0.11	0.13	0.08	0.04	0.03	0.05	0.14	0.17	0.56	0.80	0.64	0.23
5.5	4,14	0.17	0,59	0.91	0.44	0.19	0.08	0.14	0.07	0.05	0.01	0.16	0.26	0.19	0.49	0.83	0.71	0.26
5.0	6,83	0.16	0.40	0,43	0.20	0.15	0.13	0.16	0.10	0.09	0.04	0.28	0.39	0.21	0.42	0.88	0.80	0.2
4.5	11,25	0.28	0.49	0.27	0.20	0.21	0.15	0.18	0.13	0.13	0.08	0.39	0.50	0.22	0.43	0.97	0.83	0.20
4.0	18,55	0.49	0.90	1,01	0,50	0.24	0,15	0.18	0.15	0.15	0.11	0.45	0.56	0.22	0.55	1.06	0.85	0.23
3.5	30,59	0,67	1,28	122	0.68	0,25	0.12	0.17	0.15	0.16	0.12	0.47	0.54	0.20	0,63	1.03	0.77	0.1
3.0	50.43	0.44	1.18	121	0,69	186	0.08	0,15	0.14	0.14	19 U.12	0,42	0,47	0.16	0.59	0.88	0,61	0.14
2,5	83.15	0.24 24	0.74 104	121 1,23 121	0.55 129	0.16 166	0.05 171	0.11 41	0.10	36 0.10 35	0.09	0.32 355	0.35	0.11	253 0,46 258	0,63 265	258 0,42 264	0.09
SEPTEME	ER MEAN	GEOPOTE	NTIAL	HE IGHT	AMPL I	TUDE ((dam) A	ND PH	SE I	AVE 2								
SCALE HEIGHT	PRESSURE (mb)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
12.0	0,0062	2.4	5,6	11.2	9.7	3.1	0.9	1.5	2.2	4.1	1.9	3.1	4.2	3.0	4.7	2.1	3.4	2.6
11.5	0.0103	2.0	5.7	10.9	9.0 278	2.7	1.2	1.2	1.7	3.2	1.5	2.7	3.7	3.2	4.6	2.1	2.4	1.5
11.0	0.0169	1.6	6.0	10.8	8.4	2.3	1.4	1.5	1.3	2.3	1.2	2.7	3.3	3.3	4.5	2.1	1.3	0,
10.5	0.0279	1.1	6.3	10.7	7.7	1.8	1.7	1.7	0.9	1.6	1.0	2.8	3.2	3.4	4.4	2.3	0.3	0.6
10.0	0.0460	0.9	6.8	10.7	7.1	1.2	1.8	1.7	0.6	0.9	0.8	3.0	3.1	3,4	4.3	2.5	0.8	264
9,5	0.0758	1.3	7.5	10.9	6.5	0,6	1.9	1.5	0.4	0.3	0.6	3.0	3.2	3.4	4.2	2.8	1.7	257
9.0	0.1250	1.9	8.2	11.1	6.0	0.5	1.9	1.1	0.7	0.2	0.3	2.7	3.3	3.2	4.1	3.1	2.5	1.6
8.5	0.2061	2.5	8.8	11.3	5.9	1.2	1.8	0.9	1.0	0.6	0.1	2.4	3.5	3.1	3.8	3.3	3.1	1.7
8.0	0.3398	328	9.0	11.4	6.1	2.1	1,6	1.0	1.3	0.9	0.2	2.2	3.6	3.0	3.3	3,3	3.4	1.4
7.5	0,5603	327 2.8 325	8.7	303	503	2.7	1,4	1.2	1,5	1,1	0.4	2.1	3,6	2.9	2.6	163 3.1 173	3.3 201	1.
7.0	0.9237	325 2.4 327	8.1 335	308 10.4 312	509 6.4 311	352 2.9 342	1.1	1.6	1.5	1.1	0.4	2.2	3,6	2.9	1.9	2.9 185	3.1	1.
6.5	1.52	327 2,0 335	7.2	9,4	5.9	2.8	0.8	1.8	1.5	1.2	0.5	2.3	358	2.8	1.2	2.6	208	0.9
6.0	2,51	1.8	6,4	316 8,0	5.1	332	0.6	1.9	1.6	1.3	0,6	2.3	357	2.6	0.4	2.4	2.5	0.6
	4,14	1.7	5.7	320 6.6	308	324	0.5	1.8	1.6	1,3	0.6	2.1	356	16	0.4	2.3	237	0.
		359	5.7 356 5.1	326 5.8	307	2.0 321 1.8	63	1.7	1,6	1.3	0.6 30 0.6	2.1 355 1.8	3.2 357 2.7	2.4 13 2.1	0.4 312	2.3 254 2.3	2.2 260 2.0	0.1
5.5	6.83				200	324	47	53	30	29	29	355	357	11	319	286	289	326
5.0	6.83		360	531	308						0.6	2.2	2.0	1.0	1 .	2 4	2.0	0.4
5.0 4.5	11,25	1.3	360 4.6 357	5.7 333	3.9	1.8	0.7	1.5	1.5	1.1	29	357	357	1.8	334	319	324	0.5
5.0 4.5 4.0	11,25	1.3 2 0.8 345	360 4.6 357 4.4 345	5.7 333 6.6 329	3.9 311 4.4 312	1.8 331 2.0 339	0.7 33 0.9 24	1.5 47 1.3 42	1.3 21	0.9 18	0.3 31	357 0.7 360	357 1.3 357	1.5	334 1.9 353	319 2.8 350	324 2.3 356	0,9
5.0 4.5 4.0 3.5	11.25 18.55 30.59	1.3 2 0.8 345 0.7 274	360 4.6 357 4.4 345 5.0 326	5.7 333 6.6 329 8.3 323	3.9 311 4.4 312 5.3 313	1.8 331 2.0 339 2.4 344	0.7 33 0.9 24 1.0	1.5 47 1.3 42 1.1	1.3 21 1.1 16	0.9 18 0.7 9	0.3 31 0.2 44	357 0.7 360 0.1 80	357 1.3 357 0.5 351	1.5 4 1.2 360	334 1.9 353 2.4 12	319 2.8 350 3.6 15	324 2.3 356 3.0 18	0.0
5.0 4.5 4.0	11,25	1.3 2 0.8 345 0.7	360 4.6 357 4.4 345 5.0	5.7 333 6.6 329 8.3 323 10.5 318	3.9 311 4.4 312 5.3	1.8 331 2.0 339 2.4	0.7 33 0.9 24	1.5 47 1.3 42	1.3 21 1.1	0.9 18 0.7	0.3 31 0.2	357 0.7 360 0.1	357 1.3 357 0.5	1.5	334 1.9 353 2.4	319 2.8 350	324 2.3 356 3.0	0,9

OCTOBER MEAN TEMPERATURE AMPLITUDE (K) AND PHASE WAVE 1 12.0 0.0062 1,19 196 1.94 1,48 11.5 0.0103 213 1,09 0.19 0.77 0.56 1,45 1.70 1.14 1.10 1.91 1.75 1,64 11.0 0.0169 1,88 1.18 1,48 1,29 0.42 0.50 1.47 1.62 1.00 1,72 2,51 3,52 10.5 0.0279 1.24 0.80 209 0.12 0.53 1.47 1.49 1.06 0.81 1.38 1,52 2.25 3,02 2.00 10.0 0.0460 0.99 1,39 1,61 1,26 0.30 1.34 0.62 1.48 3,63 9.5 0.0758 1,24 1,56 1,45 1,67 1.03 0.76 1.16 0,45 3,30 2.11 0.76 122 1.72 9.0 0.1250 1,65 1.47 1,15 1.22 0,89 0.41 8.5 0.2061 2.31 3.10 306 2,26 1,67 1.30 0.67 0.77 0.52 0.34 0.34 0.34 1.51 3,18 5.05 0.3398 1.15 0.15 304 339 0.46 1.15 352 3,55 3,97 2,18 3,11 5.57 6,02 4.29 2,16 0.72 0.26 269 283 280 0.60 1.16 2,56 3,54 4.26 2.76 7.0 0.9237 2.78 5.35 4.85 2,62 0.80 0.49 0.66 0.41 0.56 0.65 1.61 3.57 0.56 0.64 0.98 4.89 1.52 4.71 2.24 7.24 1.95 4.06 6.0 2.51 5,49 4,54 2,95 322 0.59 0.50 0.31 264 0.74 1.29 2.87 6.35 10.20 10.55 4.14 1.90 3.20 3.86 2.63 4,40 0.59 0.49 0.36 0.47 3,12 1.05 9,82 1.37 7.11 11.34 11.75 5.0 6.83 2.25 2.81 3,53 3,18 2.22 0.86 0.57 0.46 0.37 0.46 0.90 1.36 2.94 6.94 10.81 70 105 122 6.64 4.5 11,25 4.18 4.33 3,59 2.05 0.59 0.43 0.93 2,34 4.0 18,55 2.25 6,56 0.52 0.32 0.89 1.21 1.50 4.31 6.36 3.5 30.59 5,20 7,80 7.92 2.43 0.44 263 0.25 0.27 0.39 304 1.12 C.71 3,07 4.85 3.0 2.5 83.15 0.12 0.16 0.17 0,29 0,45 305 0.16 1.62 2.57 OCTOBER MEAN GEOPOTENTIAL HEIGHT AMPLITUDE (dam) AND PHASE WAVE 1 SCALE PRESSURE HEIGHT (mb) -80 -70 -60 -50 -20 10 30 40 50 60 70 80 12.0 0.0062 11.1 14.9 11.6 4.0 10.2 4.9 171 10.4 5.3 11.8 11.5 0.0103 9,5 13.0 230 279 3.3 5.7 4.7 8.5 7.7 2.4 5.1 312 14.2 28.3 11.0 0.0169 8.8 5.4 7.5 29.7 30.9 10.5 0.0279 6.3 8.7 7.1 4.3 3.1 6.7 5.7 4.8 3.3 1.0 503 8.7 18.5 33.8 49.5 32.3 10.0 0.0460 2.5 6.9 308 20.1 37.1 54.4 9.5 0.0758 5.3 5.1 196 9.0 0.1250 5.2 7.0 358 3.8 6.0 4.5 3.8 5.0 264 8.2 10.9 22.1 44.8 65.9 62.8 124 4.7 8.5 0.2061 9.9 8.2 1.7 8.2 5.6 5.1 3,6 6.1 5.7 8.4 22.5 6.9 14.0 6.5 2.7 6.2 6.2 5.1 5.8 8.2 10.1 22.5 50.5 76.5 45.4 0.5603 18.0 14.7 10.7 7.3 2.3 5.3 7.5 21.7 7.0 0.9237 22.2 29.9 23.6 8.0 1.5 5.5 5.3 4.2 4.5 6.6 298 8.4 20.2 48.1 76.0 25.7 1.52 37.2 0.3 4.9 4.6 3.7 3.9 5.7 17.7 7.2 68.2 43.6 69.5 40.5 2.51 1.4 6.0 28.6 43.7 40.6 24.6 11.1 4.1 3.9 3.3 4.8 5,6 58.0 59.0 4.14 48.7 30.5 29.4 47.5 13.3 138 3.4 3.2 2.7 2.6 3.8 10.4 29.0 45.2 26.0 3.9 6.83 5.0 31.3 51.5 51.8 145 2.5 2.0 2.7 2.3 6.7 11.25 32.4 2.0 1.8 1.9 1.5 144 13.8 4.0 18.55 28.4 47.7 30.2 1.7 4.3 48.6 5.7 1.5 1.5 13.9 162 2.3 4.9 3.0 50.43 37.5 6.7 8.4 296 510 83.15 2.5 2.0 1.8 2.8 5.7

OCTOBER	HEAN	TEMPERA	TURE	MPLITU	DE (K)	AND P	HASE	WAVE	2	OF	PO	OR	QU	JAL	ITY	100		
SCALE	PRESSURE	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	50	40	50	60	70	60
HEIGHT 12.0	(mb)	0.63	0.27	0.06	0.03	0.30	0.91	1.02	0.87	0.75	J.50	1.03	0.71	0.24	0.50	0.75	0.54	1.43
11,5	0.0103	0.69	0.29	0,10	0.07	0.31	0.92	0.99	0.82	0.72	0.49	0.98	0.70	0.23	0.47	0.77	0.63	1,39
11.0	0.0169	0,68	0.28	0.16	0.10	0.27	0.85	0.87	0.69	0,63	0,44	0.84	0.63	0,21	0.43	0.75	0.71	1.25
10.5	0.0279	0,59	0.25	0.27	0.15	0.21	0.73	0.70	0,51	0.51	0.37	0.61	0.50	0.17	0.34	0.70	0,79	1.03
10.0	0.0460	0.46	0.22	0.38 135	0.21	0.12	0.57	0.48	355 0.31 338	0.36	192 0.50 176	0.33	118 0.33 110	327 0.14 343	0.31	0.61	0.83	133 0.77 126
9.5	0.0758	0.29	0.20 321	0.44	0,27	0.04 333	0,45	0.25	0.18 291	0.20	0.24	0.10	0.14	0.12	0.33	0.50	0,60	0.55 111
9.0	0.1250	0.14	0.19	0.38	0.31	333	0.32	0.12	0.21	266	0.21	0.27	0.10	0.12	0.39	0.44	0.60	0.37
8.5	0,2061	0.17	0.16	0.25	0.37	256 0.19	0.16	0.09	0.15	0.14	0.15	0.35	0.24	0.12	0.37	73	0.33	85 0.27
8.0	0.3398	0.26	0.20	0,47	0.45	0.24	0.15	0.02	0.10 332	92	0.05	0,23	0.32	0.14	0.30	0.93	0.68	0.24
7.5	0.5603	0.22	0,28	0,59	0,43	0.19	0.30	0.16	0.22	0.08	0.11	0.04	0.22	352	0.33	1.14	1.16	0,10
7.0	0.9237	0.09	0.40	0,15	0.09	0.14	0.30	0.19	357	0.07	0.15	90	0.16	0.05	0.46	1.19	1,32	0,30
6.5	1.52	0.31	1.04	0.94	0.59	0.36	0,21	0.12	0.13	0.17	0,13	0.16	0.13	0.08	0,63	1,18	1,33	0,47
6.0	2,51	0.46	1.74	1.95	1.29	0.64	0.20	0.09	0.12	268	263	0.19	0.17	0,20	0.79	1.23	195	0.55
5.5	4.14	0.41	1.78	2.13	1.38	0.56	0.10	0.07	0.05	0.09 277	0.09	0,12	0.12	0.20	166	191	217 1,52 233	0,60
5.0	6.83	0.25	1.51	1.92	1.17	0.33	76	0.09	302	0.02	0.03	261	0.05	193	0.75	1,29	1,34	255
4.5	11.25	95	76	1.35	0.68	0.25	0,24	0.13	0.13	0.08	0.08	336 0.27	0.19	0.21	0.92	1,38	1.07	268
4.0	18,55	0.50	0.50	78 0.58	72	0.54	0.40	0.16	0.18	0.13	0.17	0,41	0.34	266	265	269	0.90	281
3.5	30,59	0.86	0.88	0,23	0.40	0.75	0,47	0.18	76	0.16	0.21	0.49	0.42	0.32	1.27	1.43	0.79	299
3.0	50.43	0.92	1.15	0.59	0,62	267	0.46	125	78	72	0.22	0.50	0.44	305	298	1.19	321	0.09
2.5	83.15	0,65	0.97	0.62	0.59	263	250	0.13	0.15	0.13	0.18	0.40	0.34	311	304	312	339	18
		308	284	272	256	260	251	115	82	74	62	31	43	316	309	318	350	45
OCTOBER	MEAN	GEOPOTE	NTIAL	HEIGHT	AMPLI	TUDE (dam) A	ND PHA	SE .	AVE 2								
SCALE HE IGHT	PRESSURE (mb)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
12.0	0.0062	5,6	11.2	18.0	9,6	4.0	6.5	5.6	4.9	2.2	2.3	2,6	2.0	4.5	6.1	6.1	8.5	3.7
11.5	0.0103	4.6	11.6	17.9	9.6	3.5	5.1	4.2	3.7	1.5	1.6	1.1	1.2	4.2	5.5	5.1	8.0	1.7
11.0	0.0169	3.6	12.0	17.7	9.6	3.1	3.8	2.8	2.7	0.8	0.9	0.3	1.1	3.9	4.9	4.2	7.4	0.5
10.5	0.0279	2.7	12.3	17.5	9,5	2.7	2.7	1.7	1.9	0.3	0.4	1.3	1.5	3.6	4.3	3.5	6.9	2.0 325
10.0	0.0460	1.9	12.6	17.2	9.4 87	2.5	1.7	0.9	1.3	0.1 340	0.2	2.0 335	1.9	3.4 334	3.9	3.1	6.6	3.3
9.5	0.0758	1.4	12.8	16.9 78	9.4 85	2.4	1.1	0.5	1.0	0.2	0.5	2.3	2.2 324	3.2 332	3.6 326	3.2	6.5	4.2 314
9.0	0.1250	1,1	12.9	16.7 76	9.4 82	2.5	1.0	0.2	0.9	0.3 359	0.8 347	2.1 342	321	3.1 330	3.5	3.6	6.8	4.8 310
8.5	0.2061	1.1	13.1	16.8	9.7 79	2.8 75	1.2	0.1	1.0 350	0.5 332	0.9 333	1.7 350	1.9	3.0 328	3.7	4.3	7.2 265	5.0 305
8.6	0.3398	1.4	13.3	17.3	10.2 78	3.0 72	1.2	0.1	1.0	0.7 316	1.0 326	1.4	1.6 331	2.9 325	4.0	5.3	7.7 268	4.9
7.5	0.5603	1.8	13.6 82	18.1 75	10.8	3.2 67	0.9	0.1	0.7	0.7 307	0.9 326	1.3	1.5	2.7 323	4.5	6.7	8.3	4.8
7.0	0.9237	2.0 87	13.6	18.5 76	11.2	3.2 63	0.5	0.3	0.4	0.6 309	0.8 337	1.4 358	1.5	2.6 322	5.0 303	8.1 296	9.0 288	4.7 303
6.5	1.52	1.8	12.7	17.9 76	10.8 78	2.9	0.4	0.5	0.3	0.4 330	0.7 352	1.6	1.6	2.6 322	5.8	9.5	9.6 299	4.7
6.0	2.51	1.4	10.7	15.8 75	9.5 78	2.2	0.5	0.7	0.5	0.3	0.7	1.8	1.8	2.8 323	6.7	10.6	9.9	4.6
5.5	4.14	1,1	8.1	12.8	7.5 78	1.3	0.7 228	0.7	0.5	0.4	0.8	1.9	1,9	3.0 327	7.5 316	11.3	10.0	4.4 330
5.0	6.83	1.0	5.7	9.8 70	5.6 79	0.7	0.8	0.7	0.5	0.4	0.8	1.8	2.0	3.2	7.9 323	11.5	10.0	4.2 341
4.5	11.25	0.8	3.9	7.5	4.2	0.5 76	0.6	0.6	0.4	0.3	0.7	1.6	1.8	3.1 336	7.7	11.0	9.7 346	4.0 350
4.0	18,55	0.5	3.1	6.1	3.7 83	1.0	0.2	0.4	0.2	0.2	0.6	1,1	1.4	3.0	6.9	10.1	9.1 354	3.8
3.5	30.59	1.0	3,6	5.7	3.9	2.0	0.7	0.2	0.1	0.3	0.4	0.4	1.0	2.7	5.9	9.0	8.3	3.6
3.0	50.43	2.3	5.0	6.2	4.7	3.1	1.3	0.3	0.4	0.5	0.5	0.4	0.8	2.3	5.1	8.0	7.4	3.4
2.5	83,15	3.5 122	6.6	7,1	5.6	4.1	1.9	0.4 330	0.6	0.7 272	0.6	1.0	0.9	2.0	4.7	7.2	6.6	3.3

4.5 11.25

4.0

3.5 30.59

3.0 50.43

18.55

11.2 16.4

12.2

15.3

13.2 14.4 11.4 5.8 2.6 2.2 2.3 2.0 2.6 201 193 187 170 139 127 150 148 144

13.0

11.9 5.9 2.4 2.0 158 154 146 148

18.1 13.3 5.8 2.2 2.1 1.9 1.3 0.9 0.8 3.3 142 138 142 156 169 179 178 138 116 127

NOVEMBER MEAN TEMPERATURE AMPLITUDE (K) AND PHASE WAVE 1 30 SCALE PRESSURE -80 HEIGHT (mb) -10 12.0 0,0062 0.36 0.01 0.31 0.16 0.22 0.52 132 90 167 135 360 313 0.18 1.14 0.70 0.41 0.97 332 1,53 3,26 4,82 4,05 11.5 0.0103 0.20 0.88 5,32 0.41 0.07 6.41 0.23 0.51 0,19 1.14 0.73 0.48 1.11 1.64 3,56 0.74 0,0169 0.17 0.17 1.07 307 1.72 3.79 5.80 337 0.42 0.34 315 0.75 0.21 0.19 0.94 0.75 0.72 0.92 2,58 10.5 0.0279 0.43 0.69 0.48 0.67 1,88 6.36 344 0.41 0.52 0.85 0.64 0.38 0.27 0.77 0.72 0.80 1,02 1.24 2.11 4.22 7.03 6,34 3.07 0.0758 0.42 0.68 0.97 0.77 0.57 0.09 0.35 0.57 0.70 0.92 1,52 1.76 7,58 7.08 3,65 4,36 0.21 0.39 0.35 7,81 7.56 4.21 0.2061 0.46 0.67 0.81 0.72 0.55 0,36 0.22 0.45 1.82 2.09 1,84 4.33 7.62 163 0.3398 0.57 0.20 351 0.19 1.21 1,77 4.55 7,53 268 0.63 0.31 0.43 0.5603 0.25 0.68 336 0.09 0.39 316 0.16 1,14 2,34 3.93 6.62 7.0 0.9237 1.18 2.04 0,43 0.02 0.33 0.29 0.53 0.76 1.36 2.34 3.32 6.20 3,52 1.36 0.03 1,52 1.24 1.57 6.5 4,21 2,54 0.86 0.25 0.29 0.43 0.67 6.59 5.83 6.0 2.51 3.89 318 3,73 1,30 0.10 0.22 0.32 357 0.68 1.65 2.06 2.28 4.14 8.08 4.14 3.94 6.23 0.29 3.21 5.0 6.83 3.14 4.69 4,51 2.88 1.17 0.25 0.28 0.39 0.79 2.08 3.03 3.92 7,25 11,20 10,80 231 331 4.5 11.25 1.66 2.73 2,86 1.91 0.25 0.31 0.78 1,91 2.87 4.08 7.85 11.50 10.96 147 168 178 2.67 4.0 18,55 1.21 3,44 2.54 0.67 0.32 239 0.37 300 2.39 3,68 7,64 10,90 6.73 333 345 30,59 1,01 0.29 0.38 3.5 2.63 4.71 5.19 123 106 92 3,69 0.53 0.39 0,61 1.32 1.79 6.66 0.37 307 1.29 5,14 2.5 83,15 2.84 4.73 4.66 0.18 0.45 0.32 0.28 0.33 292 3,45 4,62 183 209 3.30 1.04 NOVEMBER MEAN GEOPOTENTIAL HEIGHT AMPLITUDE (dam) AND PHASE WAVE 1 SCALE PRESSURE -70 -60 -50 -40 -30 -20 -10 0 10 20 30 40 50 60 12.0 0.0062 18.1 32.6 9.5 12.2 6.8 193 1.3 1.5 12.1 5.8 118 145 7.3 11.2 18.6 36.5 1.5 3.6 343 10.7 23.5 40.0 11.0 0.0169 10.7 18.3 12.9 1.9 9.1 11.3 0.0279 18.5 13.5 7.3 2.8 168 1.3 1.7 1.3 75 334 8.4 12.5 34.4 131 8.8 10.0 0.0460 0.9 7.7 1.1 14.8 135 0.0758 12.1 19.4 8.2 165 0.7 1.8 1.4 10.3 15.1 350 17.8 45.7 74.8 2.8 0.1250 3.0 0.3 332 8.9 12.9 20.9 50.8 83.6 0.2061 9.1 0.5 8.5 12.3 318 16.6 90.7 3.4 177 11.6 0.3398 12.0 20.4 9.1 16.8 3.8 2.5 0.8 1.9 328 5.9 13.9 18.5 25.1 138 94.9 93.5 169 200 0.5603 11.7 323 16.5 8.7 3.9 2.5 329 14.8 25.7 95.6 0.9237 15.0 7.5 3.7 2.5 1.5 1.1 328 5.5 14.4 19.6 26.0 150 93.8 93.3 55.4 32 6.5 1.52 8.1 13.9 4.8 1.9 2.8 13.0 18.3 6.0 2.51 2.0 3.4 6.6 5.9 1.7 190 2.2 1.0 1.3 3.7 10.9 16.1 53.9 179 5,5 4.14 0.9 152 103 7.6 5.8 2.1 2.3 12.8 184 1.3 2.6 8.2 22.9 166 76.8 76.6 5.0 6.83 7.7 11.5 10.4 13.8 179 185 1.5 0.8 1.5 5.2 8.7 19.1 42.7 195

1.0

1.6

2.3

2.3 4.8

142

5.0

7.1

33.9 53.1 185 206

25.0 40.0

13.2

28.1 29.2

19.8

7.3

NOVEMBE	D HEAD 1	TEMPERA	TUDE A	MDI 170	ne // 1	AND 6	MASE	WAVE	,					QU.		••		
SCALE	PRESSURE	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
HEIGHT 12.0	(mb) 0.0062	0.08	0.30	0.18	0.01	0.41	0.49	0,12	0.17	0.60	0.77	1.27	1.02	0.52	0.64	0.37	0.47	0.29
11.5	0.0103	0.10	0.36	0.4	0.04	0.47	0.51	0.10	0.17	0,61	0.74	1.22	0.94	0.44	0.64	0.45	0.49	0.25
11.0	0.0169	0.09	0.39	0.30	0.08	0.55	0.50	0.06	0.14	0,58	0.65	1.05	0.75	0.32	0.65	0.52	0.51	354
10.5	0.0279	0.08	0.41	75	0.15	0.61	0.47	0.08	0.10	0,54	0.50	92	0.47	70	0.73	0,58	0.54	0.21
10.0	0.0460	0.05	70	73	0.24	0.67	0.41	0.15	0.07	0,48	0.32	0.41	0.15	0.48	349 U.89	0,60	0.58	0,32
9.5	0.0758	0.04	0.33	0.94	.51	0.68	0.32	0.21	0,05	0.40	0.13	90	0.41	0.76	0,99	0.51	0.55	0.44
9.0	0.1250	0.03	0.24	74 0,52	52	0,56	63	0.22	335	118	0.10	333	327	0.95	323	359	0.40	0.52
8.5	0.2061	162	95	78	58	36 0,26	78	63	0.12	0.21	0,23	0.62	318	327	322	19	353	0.50
8.0	0.3398	0.13	0.09	0.24	73	38	0.12	72	0,22	173	249	0,60	319	334	338	116	301	0.35
7.5	0.5603	0,17	0.12	0.19	0,21	201	178	173	192	0,30	240	273	326	355	1,37	140	189	0.19
7.0	0.9237	0.21	0.09	163	152	0.33	191	207	180	0.22	0.03	315	0.74	1,25	101	1.62	182	206
6.5	1.52	0.19	190	161	147	175	151	216	183	254	252	0.16	46 0.67	76	112	154	1.88	201
6.0	2,51	201	124	116	130	130	106	0.03	287	279	315	57	0.53	93	127	167	1,20	257
5.5	4.14	174	113	105	127	113	105	342	333	329	270	159	102	112	146	182	1,06	286
5.0	6.83	175	107	103	132	126	133	121	94	30	169	165	133	135	156	199	241	306
4.5	11.25	0.11	97	103	137	152	0.12 178 0.18	131	108	76	119	151	146	162	194	228	270	330
		187	82	0.56	140	200	203	131	109	0.15	96	116	147	196	234	267	310	0.25
4.0	18,55	323	61	105	140	234	216	129	107	0.20	83	0.37	132	228	267	296	340	0.27
3,5	30,59	0.12 326 0.14	0.32 36 0.27	106	0.12 135 0.03	0.42 249 0.42	0.27	0.30	0,27 105 0,26	0.22	76	0.50 57 0.58	0.22 86 0.26	251	2.08 284 1.92	310	355	0.31
3.0	50.43	326	13	108	101	256	224	128	103	82	71	48	45	265	294	319	0.88	92
2.5	83.15	332	0.21	111	350	261	225	129	102	0.16	67	0.50	32	273	300	1.22 324	0.62	98
NOVEMBE	R MEAN (PARATE																
		BEUPUIC	NITAL	HEIGHT	AMP LI	TUDE (gam) A	IND PHA	SE .	AVE 2								
SCALE HEIGHT	PRESSURE (mb)	+80	-70	-60	-50	-40	-30	-20	-10	O O	10	20	30	40	50	60	70	80
	PRESSURE										10 4.2 103	20 5.3 85	30 6.3 53	40 6.2 45	50 3.7 18	60 5.6 334	70 10.1 350	80 5.0 327
HEIGHT	PRESSURE (mb)	-80 3.6	-70 5.6	-60 8.9	-50 5.9	-40 4.7	-30 3.7	-20 2.6	-10 2.2	0	4.2	5.3	6.3	6.2	3.7	5.6	10.1	5.0
HEIGHT 12,0	PRESSURE (mb) 0.0062	-80 3.6 208 3.5 209 3.3	-70 5.6 106 5.3	-60 8.9 108 8.6	-50 5.9 130 5.9 131 5.9	-40 4.7 97 4.3	-30 3.7 86 3.2	-20 2.6 126 2.5 123 2.5	-10 2.2 121 2.0	0 4.7 120 4.0 123 3.3	4.2 103 3.1 104 2.0	5.3 85 3.5 80	6.3 53 5.7 40 5.5	6.2 45 5.8	3.7 18 2.8	5.6 334 5.1	10.1 350 9.9	5.0 327 4.6 325 4.3
12.0 11.5	PRESSURE (mb) 0.0062 0.0103	-80 3.6 208 3.5 209 3.3 210 3.2	-70 5.6 106 5.3 110 4.9 114 4.5	-60 8.9 108 8.6 109 8.3 110 7.9	-50 5.9 130 5.9 131 5.9 131 5.9	-40 4.7 97 4.3 103 3.9 111 3.6	-30 3.7 86 3.2 96 2.8 108 2.6	-20 2.6 126 2.5 123 2.5 121 2.4	-10 2.2 121 2.0 126 1.9 131 1.8	0 4.7 120 4.0 123 3.3 127 2.6	4.2 103 3.1 104 2.0 105	5.3 85 3.5 80 1.8 69 0.8	6.3 53 5.7 40 5.5 27 5.5	6.2 45 5.8 39 5.4 35 5.0	3.7 18 2.8 13 1.9 9	5.6 334 5.1 330 4.5 326 3.9	10.1 350 9.9 346 9.6 342 9.2	5.0 327 4.6 325 4.3 323
12.0 11.5 11.0	PRESSURE (mb) 0.0062 0.0103 0.0169	-80 3.6 208 3.5 209 3.3 210 3.2 211	-70 5.6 106 5.3 110 4.9 114 4.5 120	-60 8.9 108 8.6 109 8.3 110 7.9 112 7.4	-50 5.9 130 5.9 131 5.9 131 5.9 133 5.9	-40 4.7 97 4.3 103 3.9 111 3.6 123 3.6	-30 3.7 86 3.2 96 2.8 108 2.6 122	-20 2.6 126 2.5 123 2.5 121 2.4 121	-10 2.2 121 2.0 126 1.9 131 1.8 136	0 4.7 120 4.0 123 3.3 127 2.6 131	4.2 103 3.1 104 2.0 105 1.2 107 0.6	5.3 85 3.5 80 1.8 69 0.8 30	6.3 53 5.7 40 5.5 27 5.5 18	6.2 45 5.8 39 5.4 35 5.0 34	3.7 18 2.8 13 1.9 9 0.9 19	5.6 334 5.1 330 4.5 326 3.9 319 3.3	10.1 350 9.9 346 9.6 342 9.2 339 8.6	5.0 327 4.6 325 4.3 323 4.1 324
12.0 11.5 11.0 10.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279	-80 3.6 208 3.5 209 3.3 210 3.2 211 3.2 212	-70 5.6 106 5.3 110 4.9 114 4.5 120 4.1 126 3.8	-60 8.9 108 8.6 109 8.3 110 7.9 112 7.4 116	-50 5.9 130 5.9 131 5.9 131 5.9 133 5.9	-40 4.7 97 4.3 103 3.9 111 3.6 123 3.6 138 3.8	-30 3.7 86 3.2 96 2.8 108 2.6 122 2.5 136 2.4	-20 2.6 126 2.5 123 2.5 121 2.4 121 2.3 123	-10 2.2 121 2.0 126 1.9 131 1.8 136 140	0 4.7 120 4.0 123 3.3 127 2.6 131 2.1 137	4.2 103 3.1 104 2.0 105 1.2 107 0.6 112	5.3 85 3.5 80 1.8 69 0.8 30 0.9 326	6.3 53 5.7 40 5.5 27 5.5 18 5.4 14	6.2 45 5.8 39 5.4 35 5.0 34 4.6 38	3.7 18 2.8 13 1.9 9 0.9 19 0.7 108 2.0	5.6 334 5.1 330 4.5 326 3.9 319 3.3 309	10.1 350 9.9 346 9.6 342 9.2 339 8.6 335	5.0 327 4.6 325 4.3 323 4.1 324 3.9 329
11.5 11.0 10.5 10.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460	-80 3.6 208 3.5 209 3.3 210 3.2 211 3.2 212 3.1 213 3.1	-70 5.6 106 5.3 110 4.9 114 4.5 120 4.1 126 3.8 131 3.5	-60 8.9 108 8.6 109 8.3 110 7.9 112 7.4 116 6.9 120 6.4	-50 5.9 130 5.9 131 5.9 131 5.9 136 5.9 140 5.8	-40 4.7 97 4.3 103 3.9 111 3.6 123 3.6 138 3.8 153 4.3	-30 3.7 86 3.2 96 2.8 108 2.6 122 2.5 136 2.4 149 2.4	-20 2.6 126 2.5 123 2.5 121 2.4 121 2.3 123 2.1 129 2.0	-10 2.2 121 2.0 126 1.9 131 1.8 136 1.8 140 1.9	0 4.7 120 4.0 123 3.3 127 2.6 131 137 1.6 142	4.2 103 3.1 104 2.0 105 1.2 107 0.6 112 0.3 117	5.3 85 3.5 80 1.8 69 0.8 30 0.9 326 1.1 313	6.3 53 5.7 40 5.5 27 5.5 18 5.4 14 5.1 16	6.2 45 5.8 39 5.4 35 5.0 34 4.6 38 4.3 49	3.7 18 2.8 13 1.9 9 0.9 19 0.7 108 2.0 134	5.6 334 5.1 330 4.5 326 3.9 319 3.3 309 2.8 297 2.6	10.1 350 9.9 346 9.6 342 9.2 339 8.6 335 7.9 331 7.3	5.0 327 4.6 325 4.3 323 4.1 324 3.9 329 3.9 337 4.0
HEIGHT 12,0 11.5 11.0 10.5 10.0 9.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758	-80 3.6 208 3.5 209 3.3 210 3.2 211 3.2 212 3.1 213 3.1 214 3.1	-70 5.6 106 5.3 110 4.9 114 4.5 120 4.1 126 3.8 131 3.5 136 3.3	-60 8.9 108 8.6 109 8.3 110 7.9 112 7.4 116 6.9 125 5.9	-50 5.9 130 5.9 131 5.9 133 5.9 136 5.8 140 5.8	-40 4.7 97 4.3 103 3.9 111 3.6 123 3.8 153 4.3 164 4.7	-30 3.7 86 3.2 96 2.8 108 2.6 122 2.5 136 2.4 149 2.4 158 2.3	-20 2.6 126 125 123 2.5 121 2.4 121 2.3 123 2.1 138 1.9	-10 2.2 121 2.0 126 1.9 131 1.8 136 140 1.9 142 1.9	0 4.7 120 4.0 123 3.3 127 2.6 131 1.37 1.62 142 1.2 144 0.9	4.2 103 3.1 104 2.0 105 1.2 107 0.6 112 0.3 117 0.2 103 0.5	5.3 85 80 1.8 69 0.8 30 0.9 326 1.1 313 0.9 325 0.7	6.3 53 5.7 40 5.5 27 5.5 18 5.4 14 5.1 16 4.7 24	6.2 45 5.8 39 5.4 35 5.0 34 4.6 38 4.3 4.9 4.3 66 4.7	3.7 18 2.8 13 1.9 9 0.9 19 0.7 108 2.0 134 3.4 137	5.6 334 5.1 330 4.5 326 3.9 319 3.3 309 2.8 297 2.6 285 2.8	10.1 350 9.9 346 9.6 342 9.2 339 8.6 335 7.9 331 7.3 329 6.9	5.0 327 4.6 325 4.3 323 4.1 324 3.9 329 3.9 3.9 3.9 3.9 3.9 3.9
HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250	-80 3.6 208 3.5 209 3.3 210 3.2 211 3.2 212 3.1 213 3.1 214 3.1 215 2.9	-70 5.6 106 5.3 110 4.9 114 4.5 126 3.8 151 3.5 136 3.3 139	-60 8.9 108 8.6 109 8.3 110 7.9 112 7.4 116 6.9 120 6.4 125 5.9	-50 5.9 130 5.9 131 5.9 131 5.9 136 5.9 140 5.8 149 5.6	-40 4.7 97 4.3 103 3.9 111 3.6 123 3.6 138 153 4.3 164 4.7 170 4.8	-30 3.7 86 3.2 96 2.8 108 2.6 122 2.5 136 2.4 149 2.4 158 2.3 164 2.1	-20 2.6 126 2.5 123 2.5 121 2.4 121 2.3 123 2.1 129 2.0 138 1.9 146	-10 2.2 121 2.0 126 1.9 131 1.8 140 1.9 142 1.9 141 1.9 142 1.9	0 4.7 120 4.0 123 3.3 127 2.6 131 1.37 1.6 142 1.2 144 0.9 137 0.7	4.2 103 3.1 104 2.0 105 1.2 107 0.6 112 0.3 117 0.2 103 0.5 85 0.8	5.3 85 3.5 80 1.8 69 0.8 30 0.9 326 1.1 313 0.9 325 0.7 23	6.3 53 5.7 40 5.5 27 5.5 18 5.4 14 5.1 16 4.7 24 4.3 41	6.2 45 5.8 39 5.4 35 5.0 34 4.6 38 4.3 4.9 4.3 66 4.7 84 5.1	3.7 18 2.8 13 1.9 9 0.7 108 2.0 134 137 4.4 139	5.6 334 5.1 330 4.5 326 3.9 3.9 2.8 297 2.6 285 281 3.5	10.1 350 9.9 346 9.6 342 9.2 339 8.6 335 7.9 331 7.3 329 6.9 328 7.1	5.0 327 4.6 325 4.3 323 4.1 324 3.9 329 3.9 337 4.0 348 4.4 357 4.8
HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061	-80 3.6 208 3.5 209 3.3 210 3.2 211 3.2 212 3.1 213 3.1 215 2.9 2.7	-70 5.6 106 5.3 110 4.9 114 4.5 120 4.1 126 3.8 131 3.5 136 3.3 139 3.2	-60 8.9 108 8.6 109 8.3 110 7.9 112 7.4 116 6.9 120 6.4 125 5.9 129 5.5 5.2	-50 5.9 130 5.9 131 5.9 133 5.9 136 5.8 149 5.8 149 5.8 149 5.8	-40 4.7 97 4.3 103 3.6 123 3.6 138 3.6 158 164 4.7 170 4.8 171 4.4	-30 3.7 86 3.2 96 2.8 108 2.6 122 2.5 136 2.4 158 2.3 164 2.1 165 2.0	-20 2.6 126 2.5 123 2.5 121 2.4 121 2.3 123 2.1 129 2.0 138 1.9 146 1.9 148 1.7	-10 2.2 121 2.0 126 1.9 131 1.8 140 1.9 141 1.9 141 1.9 137 1.8	0 4.7 120 4.0 123 3.3 127 2.6 131 2.1 137 1.6 142 1.2 144 0.9 137 0.9	4.2 103 3.1 104 2.0 105 1.2 107 0.6 112 0.3 117 0.2 103 0.5 85 0.8 76	5.3 85 3.5 80 1.8 69 0.8 30 0.9 326 1.1 313 0.9 325 0.7 23 1.3 62 1.8	6.3 53 5.7 40 5.5 27 5.5 18 5.4 14 5.1 16 4.7 24 4.3 41 4.3 5.9	6.2 45 5.8 39 5.4 35 5.0 34 4.6 38 4.3 66 4.7 84 5.1 97	3.7 18 2.8 13 1.9 9 0.9 19 0.7 108 2.0 134 137 4.4 137 4.4 139 4.6 144 3.7	5.6 334 5.1 330 4.5 326 3.9 319 3.3 309 2.8 297 2.6 285 2.8 281 3.5 288 4.9	10.1 350 9.9 346 9.2 339 8.6 335 7.9 331 7.3 329 6.9 320 8.0	5.0 327 4.6 325 4.3 323 4.1 324 3.9 329 3.9 337 4.0 348 4.4 357 4.6 557
HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 8.0	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398	-80 3.6 208 3.5 209 3.2 210 3.2 211 3.2 212 3.1 215 2.9 215 2.7 214	-70 5.6 106 5.3 110 4.9 114 4.5 120 4.1 1126 3.8 131 3.5 136 3.2 138 3.2 138 3.2	-60 8.9 108 8.6 109 110 7.9 112 7.4 116 6.9 120 6.4 125 5.9 132 5.5 132 5.5	-50 5.9 130 5.9 131 5.9 131 5.9 136 5.9 145 5.8 145 5.8 145 5.8 145 5.8 150 5.9 5.9 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0	4.7 97 4.3 103 3.9 111 3.6 123 3.6 138 4.3 164 4.7 170 4.8 171 4.8 171	-30 3.7 86 3.2 96 2.8 108 2.6 122 2.5 136 2.4 158 2.4 158 2.3 164 2.1 165 2.0 163 164 2.1 165 2.0 165 165 165 165 165 165 165 165	-20 2.6 126 2.5 123 2.5 121 2.4 121 2.3 123 2.1 129 2.0 138 1.9 146 1.9 148 1.7 143	-10 2.2 121 2.0 126 1.9 131 1.8 136 140 1.9 141 1.9 141 1.9 141 1.9 141 1.9 141 1.9 141 1.9	0 4.7 120 4.0 123 3.3 127 2.6 131 1.2 1.4 1.2 1.4 1.7 1.7 1.0 0.9 137 0.7 110 0.9 12 12 12 13 13 13 13 13 13 13 13 13 13 13 13 13	4.2 103 3.1 104 2.0 105 1.2 107 0.6 112 0.3 117 0.2 103 0.5 85 0.8 76	5.3 85 3.5 80 1.8 69 0.8 30 0.9 326 1.1 313 0.9 325 0.7 23 1.3 62 1.8	6.3 53 5.7 40 5.5 27 5.5 18 5.4 14 4.7 24 4.3 4.1 4.3 5.9 4.0 74	6.2 45 5.8 39 5.4 35 5.0 34 4.6 38 4.3 4.3 66 4.7 84 5.1 97 4.8	3.7 18 2.8 13 1.9 9 0.9 19 0.7 108 2.0 134 3.4 139 4.6 144 3.7 160 3.0	5.6 334 5.1 330 4.5 3.9 319 3.3 309 2.8 2.97 2.6 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8	10.1 350 9.9 346 9.6 342 9.2 339 8.6 335 7.9 331 7.3 329 6.9 328 7.1 330 8.0 8.3 9.2 9.2 9.2 9.3 9.3 9.3 9.3 9.3 9.3 9.3 9.3 9.3 9.3	5.0 327 4.6 325 4.3 325 4.1 324 3.9 329 3.9 329 3.9 3.7 4.0 348 4.4 357 4.8 3 5.1 6 5.3
HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 8.0 7.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398	3.6 208 3.5 209 3.3 210 3.2 211 213 3.1 215 2.9 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1	-70 5.6 106 5.3 110 4.9 114 4.5 120 3.8 131 3.5 136 3.2 135 3.2 135 3.2	-60 8.9 108 8.6 109 8.3 110 7.9 112 7.4 116 6.9 129 5.5 131 5.0 129 129 129 131 147 147 147 147 147 147 147 147 147 14	-50 5.9 130 5.9 131 5.9 133 5.9 136 5.8 140 5.8 149 5.6 152 5.9 144 149 154 155 156 157 158 158 158 158 158 158 158 158	4.7 97 4.3 103 5.9 111 3.6 123 3.6 138 153 4.3 164 4.7 170 4.8 169 3.9 166 3.5	-30 3.7 86 3.2 96 2.8 108 2.6 122 2.5 136 2.4 158 2.3 164 2.1 165 2.0 163 1.9 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2	-20 2.6 126 2.5 123 2.5 121 2.4 121 2.3 123 2.1 129 146 1.9 146 1.7 143 1.7	-10 2.2 121 2.0 1.9 1.51 1.8 136 140 1.9 141 1.9 137 1.8 130 1.9 141 1.9 151 1.9 151 1.9 151 1.9 151 1.9 151 151 151 151 151 151 151 151 151 15	0 4.7 120 4.0 123 3.3 127 2.6 131 1.2 1.4 1.2 1.4 1.2 1.4 0.7 1.10 0.9 86 1.3	4,2 103 3,1 104 2,0 105 1,2 107 0,6 112 0,3 117 0,5 85 0,8 76 1,1 1,2 1,2 103 1,1 1,2 103 1,1 1,2 1,0 1,0 1,0 1,0 1,0 1,0 1,0 1,0 1,0 1,0	5.3 85 3.5 86 9 0.8 30 0.9 326 1.1 313 325 0.7 23 1.3 62 1.8 75	6.3 53 5.7 40 5.5 27 5.5 18 5.4 14 4.7 24 4.3 41 4.3 41 4.3 4.0 74 4.0 74 4.0 74	6.2 45 5.8 39 5.4 4.3 5.0 34 4.3 66 4.7 84 109 3.9 9.126 2.7	3.7 18 2.8 13 1.9 9 0.9 19 0.7 108 2.0 134 4.4 139 4.6 144 3.7 160 3.0 3.8	5.6 334 5.1 336 5.9 319 3.09 2.8 297 2.8 281 3.5 288 4.9 298 6.8 39.0	10.1 350 9.9 346 342 9.2 339 7.9 331 7.5 329 6.9 328 7.1 330 8.0 334 9.4	5.0 327 4.6 325 4.3 325 4.1 324 3.9 329 3.9 337 4.0 348 4.4 357 4.8 357 4.8 5.7 6 5.3 6
HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 8.0 7.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.758 0.1250 0.2061 0.3398 0.5603 0.9237	-80 3.6 208 3.5 209 3.3 210 3.2 211 213 3.1 214 3.1 215 2.9 215 2.7 216 2.7 217 218 2.7 218 2.7 218 2.7 218 2.7 218 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7	-70 5.6 106 5.3 110 4.9 114 4.5 120 4.1 126 131 3.6 135 136 3.3 139 3.2 138 3.2 138 3.2 138 3.3 3.2 138 138 138 138 138 138 138 138	-60 8.9 108 8.6 109 8.3 110 7.4 116 6.9 125 5.9 129 5.5 132 131 5.2 131 5.2 147 129 4.7 129	-50 5.9 130 5.9 131 5.9 133 5.9 140 5.8 149 5.6 152 5.5 152 4.6 4.0	4.7 97 4.3 103 103 5.6 111 5.6 123 3.6 138 4.3 164 4.7 170 4.8 171 4.4 169 9 166 5.5 168 3.9	-30 3.7 86 3.2 96 2.8 108 2.6 122 2.5 136 2.4 149 2.4 165 2.3 164 2.1 165 2.0 163 1.6 165 1.6 165 1.6 165 1.6 165 165 165 165 165 165 165 165 165 16	-20 2.6 126 2.5 123 2.5 121 2.4 121 2.3 1.25 2.1 129 2.0 1.8 1.9 146 1.9 146 1.7 143 1.7 145 1.7 145 1.7 145 1.7 145 1.7 145 145 145 145 145 145 145 145 145 145	-10 2.2 121 2.0 1.26 1.9 131 1.8 140 1.9 141 1.9 141 1.9 137 1.8 130 1.7 1.2 1.6 1.5 1.6 1.6 1.7 1.7 1.8 1.8 1.8 1.8 1.8 1.8 1.8 1.8 1.8 1.8	0 4.7 120 4.0 123 3.3 127 2.6 131 1.6 142 1.2 1.2 1.4 0.9 157 0.7 110 0.9 86 1.3 1.3 1.3 1.3 1.3 1.3 1.3 1.3 1.3 1.3	4.2 103 3.1 1104 2.0 105 1.2 107 0.6 112 103 0.5 85 0.8 76 1.1 70 1.2 70 1.3 71 1.3	5.3 85 3.5 80 1.8 69 0.9 326 1.1 313 30.9 325 0.7 75 1.8 75 1.8 85 1.8 85 1.8	6.3 53 5.7 40 5.5 27 5.5 18 5.4 14 4.7 24 4.3 5.9 4.0 74 86 2.5 98 1.7	6.2 45 5.8 39 5.4 35 5.0 34 4.3 66 4.7 84 5.1 97 4.8 197 4.8 197 196 2.7 154	3.7 18 2.88 13 1.9 9 0.9 19 0.7 108 2.00 134 137 4.6 144 3.7 160 3.0 200 3.8 8 2.8 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	5.6 334 5.1 330 4.5 326 3.9 3.3 309 2.8 287 2.6 285 2.8 2.8 2.8 2.8 2.8 3.9 2.8 3.9 2.8 3.9 3.9 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0 3.0	10.1 350 9.9 9.6 342 9.2 359 8.6 335 7.9 351 7.3 329 6.9 328 7.1 330 8.0 334 9.2 8.3 9.2 9.2 9.2 9.2 9.2 9.2 9.3 9.3 9.3 9.3 9.3 9.3 9.3 9.3 9.3 9.3	5.0 327 4.6 325 4.3 325 4.1 324 3.9 337 4.0 348 4.4 357 4.8 357 6 5.3 6
HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 8.0 7.5 7.0	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603 0.9237	3.6 208 3.5 209 3.3 210 3.2 211 3.1 214 3.1 215 2.9 215 2.7 214 2.1 213 3.1 213 2.1 213 2.1 213 2.1 213 2.1 213 2.1 215	-70 5.6 106 5.3 110 4.9 114 4.5 120 4.1 126 5.8 131 5.5 5.2 135 5.2 135 5.2 135	-60 8.9 108 8.6 109 8.3 110 7.4 116 6.9 120 6.4 125 5.9 129 131 5.0 129 4.7 129	-50 5.9 130 5.9 131 5.9 133 5.9 135 136 5.8 145 5.8 145 5.6 152 5.6 152 4.6 154 4.0 158	4.7 97 4.3 103 3.9 111 3.6 138 3.6 153 4.3 164 4.7 170 4.8 171 4.4 169 3.9 166 3.5 168 3.5 168 3.5 168 3.5 168 3.5 171	-30 3.7 86 3.2 96 2.8 108 2.6 1.2 2.5 1.36 2.4 149 2.3 164 2.1 165 2.0 163 1.9 162 1.8 165 1.8 165 1.8	-20 2.6 126 2.5 123 2.5 121 2.3 123 2.5 121 2.3 129 146 1.9 148 1.7 143 1.7 143 1.7 143 1.7 143 1.7	-10 2.2 121 2.0 1.26 1.9 131 1.8 140 1.9 141 1.9 137 1.8 1.9 141 1.9 137 1.8 1.9 141 1.9 1.9 1.9 1.9 1.9 1.9 1.9 1.9 1.9 1.	0 4.7 120 4.0 123 3.3 127 2.6 131 1.6 1.42 1.2 1.44 0.9 137 0.7 110 0.9 86 1.3 81 1.4 84 84 84	4.2 103 3.1 104 2.0 107 0.6 112 107 0.5 85 0.8 85 0.8 76 72 1.2 1.2 1.3 71 1.3 71 1.3 72	5.3 85 85 80 1.8 69 9.326 6.30 0.9 3.25 0.7 23 1.3 1.3 6.2 1.8 75 1.8 85 1.6 93 1.6 1.6 93 1.6 9 1.6 9 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6	6.3 53 5.7 40 5.5 27 5.5 18 5.4 14 4.7 24 4.3 3.5 9 4.0 74 4.3 3.4 86 2.5 98 10 10 10 10 10 10 10 10 10 10 10 10 10	6.2 45 5.8 39 5.4 35 5.0 34 4.6 4.7 84 109 3.9 4.8 109 2.7 1154 2.2 2.03	3.7 18 2.8 13 1.9 9 9 9 9.7 19 0.7 134 3.4 139 4.6 144 3.7 160 3.0 3.8 248 5.8 248 5.8 278	5.6 334 5.1 330 4.5 3.9 3.3 3.9 3.3 2.8 2.8 2.8 2.8 4.9 2.98 6.8 9.0 3.17 11.4	10.1 350 9.9 9.5 346 9.6 342 9.2 9.339 8.6 335 7.9 331 7.3 329 6.9 328 7.1 1330 8.0 334 9.4 9.3 351	5.0 327 4.6 325 4.3 323 4.1 324 3.9 329 337 4.0 337 4.6 357 4.6 357 4.6 5.5 6 5.5 8
HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 8.0 7.5 7.0 6.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3598 0.5603 0.9237 1.52 2.51	-80 3,6 208 3,5 209 3,3 210 3,2 211 3,1 213 3,1 215 2,7 214 2,4 2,4 2,1 1,9 216 1,7 222	-70 5.6 106 5.3 110 4.9 114 4.5 120 3.8 131 126 3.8 131 3.5 136 3.2 138 3.2 138 3.2 138 3.2 138 146 141	-60 8.9 108 8.6 109 110 7.9 1112 7.4 116 6.9 120 6.4 125 5.5 129 131 5.0 129 4.7 129 129 129 129 129 129 129 129 129 129	-50 5.9 130 5.9 131 5.9 135 5.9 136 5.8 140 5.8 149 5.8 149 5.8 149 5.8 149 5.8 140 5.8 140 5.8 140 5.8 140 5.8 140 5.8 140 5.8 140 5.8 140 5.8 140 5.8 140 5.8 140 5.8 140 5.8 140 5.8 140 5.8 140 5.8 140 5.8 140 6.8 6.8 6.8 6.8 6.8 6.8 6.8 6.8	4.7 97 4.3 103 5.9 111 3.6 123 3.6 153 3.6 4.7 170 4.8 171 4.4 4.7 170 4.8 171 170 170 170 170 170 170 170 170 170	-30 3.7 86 2.8 96 2.6 102 2.5 1.56 2.4 158 2.3 164 2.1 163 1.9 2.0 163 1.7 170 1.7	-20 2.6 126 2.5 123 2.5 121 2.4 121 2.3 125 2.0 138 1.9 146 1.7 143 1.7 143 1.7 145 1.7 145 1.7 145 1.7 145 1.7 145 1.7 145 1.7 145 1.7 145 1.7 145 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7	-10 2,2 121 1,9 1,9 141 1,9 141 1,9 141 1,9 141 1,9 141 1,9 141 1,9 1,0 1,0 1,0 1,0 1,0 1,0 1,0 1,0 1,0 1,0	0 4.7 120 4.0 1.23 5.3 1.27 2.6 131 1.37 1.6 142 1.2 144 9.1 1.7 0.7 1.0 0.9 86 1.2 1.2 1.2 1.3 1.3 1.3 1.3 1.3 1.3 1.3 1.3 1.3 1.3	4.2 103 3.1 104 2.0 0.5 112 107 0.5 117 0.2 103 0.5 76 76 1.1 72 1.2 1.3 71 1.3 71 1.3	5.3 85 3.5 80 0.8 30 0.9 326 1.1 313 325 0.7 723 1.8 81 69 1.8 81 81 81 81 81 81 81 81 81 81 81 81 81	6.3 53 5.7 40 5.5 5.7 7.8 5.4 4.7 4.3 4.3 4.3 4.3 4.3 4.3 4.3 8.6 2.5 9.8 1.7 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5	6.2 45 5.8 39 5.4 4.6 66 4.7 84 4.3 4.3 4.9 7 7 8 4.8 109 126 2.7 154 2.7 2.7 2.7 2.5 3.6	3.7 188 2.8 13 1.9 9 0.9 19 0.7 108 2.0 134 4.4 137 4.6 144 3.7 160 3.0 200 3.8 248 5.8 248 7.9 9.9 9.9 9.9 9.9 9.9 9.0 9.0 9.0 9.0 9	5.6 334 5.1 3.30 4.5 3.26 3.9 3.19 3.33 2.8 2.8 2.8 2.8 2.8 3.5 2.8 8 4.9 8 6.8 3.9 3.7 11.4 11.5 11.5 11.5 11.5 11.5 11.5 11.5	10.1 350 9.9 9.6 342 9.2 359 8.6 335 7.9 351 7.3 329 6.9 328 7.1 330 8.0 334 9.2 8.3 9.2 9.2 9.2 9.2 9.2 9.2 9.3 9.3 9.3 9.3 9.3 9.3 9.3 9.3 9.3 9.3	5.0 327 4.6 325 4.3 323 4.1 3.9 329 329 337 4.0 4.8 5.7 6 5.3 6 5.5 8 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9
HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 6.0 7.5 7.0 6.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0798 0.1250 0.2061 0.3398 0.5603 0.9237 1.52 2.51	-80 3.6 208 3.5 209 3.3 210 3.2 211 3.2 212 212 213 3.1 213 3.1 215 2.7 214 2.4 2.4 2.1 213 2.1 213 2.1 216 2.2 216 228 1.6 228	-70 5.6 5.3 110 6.9 114 4.5 120 4.1 126 5.3 139 5.2 136 5.2 136 5.2 137 5.2 138 6.2 135 1.2 136 1.3 139 132 135 1.2 136 1.3 139 131 131 139 131 141 141 141 141 141 141 141 141 141	-60 8.9 108 8.6 109 8.3 110 7.9 120 6.4 115 5.9 125 5.9 132 5.2 131 5.0 129 4.7 129 4	-50 5.9 130 5.9 131 5.9 131 5.9 133 5.9 130 5.8 140 5.8 149 5.8 149 5.8 152 4.6 154 4.0 158 158 159 150 150 150 150 150 150 150 150	4.7 97 4.3 103 3.9 111 3.6 123 3.6 153 4.3 164 4.7 170 4.8 171 4.8 169 3.9 166 5.5 168 5.5 174 2.9 174 2.9 183 2.6 193 2.6 193 2.6 193 2.7 193 193 193 193 193 193 193 193 193 193	-30 3.7 86 3.2 96 108 2.6 1108 2.5 136 2.5 163 1.9 1.6 1.6 1.6 1.7 1.6 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7	-20 2.6 126 127 123 2.5 121 2.3 121 2.3 129 146 1.7 132 1.7 132 1.7 132 1.7 132 1.7 132 1.7 132 1.7 132 1.7 132 1.7 132 1.7 132 1.7 132 1.7 132 1.7 132 1.7 132 132 148 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7	-10 2,2 121 1,2 1,2 1,2 1,2 1,3 1,3 1,4 1,4 1,9 1,4 1,9 1,4 1,9 1,7 1,6 1,6 1,7 1,7 1,6 1,6 1,7 1,7 1,6 1,7 1,7 1,7 1,7 1,7 1,7 1,7 1,7 1,7 1,7	0 4.7 120 4.0 123 3.3 127 2.6 131 1.7 1.6 1.4 1.9 1.9 1.9 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	4.2 103 3.1 104 2.0 0.105 1.2 107 0.6 112 103 0.5 85 85 1.1 72 1.3 72 1.3 72 1.3 72 1.3 72 1.3 72 1.3 71 1.3 71	5.35 85 80 1.88 69 0.8 30 0.9 325 0.7 23 1.31 31 31 31 31 31 31 31 31 31 31 31 31 3	6.3 53 5.7 40 5.5 7 7 5.5 18 6.4 4.7 24 4.3 4.3 4.3 4.0 74 4.3 8.6 8.6 9.6 9.6 9.6 9.6 9.6 9.6 9.6 9.6 9.6 9	6.2 45 5.8 39 5.4 4.3 5.0 34 4.3 66 64 4.7 84 109 3.9 126 2.7 7 154 2.2 203 2.7 154 2.2 203 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7	3.7 188 2.8 13 1.9 9 0.9 19 0.7 108 2.0 134 137 4.6 137 160 3.0 200 5.8 278 7.9 9.6 298 9.6 298 298 298 298 298 298 298 298 298 298	5.6 334 4.5 3.9 3.9 3.9 3.9 2.6 2.8 2.8 2.8 3.5 2.8 2.8 3.5 3.8 2.8 3.8 2.8 3.8 3.8 3.8 3.8 3.8 3.8 3.8 3.8 3.8 3	10.1 350 9.9 346 9.6 342 9.2 339 6.9 331 7.3 329 6.9 331 7.3 328 7.1 339 10.6 351 12.9 351 12.0 351 12.0 351 12.0 351	5.0 327 4.6 325 4.3 323 329 329 329 339 340 4.1 4.8 557 6 5.3 6 5.5 8 8 5.5 8 8 5.5 8 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9
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HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 7.0 6.5 6.0 5.5 5.0	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3398 0.5603 0.9237 1.52 2.51 4.14 6.83	3.6 208 3.5 209 3.3 210 3.2 211 3.1 213 3.1 214 3.1 215 2.9 217 213 2.1 1.6 2.9 216 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1	-70 5.6 106 5.3 110 6.9 1.14 4.5 120 4.1 1.26 6.3 131 5.5 1.56 5.3 1.39 5.2 1.35 5.2 1.35 5.2 1.35 5.2 1.36 1.46 1.31 1.46 1.31 1.49 1.49 1.49 1.49 1.49 1.49 1.49 1.4	-60 8.9 108 8.6 109 8.3 110 7.9 120 6.4 125 5.9 129 132 5.2 131 5.0 129 4.7 129 129 129 129 129 129 129 129	-50 5.9 130 5.9 131 5.9 131 5.9 133 5.9 140 5.6 152 5.6 152 4.6 152 4.6 154 154 154 154 154 154 154 154	4.7 97 4.3 103 5.9 111 3.6 123 3.6 123 3.6 123 138 4.3 164 4.7 171 4.4 169 168 174 183 2.6 193 192 1.8 193 193 193 193 193 193 193 193 193 193	-30 3.7 86 3.2 96 108 2.6 108 2.5 132 2.4 149 2.3 164 2.1 163 1.6 1.7 170 1.6 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7	-20 2.6 126 2.5 121 2.5 121 2.5 121 2.5 121 2.3 1.3 1.9 1.9 1.6 1.7 1.3 1.7 1.3 1.7 1.3 1.7 1.3 1.7 1.3 1.7 1.3 1.7 1.3 1.7 1.3 1.7 1.3 1.7 1.3 1.7 1.3 1.7 1.3 1.7 1.3 1.7 1.3 1.7 1.3 1.7 1.3 1.7 1.3 1.7 1.3 1.7 1.3 1.7 1.7 1.7 1.3 1.7 1.7 1.7 1.7 1.7 1.7 1.3 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7	-10 2.2 121 2.0 126 1.9 131 1.8 136 1.8 140 141 1.9 141 1.9 137 1.6 1.6 113 1.6 115 1.6 115 1.6 115 1.6 1.6 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7	0 4.7 120 4.0 123 3.127 2.6 131 1.6 142 1.2 1.2 1.4 1.3 1.3 1.6 1.3 1.6 1.6 1.7 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	4.2 103 3.1 104 2.0 105 1.2 107 0.6 112 0.3 117 0.6 110 0.8 7 107 103 117 103 117 103 117 103 117 103 117 103 117 103 117 103 117 103 104 105 105 105 105 105 105 105 105 105 105	5.3 85 85 3.5 80 1.6 69 0.8 30 0.9 326 6 30 0.9 326 6 1.1 313 1.3 325 0.7 75 1.8 85 1.6 85 1.5 93 1.5 93 1.5 48 81 1.1 29 90.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7	6.3 555 5.7 40 5.5 5.7 7 5.5 14 5.1 16 4.7 24 4.3 4.1 4.3 4.1 4.3 4.1 6.6 6.6 6.7 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7	6.2 45 5.8 39 5.4 35 5.0 34 4.6 35 4.3 49 4.3 66 4.7 84 8.109 9.196 2.7 25 1.5 280 4.1 321 4.4 4.4 4.4	3.7 18 2.8 13 1.9 9 0.9 19 0.7 12.0 134 4.4 4.4 4.4 4.5 1.6 0.5 200 5.8 278 9.6 9.6 9.6 9.6 9.6 9.6 9.6 9.6 9.6 9.6	5.6 334 4.5 3.26 3.9 3.19 3.3 3.09 2.8 2.8 2.8 4.9 2.8 5.2 8 6.8 3.0 3.17 11.4 3.25 13.25	10.1 350 9.9 346 9.2 9.2 9.2 8.6 357 9.3 8.6 351 7.1 350 9.3 8.0 354 9.3 9.3 9.3 9.3 9.3 9.3 9.3 9.3 9.3 9.3	5.0 327 4.6 325 4.3 323 4.1 3.9 329 329 4.3 3.9 329 4.6 5.7 4.8 5.7 8 5.5 8 5.5 8 5.5 8 5.5 8 6 7 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8
HEIGHT 12.0 11.5 11.0 10.5 10.0 9.5 9.0 8.5 6.0 7.5 7.0 6.5 5.0 4.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.0758 0.1250 0.2061 0.3598 0.5603 0.9237 1.52 2.51 4.14 6.83 11.25	-80 3.6 208 3.5 209 3.3 210 3.2 211 3.2 212 213 3.1 215 2.7 214 2.4 2.1 213 1.9 215 2.7 214 2.4 2.1 215 2.7 216 2.7 216 2.7 217 217 218 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7	-70 5.6 5.3 110 6.9 1.14 4.5 1.20 4.1 1.26 3.8 1.31 3.5 3.2 1.38 3.2 1.35 3.2 1.35 3.2 1.35 1.25 1.35 1.25 1.35 1.25 1.35 1.25 1.35 1.25 1.35 1.25 1.35 1.25 1.35 1.25 1.35 1.25 1.35 1.25 1.35 1.25 1.35	-60 8.9 108 8.6 109 8.3 110 7.9 112 7.4 116 6.9 129 129 129 132 5.9 131 5.0 1132 5.2 131 5.0 1132 132 132 132 132 132 132 13	-50 5.9 130 5.9 131 5.9 133 5.9 136 5.8 149 5.8 149 5.8 152 5.0 152 5.0 154 4.0 158 158 159 150 150 150 150 150 150 150 150	4.7 97 4.3 103 5.9 111 3.6 138 3.6 138 4.3 164 4.7 170 4.4 169 3.9 166 3.2 2.9 174 2.9 1.9 1.9 1.9 1.9 1.9 1.9 1.9 1.9 1.9 1	-30 3.7 86 3.2 96 2.8 8108 2.6 108 2.5 136 2.3 164 2.1 165 2.0 163 1.9 162 1.7 170 1.6 1.7 1.7 1.1 1.6 0.9 144 0.9	-20 2.6 1.26 1.25 1.23 2.5 1.21 2.3 1.21 2.3 1.29 1.30 1.48 1.7 1.56 1.7 1.52 1.7 1.52 1.7 1.52 1.7 1.52 1.6 1.53 1.6 1.53 1.6 1.7 1.5 1.6 1.7 1.5 1.6 1.7 1.7 1.5 1.6 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7	-10 2.2 121 2.0 126 1.9 131 1.8 140 1.9 141 1.9 141 1.9 137 1.6 113 1.6 113 1.6 115 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6 1.6	0 4.7 120 123 3.3 127 2.6 131 1.2 1.2 1.2 1.4 1.2 1.2 1.0 1.2 1.0 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.2 1.3 1.3 1.3 1.3 1.3 1.3 1.3 1.3 1.3 1.3	4.2 103 3.1 104 2.0 0.6 112 0.5 117 0.2 107 0.6 117 103 0.5 85 85 117 117 113 68 117 117 113 117 117 118 119 119 119 119 119 119 119 119 119	5.3 85 85 80 1.8 69 9 326 1.1 1.3 62 1.8 85 1.6 93 1.5 1.8 85 1.6 93 1.4 69 93 1.4 69 93 1.4 69 93 1.4 69 93 1.4 69 93 1.4 69 93 1.4 69 1.4 6 1.4 1.4 6 1.4 6 1.4 1.4 1.4 1.4 1.4 1.4 1.4 1.4 1.4 1.4	6.3 555 5.7 40 5.5 27 7.5 5.5 18 5.4 14 4.3 4.3 4.3 4.3 4.3 4.3 4.3 4.3 4.3 4.	6.2 45 5.8 39 5.4 39 5.0 34 4.6 38 4.9 4.3 66 64.7 7 8 4.0 9 7.7 154 2.2 2.0 3.2 2.7 2.7 2.7 3.8 4.1 4.1 3.8 4.1 4.1 4.1 4.1 4.1 4.1 4.1 4.1 4.1 4.1	3.7 18 2.8 13 1.9 9 0.9 19 0.7 108 2.0 0.7 108 3.4 1.5 4.6 1.4 1.5 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0 2.0	5.6 3.34 4.5 5.1 3.30 4.5 3.26 3.9 3.3 3.09 2.8 2.8 2.8 2.8 4.9 2.8 6.8 3.08 9.3 11.4 3.25 13.5 13	10.1 350 9.9 346 9.2 339 8.6 339 7.9 328 8.0 330 8.0 334 12.0 351 12.9 351 12.9 351 13.3 13.3 13.3 13.3 13.3 13.3 13.3	5.0 327 4.6 325 4.3 323 4.1 3.9 329 337 4.0 3.9 337 4.0 3.9 557 4.8 3 5.1 6 5.3 6 5.3 6 5.5 13 4.1 4.8 24 4.8 4.8 4.8 4.8 4.8 4.8 4.8 4.8 4.8 4.
HEIGHT 12.0 11.3 11.0 10.5 10.0 9.5 9.0 8.5 6.0 7.5 6.0 5.5 5.0 4.5	PRESSURE (mb) 0.0062 0.0103 0.0169 0.0279 0.0460 0.1250 0.2061 0.3398 0.5603 0.9237 1.52 2.51 4.14 6.83 11.25 18.55 30.59	3.6 208 3.5 209 3.3 3.2 210 3.1 213 3.1 214 3.1 215 2.7 214 2.4 2.4 2.4 2.1 213 3.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2	-70 5.6 106 5.3 110 6.9 1.14 4.5 120 4.1 1.26 6.3 131 5.5 1.56 5.3 1.39 5.2 1.35 5.2 1.35 5.2 1.35 5.2 1.36 1.46 1.31 1.46 1.31 1.49 1.49 1.49 1.49 1.49 1.49 1.49 1.4	-60 8.9 108 8.6 109 8.3 110 7.9 120 6.4 116 6.9 125 132 131 5.0 129 4.7 132 4.7 132 4.7 132 4.7 153 150 150 150 150 150 150 150 150	-50 5.9 130 5.9 131 5.9 131 5.9 140 5.8 145 5.6 152 4.6 154 4.0 158 4.0 158 164 171 2.2 189 1.7 1.8 1.8 1.8 1.8 1.8 1.8 1.8 1.8	4.7 97 4.3 103 3.6 153 3.6 153 4.3 164 4.7 170 4.8 171 4.8 171 4.8 171 4.8 171 4.8 174 4.7 176 176 176 176 176 176 176 176 176 17	-30 3.7 86 3.2 96 2.6 102 2.5 136 2.4 149 2.3 163 1.9 162 1.8 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7	-20 2.6 126 2.5 123 2.5 121 2.4 121 2.3 123 2.0 138 1.9 146 1.9 147 143 1.7 143 1.7 132 1.6 1.6 1.7 132 1.6 1.6 1.7 132 1.6 1.6 1.7 132 1.6 1.7 132 1.6 1.6 1.7 132 1.6 1.6 1.7 132 1.6 1.6 1.7 132 1.6 1.6 1.7 132 1.6 1.6 1.7 132 1.6 1.6 1.7 132 1.6 1.6 1.7 132 1.6 1.6 1.7 132 1.6 1.6 1.7 132 1.6 1.6 1.7 132 1.6 1.6 1.7 132 1.6 1.6 1.7 132 1.6 1.6 1.7 132 1.6 1.6 1.7 132 1.6 1.6 1.7 132 1.6 1.6 1.7 132 1.6 1.6 1.7 132 1.6 1.6 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7	-10 2.2 121 2.0 126 1.8 1.8 140 1.9 142 1.9 141 1.9 147 1.8 130 1.6 1.6 1.1 1.6 1.6 1.1 1.6 1.6 1.6 1.6	0 4.7 120 4.0 123 3.127 2.6 131 1.6 142 1.2 1.4 1.0 9.6 1.3 80 1.3 84 1.4 84 1.4 87 1.3 88 89 90 90	4.2 103 3.1 104 2.0 105 1.2 107 0.6 112 0.5 103 103 105 103 104 103 104 105 103 105 105 107 107 108 108 109 109 109 109 109 109 109 109 109 109	5.3 85 85 1.8 80 0.8 69 0.9 326 0.9 326 1.1 313 0.9 325 0.7 2 1.8 85 1.5 93 1.4 81 1.4 5 48 81 1.4 29 0.7 7 23 48 81 1.4 29 0.7 23 1.5 48 81	6.3 53 5.7 40 5.5 27 5.5 18 5.4 16 4.7 24 4.3 5.9 4.3 4.3 4.3 5.9 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0	6.2 45 5.8 39 5.4 35 5.0 34 4.6 35 4.3 49 4.3 66 4.7 84 8.109 9.196 2.7 25 1.5 280 4.1 321 4.4 4.4 4.4	3.7 18 2.8 13 1.9 9 0.9 19 0.7 108 3.4 4.6 134 4.6 144 7.1 160 3.0 0.20 200 5.8 278 9.6 298 9.6 200 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	5.6 334 4.5 3.9 3.9 3.3 3.9 2.6 2.8 2.9 2.8 2.8 2.9 2.8 2.8 2.8 2.8 2.8 2.8 3.5 2.8 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5	10.1 9.9 346 9.6 9.2 9.2 9.2 9.2 8.6 339 331 7.3 329 6.9 334 9.4 12.0 357 13.3 12.0 13.5 13.0 13.0 13.0 13.0 14.0 15.0 16.0	5.0 327 4.6 325 4.3 323 4.1 3.9 329 329 4.3 3.9 329 4.6 5.7 4.8 5.7 8 5.5 8 5.5 8 5.5 8 5.5 8 6 7 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8

ECEMBI	ER MEAN T	EMPERA	TURE A		DE (K)	AND P		WAVE										
CALE	PRESSURE (mb)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	8
12.0	0,0062	0.20	0.21	0.31	0.14	0.43	0.03	0,22	0.23	0,52	0,39	0,28	0.84	0.07	2.52	4.88	4,39	2,
11.5	0.0103	0.22	0.23	0.34	0.18	0,44	0.05	0.25	0.25	0.52	0.40	0.28	0.75	0.18	2.93	5.24 270	4,63	2,
11.0	0,0169	0.23	0.25	0.36	0.20	0.42	0.08	0.26	0.26	0.47	0.37	0.30	0.65	0.57	3,38	5,47	4.73	2,
10.5	0.0279	0.21	0.20	0.30	0.24	0.36	0.11	0,28	0.26	0.37	0.35	0.37	0.74	1,12	3,93	5,67	4.78	2.
10.0	0.0460	0,18	0.14	0.19	0.27	0.31	0.17	0.30	0.25	0.24	0.37	0.55	1,17	1.83	4,58	5,89	4.83	2,
9,5	0,0758	0,14	0.09	0.08	0.28	0.30	0.20	0.51	0,19	0.08	0.41	0.74	1,79	2,64	5.19	6.08	4.81	2.
9,0	0.1250	0.16	0.12	0.08	0.28	0.37	0,20	0.30	0,07	0.10	0.40	0.93	2.33	3,40	5,54	6.11	4.72	2.
8.5	0,2061	0.16	0.12	0.11	0.25	0.40	0.17	0.23	0,19	0.30	0.28	1.02	2.54	3,85	5,49	6.05	4.80	2.
8.0	0.3398	0.20	0.11	0.05	0.16	0.35	0.21	0.16	0.48	0.47	0.16	0.95	2,41	3,80	5,25	6.28	5.45	2.
7,5	0.5603	0,22	0.21	0.01	0.03	0.15	0.22	0.16	0.53	0,38	0.30	0.89	2,55	4,19	5,92	6.89	5.94	2.
7.0	0.9237	0.18	0.23	0.11	0.07	0.02	0.18	0.18	0.35	0.21	0.28	0.64	2.36	4.39	6.89	8.05	6.73	3,
6.5	1,52	0.36	0.49	0.39	0.15	0.07	0.12	0.16	0.09	0.04	0.11	0.36	2.22	5.25	8,55	10.00	8,28	4
6.0	2,51	0.65	0.86	0.68	0.29	0.15	0.14	0.16	0.11	0.05	0.02	0.51	2,58	6.77		12.09	10.34	5
5,5	4.14	0.73	0.98	0.79	0.40	0.17	0.12	0.10	0.04	0.07	0,15	1.03	3.24	7.14		11.91	-	6
5.0	6.83	0.69	0.92	0.81	0.53	0.17	0.08	0.02	0.08	0.17	0,37	1.46	3,67			11,39		6
4,5	11,25	0.53	0.70	0.75	0.65	0.15	0.10 191	207 0.15 259	285 0,22 288	0,30	0,62	1.76	3.52			12.10		6
4.0	18,55	0.32	0.45	0.66	0.73	0.13	0.20	0.28	0.35	0.40	0.82	1.88	2.91	1.00		14.05	12.26	6
3,5	30,59	0.11	0.33	0.59	0.72	0.13	223	0.35	0.42	0.44	0.91	1.80	2.04	5.28		14 92 195	12.46	6
3.0	50.43	0.07	0.35	0.49	0.62	0.13	0.29	0.38	0.43	0.43	0.89	1,61	1.15	4.80	10.25	12.95	10.74	5
2.5	83.15	0.11	0.32	0.37	0.45	0.11	0.25	0.32	0.37	0.33	0.68	1.17	0.47	3,69	7,59	9,36	7,63	3
		267	300	334	4	311	229	262	290	306	325	323	38	167	194	212	227	
	PRESSURE	-80	-70	-60	-50	-40	-30	-20	-10	AVE 1	10	20	30	40	50	60	70	-
EIGHT	(mb)																	
12.0		137	162	169	167	115	147	324	219	234	2.5	300	325	50.3	53	133	29.8 148	2
11.5		133	158	168	167	1.9	148	310	247	284	239	7.8 301	324	30.2	17.0	119	140	2
11.0		130	154	166	168	138	149	244	281	308	247	7.4 302	323	30.3	62	113	135	3
10.5		127	151	165	168	145	150	179	304	318	265	7.1 305	325	30.3	26.3	37.4	133	3
10.0		124	149	164	169	151	150	165	314	321	291	6.9 310	328	30.6	73	45.9	132	3
9.5	0.0758	125	149	5,2 164	171	157	151	1.3	319	322	1.6 308	7.0 317	334	31.1	38.0 79	54.3 114	133	4
9.0	0.1250	128	150	165	174	3.4 165	152	157	319	2.7 321	316	7.3 327	20.4 343	32.0	44.5 85	62.3	67.9 135	4
8.5	0.2061	133	3.2 152	5.2 167	3.3 177	3.2 175	155	2.1 157	1.7 315	2.5 319	2.6 320	7.8 337	21.2 353	33.3	50.4 91	68.8 123	72.9 139	4
8.0	0.3398	2.9 136	5.3 153	5.3 168	3.0 180	2.9 184	2.8 160	160	1.3 304	2.1 313	2.9 323	8.5 346	22.0	34.8 45	54.9 98	73.3 129	75.9 144	5
7.5	0.5603	3.2 136	5.5 153	5.3 168	2.9	2.6 189	2.8 166	2,4 165	0.8 270	1.6	2.7 329	9.0	22.1	36.0 54	58.1 106	76.0	77.4 150	5
7.0	0.9237	3.5	5.8	5.3	182	2.5	2.7	170	0.9	1.2	2.4 336	9.3	21.7	36.6	60.4	78.2	78.4 157	5
6.5	1.52	3.6 142	6.0	5.5 172	3.0 184	2.6	2.7	2.4 176	1.1	1.0	2.1 340	9.2	20.5	35.5	61.3	79.9	78.8 165	5
	2.51	3.6	6.2	5.8 179	3.2	2.7	2.8	2.3	1.2	1.0	2.1 341	8.8	18.3	32.7	61.2	81.5	78.5 175	4
6.0		3.8	6.5	6.3	3.6	2.9	2.8	2.3	1.2	0.9	2.0	7.6	14.8	28.6	59.4 153	81.4	76.4 186	4
5.5	4.14				4.2	3.1	2.8	2.3	1.2	0.8	1.6	5.8	10.3	24.6	55.3 168	77.7	71.5	4
	6.83	4.2	7.1	7.2	200	198					246		21					
5.5		4.2 183 4.7	7.9	8.2	5.0	198 3.3	2.7	2.2	1.1	0.5	0.9	3.4	6.1	20.7	47.6	68.0	61.7	3
5.5	6.83	4.2 183 4.7 193 5.2	7.9 196 8.6	8.2 199 9.2	5.0 202 6.0	3.3 200 3.5	2.7 188 2.5	2.2 186 2.2	1.1 210 1.1	0.5 268 0.4	350	1.3	4.4	20.7 149 16.8	47.6 182 36.7	68.0 200 52.9	61.7 207 47.5	3
5.5 5.0 4.5	6.83	4.2 183 4.7 193 5.2 198 5.4	7.9 196 8.6 199 9.1	9.2 199 9.2 201	200 5.0 202 6.0 202 7.1	3.3 200 3.5 200 3.6	2.7 168 2.5 187 2.2	2.2 186 2.2 178 2.2	1.1 210 1.1 188 1.4	0.5 268 0.4 188 0.9	350 0.4 96 1.6	12 1.3 57 2.7	4.4 131 5.9	20.7 149 16.8 172 12.8	47.6 182 36.7 197 24.0	68.0 200 52.9 211 34.1	61.7 207 47.5 217 30.4	20
5.5 5.0 4.5 4.0	6.83 11.25 18.55	4.2 183 4.7 193 5.2 198	7.9 196 8.6 199	9.2 201	5.0 202 6.0 202	3.3 200 3.5 200	2.7 188 2.5 187	2.2 186 2.2 178	1.1 210 1.1 188	0.5 268 0.4 188	350 0.4 96	1.3 57	4.4 131	20.7 149 16.8 172	47.6 182 36.7 197	68.0 200 52.9 211	61.7 207 47.5 217	3

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SCALE	R MEAN PRESSURE	-80	-70	-60	-50	-40	+30	-20	-10	0	10	20	50	40	50	60	70	80	
HEIGHT	(mb)		0.00	0.04			0.00										0.06		
12.0	0.0062	104	0.02	342	309	318	306	292	292	105	115	59	53	13	1.11	1.33	38	179	
11.5	0.0103	101	338	341	0.18 315	321	304	290	294	101	116	57	0.68 52	13	1.12	1.35	63	172	
11.0	0.0169	100	345	346	321	323	0.17 298	289	298	0.36 96	118	61	0.83 52	0.58	1.07	1.26 59	70	163	
10.5	0,0279	95	341	348	333	326	286	300	305	0.29	121	62	0.74	10	0.97	1.09	77	138	
10.0	0.0460	0.39	339	352	350	333	259	101	319	0.25	128	0.09	0.52 50	0.26	0.89	0.88	0.53 80	95	
9.5	0.0758	0.31	333	0.26 358	0.21	0.08 360	217	106	0.13 351	0.21	0.18 150	0.05	0.49	0.08	103	107	0.62 85	0.33	
9.0	0.1250	0.16	330	0.26	0.22	0.07 56	177	109	0.12	0.19	212	76	0.40 57	122	127	0.72 142	90	0.49	
8.5	0.2061	169	322	0.24 16	0.22 50	90	0.12 146	110	0.10	0.13	0.13 258	0.09 56	0.40 69	119	1.01	171	100	0.63	
8,0	0.3398	202	0.07 298	0.19	0.19 70	0.18	0.12 107	0.11	0.11	124	0.09 270	0.19	U.49 82	0.65	1.03	1.09	0.23	0.71 34	
7.5	0.5603	199	0.03 261	0.12	0.11	105	0.10 80	0.14 274	0.12 213	0.16	0.02 324	0.21	0.26	0.07	0.85	213	0.43 197	0.43	
7.0	0.9237	0.35	0.02	0.07	0.04	0.06	0.07	0.18	0.16	0.14	0.03	0,16	0.42 301	0.90	1.20	230	0.92	0.12 318	
6.5	1.52	201	0.02	0.04 82	0.01	0.00	0.02	263	0.14 275	0.10 256	0.13 260	0.37	1.16	2.02 307	1.58	1.18	1.57	0.72 273	
6.0	2.51	0.21	0.05	0.07	0.05	0.03	0.03	0.03	0.10	0.13	0.22	0.65	1.80	3.04	1.94 323	1.05	2.19	1.45	
5.5	4,14	0.18	0.08	0,11	0.07	0.06	0.04	0.06	0.03	0.07	0.17	0,62	1.71	2.96	2.06 332	0.98	2,10	1.57	
5.0	6,83	0.15	0.10	0.15	0.09	0.09	0.05	0.11	0.06	0.04	0.08	0.47	1.31	2.43 325	2.07	1.20	1,63	1.34	
4,5	11.25	0.09	0.11	0.18	0.10	0.13	0.06	0.17	0.16	0.12	0.08	0.22	0,66	1,57	1.92	1,68	1,29	0.77	
4.0	18,55	0.06	0.11	0.20	0.11	0.14	0.06	0.21	0.23	0.19	0.19	0.19	0.26	0.67	1,67	2.14	1.70	0.45	
3.5	30,59	0.05	0.10	0.19	0.10	0.15	0.06	0.21	0.26	0.23	0.26	0.40	0.72	0.42	1.50	2.25	2.10	0.87	
3.0	50.43	0.05	0.08	0.16	0.08	0.13	0.06	0.21	0.26	0.23	0.29	0.53	0.99	0.75	0.88	1.90	2.00	1.05	
2,5	83,15	0.04	0.05	0.11	0.05	0.10	0.04	0.16	0.21	0.19	0.24	0.47	0.88	0.74	0.52	1.33	1.50	0.86	
																,,,		**	
SCALE	R MEAN (-80	-70	HEIGHT	-50	TUDE (dam) A	ND PHA	SE W	AVE 2	10	20	30	40	50	60	70	80	
HEIGHT	(mb)												-						
12.0	0.0062	149	230	33	12	0.4 320	211	1.2	311	76	109	3,6 333	10.9 347	23.6 337	24.3	23.1	15.3	8.8 360	
11.5	0.0103	155	227	39	32	0.1 321	187	1.6	0.8 324	2.0 69	105	3.6 328	10.4 341	22.8 336	23.0	21.3 26	15.2	9.5 360	
11.0	0.0169	163	0.4 220	0.7 49	0.6 57	143	170	120	0.4	62	0.7 89	3.6 323	10.0 334	335	21.9	19.7 23	15.0	359	
10.5	0.0279	174	210	0.6 66	0.7 82	143	160	119	70	55	0.4 359	3.6 319	9.9 327	333	21.0	18.4	14.8	10.4 358	
10.0	0.0460	2.9 186	199	91	103	0.5 145	1.1	120	0.7 96	51	0.9 326	3.6 517	9.8 322	21.0 333	20.6 359	17.6 16	14.5	10.5 357	
9.5	0.0758	3.0 196	0.7 188	0.7	0.9	0.6	1.1	122	109	0.9	1.3 323	3.7 315	9.8 317	20.9 332	20.7 355	17.3	14.3	10.5 354	
9.0	0.1250	3.1	180	1.0	1.0	0.7 156	1.0	1.5	0.9	0.6 64	1.5 327	3.7 314	9.9 313	20.9 332	21.4 352	17.7	14.2	10.2 351	
8.5	0.2061	205	1.1	1.3	1.1	0.7 168	135	1.0	129	0.5 79	1,5 334	3.7 313	10.1 310	331	22.6 350	18.7	14.2 360	9.7 348	
8.0	0.3398	2.8	1.2	163	1.2	0.u 188	0.7 136	0.7	132	0.5 82	1.4 340	3.8 310	10.5 307	22.0 330	24.1 349	20.2	14.4 358	9.1 343	
7.5	0.5603	2.4 207	1.2	1.6	1.2	0.7 209	0.6	0.8	0.6	0.5 63	1.4 342	3.8 305	10.9 305	22.4 329	25.2 351	21.7	14.8 358	8.6 338	
7.0	0.9237	1.8	1.2	1.6	1.2	0.7	160	1.0	0.7 106	0.7 48	1.4 343	3.7 302	10.7 304	22.0 330	25,4 354	23.1	15.6 360	8.4 336	
6.5	1.52	213	1.2	1.6	1.2	0.7	166	1.1	101	0.9	1.4 348	3.4 303	9.6 306	333	24.6 358	24.3	16.7	8.2 340	
6.0	2.51	1.1	1.1	1.6	1.2	0.7	166	1.2	1.1	1.0	1.4 359	2.8 310	7.5	16.7 338	23.0	25.2	18.0	7.6 350	
5.5	4.14	0.8	1.1	1.5	1.1	0.7	0.5	1.1	1.2	1.1	1.4	2.1 326	5.2 321	12.7	20.6	25.5	19.3	7.0	
5.0	6.83	0.5	1.0	1.4	1.0	0.6	0.4	1.0	1.2	1.1	1.4	1.7	3.4	9.1 355	18.1	24.9	20.0	6.9	
4.5	11,25	0.4	0.9	1.2	0.9	0.5	0.4	0.8	1.0	0.9	1.4	1.6	2.6	6.7	15.5	23.3	19.6	6.9	
4.0	18.55	0.3	0.8	1.1	0.7	0.4	0.3	0.6	0.7	0.7	1.2	1.4	2.3	5.3	13.2	20.8	17.8	6.5	
3.5	30,59	0.3	0.6	0.9	0.6	0.4	0.3	0.3	0.3	0.5	1.0	1.1	2.0	4.7	11.2	17.7	15.0	5.7	
3.0	50.43	0.3	0.6	0.9	0.5	0.6	0.3	0.2	0.1	0.4	0.8	1.1	2.4	4.9	9.7	14.8	12.0	4.7	
2.5	83.15	0.4	0.5	0.9	0.4	0.7	0.3	0.4	0.4	0.6	0.9	1.5	3.5	5.6	8.8	12.6	9.5	4.3	
		110	216	231	611	111	88	329	296	313	312	290	305	353	33	40	32	11	

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2.3.1b PLANETARY WAVES

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INTERANNUAL VARIABILITY

The zonal wave fields given in Section 2.3.1a show the climatology of the quasi-stationary planetary waves. The middle atmosphere exhibits variation on a time scale of a few days, and such short-term variations are missing from these means. Short-term variations include travelling waves which are found at all seasons (although those occurring in summer have very small amplitudes), e.g., see MADDEN (1978) or RODGERS and PRATA (1981). However, stratospheric warmings which are connected with a very strong intensification of the planetary waves one or two, have the largest effect. They affect the stratosphere and mesosphere over periods varying between a few days and several months. They are described in reviews by QUIROZ et al. (1975), SCHOEBERL (1978), LABITZKE (1981) and McINTYRE (1982).

Figure 1 shows the magnitude of temperature changes which can occur. In this case at some level (e.g. 50 km) changes exceed 70 K over 15 days from 28 December to 18 January. The sudden warming is such a large phenomenon that it strongly affects individual monthly means, giving larger planetary wave amplitudes than for months without large warmings. However, sudden warmings are part of the climatology, and their mean effect needs to be included (it would be difficult to do otherwise), but an average over a small number of years for a given month can possibly be inadequate to obtain a reliable mean. Consequently, the means given here must be treated with caution.

During the summer season, planetary wave amplitudes are small (a few K) so the year-to-year variability will cause little absolute error in the amplitude. Year-to-year variability of the monthly mean is illustrated by Figures 2 - 7, which are derived from Nimbus 6 PMR retrieved temperature fields. Figures 2 - 4 are temperature analyses on constant pressure surfaces for 1 and 0.01 mb for December and January for the three Northern Hemisphere winters measured by the PMR. Figures 5 - 7 are the corresponding wave number one amplitude and phase components.

Fortunately, three very different types of stratospheric warmings took place (cf. Section 2.3.7, Figure 7), which are also reflected in the very different maps of the 0.01-mb temperatures. The first winter, 1975/76 (Figure 2) belongs in the group with several "minor" warmings, no breakdown of the stratospheric polar vortex, and a late reversal into summer. The maps of the stratosphere show a typical wave one situation, particularly well developed in January. This wave is obvious also in the upper mesosphere with the typical westward slope with height, as discussed in Section 2.3.1a. Overall, the amplitude of wave one is, however, not very large (Figure 5) and the pattern of the temperature still rather regular. It is of interest to note that a correlation exists between the polar minima at the 1-mb level and the polar maxima at the 0.01-mb level. This confirms earlier studies based on rocketsonde data (LABITZKE, 1972).

The second winter, 1976/77 (Figure 3) belongs to the group of "major" warmings which commonly terminate with the "breakdown" of the stratospheric

polar vortex and a "late winter cooling period". This time the warming developed already in December 1976 and this is reflected in the mean map of the 0.01-mb temperatures for December. A large wave one had developed and this wave is very pronounced also at the 0.01-mb level, i.e., in the upper mesosophere where the pattern is now very asymmetric compared with December 1975 (Figure 2).

January 1977 (Figure 3) is a period of "late winter cooling". The polar vortex was broken down at that time, the planetary waves were weak in the troposphere and stratosphere, no wave energy was therefore transported upwards and the radiational cooling resulted in a very cold polar stratosphere. At the same time we observe a very warm polar mesosphere with a rather symmetric temperature pattern, undisturbed by planetary waves.

The third winter, 1977/78 (Figure 4), belongs again in the group with "minor" warmings without a "breakdown", but the minor warming is very intense in January 1978. Accordingly, we find a rather undisturbed, regular December and a highly disturbed January, both in the stratosphere and in the upper mesosphere.

Thus the amplitude structure of the three winters is seen to be very different (Figures 5 - 7), and there is as much difference among the different sections for January and for December as between January and December. It is interesting that the phase fields are quite similar; if they were not, the three-year mean amplitude would be much reduced. Hence reference to Figures 3.1 and 3.12 in Section 2.3.1a shows that the three-year mean amplitude approximately equals the arithmetic mean of the amplitudes for the three years.

As pointed out before, "minor" warmings take place during the southern winters but they are not so intense as to be reflected in a monthly mean at upper mesospheric levels.

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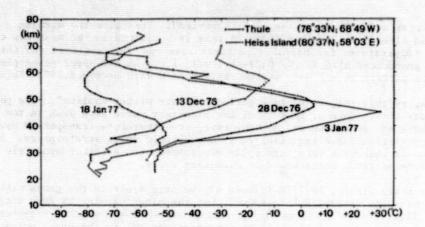


Figure 1. Rocketsonde measurements during the winter 1976/77.

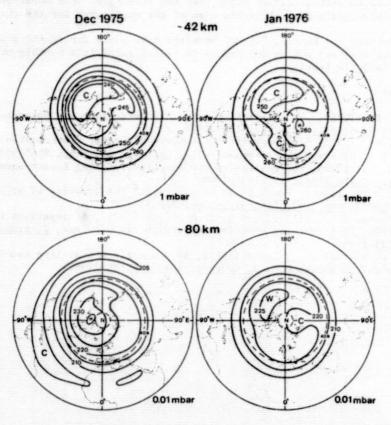


Figure 2. Monthly mean 1- and 0.01-mb temperature maps for December 1975 and January 1976.

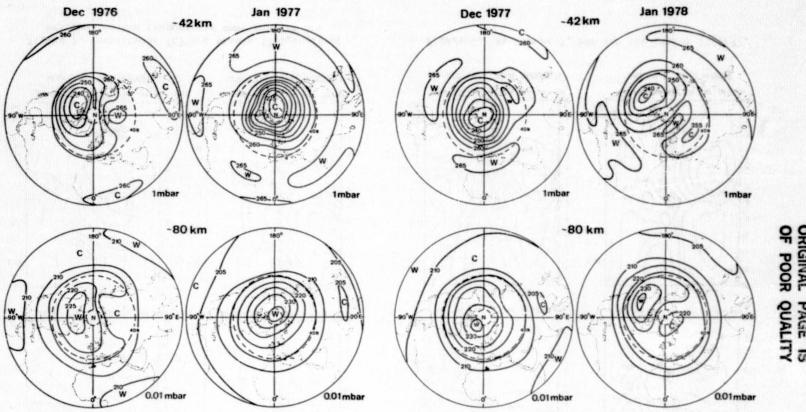


Figure 3. As Figure 2, but for the winter 1976/77.

Figure 4. As Figure 2, but for the winter 1977/78.

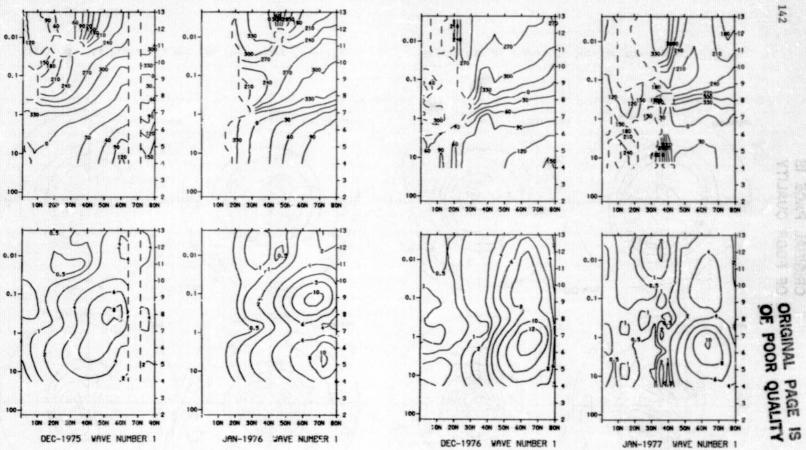


Figure 5. Amplitudes (K) and phases (longitude of maximum) of the temperature wave one for the winter 1975/76.

Figure 6. As Figure 5, but for the winter 1976/77.

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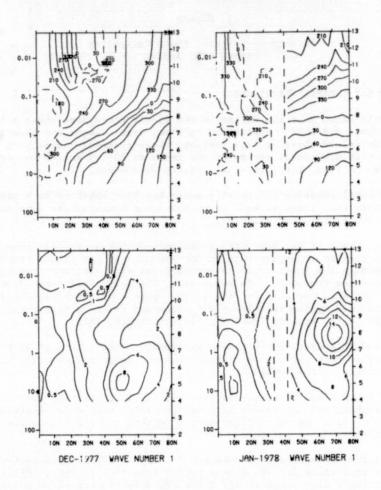


Figure 7. As Figure 5, but for the winter 1977/78.

2.3.2a GRAVITY WAVES

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SEASONAL AND LATITUDINAL VARIATIONS

It is well known that the motion in the middle atmosphere shows a broad spectrum in space and time. Superposed on zonal mean motions and planetary-scale waves described above in this section, there certainly exist wind fluctuations with horizontal scales of the order of 10-100 km and periods of the order of hours or less, i.e., internal gravity wave modes.

Observational evidence for gravity waves has been obtained by a wide variety of radar techniques as well as rocket-borne measurements (see the review of FRITTS et al. (1984), for example).

In recent years it has been widely recognized that vertically propagating gravity waves play an important role in the dynamics of the middle atmosphere in partly determining the large-scale temperature and wind structure through their energy and momentum transport. In particular, the meridional temperature distribution and the mean wind profile in the upper mesosphere are considered to be largely affected by the turbulence diffusion and friction that gravity waves induce through their breaking (HOUGHTON, 1978; LINDZEN, 1981).

For an understanding of the middle atmosphere circulation, it is therefore very important to know the global distribution and temporal variation of gravity waves in a climatological sense.

In this subsection the result of the statistics for gravity wave activity in the stratosphere and mesosphere is presented as a function of latitude and month, with the aid of meteorological rocket network observations. For detail see HIROTA (1984).

High altitude meteorological data supplied by the World Data Center A are used in these statistics for the 4-year period from 1977 to 1980. Thirteen stations covering a wide range of latitudes are selected for which a large number of rocket data are available. The average number of observation days at each station is about 360 for the four years.

Rocket observations of zonal wind component U, meridional wind component V and temperature T are used at an interval of 1 km. The height range is between 20 and 65 km in most cases.

First, in order to remove the contribution of large-scale components such as the mean field, planetary waves and tides, a high-pass filter is applied to the daily data with respect to height. By this filtering, the fluctuations with characteristic vertical scales less than about 10 km are separated.

Figure 1 shows an example of the wind and temperature fluctuations at Thule (77°N). In the filtered data, wave-like disturbances with a vertical scale close to or less than 10 km are seen. They are considered to be due to internal gravity waves.

Then, as a measure of the gravity wave intensity, an estimate is made of the root-mean-square (rms) of the second-order derivatives with respect to height for each component (U,V,T) and for each observation day.

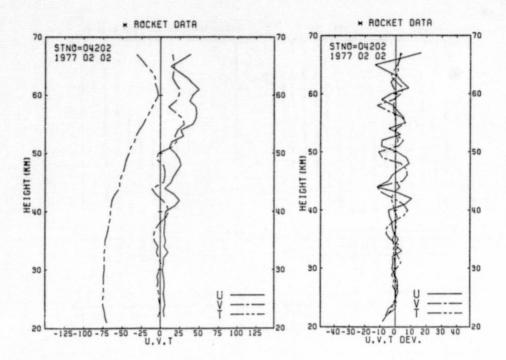


Figure 1. An example of the vertical distribution of wind and temperature at Thule (77°N) for February 2, 1977. (left) raw data, (right) filtered data. Units are m/s for wind and K for temperature.

It is found that the daily values of the intensity of zonal and meridional wind components are considerably variable and random with each other, but the rms values of the two components are almost equal in magnitude in a statistical sense. This is an indication of the isotropy of gravity waves in their orientation. Hence, in the following statistics, the two components are averaged to give a measure of the intensity of wind fluctuations.

The gravity wave intensity thus defined is again averaged for each month (of the four years) to obtain climatological mean values at each station, together with the estimate of the standard deviation around the monthly mean.

Figure 2 shows the seasonal variation of the gravity wave intensity, i.e., rms amplitudes of wind and temperature, for four typical stations. The standard deviation around the monthly mean is denoted by vertical bars.

In high latitudes (Thule, 77°N and Primrose Lake, 55°N), it can be seen that both the wind and temperature rms value show a notable annual cycle with the maximum in winter. Roughly speaking, the maximum value in winter is twice as large as the minimum in summer for wind, while the annual variation in percent for temperature seems to be larger than that for wind.

On the other hand, in lower latitudes (White Sands, 32°N and Ascension Island, 8°S), such a notable annual variation cannot be seen. Results of harmonic analysis indicate that the semiannual component is rather larger than the annual component, especially in the temperature variation. The maximum value of the semiannual cycle appears near the equinox. This fact is probably

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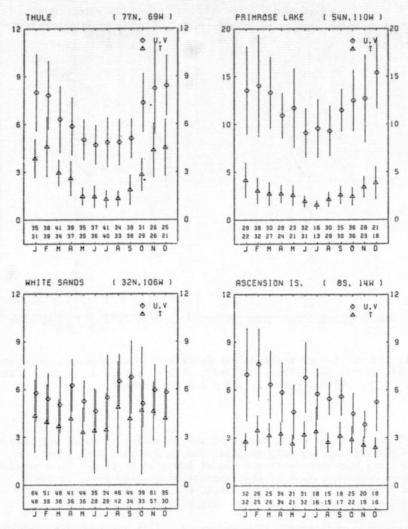


Figure 2. Seasonal variation of rms values of gravity wave intensity at four stations. Vertical bars denote the standard deviation. Units are m sec 1 km 2 for wind and K km 2 for temperature. Figures above the abscissa are total number of rocket observations used in these statistics for wind (above) and temperature (below).

related to the seasonal variation of the mean zonal wind in the middle atmosphere presented in a previous subsection.

The seasonal and latitudinal dependency of the gravity wave intensity is summarized in Figure 3. The values at two stations adjacent in latitude are not always close to each other, so that in this figure the latitudinal variation is smoothed to some extent. Moreover, there are no data in a latitude zone between 38°N and 54°N. Nevertheless, the contrast in the seasonal change is clearly seen between high and low latitudes.

Another interesting aspect of gravity wave activity is transiency. In the middle atmosphere, gravity waves are likely to be as variable as their generation

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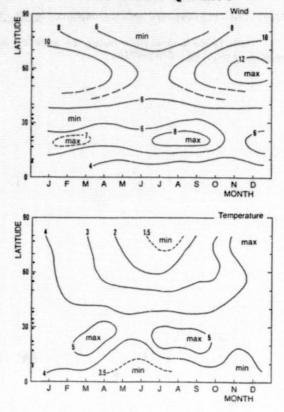


Figure 3. Latitude-time section of rms values for wind (above) and temperature (below) in the same units as those of Figure 2. Circles on the ordinate denote the rocket stations.

processes in the lower atmosphere which have a wide range of time scales from hours to days.

Such transient variability can indeed be observed in Figure 2. With regard to the wind fluctuation, the standard deviation is about one third as large as the monthly mean value throughout a year. Since the launch frequency for the present rocket network is approximately once per four days on the average, the typical time scale of the gravity wave transiency cannot be inferred.

In conclusion, the climatology of gravity waves in the middle atmosphere as shown in Figures 2 and 3 should be regarded as an ensemble mean of time-dependent, stochastic processes, in contrast to the quasi-steady state of large-scale motions such as mean zonal wind and planetary waves.

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2.3.2b GRAVITY WAVES

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SPECTRAL DESCRIPTION OF MESOSCALE FLUCTUATIONS

Atmospheric parameters fluctuate on all scales. In the mesoscale these fluctuations are occasionally sinusoidal so that they can be interpreted as gravity waves. Usually, however, the fluctuations are noise-like, so that their cause is not immediately evident. VANZANDT (1982) and others have suggested that they are due to a random field of gravity waves. GAGE (1979) suggested that they are the result of two-dimensional turbulence. See LILLY (1983) for a review of the situation.

For the purposes of this section, the term mesoscale is defined as including motions with vertical scales ranging from roughly 5 km down to less than 40 m, horizontal scales from a few hundred kilometers down to about a kilometer, and time scales from roughly a day down to the buoyancy (Brunt-Vaisala) frequency of 5 - 10 minutes.

Results of mesoscale observations in the 20 to 120 km altitude range that are suitable for incorporation into a model atmosphere are very limited. In the stratosphere and lower mesosphere observations are sparse and very little data has been summarized into appropriate form. There is much more data in the upper mesosphere and lower thermosphere, but again very little of it has been summarized.

A convenient and commonly used statistical description of these fluctuations is in terms of power spectra. This description is made simpler and more useful because it turns out that both the shape and amplitude of the spectra appear to be remarkably insensitive to variations of related geophysical variables, such as background wind, atmospheric stability, altitude, latitude, underlying topography, etc.

Spectral amplitudes will be denoted by F. The dependent variables to be considered are the horizontal and vertical velocity, u and w, and the independent variables are the horizontal wave number k, the vertical wave number m, and the frequency ω . In the graphs the independent variable is log k, log m, or log ω , as is usual. The amplitude of the spectra is plotted as log (kF(k)), log (mF(m)) or log F(ω).

mF_u(m)

The available mesoscale spectra of horizontal wind u versus vertical wave number m in the 20 to 120 km altitude range are shown in Figure 1, together with a spectrum from the lower atmosphere for comparison. Further information about these spectra is given in Table 1. In spite of the large range of altitudes and latitudes, the spectra from the lower atmosphere (NASA, 1971 and DEWAN, 1984) are remarkably similar in both shape and amplitude. The mean slopes of -2.38 for the NASA spectrum and -2.7 for the Dewan spectra are supported by the mean slope of -2.75 found by POSENBERG et al. (1974).

The mesospheric spectrum (VINCENT, $66-96~\mathrm{km}$) is too short to establish a shape. Its amplitude is about an order of magnitude larger than the NASA

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spectrum in the same wave number range.

The NASA and Dewan spectra suggest that the mesoscale spectra in the lower atmosphere are insensitive to meteorological conditions. Meteorological data of the Dewan spectra were not given, but presumably the conditions for the five spectra were diverse. The NASA spectra were taken throughout the year under a wide variety of weather conditions at Cape Kennedy, yet the standard deviation of the 1200 independent spectra about the mean spectrum is only about a factor of two. Moreover, ENDLICH et al. (1969) show mean spectra (from the same data set as the NASA spectrum) on three days with peak winds of 18, 41, and 62 m/s, that is, with energy densities per unit mass in synoptic scales ranging over about a factor of 10. Yet the spectral shapes for scales smaller than 5 km were essentially identical and the spectral densities ranged over a factor of only 2 - 3, with the 18 m/s day always the smallest but with the 41 m/s day the largest in the 1 to 5 km range.

HIROTA (1983) also studied the climatology of mesoscale fluctuations between 20 and 65 km using vertical profiles of horizontal wind data from the Meteorological Rocket Network. In order to characterize the amplitude of the fluctuations, he used the rms value of the second derivative of the wind versus altitude, which emphasizes the smaller scale fluctuations. The range of amplitudes of this quantity was found to be about a factor of three, from a minimum at low latitudes to a maximum at about 60 deg latitude in winter. This result is not inconsistent with the weak dependence of the amplitude of spectra found in the present study.

kF_u(k)

Because of obvious experimental difficulties, no spectra of F_(k) are available in the altitude range from 20 to 120 km. There are many studies of F_(k) at lower altitudes, however, which, because of the apparent insensitivity of the spectra to altitude, should be relevant to the 20 to 120 km range. The definitive study of NASTROM and GAGE (1985) used very extensive, homogeneous, aircraft data between 9 and 14 km. A straight line approximation to the sum of their zonal and meridional spectra, that is, to the spectrum of the vector wind, is shown in Figure 1 as "NG, 9-14 km". Further information is given in Table 1. They found that the mean zonal and meridional spectra were the same, that the amplitude of the mean spectra depended only weakly on atmospheric stability (the stratospheric amplitude was 1.2 to 1.5 times larger than the tropospheric amplitude) and season (with summer being smallest), and that there was an apparent latitude variation of a factor of 2 to 4 between the 15°S to 15°N zone and the 45°N to 60°N zone. The standard deviation of 2718 independent spectra was about a factor of 2.5.

It may be noted that the same spectral energy density is found in the kF (k) and mF (m) spectra but at values of k from 10 to 100 times smaller than the corresponding values of m (that is, at horizontal scales from 100 to 10 times larger than the vertical scales). This is a result of the horizontal elongation of the mesoscale motions relative to the vertical because of the suppression of vertical motions by buoyancy forces. Such stratification is also evident in the stratosphere and lower mesosphere in horizontally separated simultaneous wind profiles (LESTER and TOLEFSON, 1964; MAHONEY and BOER, 1968; MARSHALL, 1969) and sequential profiles (WEINSTEIN et al., 1966; ENDLICH et al., 1969; JOHNSON and VAUGHAN, 1978).

Table 1 Information on the Spectra

Fig.	Spectrum	Designation	Reference	Altitude (km) Range Mean		Latitude	Method	Comments
1.	mF _u (m)	NASA	NASA	4-16	10	28.5°N	Jimsphere balloon	scalar wind
		Dewan A	(1984a,b)	29-42	36	38°N	smoke trail	scalar wind
		В		22-34	28	38°N		
		C		18-28	26	33°N		
		D E		20-31	28	33°N		
		E		16-32	27	59°N		
		Vincent	(1984)	66-96	81	35°S	radar	vector wind
1.	kF _u (k)	NG	Nastrom & Gage (1984)	9-14	11.5	50°N ⁽¹⁾	aircraft	vector wind
2.	F _u (ω)	ВС	Balsley & Carter (1983)	7.0-9.2	8.1	65°N	radar	zonal wind
		Vincent	(1984)	85-87	86	65°N (35°S)	radar	zonal wind
			82.	75-87.25	85	35°S (19°S (radar av. zo	onal + merid.
3.	F (a)	Ecklund et al.	(1983)	3.9-6.1	5.0	43.5°N	radar	
٠.	$F_{w}(\omega)$	Eckiuna et al.		10.6-12.9		43.3 N	radar	
		Röttger	(1981) 21.	75-23.25	22.5	52°N	radar (plotte	ed on a
	$\omega F_{W}(\omega)$	Tolstoy & Montes	(1971)		130 175 240	41°N	radio relati	ive scale

⁽¹⁾ Mean latitude. The range was 22°N to 61°N.

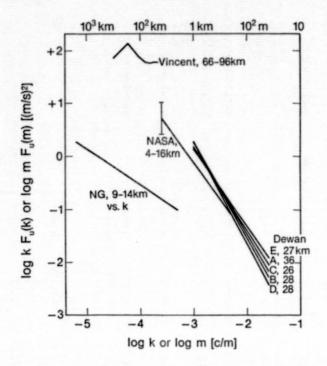


Figure 1. Spectra of log kF (k) or mF (m) versus log k or log m, where u is the horizontal wind and k and m are the horizontal and vertical wave numbers, respectively. For further information see Table 1.

The available mesoscale spectra of horizontal wind u versus frequency in the 20 to 120 km altitude range are shown in Figure 2, together with a typical tropospheric spectrum. Further information on these spectra are given in Table 1. Again, in spite of the wide range of latitudes and season, the spectra from Townsville, Adelaide and Poker Flat are essentially identical in both shape and amplitude. Vincent finds that all of the published mesospheric spectra have powers between -1.5 and -2. Tropospheric spectra also have slopes in the same range, as is shown in Figure 2. Indeed, LARSEN et al. (1982) find an average slope of 1.60_4^{\pm} .27 over the frequency range from $4.2 \times 10^{-6} (c/s)(66 2/3 \text{ hr})$ to $1.25 \times 10^{-4} (c/s)(2 2/9 \text{ hr})$.

$\mathbf{F}_{\mathbf{w}}(\omega)$

Spectra of vertical wind w versus frequency ω present a problem different from the other spectra considered. When the wind is small, the F (ω) spectra have similar shapes throughout the atmosphere from near the ground up to at least 250 km. When the wind is strong, however, the shape changes and becomes much more variable and the amplitude increases. The reasons for these changes are not fully understood, but they may be due to the vertical component of lee waves and to tilted isentropic surfaces that project properly horizontal motions onto the vertical. In Figure 3 are shown the available F (ω) spectra under light wind conditions. Geophysical parameters for these spectra are given in Table 1. Note that some of the spectra are plotted on relative scales and that the TOLSTOY and MONTES (1971) spectra are multiplied by ω .

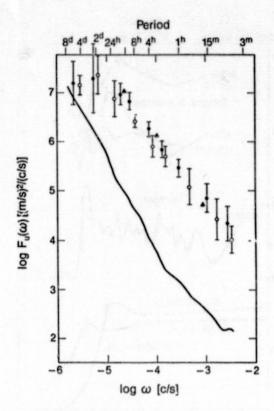


Figure 2. Spectra of log F₁(ω) versus log ω, where u is the horizontal velocity and ω is the frequency. The curve is from 8.1 km; the points, from about 85 km. The triangles are from 65°N (BALSLEY and CARTER, 1982); the filled circles, from 35°S (VINCENT, 1984); and the open circles from 10°S (VINCENT, 1984). For further information see Table 1.

The similarity of shape is apparent. In every case the peak in the spectrum is near the local buoyancy frequency. It has been shown that the very similar peaks observed in oceanic vertical current spectra are due to the behavior of gravity waves near their turning point (DESAUBIES, 1975). There can be little doubt that the atmospheric peak has the same explanation. Therefore the high frequency part, at least, of the $F_{W}(\omega)$ spectra under light wind conditions must be due to gravity waves.

VARIATION OF SPECTRAL AMPLITUDE WITH ALTITUDE

Since the spectra shown in Figures 1 -3 tend to have constant shapes in the mesoscale range, the variation of spectral amplitude with altitude can be simply characterized by the ratio of amplitudes at a typical wave number or frequency. The results are shown in Figure 4, where the logarithm of the ratio of amplitudes is plotted versus the logarithm of the ratio of atmospheric densities from the USSA 1976 model atmosphere. The corresponding nearly linear altitude scale is indicated on the right-hand ordinate. For the m spectra the amplitudes are referred to the NASA spectrum, which is taken to be at 10 km. For the ω spectra the amplitudes are referred to the BALSLEY and CARTER (1982) 8.1 km spectrum. This ratio is plotted as though the 8.1 km spectrum were actually at

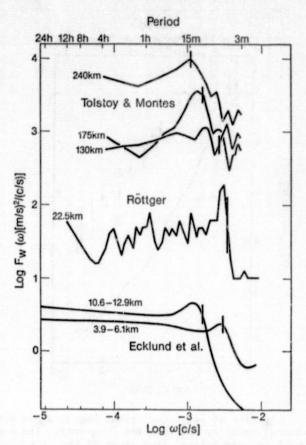


Figure 3. Spectra of log $F_{\omega}(\omega)$ versus log ω , where ω is the vertical velocity and ω is the frequency. Note that the Rottger and the Tolstoy and Montes curves are plotted on a relative scale and that the Tolstoy and Montes curves are multiplied by ω . For further information see Table 1.

10 km, which makes a negligible error. The bars through the points extend a factor of two on either side, in order to indicate in a very rough way the uncertainty of the points. The m points also extend over a considerable vertical distance, but this does not affect the conclusions.

The m ratios show very little variation with altitude. Indeed, a constant amplitude would not be inconsistent with the m ratios when all of the uncertainties are taken into account. The ω ratio indicates a larger variation with altitude, approximately as $(\rho(z))^{-0.4}$. The solid line with unit slope $((\rho(z))^{-1})$ to 60 km and the constant line above 60 km indicate the standard scenario for the growth of gravity waves in the atmosphere (FRITTS et al., 1984), corresponding to constant energy density per unit volume up to, say, 60 km and saturation with constant energy density per unit mass above. It is clear that the spectral data are inconsistent with this picture. If the observed fluctations are indeed entirely due to gravity waves then the data indicate that there is considerable loss of wave energy at all heights above 10 km.

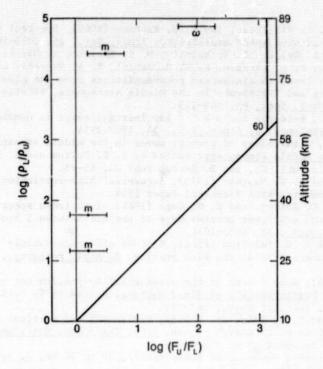


Figure 4. The ratio of spectral amplitudes in the mesoscale as a function of altitude. A 45° line corresponds to constant energy per unit volume, J/m^3 ; a constant line corresponds to constant energy per unit mass, $J/kg - (m/s)^2$, implying saturation of spectral amplitudes.

CONCLUSION

Study of mesoscale fluctuations in the atmosphere is currently a very active field. Thus, the picture described here will be significantly augmented and perhaps changed in the next few years. In the meantime, if a spectrum is needed in a region where it has not been observed, the best alternative would be to use the observed spectral shape scaled with altitude according to Figure 4.

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DIO

2.3.3 ATMOSPHERIC TIDES BELOW 80 KM

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ABSTRACT

Measurements of diurnal and semidiurnal tidal oscillations between about 25 and 80 km are reviewed. At latitudes greater than about 30 deg, S-N wind components are consistently in quadrature with and similar to the W-E components. The tidal structures are interpreted as a superposition of quasisteady higher-order modes excited in the troposphere by sources of limited extent $(^{\sim}10^3~\rm{km})$. At latitudes less than about 30 deg, steady or quasisteady diurnal and semidiurnal components are not necessarily the dominant components of daily variation. At high latitudes diurnal phases generally show little change with height in comparison with observations at lower latitudes in accord with the latitudinal properties of positive and negative diurnal modes.

DATA SOURCES

Above 80 km the main body of tidal data comes from meteor partial reflection drift, MST, and incoherent scatter radar measurements. Most of the mesosphere, however, is inaccessible to these techniques, at least for the purposes of extracting tidal information (data series covering a significant fraction (> 70%) of the day). Below 35 km ST radars are beginning to provide tidal information, but here the tidal amplitudes are relatively small and are sought after more for theoretical than practical reasons. In the intervening altitude region the primary source of tidal data is from a number of rocket launch series which have been performed between 1965 and 1974 (see Table 1). Of particular interest are 70 rockets equipped with standard Datasonde instrumentation which were launched on 19-20 March 1974 at eight Western Hemisphere sites by the NASA Wallops Flight Center in cooperation with other agencies, to study atmospheric tides and their latitudinal variations (SCHMIDLIN et al., 1957). All of these data are analyzed by GROVES (1980), and a representative sampling plus the major conclusions to emerge from that study are presented here.

SUMMARY OF TIDAL CHARACTERISTICS

Middle Latitudes

The diurnal wind oscillations derived for 23-25 October 1968 and 13-15 December 1967 at Cape Kennedy are shown in Figure 1 in comparison with theoretical phase profiles for the migrating Hough modes (1,1,1) to (1,1,5); observed phases are seen to correspond most nearly with modes of higher order than the leading (1,1,1) mode. Amplitudes lie in the range 5 - 15 m/s between 25 and 60 km. The slope of the phases with respect to height points to a tropospheric source for the oscillation. A notable property of the Cape Kennedy results of 23-25 October 1968 is that the profiles of S-N and W-E

Table 1. Diurnal launch series 1965-74.

-1282	N86			Number of successful
Site	Latitude	Longitude W	Date	launchings
Thule	76° 33' N	68° 49'	24-26 Oct 1968	14
Fort Churchill	58° 44'	93° 49'	6-8 Sept. 1966	10
			8-9 Sept. 1966	10
			4-5 Jan. 1968	12
			23-25 Oct. 1968	18
			19-20 Mar. 1974	8
Wallops Island	37° 50'	75° 29'	19-20 Mar. 1974	13
Arenosillo	37° 06'	06° 44'	24-28 Feb. 1970	27
White Sands	32° 23'	106° 29'	30 June-2 July 1965	17
			9-11 Oct. 1965	16
Cape Kennedy	28° 27'	80° 32'	13-15 Dec. 1967	25
			23-25 Oct. 1968	17
Antigua	17° 09'	61° 47'	19-20 Mar. 1974	8
Fort Shrman	09° 20'	79° 59'	19-20 Mar. 1974	8
Kourou	05° 08'	52° 37'	19-22 Sept. 1971	13
			19-20 Mar. 1974	10
Natal	05° 55' S	35° 10'	1966-68	24
			19-20 Mar. 1974	8
Ascension Island	07° 59'	14° 25'	11-12 Apr. 1966	13
			12-13 Apr. 1966	13
			24-26 Oct. 1968	14
			19-20 Mar. 1974	8
Mar Chiquita	37° 45'	57° 25'	19-20 Mar. 1974	7

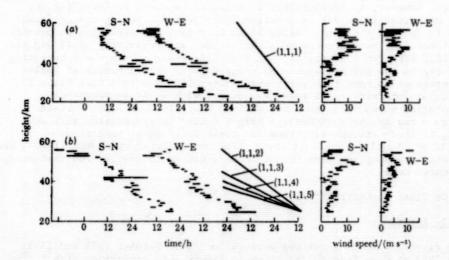


Figure 1. Diurnal wind components at Cape Kennedy. The straight lines indicate the approximate theoretical slopes of the phase profiles of the first five positive migrating modes. (a) 23-25 October 1968, 17 launchings in 48 hours. (b) 13-15 December 1967, 25 launchings in 48 hours (GROVES, 1980).

amplitudes show no significant differences and that W-E phases at all heights are later than S-N phases by close to 6 h. In other words, the diurnal wind vector at any given height rotates clockwise with no change of magnitude within the accuracy of the data. If the oscillation may be regarded as a superposition of positive (n>0) Hough modes (1,s,n), then the above property implies approximate equality of W-E and S-N Hough wird functions for each mode that is significantly present. By examination of numerical evaluations of Hough wind functions for various s and n (not shown here) it is found that this apparently stringent condition holds (to within about 20%) at latitudes between 20 and 40 deg latitude, provided that eastward travelling modes are small compared with westward travelling modes. For the 13-15 December data, however, a clockwise rotating wind vector of constant magnitude is found at less than half the heights analysed. This was traced to an unsteadiness in the W-E diurnal component from one day to the next, the cause of which is unknown. Additional data from launchings at the other midlatitude stations of the White Sands, Wallops Island, Mar Chiquita, and Arensillo, are, however, consistent with the diurnal rotation of a wind vector of approximately constant magnitude at any given height.

The measured semidiurnal wind components at latitudes greater than about 30 deg latitude (Figure 2) indicate amplitudes of 3-12 m/s between 25 and 60 km, and phase variations with height indicative of the presence of higher order modes (i.e., vertical wavelengths of 15 km or less, corresponding to modes with n as large as 10). The semidiurnal winds also indicate a similarity between S-N and W-E profiles at middle and high latitudes, and the clockwise rotation of the wind vector at northern latitudes and anticlockwise rotation at southern latitudes are in accord with the expected properties of Hough wind functions. The above properties hold for nonmigrating modes (2,s,n) s≠2 as well as migrating modes (2,2,n).

Low Latitudes

S-N and W-E Hough wind functions for positive diurnal and semidiurnal modes (not shown here) are found by inspection to become increasingly different in form at latitudes less than about 15 deg, and hence at low latitude sites S-N and W-E amplitude and phase profiles would be expected to differ appreciably. Observational results deduced from the data sources listed in Table 1 confirm this expectation (SCHMIDLIN et al., 1957). In addition, the low-latitude diurnal and semidiurnal components are not characterized by the quasi-steadiness observed at midlatitudes; rather, day-to-day differences occur which appear to arise from a nontidal source, i.e., one that does not correlate with the hour angle of the sun over several days. This confirms earlier conclusions (BEYERS, et al., 1966) for the diurnal tide based on a smaller data set. Diurnal wind components at Fort Sherman (9°N, 80°W), Kourou (5°N, 52°W), and Natal (6°S, 35°W) as shown in Figure 3 exhibit dissimilar phase and amplitude profiles even on the same day; such differences are perhaps explicable in terms of asymmetric and/or nonmigrating tidal components.

Lower stratospheric (12-35 km) tidal winds measured by the Jicamarca (12°S) radar are reported by FUKAO et al., 1978, 1981). On 23-24 May 1974 a large diurnal component in the zonal wind (1-5 m/s) was observed with downward phase progression and vertical wavelength of order 10 km. These values compare with theoretical estimates (LINDZEN, 1967) for the migrating diurnal tides of order .2 - .5 m/s and vertical wavelength near 28 km. The observations are interpreted as being connected with topographically induced nonmigrating diurnal tides similarly revealed in radiosonde data (WALLACE and TADD, 1974). The 23-24 May 1974 data show a predominance of the semidiurnal oscillation below the tropopause. By way of contrast, Jicamarca horizontal wind data for 3 - 4 October and 6 - 8 December 1977 exhibit characteristics strikingly similar to those expected of the migrating diurnal tide (LINDZEN, 1967). The observed

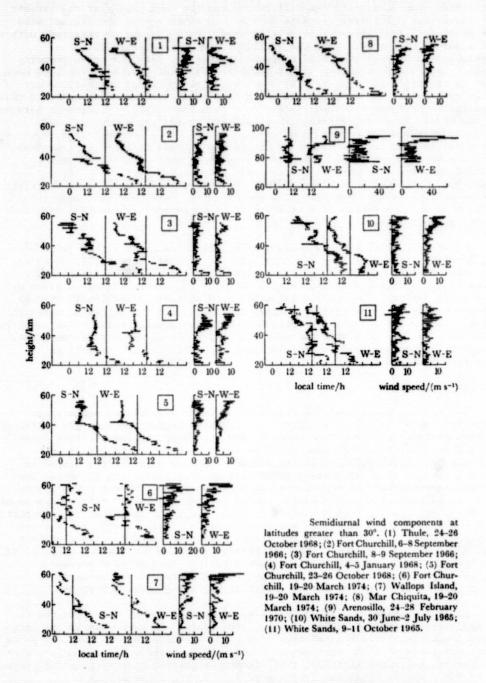
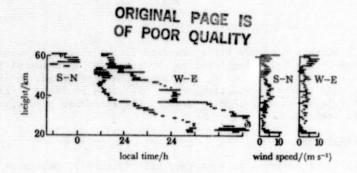


Figure 2. Semidiurnal wind components derived from rocket launchings at latitudes greater than 30 deg (GROVES, 1980).



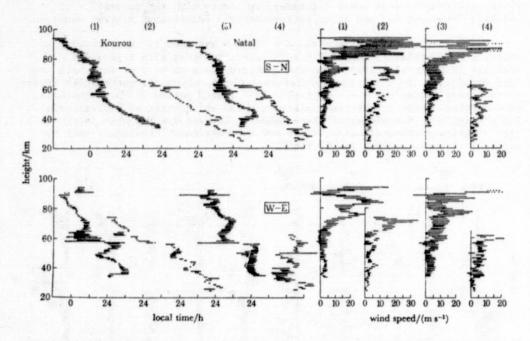


Figure 3. Diurnal wind components at (top) Fort Sherman, 19-27 March 1974, and at (middle and bottom) Kourou and Natal: (1) Kourou, 19-22 September 1971; (2) Kourou, 19-20 March 1974; (3) Natal, 1966-1968; Natal, 19-20 March 1974 (GROVES, 1980).

semidiurnal amplitudes (.5 - 1.0 m/s) are several times larger than estimated theoretically by LINDZEN and HONG (1974), and do not exhibit the characteristic mode near 30 km. The observed tendency of the semidiurnal phase to remain approximately constant with height over this altitude regime is consistent with behavior expected theoretically for the semidiurnal migrating tide.

KATO et al. (1982) investigated the generation and propagation characteristics of diurnal nonmigrating tides due to geographically localized sources of excitation. Their simulations reveal short vertical wavelength (~10 km) oscillations similar to the observations or stratospheric tides observed at Jicamarca and cited above. The perturbations are almost stationary and tend to increase in horizontal scale with altitude. The result of KATO et al. (1982) are semiquantitative in that the heat sources are poorly known, and somewhat arbitrary distributions have been adopted for the simulations. However, they

do provide information on the basic characteristics of nonmigrating diurnal tides excited by the following localized sources: (1) land-sea differences in water vapor insolation absorption, (2) topographic variations in surface heat flux due to eddy thermal conduction in the planetary boundary layer, and (3) latent heat release as suggested by diurnal variations in precipitation thunderstorm frequency.

High Latitudes

Diurnal winds observed at Fort Churchill (Figure 4) peak near 50 - 60 km at about 10 m/s and exhibit little phase change with height, characteristically different from those at lower latitudes, in accord with the properties of positive (propagating) and negative (evanescent) sequence of diurnal modes.

The S-N and W-E phases are close to 1200 h and 1800 h, respectively, as expected theoretically. The S-N results are consistent with a previous analysis (REFD et al., 1969) from the combined stations of Fort Churchill and Fort Greely. On the other hand semidiurnal winds, which are observed to remain quite steady during the 6 - 9 September 1966 launch period at Fort Churchill, show vertical phase structures similar to those which exist at midlatitudes. The consistency in semidiurnal phase behavior between low and high latitudes is also anticipated theoretically, since for the semidiurnal component only one sequence of (propagating) modes exists.

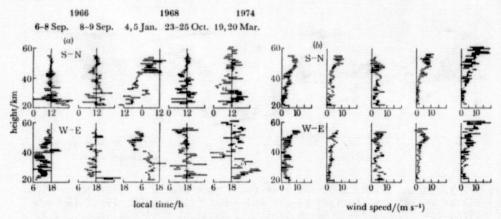


Figure 4. Diurnal wind components derived from rocket launchings at Fort Churchill (a) phases, (b) amplitudes (GROVES, 1980).

CONCLUS IONS

Atmospheric tides in the stratosphere and lower mesosphere are characterized by smaller amplitudes (5-15 m/s) shorter vertical scales (10 - 20 km), greater unsteadiness, and greater spatial variability than exhibited in the upper mesosphere and above. These properties reflect the influences of variable tropospheric excitations which occur over more local (10 3 km) than global scales. The associated short vertical scale oscillations are significantly damped by turbulent dissipation before they reach the mesopause region (ca. 85 km).

ACKNOWLEDGEMENTS

J. M. Forbes received support for this work under Grant ATM-8113078 from the National Science Foundation. G. V. Groves gratefully acknowledges the

award of a National Research Council Research Associateship at the Atmospheric Sciences Division, Air Force Geophysics Laboratory, Hanscom AFB, MA.

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2.3.4 COMPARISON OF TIME-PERIODIC VARIATIONS IN TEMPERATURE AND WIND FROM NETEOROLOGICAL ROCKETS AND SATELLITES

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(shortened for this publication by K. Labitzke, Editor)

ABSTRACT

Although the Meteorological Rocket Network operated by or in cooperation with the United States has decreased from fourteen to nine stations in the past five years, there have been many observations accumulated in the ten years since CIRA 1972 was prepared with data up to 1969. The mean, annual and semi-annual variations of temperature and wind are presented and special attention is directed to the polar semiannual wave. The results are compared with the Oxford SCR-PMR five-year data set, the CDC-SCR seven-year data, and CIRA 1972 with respect to both temperature and zonal winds, as far as presently available. The agreement among the data sets is very good.

INTRODUCTION

The purpose of this paper is to review the available variability statistics for temperature and wind in the region from 20 to 70 km to help in the selection of the best information available for a revised CIRA. There are many different data sources but they will be limited here to those with at least five years of record. They will be intercompared with respect to their means, and periodic time variations. The satellite data were not operational, realtime data, but were processed years after the observations were made, taking account of all corrections that became known in the interim. These three sets are:

Variables	Source	Abbr.	Instrument & Period of Record
т, н, w	Oxf or d	OXF	2 years of SCR (1973-1974) plus 3 years PMR (1975-1977)
T	CDC	SCR	7 years of SCR (April 1970- April 1977)
T, W	WDC-A	MRN	Meteorological rockets (MRN) (1960-1982)
	(T = temperatur	e, H = geopo	otential altitude, W = wind)

These data sets have only recently been compiled and an evaluation of their differences has begun. The preliminary results will be reviewed here.

CIRA 1972 contained no satellite data for the range 25 to 60 km. Tables and graphs were based entirely on meteorological rocket data. In revising CIRA it was agreed that both satellite and rocket data would be examined and compared before deciding which data or combination of data would suit the purpose most reliably at this time.

Each instrument has its advantages and disadvantages. Satellite data, taken by a single instrument during the life of a given satellite, are consis-

tent with each other and observations are on a global scale. Satellite radiometers, however, generally need to be recalibrated during their lifetimes because of degradation problems. Downward sensing radiometers have relatively coarse vertical resolution of 10-20 km. Scanning radiometers provide excellent horizontal coverage but the SCR and PMR instruments, for which data sets are now available, provided orbital plane data only, consisting of 13 and a fraction orbits a day separated by about 26° of longitude. The orbits shift continually from day to day returning to the same observation orbits at approximately two-week intervals. Data for fixed grids can be obtained by interpolation between orbits on a daily basis. It is not possible to obtain tidal variations from a single orbiting satellite.

For climatological purposes, variations are primarily required as a function of altitude, latitude, and time, although longitudinal variations may also be important. Meteorological satellite temperature observations have only been available since about 1970. The reduction of the radiance data to provide temperatures is generally done by one or two methods. The first is the inversion of the radiative transfer equation which requires estimates of the instrument's weighting function for each frequency observed, and a good first guess of the temperature profile in advance. It should be stressed that the inversion technique does not provide a unique solution, and that the first guess strongly influences the final result. First guesses are commonly based on climatology derived from meteorological rocket and radiosonde data. The second technique is a statistical approach which simply regresses observed radiances in several channels against coincidental rocket observations as close as possible in space and time to the radiance observations. These statistics generally produce reasonable results at those locations where there are adequate rocket observations. As will be seen below, this is not always possible. The method, however, is simple and straightforward and involves few assumptions, but depends largely on adequate samples to provide reliable regression coefficients.

Meteorological rocket data provide direct measurements of temperature and wind as a function of altitude at a given place. Vertical resolution is 1 to 2 km. The main limitation is paucity of rocket stations. Unfortunately for scientific users, rocket observation locations have been grouped mainly in the latitude belt from 30° to 40°N. North American rocket observations began about 1960, and the network gradually increased to its maximum density about 1975, and thereafter declined rapidly over North America losing five stations from 1979-82. At present, there are no operational stations in North America north of 55° and only two remain in the Southern Hemisphere, at 8°S and 68°S, although there are Russian rocket-launching ships which are gradually accumulating observations grouped by latitude and month (KOSHELKOV, 1984; cf. Section 2.1.3). The available rocket data used in this report is given in Table 1. It will be noticed that most of the Northern Hemisphere stations used here are in North America. Three Russian stations, at 80°N, 48°N, and 68°S, use the M-100 instrument which appears not to be compatible above 50 km with the sensors used in the North American rockets. Continuing efforts at intercalibration have been made, but necessary corrections to be applied to the past M-100 observations are apparently not available. The correction history changes in time, and it is difficult to learn whether data provided by the World Data Center-A have been corrected and if so, by how much, and whether this correction varied in time. A variety of sensors has also been used in American rockets. A rocket's errors and intercalibration can be found in KOSHELKOV (1984) and SCHMIDLIN (1980).

So long as one depends upon satellite data for future requirements, there will be a need for direct rocket measurements at a wide range of latitudes and throughout the year with which to verify and calibrate satellite data.

Table 1. Rocketsonde stations used.

	Latitude	Longitude	N	Period of	Record
Heiss Island	80°37°N	58°03'E	601	1957-75*	
Thule	76°33'N	68°49'W	1199	1965-80	
Poker Flat	65°07'N	147°29'W	838	1972-79	
Fort Greely	64°00'N	145°44'W	1222	1960-72	
Fort Churchill	58°44'N	93°49'W	2005	1960-79	
Primerose Lake	54°45'N	110°03'W	1238	1964-82	
Shemya	52°43'N	174°06'E	532	1975-82	
Volgograd	48°41'N	44°21'E	423	1965-75*	
Ryori	39°02'N	141°50'E	175	1970-72,	79-82
Wallops Island	37°50'N	75°29'W	2890	1960-82	
Pt. Mugu	34°07'N	119°07'W	3432	1960-82	
White Sands	32°23'N	106°29'W	4698	1959-82	
Cape Kennedy	28°27'N	80°32'W	3792	1960-82	
Barking Sands	22°02'N	159°47'W	2580	1960-82	
Grand Turk Island	21°26'N	71°09'W	223	1963-66	
Antigua	17°09'N	61°47'W	1319	1963-82	
Fort Sherman	09°20'N	79°59'W	1554	1966-79	
Kwajalein	08°44'N	167°44'E	1668	1963-82	
Katal	05°55'S	35°10'W	78	1969-76	
Ascension Island	07°59'S	14°25'W	2316	1962-82	
Woomera	30°56'S	136°31'E	96	1962-72	
Mar Chiquita	37°45'S	57°25'W	58	1969-76	
Molodezhnaya	67°40'S	45°51'E	253	1969-75*	

^{*} Later data exist but unavailable from WDC-A

DATA

OXF

The Oxford satellite temperatures and derived heights and winds were assembled from two years (1973-74) of radiances from the Selective Chopper Radiometer plus three years (1975-77) from the Pressure Modulated Radiometer. A discussion of the data is given in Section 2.1.1. It should be noted, however, that the PMR instrument retrieves temperatures up to near 85 km, and thus provides information beyond the reach of standard meteorological rockets. This means that only radiative equation inversions can be used to obtain temperature with PMR.

SCR

The SCR temperature data from CDC for the seven years (1970-77) were obtained from radiances calibrated by Oxford, or by CDC with Oxford calibration factors, and the use of a multiple nonlinear regression against rocket data. The regressions were done by winter and summer seasons with April 1 and October 1 being the dividing dates. To account for possible drifts in the radiances, the regressions were recomputed every six months. The errors of regression were generally 2 to 4 C as estimated from five different, random, independent sets of rocket data, each set consisting of 15% of the total data available. As there are so few reliable rocket data in the Southern Hemisphere, the regressions for the Northern Hemisphere were applied to the Southern Hemisphere

radiances six months later. This means that for any Northern Hemisphere winter which experienced large sudden warmings, the regression coefficients may be slightly different from true Southern Hemisphere winter coeffficients where warmings are not as frequent or as intense. To extend the cross section downward from 30 to 20 km, north of 20°N, NMC radiosonde data were added to the altitude-latitude sections for the same dates.

MRN

Only meteorological network data as available from World Data Center-A were used here. Unfortunately, despite very long delays in processing rocket data at WDC-A, there is no real quality control of the observations. It is assumed that each individual station, or its processing center, carefully does this. Meteorological rocket data received by teletype for operational use frequently contain serious errors and are not recommended for any scientific purpose when there is time to obtain more reliable data. Russian rocket data taken since 1975 are not available from WDC-A, so it is doubly unfortunate that many North American stations at high latitudes have been closed since 1977. This also prevents the future use of rocket data to retrieve satellite temperatues at high latitudes.

With respect to possible solar cycle influences above 50 km, the dates of the establishment and the reduction of the rocket network were not helpful. The major solar maximum of 1959, and the recent one of 1980, both occurred at a time when there were few rocket stations, especially at high latitudes where any solar effect is likely to be strongest.

Only stations with the most observations were used at a given latitude where there were several to choose from (e.g., Thumba was not used). Stations with less than 150 observations were generally not used unless there was no other station near that latitude; also if the distribution of observations was not spread over the year, the station was not used (Gan). It is highly recommended that meteorological rocket network stations be distributed more evenly with respect to latitude, including the Southern Hemisphere.

The influence of standing planetary waves introduces much irregularity when stations from all longitudes are combined onto a single cross section. Elimination of five Pacific region stations (Poker Flat/Ft. Greely, Shemya, Ryori, Barking Sands, Kwajalein), despite the many observations at the latter two stations, would have produced smoother analyses. The five stations were analysed separately from the continental stations and the altitude-latitude patterns were very similar although absolute values differed, due to planetary wave influence, as shown in Section 2.3.1.

A further caveat in the interpretation of all rocket and satellite data is that so far no tidal corrections have been applied although the regions to which the data apply are known to have large tides. It is possible that in the near future tidal estimates, as discussed in Section 2.3.3., can be applied to both past and future observations.

ANALYTICAL METHOD

A multiple regression is used to determine the amplitudes and phases of periodic features in the bi-weekly averages of daily data. Sine and cosine function pairs are used to represent the annual, semiannual, and terannual oscillations; a mean and trend are also determined during the regression. The QBO is represented by two empirically determined time series of amplitudes derived from tropical data. The method by which these series are generated requires further elaboration.

The QBO is observed to have a continuously variable period and amplitude. For these reasons, the QBO signal in the tropical lower stratosphere was used to define a reference signal with variable period and amplitude from cycle to cycle. This signal was then used in the regression. A second time series of equal variance which was orthogonal to and 90° out-of-phase with the original QBO signal was created using a Hilbert transform. This transformed signal was also used in the regression. The original QBO reference signal was obtained from the zonal winds at 30 km altitude from Fort Sherman (9.33°N), Kwajalein (8.73°N), and Ascension (7.98°S). Thirty-day means were obtained from each station, and the mean, trend, annual, semiannual, and terannual signal were removed using the regression technique. The residual means were then averaged over the three stations to provide a continuous QBO record from late 1962 through 1982. The exact values of the series at bi-weekly intervals are obtained through three-point Lagrangian interpolation.

The errors in fitting periodic functions to the data were used to evaluate the reliability of the data in the contouring of amplitudes and phases. Diagrams of the annual, semiannual, terannual and QBO were made using only those amplitudes (and corresponding phases) that were equal to or larger than the associated standard deviation. Also, at least 45 bi-weekly periods of data were required. The means for all stations were adjusted to a common reference data (1972) to avoid the effect of long period trends. In Figures 1-10, tick marks along the upper edge indicate rocket launch sites.

COMPARISON OF VARIATIONS

Figures 1-10 present the amplitudes of the means, annual and semiannual waves. The values in Figures 1-6 are for SCR and MRN temperature, and those in Figures 7-10 are for MRN wind. The values of OXF are discussed in more detail in Section 2.3.5.

All these data sets are preliminary and may be revised before use in a new CIRA. Periodic variations of the wind are presently available only from MRN. Note that these cross sections are machine contoured and lack smoothness, especially at highest altitudes due to the inhomogeneity of the data. The general patterns of maxima are not affected, however, and the amplitude and phase values discussed below were taken from tabulations rather than the plots, whenever possible.

Sample values at three latitudes are summarized in Table 2. The agreement is far better than expected considering the different sensors, data sources, methods of reduction of the raw data, interpolations to latitude-altitude grids for automated contouring, graphical smoothing techniques, and problems of different longitudes of the stations, periods of record, sample size and uneven distribution of data in space and time.

For the annual variation in temperature (Figures 3 and 4, also Figure 1 in Section 2.3.5.), the most noticeable difference is in the altitudes of the maximum amplitude shown by SCR and OXF. SCR shows a maximum near 3 mb (40 km) at 80°S, while the OXF maximum lies near 11 mb (29 km). OXF is in fair agreement with MRN, where their data overlap. Phase dates are at the solstices. The corresponding annual amplitude of the wind (Figure 8) shows large midlatitude maxima centered near 60 km, in general agreement with Figure 38 in CIRA 1972.

The semiannual wave in temperature (Figures 5, 6, Table 2; cf. 2.3.5, Figure 1) is of interest because it is as strong or stronger at both polar regions than at the equator. Although the polar waves have generally not been recognized, they are shown by VAN LOON et al. (1972) and BELMONT et al. (1975), and are strongly confirmed by all three present data sources. The phase of the

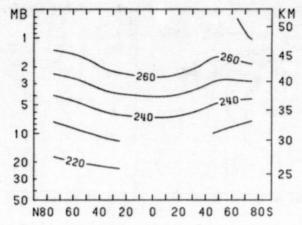


Figure 1. Mean temperature, K, 1970-1977, from SCR.

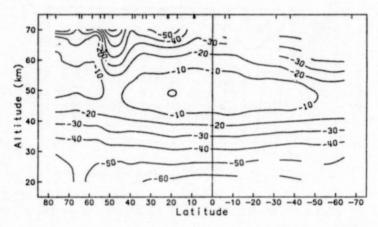


Figure 2. Mean temperature, C, 1960-1982, from MRN.

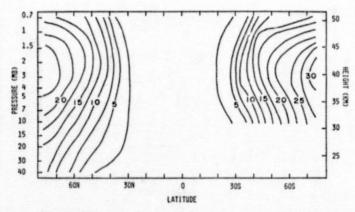


Figure 3. Amplitude of the annual wave in temperature, K, from SCR, 1970-1977.

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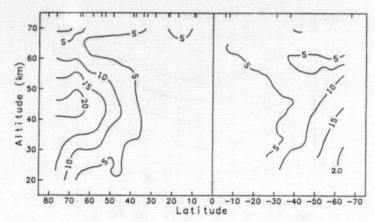


Figure 4. Amplitude of the annual wave in temperature, K, from MRN, 1960-1982.

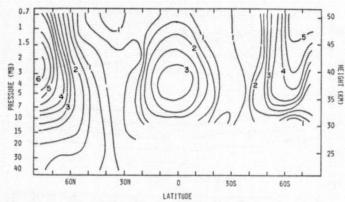


Figure 5. Amplitude of the semiannual wave in temperature, K from SCR, 1970-1977.

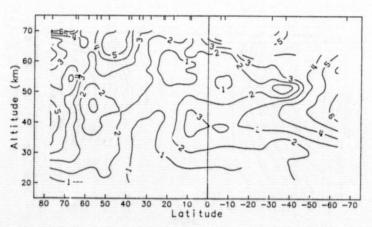


Figure 6. Amplitude of the semiannual wave in temperature, K from MRN, 1960-1982.

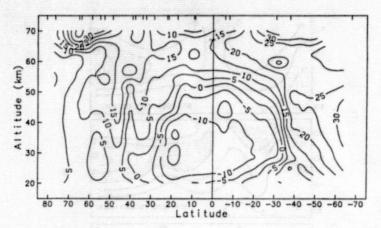


Figure 7. Amplitude of the mean zonal wind, m/s, from MRN, 1960-1982.

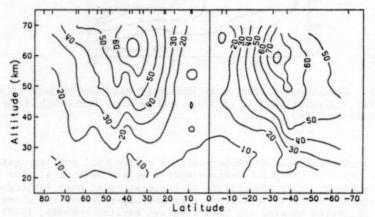


Figure 8. Amplitude of the annual wave in zonal wind, m/s, from MRN, 1960-1982.

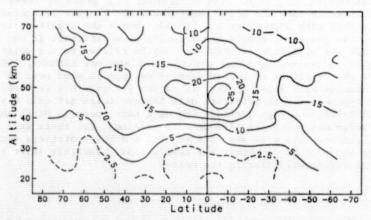


Figure 9. Amplitude of the semiannual wave in zonal wind, m/s, from MRN, 1960-1982.

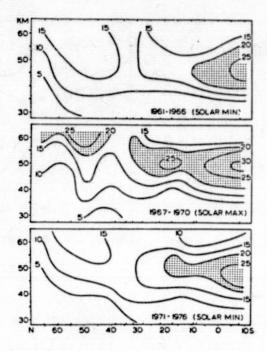


Figure 10. Semiannual variation in MRN zonal wind for periods of solar activity minimum (1961-66, 1971-76) and maximum (1967-70), from NASTROM and BELMONT, 1980).

equatorial semiannual wave in temperature is equinoctial and propagates downward, while those of the polar centers near 3 mb are solstitial. The OXF data show the semiannual amplitude pattern in temperature at high latitudes as a vertical sequence of cells continuing into the upper mesosphere where the semiannual variation in wind has been reported earlier (GROVES, 1972).

The MRN semiannual wave in the wind (Figure 9) shows the well-known tropical maximum near 50 km, south of the equator, with bands of maxima extending poleward (BELMONT et al., 1974). The semiannual wind phase at these centers of maximum amplitude in both the polar regions and the tropics is equinoctial and agrees in general with BELMONT et al. (1974). Where the amplitude is weak, below 35 km, the phase may appear occasionally as solstitial. It has been suggested that the amplitude of this wave may be related to the solar cycle, showing higher values during solar maximum (NASTROM and BELMONT, 1980). Figure 10 shows how the amplitude of the semiannual maximum in wind near 50°N apparently changes with solar cycle. It is not yet possible to confirm this solar cycle hypothesis with satellite data because there are only 8 years of SCR data (1970-78), and high latitude MRN data have ended in North America. The recent solar maximum years 1978-82 were examined, but there were only Shemya and Primrose Lake with any data to 1982 and these stations had too few observations above 50 km to permit any conclusions. Possibly later satellite data for this region will clarify the matter.

Table 2. Comparison of OXF, SCR, MRN, CIRA 1972.

	<u>T</u>	Temperature						Wind ((m/s)
	OXF	SCR	MRN	CIRA Annual	(1 MB)		0XF	MRN .	CIRA
80°N	263	264	263	(264)	70	°N	18	5	(1)
0	268	270	271	(269)	10	°N		-5	(-13)
80°S	270	271	263		70	°S	30	30	1,000
				Annua1	(10 MB)				
80°N	224	227	224	(223)	70	°N	10	5	(17)
0	233	234	232	(231)	10	°N		-10	(-21)
80°S	222	226	226	DAL WIT	70	°S	35	30	10014
				July Me	an (1 MB)			
80°N	284	285		283	10000	Trees.			
0	263	268	-	269					
80°S	254	259	-						
				December	Mean (1	MB)			
80°N	247	250		257					
0	265	269	-	271					
80°S	288	291	-						

				S	CR				MRI	V					
	Max	imu	ım A	nnua1	Tempera	tu	re	Amplitude	K	(at	any	alt	it	ude)
80°N	42	(.	006	mb)											
80°N	26	(2.5	mb)	2	4	(3	mb)		28	(44	km)	(1.3	mb
0	3	(0.1	mb)		1	(1	mb)		4	(42	km)	(2.5	mb !
80°S	41	(.	006	mb)								-			
80°S					3	1	(3	mb)				-			
80°S	35	(11	mb)			,			24	(26	km)	(25	mb
		1	1axi	mum S	emi-Annu	al	A	nplitude K	(at a	ny a	ltit	ud	e)	
80°N	11	(4	mb)		6	(3	mb)		6	(40	km)	(3	mb
0	4	(1.5	mb)		3	(3	mb)		3	(40	km)	(3	mb
80°s	6	1	0.3	mb)											
80°S	4	(1.5	mb)		6	(1	mb)		7	(46	km)	(1.5	mb

Notes to Table 2

- Values are taken from tables, if available, interpolating when necessary.
 Figures are used if tables not available.
 - 2. Values in parentheses were estimated from mean of January and July values read from tables.
 - 3. No SCR data available below 10 mb south of 15°S.

SUMMARY OF RESULTS

The three sets of data agree remarkably well. This may be due in part to ultimate reliance upon a climatology based on meteorological rocket profiles which still serves as the only large body of independent data for the middle atmosphere.

Semiannual variations in wind and temperature at high altitudes of both hemispheres are confirmed, but the cause of the semiannual oscillation at high latitudes is still unknown. Possible solar modulation of the semiannual wave during the 1979-81 maximum could not be detected at high latitudes due to reduction in the MRN rocket network.

Meaningful comparisons of data require data for the same years and place, not just for equal periods of records.

Resultant, observed temperatures or winds are made up of many periodic and quasi periodic components, possibly including solar effects, that modeling must take into account.

RECOMMENDATIONS

Best present estimates of middle atmosphere climate are from satellite global data. A data set consisting of PMR and SAMS to 85 km for 8 years, plus 5 years of SCR, plus continued SSU and similar instruments which sense to 50 km, is now within reach. Resumption of the PMR type measurements is highly recommended.

MRN data must be separated by region. Longitudinal variations due to planetary waves may be large. Thus the sparse MRN data are best used for vertical resolution at a given place, and not for representative global coverage.

Added MRN stations are needed for satellite temperature retrievals, calibration and verification, especially at high latitudes.

MRN data need to be carefully quality controlled. Tidal corrections are needed to adjust single observations per day into more representative values.

ACKNOWLEDGEMENT

Thanks are extended to D. E. Venne and J. Roe for computation and figure preparation.

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2.3.5 ANNUAL AND SEMIANNUAL CYCLES BASED ON THE MIDDLE ATMOSPHERE REFERENCE MODEL IN SECTION 2.2

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The SCR/PMR monthly temperature mean values have been Fourier analysed at each latitude and pressure level to obtain the annual mean and the amplitude and phase of the annual and semiannual cycles (Figure 1 and Table I). The phase is the month of the maximum, such that 1 = January 1, 1.5 = January 16, 2 = February 1, etc. There are some very marked hemispheric differences, notably:

- (a) At $80\,^{\circ}N$ there is a maximum amplitude of the annual cycle of 26 K at 2.5 mb, the corresponding maximum at $80\,^{\circ}S$ is much stronger (35 K) and at a lower altitude (11 mb).
- (b) The semiannual amplitudes show the well-known maximum over the tropics in the upper stratosphere, but also maxima at high latitudes. There the maximum in the Southern Hemisphere, which is at 65°S, is weaker than that in the Northern Hemisphere; (cf. also Section 2.3.4).
- (c) The annual mean shows a minimum at 50°S, 1 mb, and a corresponding weaker minimum at 60°N. This has already been noted in Section 2.1.1 (Figure 4), and is a general feature of the Southern Hemisphere winter, occurring to a smaller extent in the Northern Hemisphere, and clearly strong enough to affect the annual mean.

In general, the hemispheres are remarkably similar and six months out of phase above about 0.3 mb (56 km). It can be seen from Section 2.2 (Figures 1.1 to 1.12) that the two hemispheres are significantly different especially in winter after allowing for a six-month shift. However, changes from summer to winter are so large by comparison that the annual cycles appear to be very similar.

Because of the existence in winter of large longitudinal temperature variations which are repeatedly in the same phase for several months (cf. Section 2.3.1), a given longitude might be consistently warm at some levels and cold at others, leading to annual and semiannual cycles which differ markedly from those of the zonal mean. This is shown for the annual wave by means of horizontal maps of the 30-mb level (Figure 2). Over the Northern Hemisphere large changes in phase occur within the Aleutian anticyclone. Here, the amplitude of the annual wave is small because it is warm in winter as well as in summer.

Over the Southern Hemisphere large phase changes occur over the southern part of South America. Here the maximum of the annual wave is reached late because the "Final Warmings" always start over the Australian section of Antarctica and the transition into summer finishes last over South America.

The variations around the globe of annual and semiannual cycles should be largest at $60 - 70\,^\circ\text{S}$ or N where planetary wave amplitudes are largest (cf. Section 2.3.1), and Figure 3 shows the temperature amplitudes and phase (time of maxima) for $64\,^\circ\text{N}$ as a function of longitude and pressure. Phase variations

are relatively minor (except where the amplitudes are very small). However there are large amplitude variations, e.g. from 16 to 26 K at 3 mb for the annual cycle, 5 to 8.3 K at 5 mb for the semiannual cycle.

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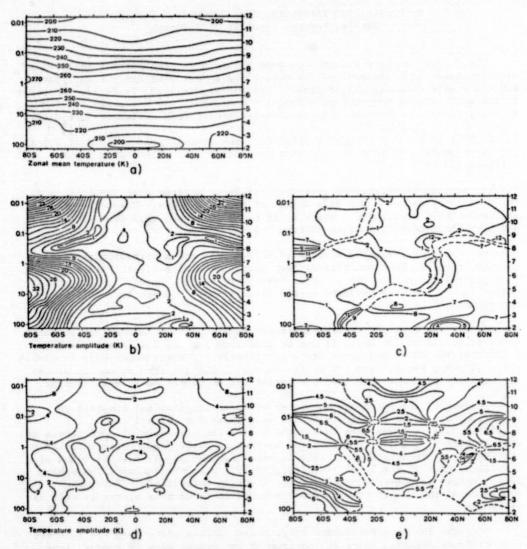


Figure 1. Components of the annual variation of temperature (K) derived from the SCR/PMR combined means. a) annual mean; b) amplitude of annual cycle; c) phase of annual cycle; d) amplitude of semiannual cycle; e) phase of semiannual cycle; phase is given as the month of maximum temperature, e.g., 12 means December 1.

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Table 1.

ANNUAL	MEAN TEM	PERATU	RE (K)																
SCALE HEIGHT	PRESSURE (mb)	-60	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80	
12.0 11.5 11.0 10.5	0.0103	201.5	201.4	195.1 201.7 209.3 217.1	203.0	204.3	204.9	205.0	206.1	207.6	207.1	206.4	206.3	204.5	203.1	201.6	201.0	200.9	
9.5	0.0460 0.0758 0.1250	225.5 235.4 246.0	224.8 233.7 242.9	224.8 232.1 239.7	222,2 228,6 235,5	218.7 224.8 231.8	215.7 222.3 230.5	213.2 220.3 230.0	211.2 218.7 229.5	210,6 218,3 229,6	212.0 219.3 229.9	214.3 221.2 230.4	216.4 222.7 230.4	217.8 223.5 230.2	220.1 225.7 232.2	222.5 229.2 236.1	222.8 230.9 239.6	232.7 232.7 242.3	
8.5 8.0 7.5 7.0	0.3398 0.5603 0.9237	265.5 269.9 269.8	261.3 267.0 268.1	247.6 255.6 262.5 265.3	251.3 259.2 263.5	248.6 258.5 264.8	249.0 259.5 266.5	250.6 260.9 267.7	253,4 263,0 268,0	254.6 264.0 268.0	253.2 262.8 267.8	250.4 260.4 267.4	248.5 259.1 266.4	247.7 258.3 265.4	249.3 258.6 263.8	252.2 260.1 263.1	256.6 262.6 263.5	259.9 264.4 263.8	
6.5 6.0 5.5 5.0	4.14	258.2	257.3	262.4 255.0 244.4 233.8	253.7	255.7	258.2	260.3	260.8	251.0	260.6	250.4	258.7 248.7	257.3	254.5	252.3	250.2	239.4	
4.5	11,25 18,55 30,59	218.9 209.3 211.4	222.0 213.9 214.3	224.2 218.9 218.1 217.0	225.8 222.2 220 6	227.9 223.9 221.0	230.2 224.7 219.8	231.0 224.3 218.4	231.0 223.7 217.3	230.7 223.3 216.7	230.9 223.4 216.7	230.9 223.8 217.5	230.3 223.9 218.3	228.5 222.9 219.0	227.1 222.1 219.6	226.0 221.0 219.7	219.7 219.7 219.0	223.1 218.4 218.3	
2.5	83.15	212.5	214.7	217.0	217.5	214.3	208.1	202.3	199.4	198.7	199.3	202.1	207.0	213.5	218.4	220.8	221.0	220.4	

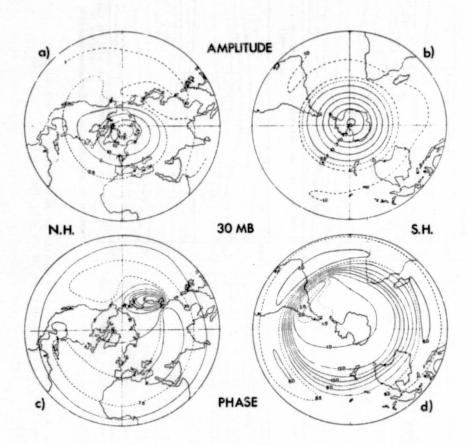
ANNUAL	TEMPERAT	URE CY	CLE	AMPL	TUDE	K) AND	PHASE	(MONT	H OF M	AXIMUM	1)							
SCALE HEIGHT	PRESSURE (mb)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
12.0	0.0062					13.95												
11.5	0.0103					11.69			1.74									35.99 12.85
11.0	0.0169			23,52				0.96	1.84		2,60	2,93	5.80					28.44
10.5	0.0279			18.63				1.49	2,48		2,27	2.45	5.02		14.65			
10.0	0.0460			14.18	10.96	6.25		2.29	3,39	2.88	1.78	1.92	4.06	6,87				14.53
9,5	0,0758	13.41			8.06 7.34	4.67	1.10	2,35	3.91	3.17 1.23	1.76	1.63	2.99	4.31	5.56			9.83
9.0	0,1250		9.52		4.73	2.07	0.97	2.75	1.22	3,36	1,91	1.40	1.56	1.30				7.14
8.5	0,2061	8.55		3.80 6.73	1.03		2.04	3,61	3.98	3,30		1.30	0.45	2,23				3.19
8.0	0,3398			1.43			2.63		2.83	2,93		1.41	0.69					2.75
7.5	0,5603			6.29			2.92	0.98	1.58	2.16	2.28	1.90	0.95	3.72 6.25				9.99
7.0	0.9237					8.37			1.32	1.85	2.06		1.85				16,02	18.61
6,5	1,52					12.16			1.38	1.85		2.38	3.08 4.78					23.94
6.0	2,51					15.84			1.70	1.96			3,59	9.08				25.63
5,5	4,14					16.06			1.33	1.41		2.38	3.75					24.38
5.0	6,83					13.35		2.75	0.51	0.54								22.26
4.5	11,25					8.75			0.92									21.02
4.0	18,55					4.74			1.15		1.03		2.53					19.37
3,5	30,59					2.37			1.01		1.21							16.47
3.0	50.43					1.38		1.91	2.26		2.39	2.19 8.05						13.92
2.5	83,15					9.05						1.45						11.92

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Table 1 continued.

SEMI-N	NNUAL TEM	FINIU	E CICL		NA.	FILLOGE	(K) A	HU PHA	ing the	MTH OF	MAXIM	UM)						
SCALE HEIGHT	PRESSURE (mb)	-80	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	80
12.0	0.0062	11.94	11.42	9,57	6.59	4.24	2.30	2,50		5.90	4,18	2,87	2,18	3.36	4.87	7.17	9.23	
11.5	0.0103	11.43	10.97	9.28	6.04	3.98	2.42 3.70	1.58	3.06 4.75	4.31	2.94 4.67	2.01 3.94	2.44 3.63	3,40	4.64 3.92	7.30	9.24	
11,0	0.0169	9,32		8,18	5.22	3.41 3.97	2.73 3.56	1.70	1.68	1.90	1.68	2,04	2,88 3,48	3.26	4.46	6.72	8.05 4.26	7.99 4.25
10.5	0.0279	6.64		6.31	3.94 4.54	2.82	2.82 3.70	2.38	2.16	2.12 3.12	2.31	2.67 3.36	3,19	3.03 3.80	3.87 4.17	5.52 4.44	6.30	
10.0		3.97 4.72	4.98	5,14	3.02 5.18	2.60 4.67	4.03	3,20	2,94	3,67 2,72	3.19 2.90	3.37	3.31	2.98 4.10	3.06 4.45	3.96 4.68	4.40	4.01
	0,0755	0.85 5.70	5,85	4.15 5.87	5.83	2.76 5.24	2.87 4.49	2.51 3.58	2.77	3.88 2.38	2.90	3,53	3,15 4,11	4,45	2.66 4.78	2.82 5.16	5.07	
	0,1250	1,51	6.82	5.16 6.41	4.58 6.18	3.28 5.69	2.52 5.04		1,99	1,82	2.39	0.74 3.23	4,43	2.80 4.77	2.89 5.14	2,65 5,74	6.49	1.93
8,5		1,60	1,13	5.96 6.77	5.25 6.43	6.05	5,95	1.38	1.35	1,43	1.39	1.31	5.25	5.02	3,14 5,45	6,15	3.28 6.89	1.38
8.0		1.70	1.31	1.05	6.65	6.19	1.86 6.32	1.63	1.46	1.56	1,55	1,36	5.73	2.47 5.17	3,15 5,58	6.35	6.83	1.17
7.5		1.90	1.53	1,34	6.92	1.70 5.92	1.06	1.04		2.57	1.60	0.38	4.89	5.02	5.44	6,12	6.43	
7.0		2,97	2.03	1.95	1.74	5.44	5,19	0.67 4.41	3,60	3.62	3,60	4.01	4.80	1.80	4.75	5.71	6.54	6.67
6.5		2,44	2,22	2.22	2.30	6.30	5.51	4,36	3.99	3,93	4.00	1,58	5,15	5.22	4.08	1.44	1.18	1.13
6.0		2.67	2.30	2.25	2,47	2.36	5,84	4,64	4,27	4,05	4.30	4,64	0.99	4.37	2.53	1.59	1,42	-
5.5		2.71	2,48	5,55	2,60	2,73	5.45	1.78	3,18 4,64	3,18 4,68	3,25 4,69	4.86	5,33	2,55	1.93	1.73	1.62	- 50000
5.0		3,52	2.85	2.67	2,65	2.46	3, 15	4,75	4.92	5.07	4.98	4,93	0.47 5.27	1.63	1.90	1.84	1,85	1.86
4.5		4,48	3,69	2.80	2.60	2.27	2,38	4.61	1,61	4.97	5.02	1.29	6.93	1,95	1.78	1.91	2.14	2.29
4.0		5.21	4.86	1.80	3.09	2.50	2.48	4.71	4,85	4,85	0.98 5.23	0.98 5.34	6,98	1.64	1.87	2.96	2.57	2.
3,5		5.79	5.72	5,12	0.92 4.34	3.15	0.28 3.07	0.26 5.37	5.27	5.22	0,86 5,82	5.81	6,37	1.66	2.00	2,45	3.25	3,69
3.0		6.07	5,12	5,96	0.69 4.66	0.80 3.72	0.51 3,46	2.43	6.01	0.34	0.26 5.34	0.26 5.54	3,90	0.52 2.00	2.05	2.11	2.00	1.39
2.5	83.15	3.57 6.27		6,14	0,84	0.69	4.50	2.86	0.61	0.67	0,55	0.22	0.21	0.05	0.60	2.06	0.22	

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AMPLITUDE AND PHASE OF THE ANNUAL TEMPERATURE WAVE

Figure 2. a) and b): amplitude (K); c) and d): phases (month of maximum) of the annual temperature wave at the 30-mb level (LABITZKE, 1977).



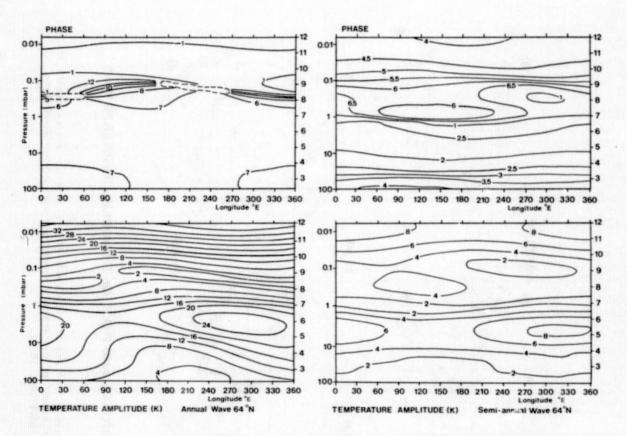
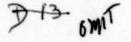


Figure 3. Amplitude (K) and phase (month of maximum) of the annual and semiannual cycles of temperature at 64°N as functions of longitude and pressure.

5



2.3.6 ON THE QUASI-BIENNIAL OSCILLATION, QBO

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The available satellite data series is too short to discuss this cycle and to enlarge the present knowledge. Therefore, only an update of the mean zonal winds over the tropics is given which is based on radioscode data (Figure 1).

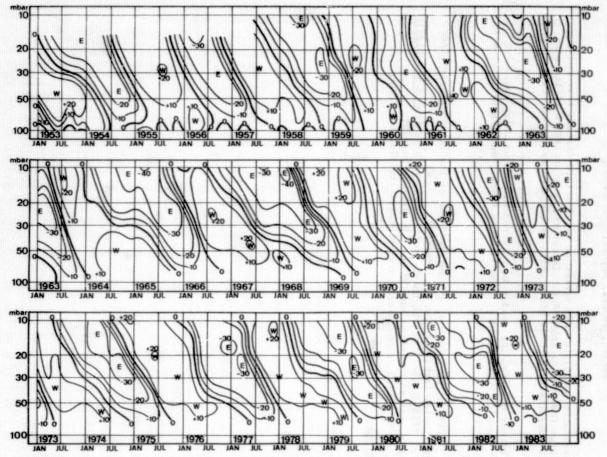
For further details, the reader is referred to reviews which have been published recently, e.g., NAUJOKAT (1985), PLUMB (1984), and TRENBERTH (1980).

REFERENCES

Naujokat, B. (1985), An update of the observed QBO of the stratospheric winds over the tropics (submitted for publication).

Plumb, R. A. (1984), The quasi-biennial oscillation, in <u>Dynamics of the Middle Atmosphere</u>, edited by Holton and Matswno, D. Reidel, 217-251.

Trenberth, K. E. (1980), Atmospheric quas -biennial oscillations, Mon. Weather Rev., 108, 1370-1377.



TIME-HEIGHT CROSS SECTION OF MONTHLY MEAN ZONAL WINDS [ms-1] AT EQUATORIAL STATIONS (UNTIL 1963 FIGURE WAS TAKEN FROM REED, 1965) [JAN 53-AUG 67: CANTON ISLAND, 3*S/172*W; 5EF 67-DEC 75: GAN/MALEDIVE ISLANDS, 1*S/73*E; JAN 76-DEC 83: SINGAPORE, 1*N/104*E]

Figure 1.



2.3.7 ON THE INTERANNUAL VARIABILITY AND ON TRENDS OF THE TEMPERATURE IN THE MIDDLE ATMOSPHERE

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N86-12827

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The new Reference Atmosphere presented here is based on global satellite data and forms a very useful basis for climatological studies. When using such climatologies it is important to be aware of the well-known interannual variability which in the middle atmosphere is particularly large during the northern winters and southern springs.

(a) VARIABILITY OF THE LOWER STRATOSPHERE

For a discussion of the interangual variability of the lower stratosphere a long-term series of temperature data is available for the Northern Hemisphere. This series is based on daily maps derived largely from radiosonde data (Free University Berlin). For the Southern Hemisphere only data of single radiosonde stations are available.

Variability of the Polar Regions: For a comparison of the two polar regions, the monthly mean temperature data for 90°N and 90°S are shown in Figure 1 (update of Figure 1 of NAUJOKAT, 1981) and 2 (Figure 1b, LABITZKE and NAUJOKAT, 1983) in the form of frequency distributions. The time-scale is shifted by six months so that both polar regions can be compared easily. The monthly mean values for the North Pole are based on daily 30-mbar charts derived from radiosonde data, while for the South Pole a radiosonde station is available directly.

The main features to be noted and which have been pointed out previously (e.g., BARNETT, 1974; LABITZKE, 1974; KNITTEL, 1976) are:

- (1) In the <u>lower stratosphere</u> the interannual variability during the northern midwinters (Figure 1) is much larger than during the southern midwinters (Figure 2), due to the major midwinter warmings which take place only during the northern winters; the largest interannual variations over Antarctica are observed during late spring, i.e., October and November when very intense "Final Warmings" bring about the transition into summer.
- (2) The variability in the middle stratosphere is very small in summer when the planetary waves of the troposphere cannot propagate upwards into the stratosphere due to the prevailing easterly winds. This is true for both polar regions.

<u>Variability over Middle and Low Latitudes</u>: The frequency distributions of 30-mbar temperatures for middle northern latitudes (not shown), reveal less disturbed winters and very regular summers.

Although a similar long-term series of temperatures is not available for the Southern Hemisphere, data of single radiosonde stations and satellite data indicate a similar behaviour.

At $30\,^\circ\text{N}$ (Figure 3) the variability is small throughout the year (note the changed interval in the frequency distribution), although still smallest in summer.

This is no longer valid for 10°N (Figure 4) where the variability is enlarged by the quasi-biennial oscillation (QBO).

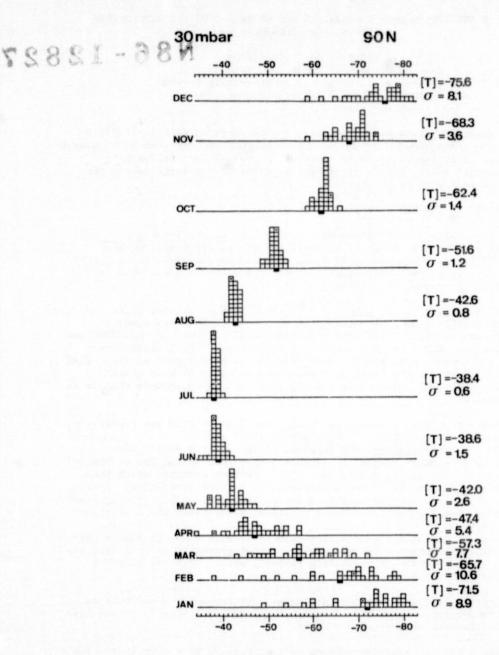
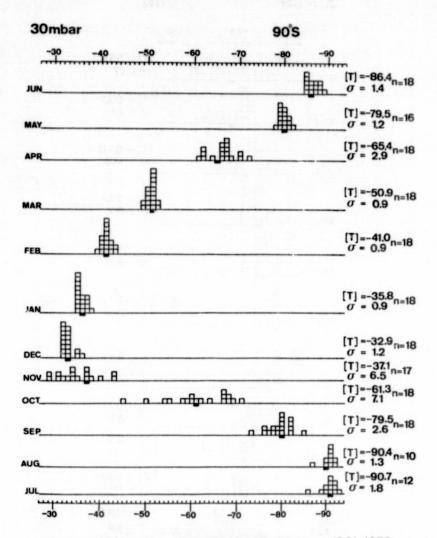


Figure 1. Frequency distribution of the monthly mean 30-mb temperatures (°C) over the North Pole, for the period July 1955 through December 1982. Interval is 1 K. The long-term average [T] is given at the righthand side of the picture, together with the standard deviation o, and [T] is also marked as a black box in the frequency distribution. The data of 1982 are marked and are not included in the long-term average [T]. (Update of Figure 1, NAUJOKAT, 1981).



AMUNDSON-SCOTT, TEMPERATURE, 30 mbar, 1961-1978

Figure 2. Frequency distribution of the monthly mean 30-mb temperatures (°C) over the South Pole, for the period 1961-1978. (Based on radiosonde data, not all months are complete, because of the very low temperatures in winter). Otherwise same notation as in Figure 1 (Figure 1b LABITZKE and NAUJOKAT, 1983).

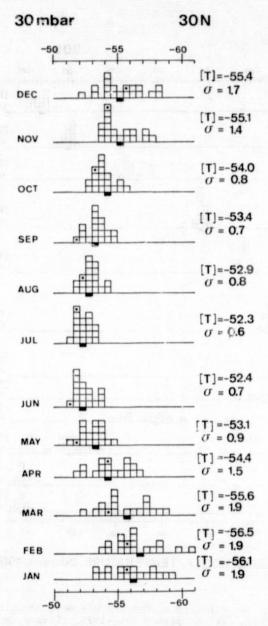


Figure 3. Frequency distribution of the monthly mean 30-mb temperatures (°C), averaged along 30°N, for the period July 1964 through December 1982, with an interval of 1/2 K. Otherwise same notation as in Figure 1. (Figure 1c LABITZKE and NAUJOKAT, 1983).

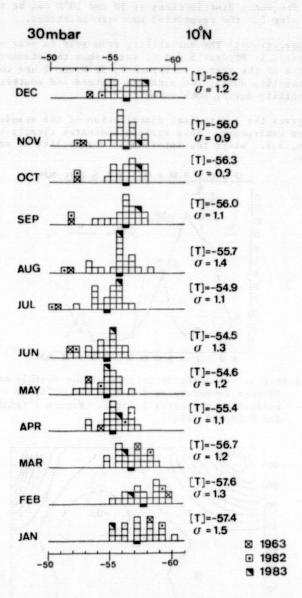


Figure 4. As Figure 3, but for 10°N, and for the period January 1963 through December 1982; the long-term average [T] is based on January 1964 through December 1981. The values for 1963 are marked ⋈, for 1982 ⊙, for 1983 ⊘. (Update of Figure 1d, LABITZKE and NAUJOKAT, 1983).

At $10\,^\circ$ N large positive deviations from the long-term mean are noticeable from July through December in 1963 and 1982. This will be discussed below in part (c). The frequency distributions at 30 and $10\,^\circ$ N can be taken as being representative also for the respective southern latitudes.

Standard Deviations: The variability from year to year as discussed above is summarized in Figures 5 and 6, which show the standard deviations during the course of the year. In Figure 5, 90°N and S are compared, with the very large variability during the northern winters and southern springs, and the small variability during both summers.

Figure 6 gives the latitudinal distribution of the standard deviations for the Northern Hemisphere. This drawing indicates clearly where one should look for trends, i.e., where the interannual variability is smallest: at 60 - 70°N, in summer.

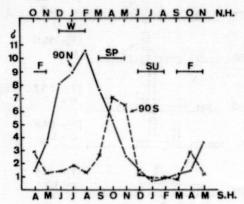


Figure 5. Standard deviations of the monthly mean 30-mbar temperatures for 90°N and 90°S, as indicated in Figures 1 and 2. (Figure 2 LABITZKE and NAUJOKAT, 1983).

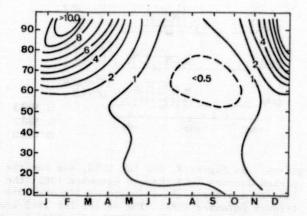


Figure 6. Latitudine 1 distribution of the standard deviations (K) of the monthly mean 30-mbar temperatures throughout the year. (90°N; July 1955-December 1981, n = 26 or 27 years; 80-10°N: July 1964-December 1981; n = 17 or 18 years.) (Figure 3, LABITZKE and NAUJOKAT, 1983).

(b) VARIABILITY OF THE UPPER STRATOSPHERE

The discussion of the interannual variability of the upper stratosphere will concentrate on satellite data which are available for this region since the winter of 1970/71.

Variability of the Polar Regions: The same features as discussed for the lower stratosphere can be found in the upper stratosphere, namely highly disturbed northern winters. This is shown with daily zonal means of radiances at 80 N from different upper stratospheric channels of the SCR (Selective Chopper Radiometer) and PMR (Pressure Modulated Radiometer) (Nimbus 4,5,6) (Figure 7). They are compared with the 10- and 30-mbar temperatures over the North Pole (LABITZKE, 1983). The data set used for the preparation of the new Reference Atmosphere (cf. Sections 2.1.1 and 2.2) includes most of these winters.

This survey over eight northern winters illustrates distinctly their high variability of the stratospheric winters with the different timing and intensity of the stratospheric warmings. The "major warmings(*)" are connected with a breakdown of the stratospheric polar vortex, followed by a "late winter cooling", thus influencing the whole winter season.

In contrast, the southern winters show very little variation from year to year over the polar region. The temperature minimum is reached in early winter and therefore in the upper stratosphere the transition into summer starts much earlier over the Antarctic than over the Arctic. This is shown in Figure 8 where the march of radiances at 80°N and 80°S is compared (LABITZKE, 1977).

These differences are most obvious in spring. Therefore the 1-mbar temperature charts of March/N.H. and September/S.H. are compared in Figure 9 (Data: New Reference Atmosphere).

(c) Temperature Trends

Much attention has been directed recently towards the detectability of changes in temperature because theoretical calculations suggest that changing concentrations of a number of anthropogenically influenced tract gases may presently be altering the global temperature structure, mostly warming the troposphere and cooling the stratosphere (greenhouse effect). A variety of natural processes and phenomena are also known to affect the middle atmosphere, e.g., variation in the solar ultraviolet flux over the ll-year sunspot cycle, or the increase of the stratospheric aerosol load due to volcanic eruptions.

Lower Stratosphere: For the investigation of long-term temperature changes in the lower stratosphere a series of temperature data for the Northern Hemisphere is available from the Stratospheric Research Group, Free University Berlin. This data set which starts in July 1964 for most pressure levels consists of daily hemispheric analyses of temperatures (and geopotential heights), based largely on radiosonde observations. The daily hemispheric analyses have been analyzed by hand and have been digitized into a latitude-longitude grid. Monthly mean statistics have been derived afterwards.

Figure 10 shows filtered zonal mean 30-mb temperatures (°C). A 39-point filter has removed the annual and the quasi-biennial cycles. Looking at these curves, several features can be noticed:

Large variations with a time scale of several years still exist.

The causes of these variations are not clear.

At higher latitudes the variations appear to be connected with the appearance of intense midwinter warmings or undisturbed cold winters.

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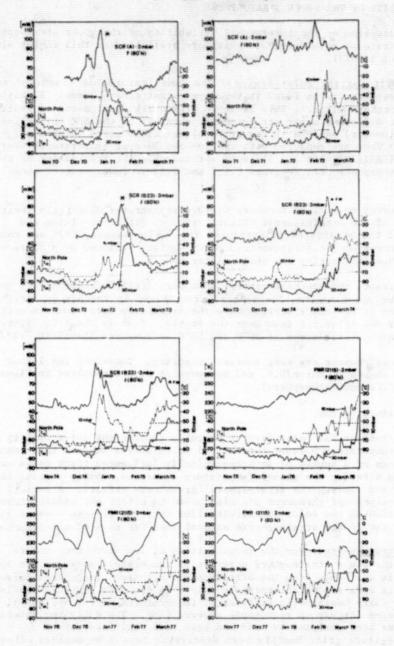
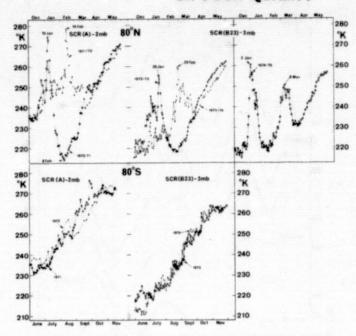


Figure 7. Course of radiances or temperatures over the polar region: zonal mean radiances at 80°N in [mW(m²sr(cm¹))⁻¹] or (K), i.e., equivalent blackbody temperature, from different experiments representing the upper stratosphere as indicated. Temperatures (°C) of the 10- and 30-mbar level over the North Pole. (Radiance data: Oxford University, UK; tempeature data: Free University Berlin.)(LABITZKE, 1983).



Daily zonal means at 80 deg. latitude of radiances of upper stratospheric channels of the SCR, flown on Nimbus 4 and 5.

(The radiances are converted into equiv. black body temperatures (°K)).

Figure 8. Daily zonal means at 80° latitude of radiances of upper stratospheric channels of the SCR flown on Nimbus 4 and 5. The radiances are converted into equivalent blackbody temperatures (from LABITZKE, 1977).

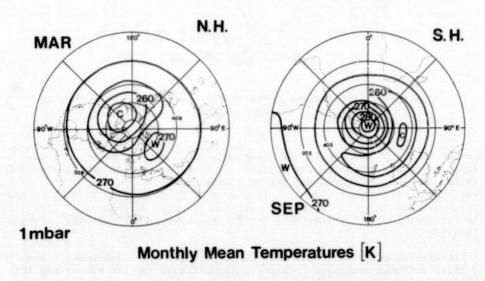


Figure 9. Monthly mean 1-mbar temperatures from March/N.H. and September/S.H. (Data are from the new Reference Atmosphere).

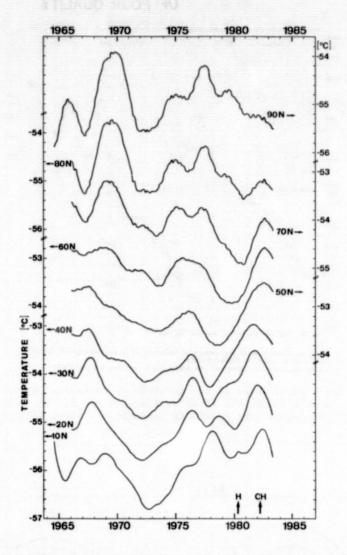


Figure 10. Latitudinal means of filtered monthly mean 30-mbar temperatures (°C). (Update of Figure 4 of NAUJOKAT, 1981).

Between 70 and 40°N a "trend" of about -0.6°/10 years can be seen in the data, if maxima or minima are considered; this is in agreement with recent calculations by De RUDDER and BRASSEUR (1985).

This "trend" is interrupted after 1979 over 40°N, after 1980 over 50°N, and after 1981 at 60°N, but appears to continue further northwards.

The interruption was earlier over low latitudes where the "cooling" stopped in 1972.

The warming over the tropics can be attributed to the increased aerosol load after volcanic eruptions. This was demonstrated for the summer and fall of 1963 and 1982, when the stratosphere warmed markedly over the tropics after the eruptions of Agung and El Chichon (Figures 4 and 11)(LABITZKE et al., 1983; LABITZKE and NAUJOKAT, 1983).

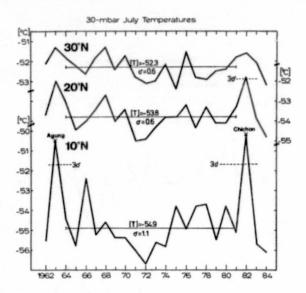


Figure 11. Zonal mean 30-mbar temperatures (°C) during July at 10, 20, and 30°N, for the period 1962 through 1984. The 18-year average [T] is for the period 1964-1981. (Update of Figuré 8 from LABITZKE and NAUJOKAT, 1983).

The filtered 30-mb temperatures (Figure 10) show that the effect of the warming is noticeable as far as 60° N. Probably the region between 40 and 60° N was also strongly affected by the increased aerosol from the eruption of Mt. St. Helens in May 1980.

Looking at the annual averages of the single years directly (Figure 12) the strong cooling over the tropics and subtropics is especially worth noting. The temperatures are as cold or even colder than during the years 1971 and 1972.

The departures of the annual mean temperatures, averaged over two years, are summarized in a time-latitude section (Figure 13). The warming episode due to the increased volcanic aerosol appears to be finished and the cooling has resumed over almost all latitudes.

An even clearer picture emerges, if only July, i.e., a relatively quiet summer month, is considered (Figure 14). The data series for July starts in 1962, cf. Figure 11, and the time-latitude section shows clearly the warming after Agung (March 1963) and after El Chichon (March 1982). If an overall cooling of approximately $0.6^{\circ}/10$ years is accepted, it is not surprising that negative deviations are observed earlier after El Chichon than after Agung, if the deviations are made from the same long-term average.

<u>Upper Stratosphere</u>: Attempts have been made to detect a temperature trend in the upper stratosphere using US rocketsonde data (eg., QUIROZ, 1979; ANGELL and KORSHOVER, 1983; JOHNSON and GELMAN, 1984). Unfortunately, a noticeable temperature decrease coincides with a change in the principal observing system from the Arcasonde system to the Datasonde system, and therefore a clear answer cannot be given at this point.

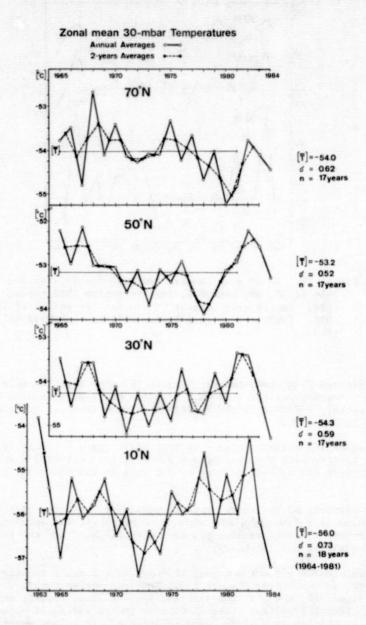


Figure 12. Annual and biennial averages of the 30-mbar temperatures (°C) at 70, 50, 30 and 10°N for the period 1965 through 1984, except for 10°N which starts in 1963. (Update of Figure 4b of LABITZKE and NAUJOKAT, 1983).

Departures ($\frac{1}{10}$ K) of the 30-mbar Temperatures, averaged over 2 years, from the 17-year mean 1965-1981

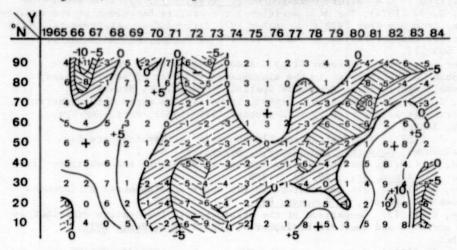


Figure 13. Time-latitude distribution of the deviations (1/10 K) of the annual averages, smoothed over two years, from the 17-year mean 1965-1981. (Update of Figure 5, LABITZKE and NAUJOKAT, 1983).

Departures (10 K) of the 30-mbar July Temperatures, averaged over 2-years, from the 18-year mean 1964-1981

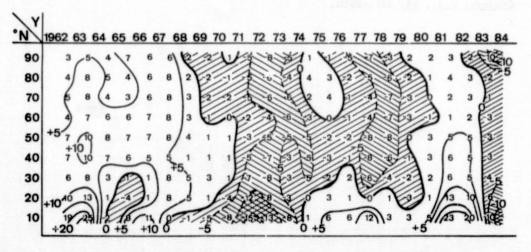


Figure 14. Time-latitude distribution of the deviations (1/10 K) of the July averages, smoothed over two years, from the 18-year mean 1964-1981. (Update of Figure 6, LABITZKE and NAUJOKAT, 1983).

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2.4 A PROPOSED INTERNATIONAL TROPICAL REFERENCE ATMOSPHERE UP TO 80 KM

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1. INTRODUCTION

With the large number of balloonsonde and meteorological rocket network (MRN) stations over the globe and satellite soundings, it is presently possible to characterise the atmosphere typical of a season, a month or even a day. However, a standard atmopshere representative of the mean annual conditions is still essential for many aerospace and remote sensing applications. An International Standard Atmosphere (ISA: see US STANDARD ATMOSPHERE, 1962; ICAO, 1964) specified up to 32 km, and its proposed extension to higher altitudes such as US STANDARD ATMOSPHERE (1976), have been formulated for meeting these needs. These have been generally inspired by conditions in the temperate region around mid-northern latitudes. However, conditions over the tropics can be substantially different from those specified in the International Standards; over the past several years the authors have sought to answer the question "Is it possible to define a standard atmosphere which is close to the mean conditions over tropical India and elsewhere?". During summer, tropical conditions prevail up to about 35 N and during winter the change from extratropical to tropical conditions occurs somewhere between 27°N and 35°N and probably around 30°N (KRISHNA RAO, 1952). Thus with the available data, a suitable Indian Standard Tropical Atmosphere (ISTA) up to 80 km and about 30°N in latitude was specified by ANANTHASAYANAM and NARASIMHA (1979, 1980, 1983, 1984a).

The following facts suggest that, with minor modification, it should be possible to provide an International Tropical Reference Atmosphere (ITRA) suitable for the whole of the tropical regions in both the Northern and Southern Hemispheres. Firstly, a study of the balloonsonde results up to 20 km for stations at other longitudinal locations in North America (see Table 1) show that conditions are not very different from those prevailing over India. Further, even at altitudes up to 80 km, COLE and KANTOR (1978) show that longitudinal variations during summer are small at all latitudes and at all altitudes above 20 km; during winter longitudinal variations become important only in arctic and subarctic latitudes.

We have considered the data at the available longitudinal stations in the topics in formulating the present proposal. Many reference atmospheres have been formulated for the tropics: e.g., PISHAROTY (1959), ARB (1966), USSA (1966), CIRA (1972), COLE and KANTOR (1978), SASI and SEN GUPTA (1979), COLE et al. (1979), and KOSHELKOV (1980); none of these cover the latitude and altitude range of the present proposal.

Finally, it is well known (COLE and KANTOR, 1978) that latitudinal variations are weaker in the tropics than in the temperate regions; hence it should be possible to formulate a meaningful global standard for the tropics. The subsequent section discusses the nature, accuracy and consistency of the data availabe for the present study.

2. DATA BASE FOR PRESENT WORK

2.1 Temperature data: The present standard is developed in three parts,

12828

Table 1. Station temperature data for the proposed ITRA.

	LT	IN	KM	-	PERIO	CA'	TION								
STATION	L	AT	LO	NG	& DAT	ľA									
TRIVANDRUM	9	N	77	E	50-71	В	300	291	283	268	242	221	208	198	211
NAGPUR	21	N	79	E	50-71	B	300	294	283	267	242	222	210	199	210
NEW DELHI	29	N	77	E	50-71	B	297	292	281	264	240	223	214	204	214
SRINAGAR		øΠ				В	286		278	260	2.36	222	217	211	
TRIVANDRUM	9	N°	77	E	73-78	В	299	290	282	267	242	220	205	-194	210
NAGPUR						B	300	294	283	267	243		209		
NEW DELHI	29	N	77	E	73-78	B	298	291	280	264	239		211	200	21
KWAJALEIN	9	N	168	W	69-76	B	304	293	285	269	243	221	207	195	20
BROWNSVILLE									281	264	237	217	207	200	21
AP.CHICOLA	30	N	85	W	71-80	B	290	286	278	263	236	217	209	204	21
					>										6
ASCENSION									243	258					23
THUMBA (a)									244	258			248		20
KWAJALEIN	9	N	77	E	69-76	T	220	230	240					246	23
FT.SHERMAN	9	N	80	W	69-76	T	222	231	243	257			267	259	-
ANTIGUA									242	256				253	23
BARK.SANDS								231	241	254					23
CP.KENNEDY								231	242	255				255	23
WHT. SANDS	32	N	106	W	69-76	T	221	229	240	254	266	268	262	254	24
					>										
ASCENSION(b)	8 (S	14	W	60-71	G	(251 259)	(261	(263	(257	(242	(222	(202	(191	-206
THUMBA (c)	9	N	77	E	71-77	T	259	267	269	256	242	227	213	205	19
KWAJALEIN															
WOOMERA (d)															
WOOMERA (e)															
				1	1000		263)	Tu.	-281)		-255)		-235)		-208

+ B = Balloon, G = Grenade, P = Pitot, S = Sphere, T = Thermistor, * = T & S (a) Without adjustment of FINGER et al. (1975); (b) Mean +/- standard deviation; (c) With adjustment of FINGER et al. (1975); (d) Approximate values from Figure 3 of PEARSON (1974); (e) Approximate range from Figure 3 of GROVES (1966).

namely, (i) in the troposphere and lower stratosphere, using balloonsonde data, (ii) in the upper stratosphere, utilising rocketsonde data, and (iii) in the mesosphere, considering grenade and falling sphere data.

Table 1 also shows the details of the station, type of instrumentation used, duration of available data and reference from which the data have been obtained.

2.2 Remarks on the quality and consistency of data. Table 1 shows the preand post-1970 IMD data when it switched from chronometric and fan type
recorders to the audio-modulated type in the radiosonde. The effect of this,
as noticed by ANANTHASAYANAM and NARASIMHA (1979) and by Van de Boogard (1977),
is that during July over Nagpur, e.g., the later temperature values are lower
by about 5 C at the 100 mb level. However, considering the variation of
temperature over the range of stations in the Indian subcontinent and during a
year, such discrepancies lower the grand mean among stations only by about 2 3 C, and thus would not strongly alter the present proposal. Table 1 further
shows data of some typical stations in India and in the American region; these
are broadly consistent and confirm that a proposal (up to 20 km) valid for the
whole tropical region over the world should be feasible.

For the 20 to 50 km range, commencing from the late sixties when several MRN stations were set up, extensive (generally once-weekly) rocketsonde data are available, as mentioned earlier. The wire type thermistor probe used on the Russian M-100 rocketsonde and the bead type thermistor probe on American

rocketsondes are fairly consistent up to 50 km. However, these probes have shown differences of as much as 15°C around 70 km during the many intercomparison experiments carried out at Wallops Island and reported by FINGER et al. (1975), IVANOVSKY et al. (1979) and SCHMIDLIN et al. (1980). It is possible that these differences are due to the free molecular conditions prevailing at altitudes beyond about 50 km, but no universally accepted resolution of these differences is yet available. Thus, rocketsonde data available at many stations over the globe have been used only in the range from about 20 to 50 km.

For the higher altitude range of 50 to 80 km we have used mainly the falling sphere and grenade data, which are consistent among themselves and possess an accuracy of about 2 - 3°C (CIRA, 1972). SMITH et al. report pitot tube data as well, but these lead to temperatures which are about 5°C higher on an average from the grenade data; as the reason for this is not clear, we have not considered the pitot data. Data in this altitude range are not as extensive as one would wish, but are perhaps barely adequate to propose a reasonable standard for describing the mean conditions.

Beyond an altitude of 80 km molecular dissociation commences, and above 100 km molecular diffusion predominates, and so air can no longer be treated as a perfect gas. It is then necessary to specify at each level the (varying) concentration of different species constituting air. Hence an altitude of 80 km is a natural limit to the present kind of standard.

3. PROPOSED INTERNATIONAL TROPICAL REFERENCE ATMOSPHERE (ITRA) UP TO 80 KM

The philosophy adopted by the authors in proposing the reference has been that it should: (a) be reasonably close to mean conditions, (b) be within the range of variation inherent in the atmosphere over space and time and the uncertainty in the data be as simple as possible, and (c) adopt, where no physical principles are violated, as many of the parameters in the ISA as possible.

3.1 Temperature distribution with altitude. Table 1 and Figure 1 show, respectively, the station mean data, and the grand mean among themselves, for the temperature between sea level and about 90 km. In the mesospheric region the grand mean is weighted towards low latitude stations. But Wallops Island data in USSA (1976) indicated that the latitudinal variations (at least between 50 and 70 km) is weak. Usually straight lines best fitting the data are used to describe the temperature distribution with altitude. This is because closed form integration of the governing equation to obtain other atmospheric properties is the possible.

As the data indicate, the proposed standard has a sea level temperature of 27°C, and a lapse rate of 6°C/km up to 6 km. Beyond this altitude the lapse rate is 6.5°C/km (as in ISA) up to 16 km, the tropopause height. This tropopause height, and the corresponding temperature of -74°C seems quite appropriate as noticed by us, and is also consistent with the various monthly reference atmospheres at the equator, 15°N and 30°N proposed by COLE and KANTOR (1978). Further, in the stratosphere, a single lapse rate of -2.3°C/km all the way up to a stratopause height of 46 km, with a temperature of -5°C, fits the data very well. Though this temperature is somewhat higher than indicated by the Thumba value (IMD, 1976), we consider it appropriate because of the fact that the stratopause temperature decreased with increasing latitudes (COLE and KANTOR, 1978). The available data in the mesosphere indicate that it would be worthwhile to extend the constant temperature stratopause up to 52 km. It should be noted that in the mesosphere inversions occur during some months and there are well-known double mesopauses with different temperature values as

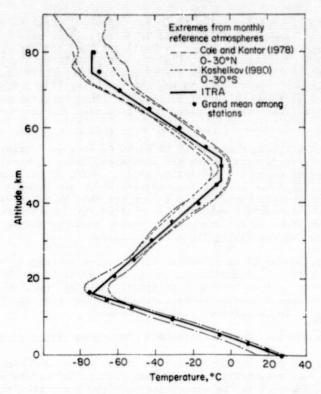


Figure 1. Comparison of ITRA with station data and monthly reference atmospheres.

well (WDC, 1969:76). But considering the totality of the data, and the average value that can be assigned at different levels over many stations, it is seen that once again a constant lapse rate of 3°C/km from 52 km to 75 km, leading to a temperature of -74°C (as at tropopause) by the beginning of the mesopause, is justified. The constant temperature mesopause extends up to 80 km, which is the limit of the present proposal.

The present tropical reference is within the range of the extremes based on the temperature values in the monthly reference atmsopheres for the tropical regions proposed for the Northern and Southern Hemispheres by COLE and KANTOR (1978) and by KOSHELKOV (1980), respectively; these are also shown in Figure 1.

3.2 Mean sea level pressure. Seasonal pressure variations like those of the temperature increase with latitude, the mean pressure being lower during summer and higher during winter. Consideration of the mean annual station level pressures at Indian stations, extrapolated to sea level conditions, gives a value of about 1010 mb based on hourly data (ANANTHASAYANAM and NARASIMHA, 1984b). In ISTA, we had used a lower value of 1005 mb, consistent with the somewhat higher sea level temperature value of 30 °C to provide a slight bias towards the hot day that was considered desirable for aeronautical work. The more appropriate sea level temperature of 27 °C now proposed, goes with the higher value of 1010 mb for sea level pressure. COLE and KANTOR (1978), using mostly data from western longitudes, also obtain a mean pressure close to this value. Only towards 30 °N and beyond does the mean pressure increase

appreciably. A further study of the Southern and Northern Hemisphere data for the years 1951 to 1960 from the WORLD WEATHER RECORDS (1967) for nearly 200 tropical stations shows that the above annual value is justified. It may be noted that the yearly variation of pressure at a given station is of the order of a few mb. Different countries adopt slightly different methods for reducing the station level pressure to sea level conditions (WMO, 1968). But these are even smaller than 1 mb and thus do not affect our proposal.

3.3 Acceleration due to gravity (g). For this we suggest a value corresponding to the Tropic of Cancer, which from Lambert's formula given in LIST (1968) gives 9.78852 m/s (to five decimal places).

4. ATMOSPHERIC TABLES

Table A below specifies the temperature distribution for the present International Tropical Reference Atmosphere, as also the other constants adopted for generating the atmospheric table.

Table A. Defining parameters and constants for the proposed ITRA

Altitude (km)	0	6	16	46	52	75	80
Temp (°C)	27(-6.0)	-9(-6.5)	-74(2.3)	-5(0.0)	-5(3.0)	-74(0.0)	-74

The bracketed quantities denote lapse rate in °C/km. Sea level pressure = 1010 mb; Acceleration due to gravity = 9.78852 ms 2. The molecular weight and the ratio of the specific heats of air, the gas constant and the other constants for the transport properties are assumed to be the same as in US STANDARD ATMOSPHERE (1976).

Tables 2 and 3 give the atmospheric properties useful in meteorological and aerospace applications. More detailed atmospheric tables and the computer code used are available on request from the authors.

ACKNOWLEDGEMENT

The authors thank the Aeronautics Research and Development Board (ARDB) for having supported this study through a grant for the project "SITA".

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Table 2. Atmospheric properties of ITRA (SI units).

PRESSURE	GEOPT ALT	NUMBER DENSITY	MEAN PARTICLE	MEAN COLLSN	MEAN FREE	DYNAMIC VISCTY	KINMATIC VISCTY	THERMAL
(mb)	(m)	(m ⁻³)	SPEED (m/s)	(s-1)	PATH (m)	kg/(m.s)	(m ² /s)	W/(m.K)
1.010 3	00	2.437 25	4.684 2	6.757 9	6.932-8	1.847-5	1.575-5	2.626-2
8,500 2	1500	2.114 25	4,614 2	5.774 9	7.990-8	1.804-5	1.774-5	2.556-2
7.000 2	3130	1.802 25	4,535 2	4.837 9	9.377-8	1.757-5	2.027-5	2.479-2
5,000 2	5820	1,365 25	4.403 2	3,559 9	1.237-7	1.677-5	2.553-5	2.350-2
3.000 2	9610	9.028 24	4.195 2	2.241 9	1.871-7	1.551-5	3.571-5	2.151-2
2.000 2	12360	6.502 24	4.036 2	1.553 9	2.598-7	1.455-5	4.653-5	2.002-2
1.500 2	14190	5.151 24	3.926 2	1.197 9	3.280-7	1.390-5	5.609-5	1.902-2
1.000 2	16610	3.611 24	3.829 2	8.185 8	4.678-7	1.332-5	7.666-5	1.814-2
5.000 1	20790	1.723 24	3.919 2	3.998 8	9.804-7	1.386-5	1.672-4	1.896-2
3,000 1	23990	9.989 23	3.988 2	2.358 8	1.691-6	1.426-	2.969-4	1.958-2
2.000 1	26610	6.480 23	4.042 2	1.550 8	2.607-6	1.459-5	4.682-4	2.008-2
1.000 1	31260	3.092 23	4.138 2	7.573 7	5.464-6	1.517-5	1.020-3	2.098-2
5.000 0	36140	1.475 23	4.236 2	3.699 7	1.145-5	1.576-5	2.221-3	2.190-2
2.000 0	42940	5.548 22	4.369 2	1.435 7	3.045-5	1,656-5	6.206-3	2.317-2
1.000 0	48350	2.701 22	4.427 2	7,078 6	6.255-5	1.691-5	1.302-2	2.374-2
5.000-1	53780	1.378 22	4.383 2	3,575 6	1.226-4	1.664-5	2.511-2	2.331-2
2.000-1	60570	5.975 21	4.210 2	1.489 6	2.827-4	1.560-5	5.428-2	2.165-2
1.000-1	65350	3.175 21	4.083 2	7.675 5	5.320-4	1.484-5	9.715-2	2.046-2
5.000-2	69850	1,688 21	3.961 2	3.956 5	1.001-3	1.410-5	1.737-1	1.933-2
2.000-2	75390	7.274 20	3.815 2	1.643 5	2.323-3	1.324-5	3.784-1	1.802-2
1.000-2	79440	3.637 20	3.815 2	8.214 4	4.645-3	1.324-5	7.567-1	1.802-2

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Table 3. Atmospheric properties of ITRA (largely SI units).

GEOPT ALT (m)	PRES ALT (m)	TEMP DEGREE (K)	PRESSURE (mb)	PRESSURE RAT70	(kg/m ³)	DENSITY	SONIC VELCTY (m/s)	NUMBER (s/m²)
-2000	-1890	312.15	1.262 3	1.250 0	1.408 0	1.202 0	354.18	7.402 0
00	30	300.15	1.010 3	1.000 0	1.172 0	1.000 0	347.31	6.348 0
2000	1940	288.15	8.010 2	7.930-1	9.684-1	8.261-1	340.29	5.412 0
4000	3840	276.15	6.290 2	6.227-1	7.934-1	6.769-1	333.13	
6000	5740	264.15	4.886 2	4.838-1	6.444-1	5.497-1	325.81	3.856 0
8000	7640	251.15	3.750 2	3.712-1	5.201-1	4.437-1	317.70	3.240 0
10000	9540	238.15		2.809-1	4.150-1	3.540-1	309.36	2.700 0
12000	11430	225.15	2.113 2	2.093-1	3.270-1	2,790-1	300.80	2.228 0
14000	13410	212.15	1.547 2	1.532-1	2.540-1	2.167-1	291.99	1.819 0
16000	15520	199.15	1.110 2	1.099-1	1.942-1	1.657-1	282.90	1.467 0
18000	17660	203,75	7.914 1	7.836-2	1.353-1	1.154-1	286.15	1.002 0
20000	19760	208.35	5.684 1	5.628-2	9.503-2	8.107-2	289.36	6.908-1
22000	21820	212.95	4.112 1	4.071-2	6.726-2	5.738-2	292.54	4.800-1
24000	23860	217.55	2.995 1	2.965-2	4.796-2	4.091-2	295.68	3.362-1
26000	25870	222.15	2.196 1	2.175-2	3.444-2	2.938-2	298.79	2.373-1
28000	27860	226.75	1.621 1	1.605-2	2.490-2	2.124-2	301.87	1.686-1
30000	29820	231.35	1.203 1	1.192-2	1.812-2	1.546-2	304.92	1.207-1
32000	31770	235.95	8.988 0	8.899-3	1.327-2	1.132-2	307.93	8.697-2
34000	33700	240.55	6.750 0		9.776-3	8.339-3	310.92	6.307-2
36000	35640	245.15	5.097 0	5 047-3	7.244-3	6.179-3	313.88	4.602-2
38000	37590	249.75	3.869 0	5.631-3	5.397-3	4.604-3	316.81	3.378-2
40000	39550	254.35	2.952 0	2.923-3	4.043-3	3.449-3	319.71	2.494-2
42000	41510	258.95			3.045-3	2.597-3	322.59	
44000	43480	263.55	1.743 0		2.304-3	1.966-3	325.44	1.381-2
46000	45460	268.15	1.349 0		1.752-3	1.495-3	328.27	1.036-2
48000	47470	268.15	1.046 0	1.035-3	1.359-3	1.159-3	328.27	8.034-3
50000	49480	268.15	8.110-1	8.030-4	1.054-3	8.988-4	328.27	6.230-3
52000	51490	268.15	6.289-1	6.226-4	8.170-4	6.969-4	328.27	4.831-3
54000	53500	262.15	4.862-1	4.814-4	6.462-4	5.512-4	324.58	3.890-3
56000	55510	256.15		3.700-4	5.083-4	4.336-4	320.84	
58000	57520	250.15	2.855-1	2.826-4	3.975-4	3.391-4	317.06	2.485-3
60000	59540	244.15			3.091-4	2.637-4	313.24	1.970-3
62000	61560	238.15	1.633-1	1.616-4	2.388-4	2.037-4	309.36	
64000	63580	232.15	1.222-1	1.209-4	1.833-4	1.564-4	305.44	1.218-3
66000	65610	226.15			1.397-4	1.192-4	301.47	
68000	67640	220.15	6.682-2	6.616-5	1.057-4	9.020-5	297.44	7.339-4
70000	69670	214.15			7.940-5	6.773-5	293.36	5.640-4
72000	71710	208.15			5.914-5	5.045-5	289.22	
74000	73760	202.15			4.367-5	3.725-5	285.02	
76000	75830	199.15			3.151-5	2.688-5	282.90	
78000	77870	199.15	1.279-2	1.266-5	2.238-5	1.909-5	232.90	1.690-
80000	79850	199.15	9.082-3	8.992-6	1.589-5	1.355-5	282.90	1.200-

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2.5 INTERIM REFERENCE OZONE MODELS FOR THE MIDDLE ATMOSPHERE

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1. INTRODUCTION

Over the last 50 years, a number of measurements of ozone in the middle atmosphere have been obtained from the ground, and from balloons, rockets and satellites. Numerous models have been developed to summarize various portions of these measurements since detailed knowledge of the global distribution of ozone is important for studies of atmospheric circulation, dynamic processes, and the radiation balance and the photochemistry of the atmosphere. From the ground-based ozone network the latitudinal-seasonal variations of total column ozone were summarized by DUTSCH (1974) and the longitudinal variations were included in a series of monthly atlases for the period 1957 to 1967 by LONDON et al. (1976). Measurements of vertical structure obtained from balloonsondes and rocket data at midlatitudes in the Northern Hemisphere were summarized in a 45 deg annual model generated by A. Krueger and R. Minzner contained in the United States Standard Atmosphere Supplements, 1976 (KRUEGER and MINZNER, 1976). BOJKOV (1969) generated models of ozone vertical structure related to total column ozone amount based on Dobson data and early Umkehr measurements. Models relating the vertical structure of ozone to total ozone based on approximately 7000 balloonsondes and a number of rocketsondes were generated (HILSENRATH et al., 1977) as a "first guess" for the Nimbus 4 Backscattered Ultraviolet (BUV) ozone experiment retrievals of total ozone and vertical structure and for the Nimbus 7 SBUV/TOMS total ozone retrievals. Similar models based on essentially the same data base were generated (MATEER et al., 1980) as a "first guess" for inversion of "short" Umkehr observations to determine vertical structure of ozone from the ground. The 22 vertical profiles of MATEER et al. were given as a function of latitude (low, mid and high) and total column ozone, but not season. Inconsistencies between rocket and balloon data were handled differently by MATEER et al. (1980) than by HILSENRATH et al. (1977). BHARTIA et al. (1984c) have developed similar models using both ozonesonde and satellite data. KLENK et al. (1983) developed a model of ozone vertical structure based on Nimbus 4 BUV data at pressures less than 15.6 mb and on balloon data at lower altitudes. This model was used as a "first guess" for vertical structure retrievals from the Nimbus 7 Solar Backscattered Ultraviolet (SBUV) ozone experiment. The model consisted of a simple parametric representation of the annual and latitudinal variations of ozone as a function of pressure and assumed symmetry between the Northern and Southern Hemispheres. Also included in this model is the ozone covariance matrix which describes the variance of ozone in individual atmospheric layers and the covariances between adjacent layers. An ozone covariance matrix is also included in the models of MATEER et al. (1980). DUTSCH (1978) compiled data on the vertical ozone distribution using chemical-type balloca soundings and early BUV results. A tabulation of monthly Nimbus 7 SBUV ozone profiles for the period November 1978 through October 1979 is provided by McPETERS et al. (1984) in 10 deg latitude increments from 0.17 mb to the surface. Results are given in terms of column density and its standard deviation, volume mixing ratio and number density. HEATH et al. (1982) have generated a set of atlases of total ozone for the period April 1970 - December 1976 based on Nimbus 4 BUV data. TOLSON (1981) has generated a ninth-order, ninth-degree spherical

harmonic model to represent the monthly mean total columnar ozone field over the 7-year period of the Nimbus 4 BUV data set. Annual and semiannual components are determined for both latitudinal and longitudinal variations, and the biennial and longer term variations are determined as a function of latitude. HASEBE (1983) has modeled the latitudinal and longitudinal variations in the total columnar ozone field over the 7-year period of the Nimbus 4 BUV data set using filtering techniques. Global mean total column ozone and its annual, semiannual, quasi-biennial and longer term components have been determined through spherical harmonic analysis (KEATING et al., 1981; TOLSON, 1981).

Data on total ozone and its vertical structure have been obtained from a number of satellite experiments. Shown in Table 1 (KRUEGER et al., 1980) is a tabulation of satellite ozone experiments through 1978. Included are solar and stellar occultation, solar backscatter ultraviolet, and infrared types. Since then, other satellites have been launched with ozone measurement capability including Applications Explorer 2 (McCORMICK et al., 1984), Dynamics Explorer 1 (KEATING et al., 1983b), Solar Mesosphere Explorer (BARTH et al., 1983), EXOS-C (MAKINO et al., 1984, and the NOAA series of satellites (PLANET et al., 1984).

With the wealth of recent satellite data allowing high precision determination of ozone variations with pressure, latitude and time, it was decided to generate models of ozone vertical structure based not just on one satellite experiment, but on multiple data sets from satellites. This is the first time such models have been generated. The very good absolute accuracy of the individual data sets allowed the data to be directly combined to generate these models. The data used for generation of these models are from some of the most recent satellite measurements over the period 1978-1982. A discussion is provided of validation and error analyses of these data sets. Also, inconsistencies in data sets are indicated which in some cases may be associated with inaccuracies in assumed ozone cross sections. The models cover the pressure range from 20 to 0.003 mb (25 to 90 km). The models for pressures less than 0.4 mb are only provisional since there was limited longitudinal coverage at these levels. The models start near 25 km in accord with previous CIRA models. The standard deviation and interannual variations relative to zonal means are also provided.

In addition to the models of monthly latitudinal variations in vertical structure based on satellite measurements, monthly models of total column ozone and its characteristic variability as a function of latitude based on 4 years of Nimbus 7 measurments, models of the relation between vertical structure and total column ozone (MATEER et al., 1980), and a midlatitude annual mean model (KRUEGER and MINZNER, 1976) are incorporated in this set of ozone reference atmospheres. Other variations of ozone in addition to the monthly latitudinal variations such as the quasi-biennial oscillation are also briefly discussed.

Future refinements which are planned for the final CIRA models are also enumerated. Among these are the inclusion of improved ozone determinations from Nimbus 7 SBUV and TOMS data based on recent determinations of ozone cross sections (KLENK et al., 1984), the incorporation of the results of intercomparison studies presently being performed on recent satellite data sets (FLEIG et al., 1984b), and the inclusion of additional data which should become available. However, considering the present fine agreement among satellite data sets (generally within 10% of the interim reference models below 0.4 mb) it is expected that the present tables will be useful for many applications.

2. SATELLITE DATA FOR REFERENCE MODELS

The reference models provided here of monthly latitudinal variations of vertical structure are based on ozone data from five satellite experiments (see

Table 1. Satellite experiments to measure ozone (KRUEGER et al., 1980).

Туре	Satellite	Wavelengths nm	Latitude Coverage	Comments	References
Occulta- tion					
Solar	Echo 1	590,529.5	17 N	Dec.1960	VENKATESWARAN et al. (1961
	USAF 1962	260	33 S-13 S	July 1962	RAWCLIFFE et al. (1963)
	Ariel 2	200-400	50 S-50 N	Apr., May, Aug. 1964	MILLER & STEWART (1965)
	AE-5	255.5	5 N	Dec. 1976	GUENTHER et al. (1977)
Stellar	0A0-2	250	16 S-43 N	Jan. 1970 Aug. 1971	HAYS and ROBLE (1973)
	0A0-3	258-343	12 S-3 N	July 1975	RIEGLER et al. (1976)
Back-					
scatter					
uv					
Profile	USAF 1965	284	60 S-60 N	FebMar 1965	RAWCLIFFE & ELLIOTT (1966)
	USSR	225-307	60 S-60 N	Apr. 1965	IOZENAS et al. (1969)
		250-330	60 S-60 N	June 1966	IOZENAS et al. (1969)
	1966-111B	175-310	80 S-80 N	1966	ELLIOTT et al. (1967)
	0G0-4	110-340	80 S-80 N	Jan.1969	ANDERSON et al. (1969)
	Nimbus 4				(1070)
	b.u.v.	255.5-305.8	80 S-80 N	Apr. 1970- July 1977	HEATH et al. (1973)
	AE-5				
	b.u.v.	255.5-305.8	20 S-20 N		FREDERICK et al. (1977a)
	Nimbus 7			Apr.1977	WELEN (1075)
	s.b.u.v.	255.5-305.8	80 S-80 N	Nov. 19/8	HEATH et al. (1975)
Total	Nimbus 4				
	b.u.v.	312.5-339.8	80 S-80 N	Apr. 1970- July 1977	MATEER et al. (1971)
	AE-5				
	b.u.v.	312.5-339.8	20 S-20 N	Nov. 1974- Apr. 1976	
	Nimbus 7				
	t.o.m.s.	312.5-339.8	global	Nov. 1976	HEATH et al. (1975)
Infrared Emission		μ m			
Profile	Nimbus 6				
	1.r.i.r.	9.6	65 S-90 N	June 1975- Jan. 1976	GILLE et al. (1980)
	Nimbus 7				
	1.i.m.s.	9.6	65 S-90 N	Oct. 1978- May 1979	NIMBUS PROJECT (1978)
Total	Nimbus 3				
	i.r.i.s.	9-10 spec- tral scan	80 S-80 N		HANEL et al. (1970)
	Nimbus 4				
	i.r.i.s.	9-10 spec- tral scan	80 S-80 N	Apr. 1970- Jan. 1971	PRABHAKARA et al. (1976)
	Block 5 m.f.r. (4	flights)	global	Mar. 1977	LOVILL et al. (1978)
	Tiros N				

Table 2): Nimbus 7 Solar Backscatter Ultraviolet (SBUV), Nimbus 7 Limb Infrared Monitor of the Stratosphere (LIMS), Applications Explorer Nission-2 Stratospheric Aerosol and Gas Experiment (SAGE), Solar Mesosphere Explorer UV Spectrometer (SME-UVS), and Solar Mesosphere Explorer 1.27 m Airglow (SME-IR). Other ozone data sets are included to define the nature of systematic variations other than the latitudinal-seasonal variation.

The nadir-viewing SBUV experiment determines the vertical structure of ozone from absorption of solar ultraviolet backscattered radiation between 250 and 340 nm. The resolution of the ozone measurements is about 8 km in the vertical. For these studies the first four years of SBUV data were employed (November 1978 - September 1982) using daily zonal averages every 10 deg in latitude over the illuminated portion of the earth from 20 mb to 0.4 mb. This data set includes the refinements given in the third and fourth year addendum to the SBUV User's Guide (SYSTEMS and APPLIED SCIENCES CORP., 1984) and refinements at high latitudes between 7 and 15 mb to remove an artifact in these data (P. K. Bhartia, private communication, 1984). Data contaminated by volcanic emissions after October 1980 (including El Chichon) have been removed (SYSTEMS and APPLIED SCIENCES CORP., 1984).

Validation studies have been performed on the SBUV data employing balloon, rocket and ground-based Umkehr measurements (BHARTIA et al., 1984b). The precison of the SBUV measurements is found to be better than 8% for pressures between 1 and 64 mb. Constant biases of generally less than 10% between the SBUV results and the balloon and Umkehr results may be largely due to errors in ozone absorption cross sections. It is planned to employ improved ozone absorption cross sections agreed upon recently by the International Ozone Commission of IAMAP for these experiments in the near future (KLENK et al., 1984; BASS and PAUR, 1984; PAUR and BASS, 1984).

The LIMS instrument, a six-channel cryogenically cooled radiometer measured O₃ and temperature in the stratosphere and mesosphere and H₂O, HNO₃, and NO₂ distributions in the stratosphere from 84°N to 64°S latitude from October 25, 1978 to May 28, 1979 (RUSSELL, 1984; GILLE and RUSSELL, 1984). The LIMS ozone channel measures emission near 9.6 pm with a field of view which at the limb is about 1.8 km in the vertical and 18 km in the horizontal (perpendicular to the line of sight).

Table 2. Satellite data used for interim reference ozone models.

Instrument	Incorporated Pressure Range	Incorporated Time Interval
NIMBUS 7 LIMS	0.4 - 20 mb	11/78 - 5/79
NIMBUS 7 SBUV	0.4 - 20 mb	11/78 - 9/82
AE -2 SAGE	4 - 20 mb	2/79 - 12/79
SME UVS	0.07 - 0.5 mb	1/82 - 12/83
SME IR	0.003 - 0.5 mb	1/82 - 12/83
NIMBUS 7 TOMS	TOTAL	11/78 - 9/82

Monthly zonal means of Kalman-filtered LIMS ozone values are incorporated in the model for the period November 1978 through May 1979 from 60°S to 80°N and from 20 mb to 0.4 mb. Validation studies have been performed using balloon and rocket underflights, Umkehr soundings, and Dobson measurements (REMSBERG et al., 1984). Comparison with the correlative measurements shows mean differences of less than 10% at midlatitudes for balloon-borne sensors and less than 16% up to 0.3 mb for rocket data. The comparison with balloon measurements near 20 mb indicates LIMS data may be high by about 8% at low latitudes. At greater pressures there is evidence of a significant bias relative to balloon data in this region.

The SAGE instrument is a four-channel sun photometer which measured solar intensity at sunrise and sunset to derive ozone, aerosol, and NO, concentrations. Absorption of 0.6 µm solar radiation by ozone allowed determination of the vertical structure of ozone to be obtained up to 30 times per day from February 1979 until September 1981. After data processing, the vertical resolution of the data is 1 km up to approximately 40 km altitude and 5 km above 40 km. The horizontal resolution is 200 to 300 km in the viewing direction and 200 km perpendicular to the field of view (CUNNOLD et al., 1984). Monthly latitudinal coverage depends on the time of year and solar geometry, but can extend from 78°S to 78°N. However, on any particular day, the vertical structure is obtained at a discrete latitude for sunrises or sunsets. Comparisons were made between balloon measurements and SAGE profiles from 18 to 28 km, and average differences were found to be less than 10% (REITER and McCORMICK, 1982; McCORMICK et al., 1984). Comparisons with rocketsondes up to 60 km yielded average differences of less than 14% (McCORMICK et al., 1984). Monthly zonal means from 4 to 20 mb over the period February 1979 through December 1979 were recently refined (October 1984) and are incorporated in the model. At these altitudes significant diurnal variations are not expected. An initial comparison between SAGE and SEUV in March-April 1979 indicated agreement to generally better than 15% between 5 and 30 mb (CUNNOLD et al., 1984). A comparative study has been performed between the three data sets SBUV, SAGE and LIMS for March 1979 (FLEIG et al., 1984a). The LIMS/SBUV comparisons are shown to be very good in the upper stratosphere, while the SBUV/SAGE comparisons are shown to be very good in the lower stratsophere. A more detailed comparison study is in progress (FLEIG et al., 1984b).

Mesospheric ozone densities have recently been made available from two limb-scanning experiments aboard the Solar Mesosphere Explorer (SME) spacecraft (which was launched October 6, 1981). The first of these, the SME-UVS, is a two-channel Ebert-Fastie spectrometer. The instrument measures the Rayleigh scattering of solar photons at the earth's limb at wavelengths of 265 nm and 296.4 nm from which the ozone profile is determined between 1.0mb and 0.07 mb (RUSCH et al., 1983). The field of view of the instrument is 3.5 km in the vertical by 35 km in the horizontal at the limb. Generally zonal means are not obtained. The primary orbits were over the longitude range from 40°W to 100°W, and the local solar time of measurement at the equator is 3 PM. An error analysis indicates total errors should range from 6% at 48 km to 15% at 68 km (1.0 to 0.1 mb) (RUSCH et al., 1983, 1984). The data chosen for the model is over the range 0.5 mb at 0.07 mb over the period January 1982 through December 1983.

The second SME experiment, SME-IR, is a near-infrared experiment that measures 1.27 µm airglow from which ozone densities from 50 to 90 km are deduced. The dayglow is principally associated with photodissociation of ozone (THOMAS et al., 1983a). Results from this experiment agree well with the SME-UVS experiment and with KRUEGER and MINZNER (1976). THOMAS et al. (1984a) describe the error analysis of this experiment in some detail. Random errors are estimated to be less than 10% from 50 to 82 km, and increase to 20% at 90 km. Systematic errors are estimated to be 15% but could be as high as 50%. The

data used for the model are monthly means over the range 0.5 mb to 0.003 mb and over the period January 1982 through December 1983. The local solar time of the measurements is again about 3 PM. Latitudinal coverage is consistent with the illuminated earth, and longitudinal coverage is principally from 40 W to 100°W. Reviews including other measurements of mesospheric ozone are found in VALLANCE JONES (1973), THOMAS (1980), NOKON (1982), VAUGHN (1984), and ALLEN et al. (1984). Ozone measurements made in the Aladdin program (WEEKS et al., 1978) by several techniques on June 29-30, 1974 are in agreement with this model below 70 km. Above 75 km Aladdin ozone is a factor of 2-3 lower than SME-IR. It is very possible that this is a real ozone variation (R. Thomas, personal communication, 1984).

Other satellite instruments which have obtained measurements of the vertical structure of ozone include the Nimbus 4 BUV experiment (HEATH et al., 1973) and the Nimbus 6 Limb Radiance Inversion Radiometer (LRIR) (GILLE et al., 1980). Since the Nimbus 4 BUV experiment had problems with a serious drift in bias, the Nimbus 7 SBUV data were considered to be a better choice for the model. The Nimbus 7 LIMS is generally considered an improvement over the Nimbus 6 LRIR experiment and was therefore chosen for the model.

The models of total column ozone given here are based on 4 years of Nimbus 7 TOMS measurements. The TOMS instrument is used to determine total column ozone by measuring backscattered solar ultraviolet radiation attenuated by ozone employing a simple monochrometer whose instantaneous field of view scans through the subsatellite point and perpendicular to the orbital plane. Backscattered and direct solar radiation are sampled at six wavelengths from 312.5 mm to 380 mm. The resolution of ozone measurements is about 50 km in the horizontal. For these studies the first 4 years of TOMS data were employed (November 1978 - September 1982) using daily zonal averages every 5 deg in latitude over the illuminated portion of the earth. Comparisons of TOMS data with ground-based Dobson and M-83 data have shown a retrieved precision of better than 2% and biases of 6% where the TOMS measurements have lower values than the Dobson measurements (BHARTIA et al., 1984a). There are indications that the absorption coefficients assumed in the TOMS experiments are somewhat in error and may be updated in the near future (KLENK et al., 1984). Global measurements of total ozone from backscattered ultraviolet measurements have also been obtained from the Nimbus 4 Backscattered Ultraviolet (BUV) and the Nimbus 7 SBUV experiments. The TOMS experiment, however, obtains more measurements per day than the other two and does not appear to have the serious drift problems which occurred on the Nimbus 4 BUV experiment. Infrared experiments which measure total column ozone from absorption of 9.6 µm radiation have included the Nimbus 4 Infrared Interferometer Spectrometer (IRIS), the DMSP Multifilter Radiometers (MFR), and the ongoing Tiros Operation Vertical Sounders (TOVS). A study of the relative biases between a limited amount of the TOMS, MFR, TOVS and SBUV results has been performed recently (LOVILL and ELLIS, 1983) showing excellent global average agreement between the TOMS and MFR (3%) but not as good agreement between SBUV and MFR (5) or between TOVS and MFR (7%), where in each case MFR gave a lower value for total ozone. Significant latitudinal biases have been noted in the IRIS data (PRABHAKARA et al., 1976; PRIOR and CZA, 1978).

3. MODELS OF TOTAL COLUMN OZONE

The monthly latitudinal models of total column ozone are based on the archived first 4 years of data from the Nimbus 7 TOMS experiment. The total column ozone values tabulated here are 6.4% higher than the TOMS data to be in accord with Dobson measurements (BHARTIA et al., 1984a). Shown in Figure 1 is total column ozone in Dobson units (the Dobson unit is defined as 10⁻⁵ meters of ozone at 0°C and at standard sea level pressure) as a function of latitude and month. Note the high values in mid and high latitudes in spring in the

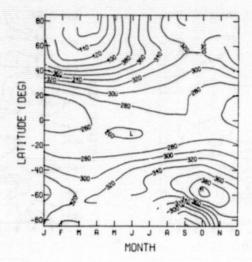


Figure 1. Zonal mean of total column ozone (Dobson units) as a function of latitude and month.

Northern Hemisphere and at midlatitudes in local spring in the Southern Hemisphere. Shown in Figure 2 is the standard deviation in percent of individual czone measurements relative to the zonal mean obtained each month for a 1-year period (November 1978 - October 1979). A comparison of monthly ozone values from year to year over the 4-year period (November 1978 - September 1982) gives an approximate idea of patterns of interannual variability in total ozone. Shown in Figure 3 is the interannual variability expressed as standard deviation (in percent) relative to 4-year means as a function of latitude and month. The variations are generally less than 4% (except near October, 80 °S) and are strongly related to quasi-biennial variation discussed briefly in the section "Other Ozone Variations."

Shown in Table 3 is a tabulation of the latitudinal variation of total column ozone in Dobson units for each month based on the dayside observations of ozone over the 4-year period. The blanks indicate no measurements were available.

4. MODELS OF VERTICAL STRUCTURE OF OZONE

As described in the section "Satellite Data for Reference Models," the vertical structure models of monthly latitudinal variations are based on the SBUV, LIMS, SAGE, SME-UVS and SME-IR data tabulated in Table 2. The 4-year mean of the SBUV data was given a weight of 2 due to the combination of extensive spatial and temporal coverage, while the other shorter data sets were each given a weight of 1.

Although there is interannual variability, comparison of the SBUV data over the 4-year period of measurements shows a remarkable similarity of structure from year to year. For example, shown in Figure 4 is the vertical structure at 0°, 20°N, 40°N and 60°N for November of 1978, 1979, 1980 and 1981. Note how the 0° and 20°N profiles come together near 4 mb. The 60°N profile changes in each case from the lowest profile at 4 mb to the highest at 1.5 mb.

Shown in Figure 5 is the interannual variability of zonal mean ozone expressed as standard deviation (in percent) relative to the mean of 4 years of

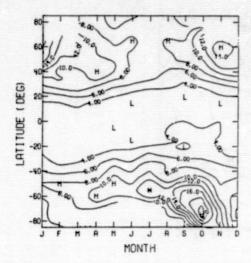


Figure 2. Standard deviation (percent) from zonal mean of total column ozone for period January 1979 through December 1979 (Nimbus 7 TOMS data).

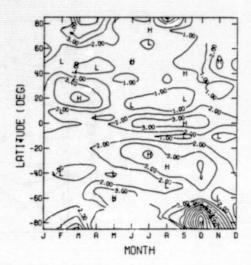


Figure 3. Interannual variability of total column ozone expressed as yearly standard deviation (percent) from 4-year zonal means (Nimbus 7 TOMS data).

Table 3. Zonal mean total column ozone (Dobson units).

		HTMCM												
LAT	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	HOV	DE		
85.			471	471	415	375	336	314	286					
80.			474	469	418	374	335	311	293					
75.		437	464	466	419	373	335	311	304	302				
70.		440	463	459	419	372	337	316	310	312	316			
65.	399	436	455	447	413	370	341	323	315	318	335			
60.	395	432	445	435	409	375	349	329	320	320	335	36		
55.	393	429	437	425	405	378	353	333	320	320	330	35		
50.	390	422	424	413	398	375	349	329	316	314	325	35		
45.	379	405	405	398	385	363	338	321	309	305	314	34		
40.	357	377	360	376	366	344	324	312	302	293	299	32		
35.	325	341	350	351	345	326	312	306	297	285	286	30		
30.	294	306	319	327	327	314	305	300	292	282	278	26		
25.	271	281	293	307	310	304	298	244	286	277	272	26		
20.	257	263	274	289	294	293	291	268	282	272	266	25		
15.	250	253	262	277	282	284	286	286	282	270	263	25		
10.	248	248	256	269	274	278	282	284	282	269	262	25		
	249	250	257	264	266	271	276	280	280	266	260	25		
0.	253	252	257	261	262	265	270	275	278	265	262	25		
-5.	257	256	259	260	260	261	264	270	275	267	266	26		
10.	262	260	262	261	259	258	201	267	272	272	272	26		
15.	268	264	264	262	261	260	263	269	275	279	280	27		
20.	273	267	266	265	266	260	270	276	284	290	289	28		
25.	280	273	271	273	274	276	281	290	298	303	300	28		
30.	289	280	279	281	283	291	298	309	316	320	313	30		
35.	298	288	286	286	294	308	317	330	335	338	326	31		
40.	308	297	292	291	305	322	333	346	351	357	338	32		
45.	322	305	299	299	315	329	343	356	363	374	353	33		
·50 ·	337	310	307	308	321	331	344	358	370	391	369	35		
55.	347	325	314	316	324	331	341	354	371	406	384	36		
-60.	347	328	319	320	326	340	347	341	356	405	393	36		
65.	340	327	319	322	324		343	328	326	377	391	36		
70.	333	319	315	315				309	294	330	379	36		
75.	327	308	307	305				297	270	299	360	36		
-80.	322	302	302						255	276	348	35		
-85.	319	297	297						232	261	344	35		

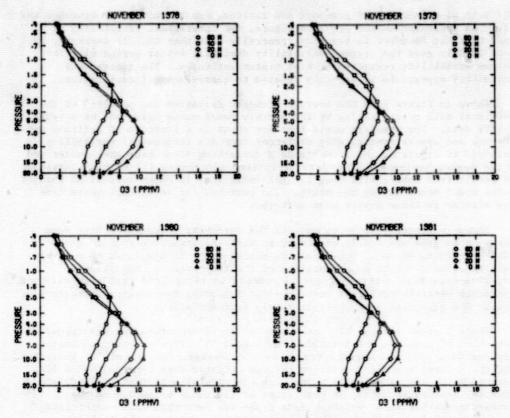


Figure 4. Similarity of ozone vertical structure in November from year to year (Nimbus 7 SBUV data).

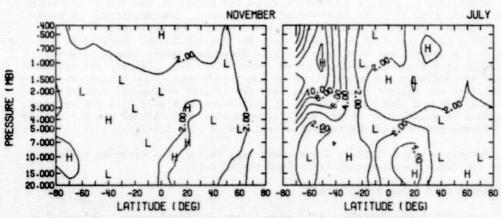


Figure 5. Interannual variability of ozone vertical structure expressed as yearly standard deviation (percent) from 4-year zonal means for the months of November and July (Nimbus 7 SBUV data).

SBUV data as a function of pressure and latitude for the months of November and July. As indicated in the previous figure, the interannual variability of zonal means in November is very low, generally less than 4%. In contrast, the month of July gave the largest variability over this 4-year period with the maximum variability occurring at high winter latitudes. The interannual variability appears to be strongly related to quasi-biennial oscillations.

Shown in Figure 6 is the average standard deviation (in percent) of the individual data points making up the monthly zonal means based on the 4 years of SBUV data. The standard deviations are shown as a function of latitude and pressure and appear considerably different from the interannual variability displayed in Figure 5. Minimum standard deviations occur near the equator and in the summer hemisphere. Standard deviations can exceed 15% at high latitudes and result from substantial longitudinal variations in ozone as well as changes in the zonal means during the month. The patterns for individual years look very similar to these 4-year mean patterns.

Shown in Figure 7 is an example of the agreement between the five data sets used to generate models of the ozone vertical structure from 20 mb to 0.003 mb (>25 to 90 km). Note that the mixing ratio is displayed on a log scale to allow accurate representation of the two orders of magnitude variation over this altitude range. It should be recognized that each data set represents entirely different techniques of measuring the vertical structure of ozone. The agreement shown here is fairly representative.

Table 4 gives the monthly zonal mean ozone volume mixing ratios (ppmv) as a function of pressure and latitude. The symbol "A" after an entry indicates only one data type was used to determine the average. The symbol "B" indicates that the percent standard deviation between weighted data types exceeded 10%. A dashed entry indicates zonal means were not available at that latitude and pressure. As may be noted, in most cases at altitudes below 0.4 mb the standard deviation among weighted data types was less than 10%. Considering the difference in techniques, this is noteworthy. Owing to the lack of longitudinal coverage above 0.4 mb and the somewhat larger differences between data types, the model above 0.4 mb should be considered only provisional. Shown in Figure 8 are the ozone distributions for the equinox and solstice months.

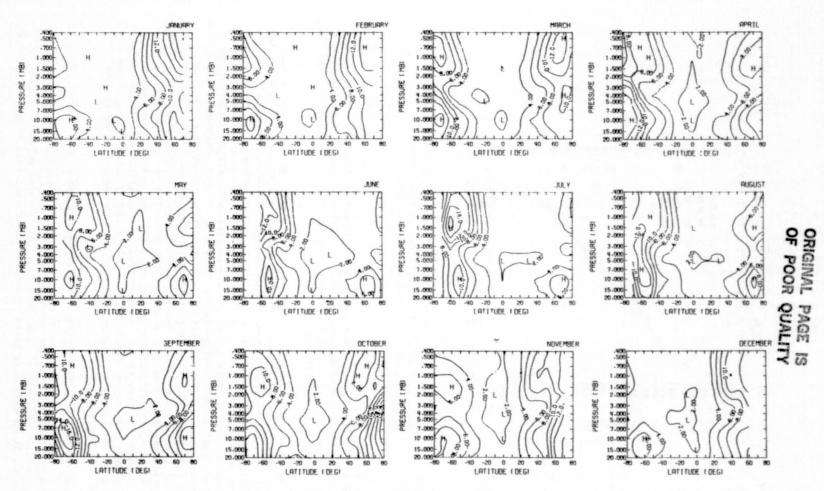
Comparison of entries in Table 4 shows the nature of the annual and semiannual variations of ozone in the middle atmosphere. The amplitudes of annual
variations are generally highest at high latitudes, and amplitudes are
especially high near 15-5 mb, 2.0-0.5 mb, and above 0.03 mb. Amplitudes are
high at low and midlatitudes near 0.1 mb. There is a sharp change in phase
near 4 mb with maximum ozone values in summer below this altitude and maximum
values in winter in the upper stratosphere. A substantial semiannual variation
occurs near the equator from 15-3 mb, but the largest semiannual variation
occurs at mid and high latitudes near 1 mb. Shown in Figure 9 is the vertical
structure of global mean ozone (weighted by cosine of latitude) and the maximum
and minimum extremes of the tabulated profiles at each level.

For convenience, Table 5 lists conversion factors for deriving common units for ozone measurements from volume mixing ratio.

5. ANNUAL MEAN MIDLATITUDE MODEL

The KRUEGER and MINZNER (1976) annual mean ozone reference model of 45° N based on balloon and rocket data is incorporated in this set of reference models. This model has proven to be very useful and was included in the U. S. Standard Atmosphere, 1976. Data from rocket soundings in the latitude range of 45° N \pm 15° N, results of balloon soundings at latitudes from 41° N to 47° N, and

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Figure 6. Average monthly standard deviation (percent) from zonal mean ozone (Nimbus 7 SBUV data).

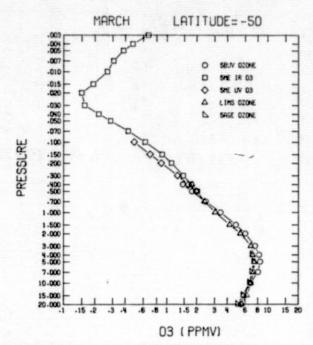


Figure 7. Comparison of measurements from five satellite experiments of zonal mean ozone volume mixing ratios for March, 50°S.

latitude gradients from Nimbus 4 BUV observations have been combined to give this estimate of the annual mean ozone concentration and its variability at heights up to 74 km for an effective latitude of 45°N. The tabulation of this model is found in KRUEGER and MINZNER (1976).

Shown in Figure 10a is a comparison of the vertical structure of the annual mean volume mixing ratio given by Krueger and Minzner with that of the annual mean determined by averaging the monthly values at 40 and 50 °N based on satellite data given in Table 4. As may be detected, there is excellent agreement between the balloon and rocket measurement model and the satellite measurement model. This agreement is even more noteworthy considering the lack of longitudinal coverage in the balloon and rocket measurement model. Shown in Figure 10b are the percent differences of the Krueger and Minzner model from the annual mean model based on Table 4 values. Below altitudes of 0.2 mb, the agreement at all levels is within 10%. Below altitudes of 2.0 mb, the agreement at all levels is within 5%. Above 0.2 mb, differences as large as 45% occur, but all differences at all levels are within the error bars indicated by the Krueger and Minzner model. It is interesting to note that both models give maximum mixing ratios near 5 mb. Minimum mixing ratios occur near 0.04 mb for the Krueger and Minzner model and near 0.03 mb for the satellite data model.

6. MODELS OF TOTAL OZONE-VERTICAL STRUCTURE RELATION

As mentioned in the introduction, MATEER et al. (1980) developed models of the vertical structure of ozone as a function of total column ozone and latitude. The models were based on balloon and rocket data. These models of

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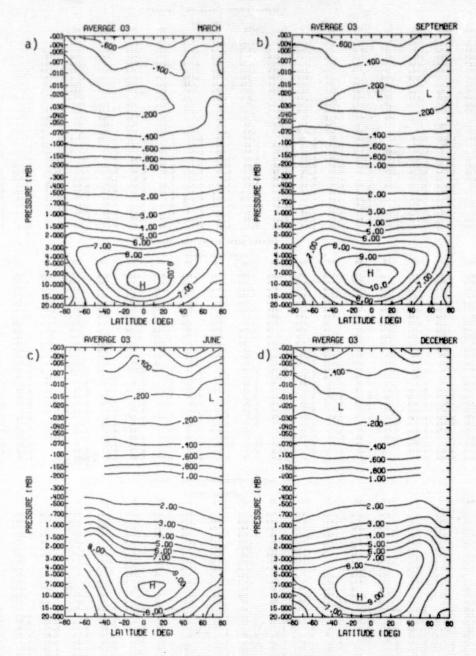


Figure 8. Monthly zonal mean ozone volume mixing ratios (ppmv) as function of latitude (deg) and pressure (mb) for (a) March, (b) September, (c) June, and (d) December.

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Table 4. Zonal mean ozone volume mixing ratios (ppmv).

							AVE	AGE DZO	NE (1V) FOR	JANUAR	*					
P(88)	-80	-70	-60	-50	-40	-30	-20	-10	TITUDE		**	10			**	**	
.003	.594	.724	.*04	.614	.73A	-50	.584	-10	.544	.524	.524	30	.014	.844	1.084	70	**
.004	.39A	.344	.584	.63A	.50A	.54A	.50A	.474 .454	.464	. 43A	.42A	.50A	.62A	-66A	. 05A		::
.010	.18A	.21A	.28A	.344	.36A	.36A	.38A	.40A	.40A	.39A	.344 .334	.32A	.32A	.29A	.31A		::
.015	.134 .154	.15A	.16A	-16A	-16A	-164 -134	.10A	.20A	.21A	. 23A	.26A	.28A	.27A	.244	.24A	**	**
.030	.19A	.20A	.19a .234	.18a	-16A	-15A	-15A	-16A	-17A	.17A	.18A	.20A	.25A	-33A	.494		
.050	.28A	.29A	.28A	.26A	.25A	.24A	.23A	.24A	.24A	. 24A	. 26A	.284 .434	.32A	.39A	.544		
.100	.73	.638	.50	.76	.528	.53	.53	.53	.51	.51	.738	.538	.508	.568	.768		
.200	1.09	1.13	1.20	1.26	1.33	1.018	1.35	.93	1.24	1.25	1.298	1.378	1.028	1.058	1.110	::	
.400	1.21	1.27	1.36	1.50	1.59	1.65	1.63	1.56	1.54	1.56	1.59	1.008	1.798	1.908	1.998	1.77	1.794
1.000	1.72A	1.62A	2.50	2.12	2.26	3.02	2.38	3.00	2.33	3.11	2.36	3.42	3.81	3.92	2.80	3.528	2.224
2.000	3.09A	3.19A	3.37	3.59	3.64	5.17	9.40	5.53	3.57	5.61	3.77	6.90	5.32	5.36	5.69	3.308	1.754
3.000	5.96A 6.75A	5.98A	7.01	7.50	7.96	7.15	7.52	7.77	9.048	7.71	7.65	7.56	7.33	6.92	6.25	5.83	1.064
7.000	6.72A	7.00A	7.42	8.09	8.68	9.18	9.62	9.958	9.788	9.448	8.91	7.98	7.57	6.90	5.90	5.66	5.39A 5.27A
15.000	4.62A	5.41A	5.59	7.50	7.24	7.80	9.57	9.99	9.95	7.93	7.17	7.40	6.66	5.04	5.39	5.28	4.91A
20.000	4.054	4.424	5.25	5.90	6.30	6.52	0.63	6.71	6.61	0.34	5.99	5.77	5.04	5.23	4.75	4.61	4.144
							AVE	AGE DZ			FEBRUA	RY					
P(M8)	-60	-70	-60	-50	-40	-30	-20	-10	0	10	50	30	+0	50	60	70	*0
.003	.424 .284	.394 .394	.64A	.50A	.614 .474	.59A .47A	.62A	.69A .55A	.74A .57A	.72A .57A	.56A	.54A	.53A	.734 .564	A58.	.984 .724	==
.007	-144	-194	.24A	.29A	.31A	.37A	.42 A	.434 .354	.354	.45A	.42A	.374 .354	.32A	.30A	.27A	.224	::
.015	-14A	-144	-144	-144	.16A	-194	.21A	.22A	.23A	.25A	.284 .214	.31A	.32A	.30A	.26A	.12A	
.030	.21A	.20A	.194	.18A	.164	.164	.16A	.16A .20A	.17A	.17A	.18a .21A	.19A	.24A	.29A	.37A	.33A	
.050	.31A	.30A	.30A	.28A	.26A	.25A	.24A	.244	.24A	.254	. 26A	.29A	.31A	.344	.42A	.48A	-:-
-100	.618	.78	.76	.568	.548	.53	.78	.76	.52	.73	. 52	.528	.558	.558	.618	.618	-:
.300	1.16	1.19	1.25	1.32	1.038	1.038	1.35	1.20	1.26	1.28	1.318	1.328	1.338	1.368	.988 1.428	1.038	-:
.500	1.34	1.30	1.72	1.568	1.648	1.67	1.62	1.56	1.55	1.57	1.59	1.62	2.02	1.77	1.00	2.02	2.164
1.000	2.08A	2.06A 2.78A	2.14	2.25	3.07	3.15	3.09	2.27	2.25	2.28	2.33	3.33	3.70	2.92	3.04	3.02	3.274
2.000	4.02A	3.90A	3.86	3.98	5.23	5.38	5.39	5.25	5.18	5.27	5.49	5.95	5.34	5.70	6.33	5.17	4.11.4
1.000	0.16A	6.40A	7.26	7.44	7.61	7.26	8.75	8.98	8.90	8.76	7.40	7.74	7.80	7.38	6.83	6.33	5.694
7.000	5.39A	6.90A	7.33	7.04	6.56	9.53 .	10.09	10.67	10.65	10.28	9.59	6.65	7.59	7.21	6.70	6.42	6.304
15.000	3.534	5.00A	5.40	7.16	6.02	7.75	0.16	8.54	8.59	8.10	7.57	7.90	6.90	5.89	5.97	5.89	5.77A
20.060	3.764	4.424	5.14	5.57	6.08	6.49	0.04	6.78	6.72	6.43	6.17	5.88	5.69	5.55	5.24	5.10	5.304
							AVE	RAGE OZ	ONE (PP	HV) FOR	MARCH						
P(MB)	-80	-70	-60	-50	-40	+30	-20	-10	TITUDE	10	20	30	40	50	60	70	60
.003	.33A	.34A	.65A	.67A	.74A	.82A	.78A	.72A	.71A	.75A	. 80A	.79A	490.	.58A	.55A	.60A	.554
.005	.21A	.28A	455.	.30A	.404	.55A	.52 4	.49A	.47A	494	.534	.524	.44A	.37A	.33A	.324	.244
.010	-12A	.10A	.21A	.27A	.234	.38A	.36A	.33A	.324 A05.	.33A	.37A	.41A	.41A	.37A	.32A	.25A	-19A
.030	.15A	-194	.14A	-154 -164	.17A	.17A	.17A	.16A	.17A	.17A	-19A	.25A	.31A	.37A	.39A	.39A	.36A
.050	.26A	.25A	.23A	4524 4624	.21 A	.20A	.21 A	.21A	.20A	.20A	.22A	AES.	.24A	.28A	.36A	.46A	.504
.100	.60	:57	.43A	.568	.40A	.374	.36 A	.344	.33A	.344	.384	.528	.42A	:578	.47A	.608	.544
.150	.97	.78	.798	1.008	1.008	.788	.78	.784	:97	.76	.938	.748	.768	.768	.758	.768	.778
.400	1.63	1.60	1.60	1.638	1.058	1.37	1.34	1.32	1.34	1.33	1.30	1.298	1.318	1.308	1.278	1.308	1.368
.500 .700	2.86A	2.684	2.47	2.44	2.44	2.40	2.34	2.31	2.30	2.32	2.38	1.92	2.46	2.54	2.02	2.15	3.03
1.500	3.98A 3.33A	3.80A 5.35A	3.41	3.30	3.25	3.18	4.16	3.94	3.07	3.96	4.21	4.54	4.86	3.58	3.88	5.00	5.38
3.000	5.93A	6.90A	7.17	7.29	7.34	7.41	7.30	5.00	4.90	5.04	7.24	7.55	7.98	6.60	7.78	7.23	6.13
5.000	5.83A 5.45A	6.67A	7.42	7.00	7.98	8.85	9.20	9.37	9.33	9.32	9.26	9.01	8.74	8.27	7.73	7.20	6.60
7.000 10.000 15.000	4.80A 3.71A 3.47A	5.74A	5.72	6.77	7.69	8.69	9.72	10.46	10.42	10.40	9.75	0.56	7.55	6.90	7.08	5.69	5.74
20.000	3.80A	4.05A	5.01	5.42	5.67	6.29	6.60	6.68	6.96	6.77	6.56	7.28	5.65	5.62	5.68	5.076	5.178

A - ONLY ONE DATA SET USED IN AVERAGE B - PERCENT STANDARD DEVIATION OF DATA TYPES IS GREATER THAN 10%

lable 4 continued.		Ta	ble	4	continued.
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							AVER	AGE OTO			APRIL						
	-80	-70	-60	-50	-+0	-30	-20	-10	TITUDE	10	20	30	40	50	60	70	*0
.003	=	::	:714	.834 .564	.934	.924 .704	.63A	. 50A	.814 .974	. 85A	.96A	1.05A	.88A	.61A	.52A	.564	.634
.005	**	**	.354		.554	. 57A	. 514	.474	.464	. 514	.64A	.74A	.554	.47A	.39A	.39A	.424
.010	::		.27A	.334	.344	:344	.334	. 35 A	.354	. 35A	. 394	.474	.514	.484	. 434	.384	.284
.015	=	::	.30A	.27A	.184	.214	.20A	.21A	.22A	.22A	.24A	.32A	.40A	.344	.42A	.39A	.304
.030	-	::	.25A	.19A	.16A	.17A	471.	.17A	.18A	.18A	.18A	.20A	455.	.24A	.26A	.31A	.364
.050	**		.314	.294	.28A	.28A	.27A	.26A	.264	.27A	.28A	.29A	.30A	.31 A	.334	.35A	.414
.100	=	.584	:43	.588	.57	.57	. 39 A	.57	.364	. 54	.54	. 538	.538	.548	+568	.578	.598
.150	=	.75A	1.05	1.058	1.028	1.02	1.03	1.03	1.00	.78	.788	.778	.768	.758	.758	.758	.758
.300	1.004	1.90	1.51	1.79	1.43	1.40	1.40	1.39	1.37	1.36	1.35	1.328	1.298	1.258	1.228	1.218	1.95
.500	2.53A 3.55A	2.40	3.068	2.17	2.04	1.96	2.39	2.38	2.30	2.36	2.42	1.92	2.36	1.60	2.31	2.40	2.50
1.000	4.844	3.46A	4.376	4.02	3.64	3.33	3.13	3.04	3.02	3.04	3.12	3.19	3.12	3.06	3.14	3.30	3.46
2.000	6.14A	7.03A	7.03	5.75	5.21	3.92	5.43	5.10	5.02	5.12	5.33	5.54	5.61	5.00	5.84	5.94	5.01
4.000	5.45A	6.70A	7.35	7.72	7.77 6.01	7.67	7.35	6.95	6.85	7.01	7.28	6.37	7.61	7.65	7.61	7.30	6.68
5.000	5.064	5.72A	6.70	7.48	0.16	8.84	9.25	9.05	8.84	9.05	9.16	9.00	0.97	8.80	8.27	7.50	6.60
7.000	3.544	5.024 4.06A	5.17	6.12	7.79	0.30	9.46	10.37	10.01	10.34	9.71	8.96	6.12	7.44	7.56	6.08	5.44
20.000	3.37A	3.80A	4.76	5.50	5.56	7.18	0.05	7.02	7.15	8.77	6.28	6.53	6.91	5.70	5.72	5.168	4.785
						-											
							AVER	AGE DZO	TITUDE		MAY						
P(88)	-00	-70	-60	-50	-40	-30	-20	-10	0	10	20	30	40	50	60	70	60
.003	=	::	::	1.00A	1.02A	.92A	.76A	.68A	.67A	.67A	.76A	. 67A	.88A	.79A	.66A	.58A	.50A
.005			**	.514 .344	.57A	.54A	.47A	.46A	.45A	. 468	.54A	.51A	.66A	.59A	.50A	.42A	.264
.010		::		.27A	.30A	.32A	.37A	.40A	.414	. 38A	. 38A	.38A	.38A	.36A	.32A	.27A	.224
.015			=	.23A	.22A	.22A	.24A	.26A	.25A	.174	. 25A	.194	.194	405.	.19A	-19A	-16A
.030		::		.19A	.18A	.17A	.17A	.17A	.17A	.18A	.19A	.19A	.20A	.21A	.20A	.21A	*15.
.050			::	.29A	.304	.29A	.28A	.28A	.27A	. 28A	. 284	.28A	.29A	.29A	.30A	ASP.	.444
.100	**	**		.60	. 59	.59	.60	.59	.57	.57	.57	.54	538	.55	. 56	.56	.76
.150	::	::	==	1.130	1.068	1.048	1.06	1.06	1.03	1.03	1.04	1.018	. 998	.978	. 95	.92	.90
.400	-	2.134	2.01	2.02	1.52	1.70	1.43	1.42	1.70	1.69	1.68	1.37	1.618	1.558	1.488	1.18	1.15
.500	=	2.70A 3.79A	3.628	3.458	2.23	2.02	2.47	2.44	2.44	2.43	1.95	2.41	2.33	1.79	2.13	2.05	2.00
1.000	**	5.26A	5.138	5.008	4.26	3.60	3.25	3.14	3.11	3.11	3.12	3.09	4.05	3.91	3.80	3.72	3.81
2.000	::	6.85A 7.20A	7.268	7.798	7.26	5.14	5.62	5.30	5.22	5.23	5.30	7.27	5.20	5.05	4.95	4.82	4.94
1.000	::	6.60A	6.80	7.61	7.90	7.93	8.10	7.10	7.04	8.30	7.25		7.19	7.07	7.53	7.19	6.40
7.000	=	3.574	5.79	6.95	7.81	0.51	9.17	9.54	9.59	9.10	9.76	9.41	9.00	1.77 7.77	7.96	7.30	6.76
10.000	=	4.22A	4.62	5.68	5.98	7.00	7.79	9.92	8.79	9.97	9.56	7.00	7.17	7.77	7.01	5.03	5.17
20.000		4.11A	4.37	5.02	5.51	6.00	6.51	6.86	7.08	7.28	7.04	6.73	6.31	5.90	5.39	4.75	4.16
							AVE	AGE OZO	NE LPP	W) FOR	JUNE						
	-80	-70	-60	-50	-+0	-30	-20	-10	TITUDE	10	20	30	40	50	60	70	80
.003	=	=	=	-	. 824	.79A	.63A	.48A	49A	. 56A	.64A	.77A	.92A	.98A	.89A	.73A	454.
.005					.514	.50A	.424	.36A	.404	. 434	. 46A	. 55A	.65A	.63A	.49A	.38A	.334
.010	::	::		=	.36A	.38A	.36A	.30A	.38A	49E.	. 27A	.284	404.	.25A	.20A	.18A	.174
.015	-				.20A	.224	.21A	-19A	.18A	.18A	.15A	-18A	.16A	.18A	.17A	.17A	-16A
.010	7	::	==	::	.17A	.18A	.17A	.17A	.17A	.184	.17A	.17A	.19A	405.	A05.	405.	.214
.050	**	**		**	.314	.32A	. 30 A	.27A	.27A	.27A	. 264	+28A	485.	.26A	40A	.29A	.294
.100		::	::	::	.45A	.598	.43A	.40A	.884	.61	. 39A	.59	.40A	.58	.628	.638	.608
.150	=	==	::		1.058	1.058	1.078	1.08	1.08	1.09	1.11	1.09	1.04	1.01	. 83	.82	.93
.300	::	=		1.924	1.51	1.66	1.45	1.47	1.40	1.48	1.48	1.44	1.39	1.33	1.27	1.21	1.16
.500	**	**	1.07A 2.54A	2.50A	2.26	2.02	1.98	2.01	2.01	1.99	1.97	1.93	1.84	1.75	1.64 1.99A	1.54 1.85A	1.46
1.000	**	::	3.68A 5.31A	3.08A	3.09A	3.724	2.52A 3.40A	3.284	3.25A	2.47A 3.23A	474.5 455.6	3.11A	2.28A 2.94A	2.144	2.54A	2.35A	2.744
2.000	=	::	7.154	7.67A	6.61A 7.766	5.32A 6.53A	4.70A 5.85A	4.45A 5.57A	4.37A	4.34A 5.47A	5.49A	4.16A 5.32A	3.96A	3.72A	3.43A	3.20A	4.214
3.000	=	=	6.72A	7.86A 7.19A	7.49	7.97A 8.17	7.57A 8.56A	7.42A 8.62A	7.40A	7.43A 6.74A	7.50A	7.33A 8.62A	7.13A 8.39A	6.87A 7.68	6.50A 7.198	6.18A	7.024
5.000	**		5.56A	6.65A	7.82	8.37	9.00A	9.31A	9.434	9.548	9.564	9.33A	9.014	8.29	7.66	7.264	6.994
7.000	::	=	5.00A	5.90A 5.25A	7.26	7.70	9.31A 8.77A	9.88A	4.984	10.03A	9.694	9.714	9.16A	7.66	0.83	7.08A	5.204
20.000	=	::	4.09A	4.84A	5.48	5.78	7.46A	8.21A	8.67A	7.12A	6.28A	7.71A	7.00A	5.76	5.69	4.68A	4.104

A - ONLY ONE DATA SET USED IN AVERAGE B - PERCENT STANDARD DEVIATION OF DATA TYPES IS GREATER THAN 10%

Table 4 continued.

							AVE	**56 020	NE 1999	W) FOR	JULY						
								LA	111406	10661							
P(M8)	-60	-70	-60	-10	-+0	-30	-20	-10	0	10	50	30	40	50	60	70	10
.003	**		**		.534	.524	.574	.104	.404	. 51A	.514	.70A	.734	.674	.71A	.55A	.194
.007	**	**	**	.224	.104	.334	.344	.344	.354	. 364	. 104	.344	.50A	.304	.31A	465.	.104
.010	::	::	::	401.	405.	.05.	.29A	.274 .174	.104	.164	.254	.104	.174	.234	-104	-174	-154
.020	**	::	**	405.	-174	-154	·154	-174	-174	-144	.164	-144	.15A	401.	.174 .05.	.17A	-154
.010	::	::	::	405.	.234	A55.	455.	425.	425.	405.	.204	405.	.224	445.	445. APS.	.234	.234
.370	::	::	::	.39	.47A	.464	. 414	. 34A	.384	.37A	. 364	.374	.404	.404	404. 850.	.394	.194
.150	::	::		1.15	1.099	1.178	1.099	1.06	1.05	1.07	1.12	1.13	1.09	1.04	1.00	.828	.775
.300		**		1.58	1.53	1.51	1.47	1.45	1.44	1.45	1.50	1.51	1.45	1.36	1.294	1.22	1.10
.500	**	1.904	1.694	2.418	18.1	2.00	2.01	2.00	1.08	1.98	1.09	1.69	1.62	1.75	1.42	1.33	1.445
1.000	::	3.514	2.97A	4.074	4.964	2.67A 3.74A	3. ***	3.30A	3.254	3.254	3.294	2.50A 3.25A	2.38A 3.08A	2.194	2.01A	2.364	2.714
2.300		5.55A	0.774	4.76A	7.354	5.324	5.99A	5.73A	4.43A	5.014	1.45A	5.524	5.264	450.4	3.49A	4.244	1.104
4.000	::	5.41A	0.744	7.554	7.70	7.75A	7.76A	7.69A	7.55A	7.00A	7.70A	7.50A	7.224	6.06A	454.0	6.03A	5.754
7.000	::	5.37A 5.00A	5.814	6.74A	7.76	8.684	9.134	9.494	9.034	9.724	7.654	9.404	9.03A	8.55A	7.35A 7.88A	7.07A	6.794
15.300	::	1.554 3.564	1.004	1.424	5.85	7.634	8.71A 7.384		9.794	10.17A	9.70A	9.10A 7.76A	7.064	7.544	0.004	3.544	4.534
20.000		3.704	3. 95A	4.664	5.41	5.70A	0.15A	0.044	7.134	7.254	6.914	6.57A	6.234	5.89A	5.35A	4.514	4.054
							AVE	AGE DZO	-	4) FOR	AUGUS	T					
P(M8)	-80	-70	-60	-50	-40	-30	-20	-10 L	TITUDE	10661	20	30	40	50	60	70	80
.003			.564	.674	. 694	.874	-63A	.624	.01A	.624	.664	.704	.694	.674	.094	.624	.454
.004		::	.344	.51A	. 554	.534	.494	.484	.484	. 494	. 53A	. 56A	. 544	45¢.	.524	.45A	.32A
.007		==	.27A	.30A	. 33A	.35A	- 36 A	.37A	.37A	. 37A	495.	.36A	.32A	40E.	.28A	.23A	-19A
.015	=	::	.25A	AES.	.23A	.23A	.22 A	-19A	-104	.18A	-18A	-17A	.15A	-15A	.14A	.14A	-14A
.030	=		.23A	.19A	.17A	-17A	. 18A	-17A	.16A	.17A	481.	.17A	.17A	.18A	.19A	.19A	.19A
.050	=	=	. 33A	.30A	.32A	.31A	.28A	.26A	.25A	. 264	. 26A	. 25A	.26A	404.	A94.	.29A	.29A
.100	**	**	.56	.568	.608	.000	.58	.56	.56	.57	. 36A	.364	.56	.57	. 56A	.59	.588
.150		::	.78	1.068	1.108	1.116	1.008	1.048	1.03	1.03	1.04	1.06	1.068	1.038	. 98	.78	.76
.400		1.594	1.39	1.78	1.568	1.758	1.48	1.66	1.41	1.39	1.42	1.45	1.45	1.36	1.29	1.22	1.17
.700		1.93A 2.57A	2.00	2.864	2.874	2.10 2.00A	2.504	2.444	2.434	2.444	2.494	2.534	2.464	2.284	1.71 2.134	2.044	1.958
1.000	::	3.52A	3.77A 5.35A	4.13A	4.094	3.70A	3.40A	3.25A	3.20A	3.22A	3.31A	450.0	3.28A	4.05A	4.02A	2.75A 3.84A	2.64A
3.000	**	5.47A	498.0	7.10A	7.044	6.47A	7.904	7.754	5.57A 7.67A	7.69A	5.76A 7.63A	7.76A	5.63A	7.174	5.11A	4.63A	4.60A
*.000	::	5.72A	6.76A	0.07A 7.80A	8.01A	8.80A	8.96A	9.64	9.65	9.74	9.64	9.23	8.20	7.78	7.208	6.92A	6.224
7.000	::	5.15A	5.02A	7.13A	7.07A	7.934	9.64A	10.12	10.22	10.31	9.83	9.46	8.86	7.30	7.318	5.18A	1.52A
15.000	=	3.88A	4.284	5.26A	6.06A	6.72A	7.574	8.22	8.54	8.65	8.20	7.50	6.97	0.20	5.32	4.414	3.664
.0.000	-	3.694	4.084	4.884	5.441	2.754	6.234	6.60	6.04	7.05	6.77	0.44	6.13	5.66	5.02	4.514	3.014
							AVE			NV) FOR	SEPTEM	ER					
*(#8)	-80	-70	-60	-50	-40	-30	-20	-10	TITUDE	10	90	30	40	50	+0	70	80
.003	.52A	400.	. 60A	.404	.71A	.784 .624	.78A	. 80A	.80A	. 77A	.77A	.78A	.69A	.614	454.	.56A	.464
.005	.354	A85.	.364 .314	.394	.46A	.534	.534	.51A	.494	. 50A	.52A	. 544	.46A	.38A	.33A	A0E.	455.
.010	.28A	.31A	.33A	.35A	.37A	.37A	A 25.	.32A	405.	.29A	455.	.33A	A16.	.25A	.21A	-19A	-17A
.020	.30A	.31A	.26A	.24A	.22A	.19A	-17A	.17A	.17A	.16A	.17A	.17A	.17A	.16A	.15A	.16A	-18A
.040	.31A	.30A	.264	.244	*25*	.224	. 22 A	.21A	.20A	.17A	.17A	.17A	.16A	.16A	471.	.18A	.224
.070	.434	.464	.32A	.314	. 30A	.29A	. 27A	.25A	.25A	.25A	. 25A	.25A	.25A	.40A	.284	404.	-30A
.150	. 828	.60	.608	.608	.598	.568	.508	.79	.79	. 77	.75	.748	.758	.758	.738	.718	.71
.200	1.018	1.34	1.028	1.488	1.488	1.448	1.028	1.01	1.37	1.34	1.33	1.35	1.368	1.36	1.32	1.25	1.24
.500	1.568	1.58	1.63	1.72	1.728	2.01	1.04	1.63	1.62	1.60	1.59	1.60	1.598	1.578	1.94	1.52	1.99
1.000	3.344	2.434	2.55A 3.58A	2.73A 3.65A	2.69A 3.78A	2.52A 3.48A	2.42A 3.25A	2.39A 3.13A	2.38A 3.10A	2.40A	454.5	2.454	2.434	2.40A 3.37A	Z. 42A	2.474	2.524
2.000	450.4 404.0	3.36A 4.72A 3.64A	5.10A 6.21A	5.51A 6.72A	5.42A 6.71A	4.95A	1.54A 5.78A	4.29A 5.47A	1.21A	3.14A	3.234 4.484 5.694	3.33A	3.35A	4.024	3.45A	3.52A 5.00A	3.48A
3.000	450.0	6.494	7.374	8.08A	6.33A	8.17A	7.88A	7.59A	7.474	7.52A	7.754	5.88A 7.83A	7.70A	7.58A	7.39A	5.07A	5.36A
5.000	5.76A	6.59A	7.168	6.11	0.03	9.27	9.58	8.99A	8.91A 9.79A	8.94A 9.81A	458.9	9.01A	9.70A	8.35A 8.59A	7.76A	6.93A	7.774
7.000	3.424 4.574	5.01A	6.79	7.67	7.58	8.46	9.47	10.214	1C. 514	10.614	9. 61A	9.034	9.07A	8.22A	7.23A	4.71A	1.064
20.000	3.054	3.744	4.61	5.60	5.69	7.08	7.79	6.954	7.36A	8.97A 7.314	8.31A	7.62A	6.83A	5.96A 5.65A	5.12A 5.13A	4.18A	3.524
														-			

A - ONLY ONE DATA SET USED IN AVERAGE B - PERCENT STANDARD DEVIATION OF DATA TYPES IS GREATER THAN 10%

ORIGINAL PAGE IS Table 4 continued. POOR QUALITY

							AVE	AGE OZO		(V) FOR	001086						
P(MB)	-60	-70	-60	-50	-40	-10	-20	-10	TITUDE	(066)	20	30	40	50	60	70	**
.003	.584	.574	.554	.024		.974	.904	.794			. 794			.774	.694	.054	.494
.004	. 46A	.48A	.474	.52A	.70A	.80A	.73A	.624 .544	.63A	:544	.62A	.67A	.67A	.57A	:49A	:31A	.30A
.010	45E.	.40A	:434	.464	.52A	.53A	.48A	.344	.43A	.42A	.514	.42A	.40A	.34A	475.	A55.	-104
.015	.26A	.31A	.33A	.33A	.30A	405.	445. 405.	.25A	.26A	.24A	.23A	A55.	.22A	AES.	.26A	405.	445.
.030	.25A	.22A	.21A	.21A	.19A	462.	.19A	.20A	455.	.18A	.18A	.184 .224	471.	AP1.	.24A	.31A	.35A
.050	.36A	.344	.32A	.31A	454.	.29A	.294	.28A	.27A	.27A	.27A	.27A	.27A	495.	.31A	.34A	.364
.100	.59	.76	.768	.768	.758	.768	. 768	.748	.720	.738	.728	.718	.708	.56A	.708	.52	.534
.200	1.25	1.24	1.28	1.318	1.338	1.358	1.368	1.358	1.33	1.32	1.33	1.36	1.36	1.38	1.37	1.34	1.41
.500	1.75	1.76	1.52	1.57	1.90	1.98	1.00	1.61	1.62	1.60	1.92	1.608	1.038	2.08	2.19	2.25	2.408
1.000	3.01A	2.24A	2.37A 3.26A	3.374	3.30A	2.35A 3.18A	2.36A 3.12A	3.10A	3.10A	3.144	3.20A	3.30A	2.51A 3.60A	2.75A	4.24A	2.97A	3.05A
2.000	5.10A	3.34A	5.79A	4.81A	4.72A	5.614	5.50A	5.38A	5.29A	5.37A	5.61A	5.95A	5.23A 6.46A	5.77A 6.91A	7.044	5.08A	5.50A 5.91A
4.000	6.854	7.46A	7.45A	7.92A	0.13A	8.014 815.0	7.75A	7.50A	7.34A	7.38A	7.63A	7.85A 8.59	7.96A 8.20	7.70	7.56A	6.65A	3.754
7.000	6.75A	7.52A 7.34A	8.35A 8.18A	8.054	9.34A		10.48A	10.694	9.77A	9.76A	10.06	9.23	0.16	7.17	7.16A 6.47A	5.57A	5.20A
000	5.31A	6.19A	7.06A 5.73A	402.0	7.02A 6.51A 5.71A	7.34A	8 . 27A	10.42A 8.78A 7.00A	8.53	8.55	8.13	7.30	7.39 6.29 5.61	5.56	3.36A	4.50A	3.714
20.000	3.784	4.434	5.25A	5.58A	2.718	0.134	0.67A	7.004	6.83	6.83	6.56	6.12	3.01	5.26	4.964	4.354	3.004
							AVER	AGE OZO	NE (PPR	V) FOR	HOVERS						
P(r8)	-60	-70	-60	-50	-40	-30	-20	-10	TITUDE	10661	20	30	40	90	60	70	**
.003	.514	.024	.714	.774	.814	.824	.784	.76A	.824	.82A	.79A	.844	.94A	.964	.67A		=
.005	.334	.504	.504 .504	.554	.584 .584	.594	. 55A	.53A	.57A	.58A	.544	.534	.57A	.51A	.30A		::
.610	.104	.314 .234	.27A	A16.	.334 .234	.334	. 33A	.34A	A66.	. 37A	.36A	.33A	.32A	.26A	.22A	::	=
.015	.174	.17A	.18A	.19A	.19A	.19A	.20 A	.20A	.21A	.21A	.21A	.21A	A15.	.25A	.31A		
.010	.22A .27A	.21A .26A	.26A	.26A	.25A	.244	.23A	.23A	.22A	.22A	.23A	.24A	.24A	.28A	.34A		
.070	.50	.434	.43A	.43A	.42A	.42A	.414 .538	.40A	.394	.39A	.40A	.41A	.41A	.444	.46A	==	
.150	.76	.76	.768	.758	.738	.748	.758	.748	.748	. 758	.738	.728	.718	.718	.738		==
.300	1.18	1.20	1.238	1.268	1.288	1.318	1.63	1.35	1.66	1.348	1.30	1.41	1.42	1.436	1.47	1.78	1.564
.500	1.58 1.93A	1.02	2.08	2.15	1.62	2.20	2.33	2.39	2.42	2.41	2.36	2.43	2.09	2.248	3.07	3.028	1.044
1.500	2.55A	2.59A	3.72	3.82	3.89	3.97	3.00	4.12	3.12	4.19	4.30	4.73	3.80	6.16	6.108	5.698	4.144
3.000	4.004	4.69A	4.82	4.96	7.08	7.17	7.23	7.16	7.05	7.00	7.25	7.60	7.78	7.14	6.838	6.298	*.744
5.000	7.19A	7.38A	7.448	7.018	8.218	9.14	9.350	9.238	8.168	8.78	8.06	8.41	7.92	7.35	6.14	5.918	*
10.000	5.73A	7.47A	7.66	7.39	6.02	8.88	9.65	9.97	9.85	9.60	9.13	8.42	7.26	5.68	4.90	3.020	3.474 3.474
15.000	4.37A	5.07A	5.78	5.62	5.90	6.36	6.76	7.00	6.62	6.60	6.31	5.46	5.34	5.02	4.58	150	3.014
							AVE	AGE DZO	NE (PP	V) FOR	DECEMB	ER					
	-60	-70	-60	-50	-40	-30	-20	-10	TITUDE	10	20	30	40	50	60	70	
.003	.57A	.71A	.81A	.63A	.76A	.674 .564	.59A	.58A	.544 .474	.51A	.61A	.78A	.91A	.91A	==	::	::
.005	.30A	.374	.45A	.53A	.53A	.484	.45 A	.404	.45A	. 42A	.42A	.48A	.56A	.54A	=		==
.015	.154	.16A	.20A	.24A	.26A	.264	.29A	.32A	.33A	.33A	.33A	.31A	495.	.25A	::		::
.020	.174	.18A	.18A	.17A	.16A	.164 .174	-17A	.18A	.18A	.18A	.20A	.23A	.25A	.29A		::	==
.050	.26A	.26A	.25A	.25A	.24A	.22A	.21 A	.22A	.22A	.21A	455.	.25A	. 28A	-36A	=		==
.070	.41A	.424	.58	.41A	.41A	.40A	.38 A	.37A	.37A	. 37A	.41A	.46A	.50A	.478	=	::	==
.200	.78	.00	.80	.788	.788	1.018	1.028	.78	.75	.758	.768	1.008	1.038	1.058			**
.300	1.16	1.32	1.25	1.50	1.328	1.365	1.41	1.37	1.65	1.33	1.388	1.458	1.748	1.648	1.64	1.494	1.464
.700	1.714	1.53 1.61A	1.62	2.08	2.19	1.90	2.36	2.43	2.48	2.45	2.40	2.43	2.108	2.298	2.02	1.71A 2.21A	2.154
1.500	2.19A 3.03A	2.29A 3.13A	3.32	3.51	3.71	3.93	3.04	4.28	3.22	3.20	3.19	3.34	3.76	5.898	3.94	3.00A	4.034
3.000	6.11A	6.17A	6.15	6.47	6.77	7.04	7.33	7.45	7.39	7.35	7.38	7.54	7.63	7.27	6.238	5.394	5.724
5.600 7.000	7.00A 7.05A 6.77A	7.06A 7.23A 7.10A	7.50	7.42 8.04 8.16	7.80 6.52 8.79	8.94	9.29	9.31	8.34	7.35 6.15 6.70	7.97	7.85	7.57	7.06	5.94	5.194	1.084
10.000	5.39A	5.85A	7.54	7.60	6.35	9.11	9.81	9.88	9.64	9.12	8.23	7.42	7.06	5.55	5.46	1.81A	4.624
20.000	4.314	4.014	3.20	5.75	7.10	7.70	6.63	6.29	6.17	6.31	5.93	5.71	5.40	2:14	::33	1:004	3.774

A - ONLY ONE DATA SET USED IN AVERAGE B - PERCENT STANDARD DEVIATION OF DATA TYPES IS GREATER THAN 10%

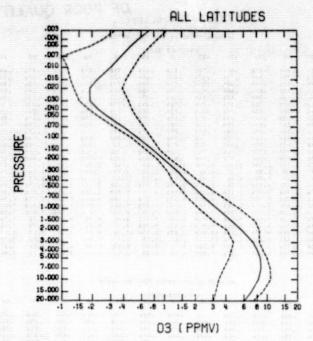


Figure 9. Global mean vertical structure of ozone volume mixing ratio (ppmv) (weighted by cosine of latitude) and the maxima and minima of Table 4 monthly latitudinal profiles.

Table 5. Ozone unit conversion table.

To convert from volume mixing ratio (ppmv) to units below, multiply by:

Mass mixing ratio (ppmm) 1.657 Mass density (kg-m⁻³) 1.657 x $10^{-6} \cdot \rho_{t}$ Number density (m⁻³) 2.079 x $10^{19} \cdot \rho_{t}$ Partial pressure (nanobars) P_{t}

where P_t is the total atmospheric pressure in mb (1 mb = 100 pascals) and ρ_t is the total atmospheric denisty in kg-m⁻³ at a given altitude.

Total column burden (Ω) in atm-cm (1 = 1000 Dobson units) above a given pressure (P_0) can be calculated by integrating partial pressure $P(0_3)$ with respect to $ln(P_t)$:

 $\Omega = 7.896 \times 10^{-4} \cdot \int_{0}^{P_0} P(\theta_3) d\ln(P_t).$

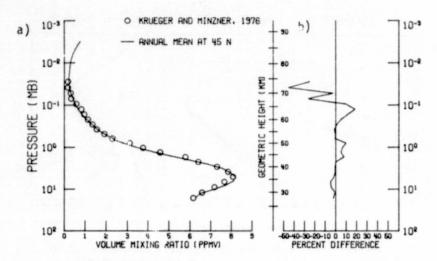


Figure 10. Comparison of annual mean ozone volume mixing ratio (ppmv) at 45°N based on the satellite data model of Table 4 and based on the balloon and rocket data model of KRUEGER and MINZNER (1976). On the left (a) is shown the vertical structure in the two models and on the right (b) the percent difference from the satellite data model of the Krueger and Minzner model.

the relation of total ozone to vertical structure are incorporated here. Shown in Figure 11a are low-latitude ($^+\pm 25^\circ$) profiles for ozone mixing ratios for total column ozone of 200, 230, 250 and 300 Dobson units (left to right). Shown in Figure 11b are similar midlatitude ($^-\!\!25$ to 58°) profiles for total column ozone in increments of 50 Dobson units from 200 to 550 Dobson units (left to right). Finally, shown in Figure 11c are similar high-latitude ($^-\!\!58$ to 80°) profiles for total column ozone in increments of 50 Dobson units from 200 to 65 Dobson units (left to right). Note that the mixing ratio variability extends to lower pressures (higher altitudes) at the higher latitudes. It should be assumed here that these profiles represent annual means since annual variability is not included. Tabulations of the models are found in MATEER et al. (1980).

7. OTHER SYSTEMATIC VARIATIONS

A number of systematic variations of ozone in addition to latitudinal seasonal variations have been analyzed. For brevity only a few references are included here. Empirical analyses have been performed on the quasi-biennial oscillation (ANGELL and KORSHOVER, 1978), solar cycle variations (KEATING, 1981), solar rotation variations (GILLE et al., 1984), diurnal variations (LEAN, 1982; REMSBERG et al., 1984), longitudinal variations (LONDON et al., 1976; WILCOX et al., 1977; HEATH et al., 1982), possible variations with volcanic eruptions (ANGELL and KORSHOVER, 1978), possible response to nuclear explosions (JOHNSON et al., 1973), long-term trends (LONDON and KELLEY, 1974; ANGELL and KORSHOVER, 1983; REINSEL et al., 1984), 4-year oscillations (HASEBE, 1983), response to stratospheric temperature (BARNETT et al., 1975; KEATING et al., 1983a; PITTS, 1981; MILLER et al., 1984), response to sudden winter warmings (GHAZI, 1974), and response to solar proton events (HEATH et al., 1977; THOMAS et al., 1983b).

The quasi-biennial variation in ozone is thought to be related to the

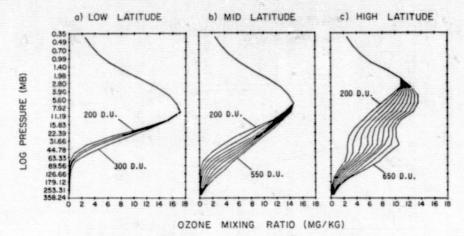


Figure 11. Variation of ozone mass maxing ratio with total ozone (from MATEER et al., 1980). (a) low-latitude ozone profiles for total ozone of 200, 230, 250 and 300 Dobson units (b) mid-latitude ozone profiles for total ozone of 200, 250, ... 550 Dobson units (c) high-latitude ozone profiles for total ozone of 200, 2500, ..., 650 Dobson units.

quasi-biennial variation in equatorial zonal winds (OLTMANS and LONDON, 1982). Shown in Figure 12 (TOLSON, 1981) is the biennial component of the zonal mean total ozone variation based on 7 years of Nimbus 4 BUV data. The contour interval is 2 Dobson units with the solid lines positive and the shaded area with dashed lines negative. Referring back to Figure 3, it may be seen that the low and midlatitude regions of large interannual variations correspond to regions of large quasi-biennial variation. However, since the variation is only quasi-biennial, the phase indicated in Figure 12 will change with time. There is also evidence that the period of the quasi-biennial variation may vary somewhat with latitude (HILSENRATH and SCHLESINGER, 1981) and that the latitude of maximum quasi-biennial variation may vary somewhat with time (HASEBE, 1983).

Evidence has accumulated that variations in ozone with a period of the order of 11 years occur at various locations. On the other hand, there has been a lack of consensus as to whether these variations are related to the 11-year solar activity cycle. The early and more recent studies which have been performed, including theoretical model results based on recent estimates of solar variations and satellite measurements of global mean ozone variations, are reviewed by KEATING (1981). It appears that there is a 2 to 3% variation in global ozone from solar maximum to minimum in accord with the photochemical effects of 11-year variations of the order of 15 to 20% from 180 to 208 nm (KEATING et al., 1981). However, studies over longer time periods of the exact variations of solar ultraviolet radiation and of ozone are needed to confirm this result. Refinement of this result is crucial for separating long-term trends of anthropogenic effects from natural variations in ozone (BLOOMFIELD et al., 1983). Latest studies on long-term variations in ozone vertical structure measured by the Nimbus 4 BUV are consistent with the scenario of 15 to 20% solar UV variability below 210 nm (CHANDRA, 1984). In addition to a global mean increase in ozone with increasing solar activity, recent empirical and theoretical studies by SOLOMAN and GARCIA (1984) indicate that there may be a decrease in ozone at high latitudes in the upper stratosphere due to a solar cycle variation of NO transported downwards from the thermosphere which catalytically destroys ozone.

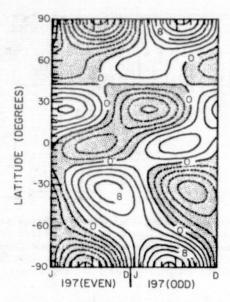


Figure 12. Biennial component of zonal mean ozone variation based on 7 years of Nibmus 4 BUV measurements. Contour interval is 2 Dobson units; solid lines are positive and the shaded area with dashed lines negative (TOLSON, 1981).

Evidence has accumulated of $\sim 3\%$ variations of solar UV between 180 and 208 nm with the 27-day solar rotation based on recent solar measurements from the Nimbus 7 and Solar Mesosphere Explorer satellites. Studies are indicating a detectable ozone response in the upper stratosphere of approximately 1% to these short-term variations (GILLE et al., 1984; HOOD, 1984).

Long-term variations in total ozone have been measured using ground-based observations from the global network. Shown in Figure 13 are estimates of percent variation in global mean ozone values based on those measurements as determined by ANGELL and KORSHOVER (1983). As may be seen, a substantial rise in total ozone occurred in the 1960s and maximum values appear to occur near the times of maxima in the 11-year solar cycle. So far there has not been a detectable decrease in total ozone associated with anthropogenic effects.

Diurnal variations of ozone are observed in the mesosphere where ozone concentrations are higher at night (LEAN, 1982; REMSBERG et al., 1984). There are also indications that the ozone mixing ratio may be higher on the dayside in the upper stratosphere.

Due to the temperature dependence of rate constants in the middle atmosphere temperature decreases result in increases of upper atmospheric ozone in regions approaching photochemical equilibrium. The latitudinal-seasonal and altitudinal relation between these two parameters has been studied in some detail using the Nimbus 4 BUV ozone measurements and Selective Chopper Radiometer (SCR) temperature measurements, and also temperature and ozone measurements from Nimbus 7 (KEATING et al., 1983a). The sensitivity of ozone to temperature variations reaches a maximum value near the stratopause of about 2% increase in ozone per °K decrease in temperature. In addition to the stratospheric ozone response, the mesospheric ozone is found to be strongly affected by temperature variations (EARTH et al., 1983).

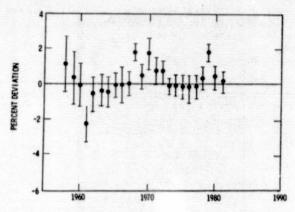


Figure 13. Variation of global yearly average total column ozone expressed as percent deviation from the mean based on ground-based Dobson spectrophotometers as well as M-83 ozonometers (ANGELL and KORSHOVER, 1983).

8. FUTURE MODEL REFINEMENTS

Currently a significant effort is under way among the investigators of contemporary satellite ozone experiments to identify and interpret relative biases among experiments (FLEIG et al., 1984b). This effort may lead to refinements in the model ozone distributions. There is evidence from studies at the National Bureau of Standards and other institutions that some of the ozone cross sections presently used for ozone determination may be in error (KLENK et al., 1984; BASS and PAUR, 1984; PAUR and BASS, 1984). This could change ozone values obtained from the SBUV experiment at some latitudes by 10% (BHARTIA et al., 1984b; KLENK et al., 1984). It is expected that more data will become available from the SME-UVS, SME-IR, SBUV, TOMS and SAGE experiments which can be incorporated later to refine the models. In addition, consideration is being given to incorporating balloon data as another data set to be included in the model, especially if the reference model is to be extended to lower altitudes.

Considering the present, very good agreement among data sets and the evidence of small interangual variability, it is expected that in many respects, refined models will not differ appreciably from those shown here.

9. CONCLUSIONS

A set of models has been generated based on six satellite experiments of the monthly latitudinal variations in total column ozone and the vertical structure of ozone from 20 mb to 0.003 mb. Generally, interannual variability in monthly zonal means is only a few percent. Comparisons of measurements using various techniques to measure global czone reveal very good agreement between the techniques. Agreement between individual satellite experiments and the reference model of monthly zonal means is generally within 10% below altitudes of 0.4 mb. This has allowed the first global model of ozone measurements to be constructed from multiple sets of satellite measurements.

The ozone measurements based on the satellite data are in excellent agreement with the KRUEGER and MINZNER (1976) midlatitude mean annual model based on rocket and balloon data. Also, models are provided of the relation between total ozone and vertical structure (MATFER et al., 1980).

Refinements to these models will be made as more data becomes available and as algorithm improvements are incorporated considering, for example, recent reevaluations of ozone absorption cross sections.

ACKNOWLEDGEMENTS

The authors wish to acknowledge the valuable contributions of the "Ad Hoc Group on Ozone Reference Models for CIRA" in reviewing the manuscript. The Group includes C. A. Barth, P. K. Bhartia, D. F. Heath, K. Labitzke, C. A. Mateer, M. P. McCormick, A. J. Miller, and J. M. Russell III. Others offering valuable comments included J. S. Chang, R. J. Thomas, M. Allen, D. W. Rusch, and W. P. Chu. The authors also wish to thank J. Y. Nicholson III, M. C. Pitts, and B. T. Marshall of Systems and Applied Sciences Corporation for their assistance in organizing and compiling the vast amount of ozone data.

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3.1.1 TEMPERATURE STRUCTURE OF THE 80 km TO 120 km REGION

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INTRODUCTION

Temperatures, densities, and pressures in the COSPAR International Reference Atmosphere (CIRA) 1972 between 80 and 120 km are given as monthly averages at 5 km height increments every 10 deg in latitude for the Northern Hemisphere. However, data are extremely sparse in this region, and as Groves (see CIRA 1972) points out, CIRA 1972 suffers from the same limitations as CIRA 1965 above 60 km:

(i) Data from all longitudes are combined without consideration of longitudinal effects. Most data are from North American sites, and so any longitudinal bias would be towards the Western Hemisphere,

(ii) Insufficient Southern Hemisphere data were available for developing a separate mode. Therefore, Southern Hemisphere data were combined with Northern Hemisphere data with a six-month change of date.

(iii) Due to insufficient data, no account was taken of local time in development of the models. Consequently the temperature and density fields may be diurnally biased as well.

Development of the temperature, density, and pressure specifications between 80 and 120 km for the new CIRA will involve building upon the existing CIRA 1972 model data base. Since the greatest abundance of experimental data is in the form of temperatures, and since temperature is one of the meteorological fields (besides winds) for which we have a firmer theoretical and intuitive base for understanding its behavior and structure, the temperature field will be the basis for development of the model. Following the procedure followed in CIRA 1972, given a specification of the pressure field at some lower boundary, the density and pressure fields at higher altitudes will be derived from the barometric and ideal gas laws. Available falling-sphere rocket measurements will be used to provide consistency checks on these densities and to possibly introduce adjustments in the final temperature model as appropriate. Also involved in the final stages of model development will be "matching" to temperature specifications below 80 km and above 120 km. All of these requirements will result in some iterations and adjustments in the final stages of model development, and it is antitcipated that these issues will be quantitatively resolved at the IAGA/IAMAP Meeting in Pragme, Czechoslovakia, in August 1985.

Without firm definition of the matching constraints at the 80 km and 120 km altitude levels, all that can be accomplished at the present time concerning the intervening altitude regime is to provide an assessment of deficiencies in CIRA 1972 given the more extensive data base now available, and to outline the scope of the new CIRA model specification between 80 and 120 km. Specifically, we will address the following questions: (i) Are there clear-cut misrepresentations in CIRA 1972 which can be rectified by the data now available? (ii) Are there sufficient data and evidence to warrant inclusion of a longitude dependence in the model? (iii) An asymmetry about the equator in the model?

SOURCES OF DATA

The following is a preliminary, and as yet incomplete, description of data which will form the basis for the $80-120~{\rm km}$ specification of temperature,

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density and pressure in the new CIRA:

(i) The CIRA (1972) temperature model between 80 and 120 km was based heavily on data from the NASA Meteorological Sounding Rocket Program (MSRP) collected prior to 1967. The primary techniques were pitot tube and grenade measurements. The MSRP was phased out in 1973. Between 1967 and 1973 32 pitot tube and 135 rocket grenade experiments were conducted which generally yielded temperature data above 80 km. The soundings were made at Wallops Island (38°N, 75°W), Ft. Churchill (59°N, 94°W) Pt. Barrow (71°N, 157°W), Natal (6°S, 35°W), Arecibo (18°N, 67°W), Arenosillo (37°N), Eglin (30°N, 87°W), and Kourou (5°N, 53°W) (SMITH et al., 1967, 1969, 1970, 1971).

(ii) GAIGEROV et al. (1984) present extensive analyses of temperatures from Soviet rocket measurements (mostly grenade method) north and south of the equator in the Eastern Hemisphere. Most of the Southern Hemisphere data were collected after 1970, and hence were not included in the 1972 CIRA. Gaigerov et al. also discuss the results of several intercomparisons with other independent measurements of temperature, and report that adjustments have been made for any biases which might have existed in their raw data. Monthly average data between 80 and 90-100 km are available from Heiss Island (81°N, 58°E), Volgograd (48°N, 44°E), Molodezhnaya (68°S, 45°E), and from research vessel soundings in the Pacific near 0°, 20°S, 40°S, and 50°S. These data now enable us to examine possible longitudinal and latitudinal asymmetries in the thermal structure of the mesopause region.

(iii) Five years (1970-1975) of temperature profiles from incoherent scatter measurements in the E region (100-130 km) over Arecibo, Puerto Rico (18°N, 67°W) and Millstone Hill, Massachusetts (42°N, 71°W) are available for analysis. These data have been analyzed in parts, mostly with regard to the semidiurnal oscillation by SALAH (1974), SALAH et al. (1975), SALAH and WAND (1974), and WAND (1976, 1983). This investigator has pooled all the available data, separated mean and semidiurnal tidal components, and constructed monthly averages. A total of over 1,500 profiles (each) are available from Arecibo and Millstone Hill. These data are considered extremely important in terms of "matching" the rocket-based temperature structure of the 80-100 km region with the satellite-based density and temperature fields above 150 km.

The data described above are utilized in the preliminary analysis presented here. Some additional supplementary data between 90 and 110 km are Esrange, Sweden (68°N, 21°E) during the November/December 1980 Energy Budget Campaign (PHILBRICK et al., 1983) and between 100 and 130 km taken at St. Santin (45°N, 2°E) and at Chatanika (65°N, 147°W) may also be included at a later time, as well as several other scattered measurements taken since 1970. There also exist temperature inferences from optical emissions (5577 Å oxygen airglow and OH(8-3) band rotational temperatures in the vicinity of 85-95 km), but these are single height (slab) determinations and are generally only available at latitudes or longitudes where the rocket data are plentiful. A fairly complete list of stations from which rocket and radar data will originate for the new CIRA is included in Table I.

ANALYSIS OF THE DATA

The 80 - 100 km Region. The main focus of the current analysis is to ascertain (1) whether evidence exists for longitudinal and latitudinal asymmetries in the temperature structure of the 80 to 100 km region, and whether sufficient data are available to delineate these dependences in a reference atmosphere; and (2) whether specific deficiencies in the CIRA (1972) representation of temperature are suggested by the updated data base.

Table 1. Locations of rocket* measurements and incoherent scatter radar**
measurements which will form the basis data for the new CIRA between
80 km and 120 km.

Western He	emisphere	Eastern Hem	isphere
Thule	(76°N, 69°W)	Heiss Island	(81°N, 58°E)
Pr. Barrow	(71°N, 157°W)	+Esrange	(68°N, 21°E)
+**Chatanika	(65°N, 147°W)	Volgograd	(48°N, 44°E)
Ft. Churchill	(59°N, 94°W)	**St. Santin	(45°N, 2°E)
**Millstone Hill	(42°N, 71°W)	Sardinia	(40°N, 10°E)
Wallops Island	(38°N, 75°W)	Guam	(13°N, 145°E)
White Sands	(32°N, 106°W)	Kwajalein	(9°N, 168°E)
Eglin	(30°N, 87°W)	Thumba	(8°N, 77°E)
Cape Kennedy	(28°N, 80°W)	Res. Vessels	(0°)
Barking Sands	(22°N, 159°W)	Res. Vessels	(20°)
**Arecibo	(18°N, 67°W)	Carnarvon	(25°S, 114°E)
Antigua	(17°N, 62°W)	Woomera	(31°S, 136°E)
Ft. Sherman	(9°N, 80°W)	Res. Vessels	(50°S)
Kourou	(5°N, 53°W)	Kerguelen I.	(49°S,)
Natal	(6°S, 35°W)	Res. Vessels	(50°S).
Ascension I.	(8°S, 14°W)	Molodezhnaya	(68°S, 45°E)

^{*} With some exceptions, data are generally available between 80 - 100 km.

** Data generally available between 100 - 130 km.

+ Not included in current preliminary analysis.

In Figure 1 variations in monthly temperatures at 85 km for individual stations are compared. The comparison between Pt. Barrow (71°N, 157°W) and Heiss Island (81°N, 58°E) suggests 5-10 K higher temperatures at Heiss Island in the summer and 5-10 deg cooler temperatures between Janaury and March. Although these two stations are separated by 10 deg in latitude, the discrepancy is opposite to what one might expect from the positive (negative) pole-to-equator temperature gradient assumed to exist in Northern Hemisphere summer (winter) months. An examination of vertical structures at the two stations indicates that the summer mesopause minimum is near 90 km at Heiss Island as opposed to 85 km at Pt. Barrow, and this in itself is an important contribution to their differences in monthly behavior at 85 km.

Although the Volgograd (48°N, 44°E) data during summer exhibit 10-15 K higher temperatures than Ft. Churchill (59°N, 94°W), their 11 deg separation in latitude is sufficient to account for more than half of this difference assuming a realistic latitude gradient in temperature (see following figures). Figure 1 also suggests a much larger temperature gradient in the Eastern than Western Hemisphere, but it must be remembered that Ft. Churchill and Pt. Barrow are only separated by 12 deg latitude, whereas the separation between Heiss Island and Volgorad is 33 deg in latitude. Obviously, to make any convincing statements about latitude structure we should examine all possible data at a given height. This will be done below.

Before leaving Figure 1, note that Southern Hemisphere data at 40° S and 50° S agree quite well with the Northern Hemisphere data at similar latitudes. Further, the monthly variation of temperature predicted by the CIRA 1972 is in excellent agreement with the measurements at Pt. Barrow, \forall t. Churchill, and

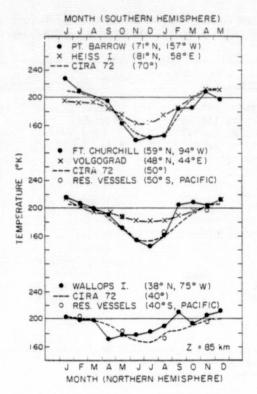


Figure 1. Temperature vs month at 85 km for various stations which allow examination of possible longitudinal or hemispheric asymmetries within specific latitude belts. CIRA 1972 values are shown for comparison.

Wallops Island. This is not surprising as considerable data from these stations prior to 1967 were used in the construction of CIRA 1972.

In Figures 2 and 3 the latitude structures of temperature during summer (mostly July) and winter (mostly January), respectively, are depicted at 80, 90, and 100 km. An obvious feature of these plots is that the Eastern/Western/Northern/Southern Hemisphere data collectively delineate fairly well-defined patterns. Further, while the CIRA 1972 curves are surprisingly successful in approximating these data in some regions, the potential for significant improvement is suggested. In particular, 100 km appears to be nearly isothermal at 200 K in January and at 190 K in summer, at least within the scatter of the data. Also, the latitude structure of temperature at 80 km and 90 km poleward of 40 deg latitude can be better modelled, and this feature is important for understanding the dynamics of the zonal mean circulation of the mesopause region.

The 100 - 130 km Region. Figure 4 depicts a selection of temperature measurements between 200 and 130 km at various latitudes during July and January. Comparisons are made with the MSIS-83 model (HEDIN et al., 1983), as this is a likely candidate for the new CIRA above 100 km or so. CIRA temperature profiles would not have compared so well with the data in Figure 4, the temperatures being some 20-60 K cooler than MSIS-83 in the 120-130 km region. The data shown in Figure 4 during January are extremely consistent

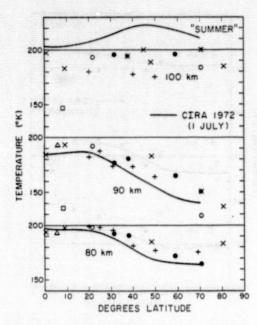


Figure 2. Temperature vs latitude for measurements representative of July north of the equator in the Western (*) and Eastern (x) Hemispheres, and January south of the equator in the Eastern Hemisphere (+). Where data under these exact conditions were not available in the Western Hemisphere, data points from 8°S August (□), 6°S August (△), August (*), and June (o) were inserted to allow a more complete delineation of the latitude structure. CIRA 1972 values are shown for comparison.

with each other and with the MSIS-83 model, and do not exhibit any significant latitude structure. During July, however, there appears to exist a significant positive equator-to-pole temperature gradient. At 115 km the temperature varies from about 168 K at Kwajalein (9°N) to 320 K at Arecibo (18°N) to 370 K at Wallops Island (38°N) and Millstone Hill (42°N). A small temperature difference (20 K) of this sense between 18°N and 42°N is specificed in the MSIS-83 model.

CONCLUSIONS AND RECOMMENDATIONS FOR THE NEW CIRA

Between 80 and 120 km the CIRA 1972 model is based heavily on NASA Meteorological Sounding Rocket Program (MSRP) data collected prior to 1967. The data are biased towards North America, are seasonally and diurnally biased, and contain significant gaps in latitude. The MSRP was phased out in 1973. Since about 1970 an abundance of E-region (100-130 km) temperature data from the incoherent scatter facilities at Arecibo, Millstone Hill, and St. Santin have also become available. The present study examines the temperature structure of the 80-120 km region given considerable additional MSRP rocket data, thus providing better seasonal, latitudinal, and longitudinal coverage in the 80-100 km region, and a combination of incoherent scatter and rocket data in the 100-120 km region which allows a much improved delineation of lower thermosphere temperature structure. Although some individual station comparisons indicate measurable asymmetries in longitude and latitude, data are still insufficient to separate these effects; that is, to provide a reliable

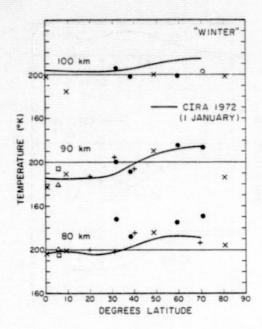


Figure 3. Temperature vs latitude for measurements representative of January north of the equator in the Western (•) and Eastern (x) Hemispheres. Where data under these exact conditions were not available in the Western Hemisphere, data points from 6°S February (□), 6°S December (Δ), and February (o) were inserted to allow a more complete delineation of the latitude structure. CIRA 1972 values are shown for comparison.

description of latitude structure as a function of longitude, or of longitude structure at any given latitude. However, by consideration of data below 70-80 km as well, GAIGEROV et al. (1984) were able to construct height-latitude temperature contours up to 100 km which are characteristic of the Asian/Pacific and American longitude sections. The Eastern Hemisphere data also extend into the Southern Hemisphere.

Specific recommendations of the new CIRA to emerge from this study are as follows:

- (i) Tabulations between 80 and 100 km should represent zonally averaged values. These can be viewed with much greater confidence than those in CIRA 1972.
- (ii) The temperature, density, and pressure specifications between 80 and 120 km should provide a smooth transition with the zonally averaged SCR/PMR data (as given in Section 2.2) below and MSIS-83 (tentative) above. In so doing, some seasonal asymmetry about the equator may be introduced via the satisfaction of matching conditions. It is anticipated that these matters will be extensively discussed and settled at the IAGA/IAMAP meeting in Prague, Czechoslovakia, in August 1985.
- (iii) To provide some measure of possible longitudinal and latitudinal asymmetries, the height-latitude contours of temperature for January, July, April and October from GAIGEROV et al. (1984) should be included in the new CJRA.

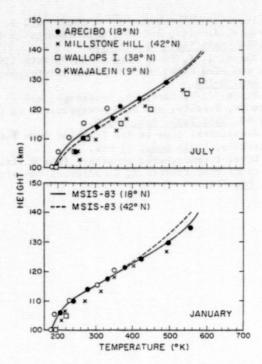


Figure 4. Vertical structures of temperature from 100 km to 130 km at various latitudes. MSIS-83 values are shown for comparison.

ACKNOWLEDGEMENTS

This work was supported under Contract F19628-82-K-0031 from the Air Force Geophysics Laboratory.

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Wand, R. H. (1983), Lower thermospheric structure from Millstone Hill incoherent scatter radar measurements 2, Semidiurnal temperature component, J. Geophys. Res., 88, 7211. 3.1.2 MEAN WINDS OF THE UPPER MIDDLE ATMOSPHERE (60-110 km):
A GLOBAL DISTRIBUTION FROM RADAR SYSTEMS (M.F., METEOR, VHF)

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ABSTRACT

During the last decade a large number of radars ($^{\circ}$ 12) have been developed, which have produced substantial quantities of tidally corrected mean winds data in the upper middle atmosphere. The distribution of the radars is not global, but many areas are well covered: the Americas with Poker Flat (65° N), Saskatoon (52° N), Durham (43° N), Atlanta (34° N), Puerto Rico (18° N); Europe and Kiruna (68° N), Garchy (47° N) and Monpazier (44° N); and Oceania with Christchurch (44° S), Adelaide (35° S), Townsville (20° S), and Kyoto (35° N).

Zonal and meridional wind height-time cross sections from 60-80 km (MF/meteor radar) to $^{\circ}110$ km have been prepared for the last 5-6 years. They are compared with cross sections from CIRA 1972 for zonal winds, and GROVES (1969) for meridional winds.

It is shown that while CIRA 1972 is still a useful model for many purposes, significant differences exist between it and the new radar data. The latter demonstrate important seasonal, latitudinal, longitudinal and hemispheric variations. The new meridional cross sections are of great value. The common features with GROVES (1969) are the equatorward cells in summer near 85 km; however, their strength ($^{\circ}10 \text{ m/s}$) and size are less. Systematic and somewhat different variations emerge at higher ($\geq 52^{\circ}N$) and lower (35-44°) latitudes.

INTRODUCTION

Since the development of the last CIRA in 1972, the number of radars providing winds in the upper middle atmosphere has increased significantly. Depending on the technique, these systems fill the data gap between 60 km (the meteorological rocket network and other small rocket systems have provided winds to that height) and ~110 km (larger rockets, and incoherent-scatter radars provide some winds above this height). The radars include medium frequency (MF) radars or partial reflection systems giving data from 60/70-100/110 km (and MST radars operating as meteor radars). Until now MST (VHF) radars have not given winds for a sufficient number of hours per day, or heights to provide cross sections of the type shown here: however, a new extended data set from Poker Flat is discussed later. We show here data from 12 locations, which represent a good Northern Hemispheric (NH) North American chain (18-65°N, 90°W), an Oceanian chain (44°S-35°N, 140°E) which is mainly in the Southern Hemisphere (SH), and some Western Europe Data (44-68°N, √0°E). (Of these, data are still being obtained at 7 locations, and also from two Antarctic stations not included here.) The methods of data analyses are discussed in detail elsewhere (MANSON et al., 1981a; MASSEBEUF et al., 1979; VINCENT and STUBBS, 1979; SALBY and ROPER, 1980; SMITH, 1981; CARTER and BALSLEY, 1982; CLARK, 1983; ASO and VINCENT, 1982). Generally, however, tidal

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oscillations have been removed from days or groups of days, and the remaining mean winds and longer period oscillations plotted as height-time contours. Time resolution varies from 10-15 days to seasonal, and will be evident from each figure.

An attempt has been made to form composite cross sections from the years 1978-1982 so that only the major temporal features remain. Detailed study of groups of years from Adelaide (ELFORD, 1976), France (MASSEBEUF et al., 1979; MANSON et al., 1983), Saskatoon (MEEK and MANSON, 1984, 1985) suggest that, at least at middle latitudes, the main features of the circulation are repeated each year with relatively small interannual variability. Here we focus on those major features and compare these with zonal winds from CIRA 1972, and meridional winds from Groves' data compilation (GROVES, 1969). Tabulations of monthly mean values for most stations appear in the Appendix. A more detailed presentation of these data, including individual years, will be made elsewhere (MANSON et al., 1985). The sign convention is as follows: for the zonal winds, positive winds are from the west (west or westerly winds) and negative winds are east or easterly winds. For the meridional winds, positive winds are from the south (south or southerly winds), and negative winds are north or northerly winds. It is also convenient to describe these latter as poleward or equatorward winds. The figures are rather consistent, but any differences are mentioned in the captions.

ZONAL WINDS

Generally, for latitudes as low as ${\sim}\,35$ deg, there are westerly/easterly flows during winter-/summer-centred months below 95/85 km, and the reverse above (Figures 1-6, 8-12) as shown in CIRA 1972 (Figures 7, 13). High latitude data, such as Kiruna and Poker Flat (Figures 1,2), which were not available for CIRA 1972, can be seen to be reasonable extrapolations of midlatitude data (e.g., Saskatoon 52°N, Figure 3). The data from Poker Flat are derived from meteor echoes. A recent analysis of the winds from meteor and turbulence echoes (BALSLEY and RIDDLE, 1984) for 1980/1 show excellent agreement; suggesting that MST radars can provide monthly mean winds, depending on their power, location and the season. For lower latitudes (\lesssim 35 deg) the behaviour may be similar, but in general is more complex. At midlatitudes ($^{\sim}$ 45 deg) the reversals in the mesopause region are less clear in winter months, and are at a greater altitude (e.g., Figures 3, 4, 5, 6). There is also more systematic mesospheric variability during the $^{\circ}$ 7 winter-like months; this is most evident in the high resolution (7-/10-d means) large altitude-range data from Christchurch and Saskatoon (Figures 6, 3). The causes of this are planetary waves, stratospheric warmings, and annual and semiannual oscillations (MANSON et al., 1981b). This is a major difference from CIRA 1972, which due to lack of data in the lower mesosphere and averaging over years, has produced an unrealistically smooth winter vortex with a maximum in December/January. Indeed at latitudes near 50 deg, the CIRA winds for February and March are quite atypical (cf. Figure 3). The differences between winter and summer circulations, especially the variability, heights of reversal and strength of lower thermospheric circulations have important implications for theories and models which now depend upon gravity wave momentum deposition to close the westerly and easterly flows (LINDZEN, 1981; HOLTON, 1982). It is likely that the characteristics of the gravity wave fluxes, e.g., sources and group velocities, and perhaps planetary waves, also have strong seasonal variations which are reflected in these contours. Winds from most of the midlatitude stations (Figures 3, 5, 6; Saskatoon, Monpazier, Garchy, Christchurch) also illustrate the regularity of the equinoctial transitions and their rapidity. This is especially evident in the Saskatoon winds, where the composite of 4 years of continuous data differs little from individual years. Because of this, September is more winter-like and May more summer-like (Northern Hemisphere), than CIRA 1972 indicates.

ZONAL WIND KIRUNA (SWEDEN, 68° N) 1974 – 1975

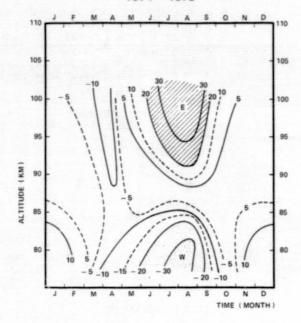


Figure 1. Kuruna, 68°N, 20°E (MASSEBEUF and FELLOUS). The positive westerly flow is marked E for eastward; and negative easterly is W for westward.

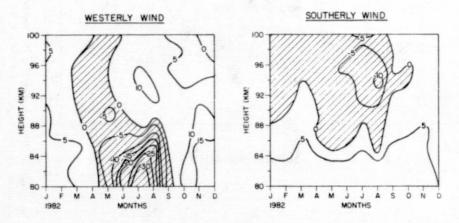


Figure 2. Poker Flat, 65°N, 147°W.

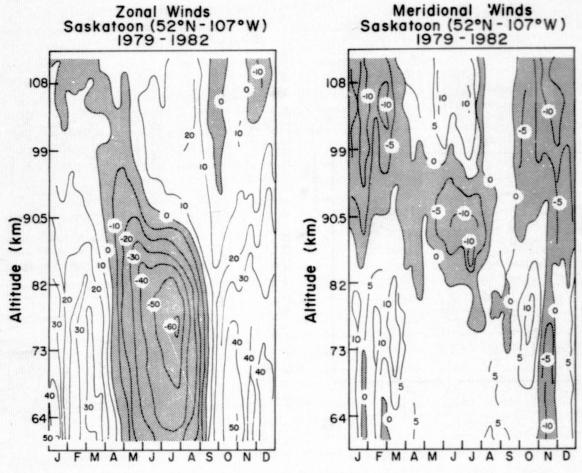


Figure 3. Saskatoon, 52 °N, 107 °W: 10 d means used; s.d. typically 6 ms⁻¹ for EW, 4 ms⁻¹ for NS at 90 km. Data above 100 km refer to a ~ 5 km layer, due to group retardation.

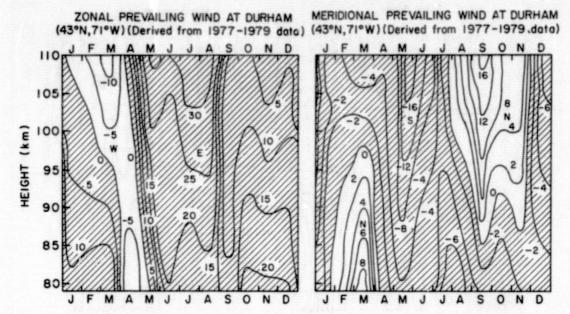


Figure 4. Durham, 43°N, 71°W: the positive easterly (E, eastward) flow is cross-hatched only in this case. Positive southerly flow is marked N for northward.

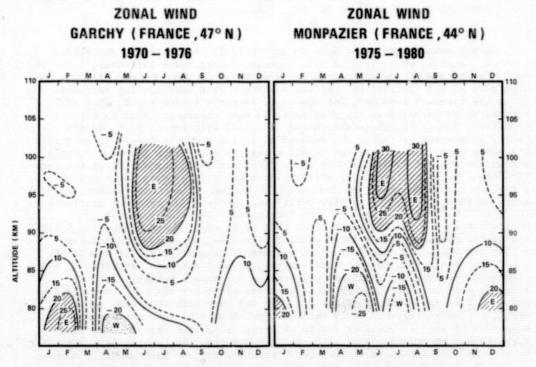


Figure 5. Monpazier, 44°N, 1°E; Garchy, 47°N, 3°E, 1970-76 (MASSEBEUF et al., 1979): westerly flow is marked E for eastward, easterly is W for westward.

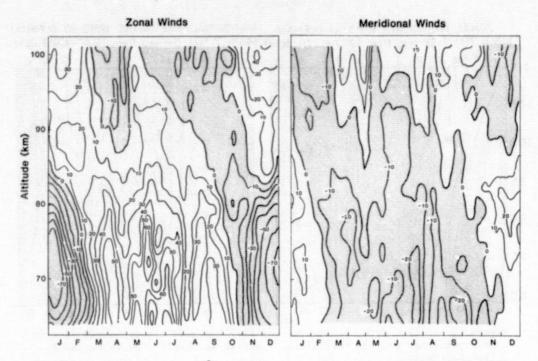


Figure 6. Christchurch, 44° S, 173° E: 7 d means used. Positive meridional flow is northward, and hence equatorward. The s.d. are 7 ms⁻¹ at 90 km, increasing to 10 ms⁻¹ at 80 km.

We now compare the winds data in more detail. For example, the summer reversal heights, which in CIRA 1972 decrease toward lower latitudes, from 90 km at 50 deg and 80 km at 35 deg, to 70-80 km at 20 deg (Figure 13). Our data show more global variability. Kiruna and Poker Flat have similar contours below the reversal (~88 lm), but the upper westerly (eastward, E) flow at Kiruna, which is based on 15 d of data, is much stronger. Near 45 deg, Saskatoon, Monpazier, Christchurch and CIRA 1972 (Figures 3, 5, 6, 7) are fairly consistent, although the descending spring easterly tongue is so strong and early over France, that the negative cell is split into two -- a feature not unlike that at 20 deg in CIRA 1972. This downward progression of the zero line could be a critical layer effect associated with gravity waves and/or planetary waves. However, the Durham (43°) contour is quite different in these summer months, with westerly flow 80-110 km, and very low vertical gradients (0.75 ms km vs 3.75 ms km at Saskatoon). This low reversal height makes it quite similar to CIRA 1972 at 35 deg. Hence, large longitudinal differences, and rapid latitudinal differences, are evidenced between Durham and Monpazier, and Durham and Saskatoon, respectively. It should be noted that the Durham meteor winds analysis assumes a linear variation of the mean wind with height, which may account for the smooth variation of the contours with height. Near 35°N, Atlanta and Kyoto are similarly dominated by westerly flow above ~80 km (Figures 8, 9); and they both show some negative easterly flow in fall and early winter. The absence of the narrow spring tongue at Atlanta is possibly due to interannual variability. It has been noted (DOLAS and ROPER, 1981), that the carculation there may be tropical (Figure 13) or midlatitude in pattern: actually to form the composite contour of Figure 8, a year which was somewhat more representative of a midlatitude circulation was eliminated. At Kyoto, there is easterly flow in February --

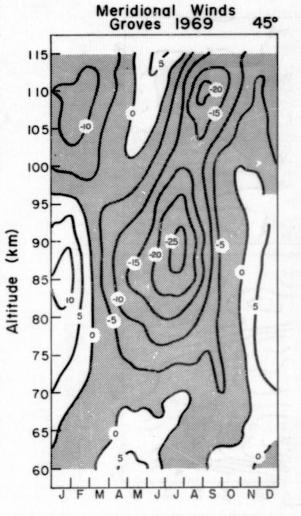


Figure 7. Model winds from CIRA 1972 (zonal) and GROVES (1969) (meridional): 45 deg.

S 0

A

Zonal Winds CIRA 1972

100

95

90

70

65

60

A

(kg)

Altitude

45°

ORIGINAL OF POOR

PAGE IS QUALITY MEAN

removed.

ZONAL

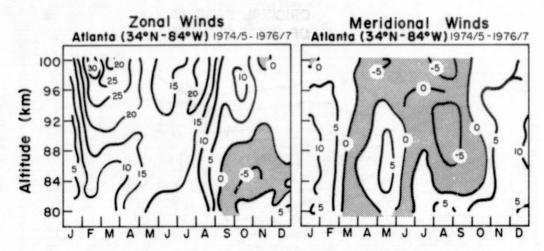


Figure 8. Atlanta, 34°N, 84°W; s.d. are 12 ms⁻¹ for the zonal, 8 ms⁻¹ for meridional winds.

WIND MEAN MERIDIONAL WIND

20.0

10.0

5.0 0.0 -5.0

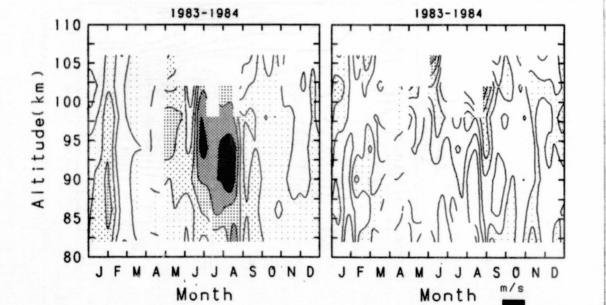


Figure 9. Kyoto, 35°N, 136°E: periods less than 25 d are

possibly associated with the stratwarm -- as well as in the spring. Other Kyoto data from 1979/80 (ASO and VINCENT, 1982) also show negative easterly flows up to 88/90 km in March and April. In summary, Atlanta and Kyoto demonstrate longitudinal differences; and also some features like CIRA 1972 at 20 deg, e.g., easterly flow near November and strong westerly flow in late summer. Meanwhile Adelaide at 35 °S (Figure 10) is more like CIRA 1972 at 35 deg or even 45 deg (Figure 7), with summer easterly flow up to 85 km. It is clear from studying CIRA 1972, that early Adelaide data strongly influenced the contours at that latitude; and that Adelaide is more like a Northern Hemisphere midlatitude (~45°) station. Winds from the previous 10 years of meteor and MF radar observations also showed the spring easterly tongue, but the easterly vortex was below 80 km. For 20 deg, CIRA 1972 (Figure 13) differs from the midlatitude pattern of Figure 7; as the descending tongue of easterly flow now dominates the NH mesopause region from November-April, and there is strong westerly flow above 90 km in late summer and early fall. Puerto Rico and Townsville (Figures 11, 12) are quite similar to each other, in that they both have prominent easterly spring tongues, and the easterly rises in height again to ~90 km in late summer: these features are similar to CIRA 1972 at 20 deg. However, the winter circulation November-January (May-July in the SH) from 80-100 km, is still dominated by westerly flow. Thus both locations still have strong remnants of the midlatitude circulation, and are not unlike CIRA 1972 at 35 deg (or Adelaide) in these respects.

The comparison betwee CIRA 1972 and the radar winds is well illustrated in height-latitude cross sections; and we show here December (an early solstice

ADELAIDE (35°S 138°E) 1978-1983

EW NS 100 - 10 98 96 94 92 90 88 20 86 84 30 82 80 40 78 50 76 74 72 70 68 66 62 60

Figure 10. Adelaide, 35°S, 138°E s.d. typically 7 ms⁻¹ for EW and 5 ms⁻¹ for NS at 90 km. Data extend down to 70 km; extensions are for numbering only.



TOWNSVILLE (20° S , 147° E) 1978-1980



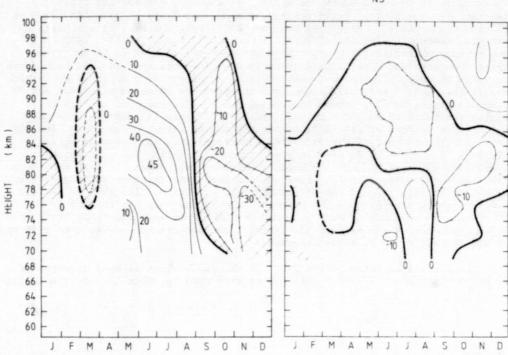


Figure 11. Townsville; 20°S, 147°E (ELFORD, VINCENT, CRAIG).

ZONAL WIND PUERTO RICO (18°5 N , 67°W) 1977 – 1978

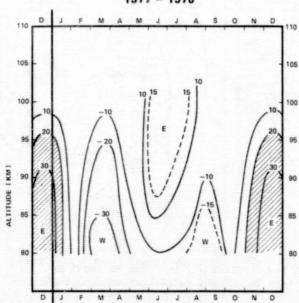


Figure 12. Puerto Rico, 18 N, 67 W (MASSEBEUF, FELLOUS): positive westerly flow is marked E for eastward.

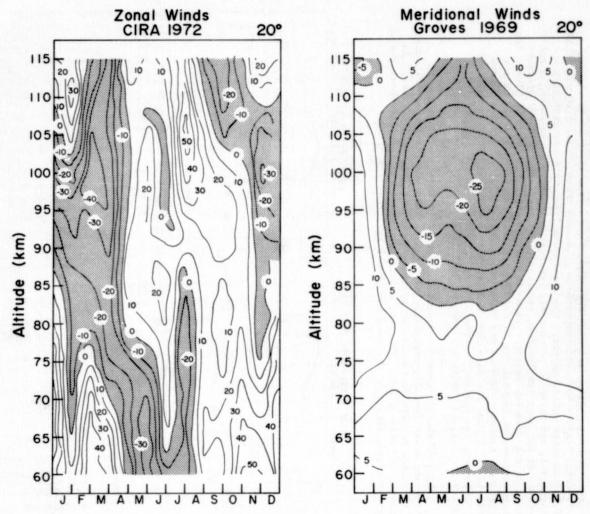


Figure 13. CIRA 1972, Groves, 1969: 20 deg.

month, clear of NH stratospheric warmings) and July for ~90°W in the NH, and ~140°E in the SH. From CIRA, July (June 15-July 15) and January (December 15-January 15) are shown (Figures 14, 15). The time rates of change are small in midseason, so that conclusions drawn here are usually typical of the entire solstitial seasons. Only the zero contours and maxima of cells are shown for CIRA 19721. The lack of hemispheric symmetry is immediately obvious: the winters are most alike, and even then the NH zero line is 10-15 km higher, reflecting smaller poleward temperature gradients there. Comparing with CIRA 1972, two other points emerge: the upper zero lines were not available for that model; and there is an easterly tropical cell above 87 km which is not evident at our four low latitude stations. For the summers, these stations again do not have the easterly flow above 87 km, which is shown in CIRA. The main differences between the SH and NH at these longitudes are due to the consistent westerly flow at and above 80 km revealed at Durham (43°N) and Atlanta (35 N) and the high reversal heights in Oceania. Thus in both hemispheres, the systematic reduction in the height of the zero line with decreasing latitude which is shown by CIRA 1972, is not in evidence.

Some of the differences evident in Figures 14 and 15 will be due to planetary waves (n=1,2), especially in the NH. These could also explain the differences between Durham and Monpazier. Satellite data will be useful in quantifying this effect. However, significant differences between hemispheres have emerged, stressing the need for global reference atmospheres.

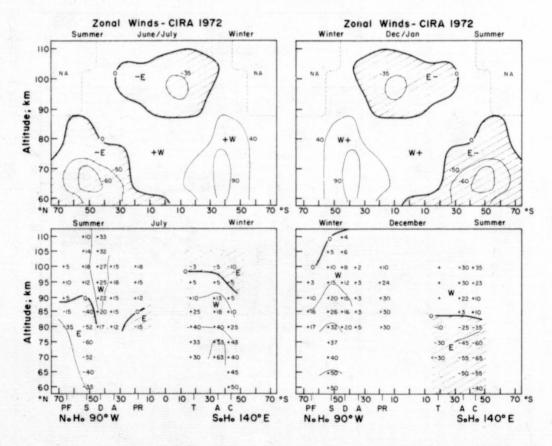


Figure 14. Zonal winds, July. Figure 15. Zonal winds, December/January.

MERIDIONAL WINDS

The tabulations of Groves show strong summer-centred equatorward flow (Figures 7, 13), which dominates the year: the centre of the core moves from 85 to 100 km from 50 to 20 deg. This summer flow has recently been studied at midlatitudes of the NH near 90 km (NASTROM et al., 1982) using data from radio and radar techniques. Although our data generally show this feature, the flow is weaker, and the seasonal and latitudinal variability is larger. As well as the summer flow (which is consistent with cooling at high latitudes, and hence the zonal winds through the thermal wind equation) Poker Flat (65°N), Saskatoon (52°N) and Christchurch (44°S) (Figures 2, 3, 6) also have poleward flow in the winter mesosphere, and equatorward above (GROVES, 1980). These may be portions of two cells, below and above the mesopause, respectively; the return flow could be in the stratosphere for the former (MEEK and MANSON, 1985), and the poleward flow would have to be above ~110 km for the latter. Notice the different contour shapes at 52 °N and 44 °S illustrating hemispheric differences. Durham also shows the summer equatorward flow (Figure 4) but overall its contour shapes differ significantly from Groves (Figures 7, 13) and neighbouring North American contours. For the low latitudes: at Atlanta (Figure 8) the phase of the changes is retarded by ~2 months; Kyoto (Figure 9) has more features in common with Durham and Saskatoon; and in the Southern Hemisphere, Adelaide and Townsville (Figures 10, 11) are quite similar to Christchurch. Our data differ considerably from Groves' compilation, and multiple meridional cells may be required to organize the data: longitudinal variations are

Finally we show meridional height-latitude cross sections as for the zonal wind, but compare here with Groves' data (Figures 16, 17). For July, the general agreement is quite good, apart from the fact already noted, i.e., the NH summer equatorward flow is weaker and more restricted in height than Groves. December's patterns (Figure 17) illustrate the lack of hemispheric symmetry, as the SH summer flow is more like Groves. The contours of the NH winter flow are quite different from Groves, although overall there is poleward flow within thermosphere in both cross sections.

CONCLUSION

The radar zonal wind cross sections differ considerably from CIRA 1972, especially regarding winter variability and heights of reversals. There is good evidence that winds from 43-52 deg in the Northern Hemisphere vary quite significantly with latitude and longitude, being near CIRA'S 45-50 deg in some cases and CIRA's 35 deg in others, and that winds $\sim 35\,^{\circ}\text{N}$ may demonstrate midlatitude ($\sim 35\,^{\circ}\text{CIRA}$ 1972) or tropical characteristics (20 deg CIRA 1972). In the Southern Hemisphere 35 deg is similar to CIRA 1972 at 35 deg or even 45 deg and is more midlatitude in behaviour. The winds from near 20 deg show a mixture of midlatitude and tropical characteristics. The meridional cross sections evidence considerable seasonal and latitudinal variability, the main feature being a summer equatorward ($^{\circ}\text{10 ms}^{-1}$) mesospheric flow. However, this does not dominate the year as in Groves' compilation. In other months at midlatitudes there is considerable poleward flow in the mesosphere. It is possible that the elimination of tidal components, which is crucial for these weak winds was not complete in the earlier data.

Overall, and based on other data from the various locations, the conclusions reached here about the zonal flows are probably valid. However, given the weakness of the meridional flow, the shapes of the contours for some of these cross sections are less certain -- given the probable importance of gravity wave momentum deposition for the zonal flow, this process will certainly also contribute to variability in the meridional flow. Nevertheless, the main differences from Groves' data are expected to remain.

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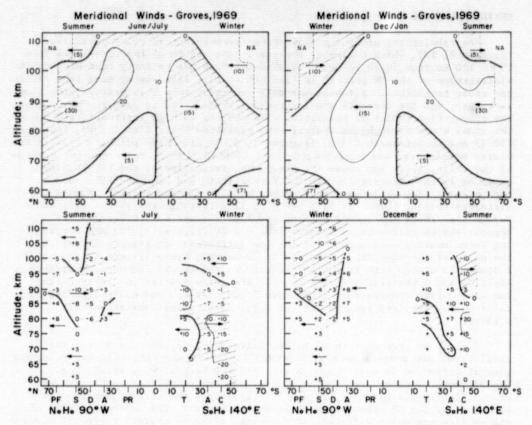


Figure 16. Meridional winds, July.

Figure 17. Meridional winds, December/ January.

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Appendix to 3.2.1: Monthly mean tabulations, with standard deviations, of the zonal and meridional winds discussed in Section 3.1.2

Saskatoon (52°N, 107°W) Mean Meridional Wind (m/s) 1979-1982

km	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
111	-9	-4	-1	1	5	6	5	3	2	-2	-10	-2
108	-10	-6	-5	1	6	5	7	2	2	-3	-9	-4
105	-15	-11	-5	1	6	6	6	2	1	-5	-10	-7
102	-9	-6	-6	1	4	5	6	3	1	-4	-8	-9
99	-12	-6	-4	-1	2	2	6	3	2	-5	-7	-7
96	-9	-4	-3	-2	-1	-3	1	2	1	-3	-4	-5
93.5	-8	-3	-1	-1	-3	-6	-5	-1	2	-2	-2	-4
90.5	-4	-1	0	-1	-4	-9	-10	-2	2	-2	-1	-4
88	-2	1	2	-1	-2	-8	-8	-2	1	1	0	-3
85	1	3	3	-1	2	-3	-6	0	1	3	1	-1
82	4	6	6	0	4	0	1	3	3	6	2	3
79	8	8	7	2	2	2	1	1	1	9	1	3
76	6	9	10	3	2	1	0	1	1	9	-1	3
73	5	9	9	3	2	2	2	3	2	7	-4	3
70	3	7	7	3	3	3	3	4	3	6	-4	3
67	5	6	5	2	3	3	2	3	3	4	-5	4
64	4	5	3	3	3	2	2	3	3	3	-5	5
61	3	5	2	3	3	4	3	4	4	2	-6	5

N.B. ~ 100 daily means per monthly mean (~ 200 values per daily mean above 80 km, ~ 100 values below 80 km).

Saskatoon Meridional Standard Deviation (m/s)

km	JAN	FE8	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
111	5	7	3	5	5	5	5	5	5	2	4	9
108	3	7	4	3	6	3	3	6	3	4	5	9
105	4	11	2	4	6	4	5	7	4	3	4	9
102	6	6	3	3	4	5	4	5	4	2	3	6
99	4	5	2	2	4	4	2	3	3	3	3	3
96	4	6	3	1	4	3	3	3	2	3	3	3
93.5	3	5	5	1	3	5	2	2	2	5	4	4
90.5	6	4	4	2	4	3	4	3	3	3	4	6
88	9	4	4	2	3	2	2	2	2	3	4	7
85	10	5	5	2	2	3	8	3	2	3	5	5
82	9	5	5	3	2	2	3	5	5	2	4	4
79	9	6	5	1	2	2	4	5	3	4	6	8
76	6	8	4	2	1	1	2	3	1	5	4	8
73	6	8	5	2	1	2	1	2	1	5	5	10
70	5	7	5	4	1	1	2	1	3	6	6	8
67	3	9	5	2	1	0	2	2	2	5	7	10
64	6	9	4	2	2	1	3	2	2	5	7	9
61	7	10	3	2	2	2	3	4	2	5	8	9

Saskatoon (52°N, 107°W) Mean Zonal Wind (m/s) 1979-1982

km	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
111	-2	-6	-1	3	4	6	11	12	1	0	0	-3
108	0	-3	-1	1	5	10	13	17	0	1	0	-5
105	-1	4	-2	-1	5	13	14	17	-1	2	2	1
102	. 4	5	1	-1	4	13	15	17	2	2	5	5
99	7	7	2	-5	3	13	13	18	4	2	5	7
96	8	8	3	-8	-2	11	15	17	5	4	5	11
93.5	10	12	2	-11	-11	3	10	14	9	4	9	15
90.5	15	15	6	-9	-19	-6	1	11	11	7	14	18
88	20	19	11	-10	-27	-20	-20	-2	12	11	20	23
85	22	23	18	-7	-33	-39	-37	-19	9	17	25	25
82	26	27	21	-5	-34	-46	-51	-33	6	27	32	30
79	29	29	25	-3	-33	-49	-55	-37	3	32	35	31
76	26	29	26	-5	-31	-49	-58	-40	2	36	36	30
73	26	30	28	-2	-28	-44	-54	-38	2	38	37	38
70	28	31	29	-1	-26	-42	-51	-38	3	39	37	42
67	33	32	31	5	-22	-39	-48	-35	5	42	40	44
64	37	34	33	8	-19	-36	- 45	-32	6	44	41	45
61	39	34	31	10	-15	-28	-35	-22	8	43	40	46

N.B. -100 daily means per monthly mean (-200 values per daily mean above 80 km, -100 values below 80 km).

Saskatoon Zonal Standard Deviation (m/s)

km	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
111	3	9	5	4	7	6	5	6	4	4	7	6
108	4	5	4	4	7	4	5	5	3	3	5	8
105	5	12	7	6	8	5	10	8	4	7	7	6
102	6	7	6	7	8	6	8	6	3	4	4	5
99	5	7	7	5	8	6	8	9	3	4	4	5
96	6	6	7	5	10	7	5	7	3	4	4	6
93.5	6	7	6	5	13	10	4	7	5	4	4	6
90.5	8	7	5	6	13	8	4	3	4	5	4	2
88	9	6	8	6	11	6	7	6	4	5	4	3
85	8	7	13	5	6	8	7	8	5	9	6	6
82	11	8	15	4	5	7	6	8	7	11	6	9
79	12	9	15	4	5	5	4	8	9	12	6	12
76	10	14	9	6	4	5	4	3	4	7	7	12
73	10	15	12	7	3	2	4	3	2	6	8	6
70	9	17	12	10	3	2	3	3	. 2	6	9	10
67	9	19	15	7	3	3	4	3	3	6	11	11
64	10	20	16	8	4	3	4	4	4	7	11	13
61	10	20	15	9	5	5	3	4	3	6	10	10

Kyoto (35°N, 136°E) Mean Meridional Winds May 1983 - May 1984

km	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
106	1	-1	1	1	,	14	1	/	-5	0	-5	-2
102	5	-2	-1	2	4	-2	-12	-8	6	-1	2	0
98	2	-3	-4	1	-3	-1	-4	4	-3	-3	-2	3
94	-4	-1	-3	-3	-5	-4	-2	-4	-1	-3	-1	1
90	-3	4	-1	-5	-4	-8	-6	-11	-6	-3	-1	-2
86	-3	-4	3	-4	-4	-6	-9	-11	-5	0	0	-1
82	-8	-1	-1	-1	-1	-3	-6	-8	3	1	3	-1

Mean Zonal Winds

km	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
106	-1	-1	1	1	5	1	1	-6	-4	0	-2	-3
102	-3	-1	3	-5	3	4	14	9	0	2	-3	-3
98	2	3	2	-2	6	10	17	13	5	2	1	-1
94	5	1	-1	-3	8	11	19	19	4	1	1	1
90	7	2	2	-2	6	12	18	19	6	3	-1	0
86	7	4	0	3	2	5	14	12	6	1	2	3
82	7	2	0	-2	1	3	5	12	6	3	2	3

Atlanta (34°, 84°W) Mean Meridional Wind (m/s) 1974/5, 1976/7

km	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
100	-2	3	1	-1	-6	-2	-4	-9	-3	2	1	5
96	5	6	3	-3	-2	0	0	0	-3	6	5	8
92	11	7	0	-2	4	0	-2	-10	-5	2	7	9
88	13	8	-1	0	8	0	0	-7	-5	-3	8	9
84	12	8	-3	1	8	-1	2	-2	-3	-2	8	8
80	4	8	-3	-2	2	-2	3	7	3	10	8	5

Mean	Zona1	Wind I	(m/s)
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km	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
100	13	34	18	26	16	13	14	24	8	8	-2	2
96	8	28	26	25	16	12	18	22	6	12	4	4
92	3	22	22	19	17	15	20	14	3	7	1	3
88	2	17	14	12	18	18	19	9	0	-1	-5	1
84	2	12	6	10	18	18	15	6	-3	-5	-5	-2
80	7	8	7	18	14	11	10	12	-5	2	4	-5

Atlanta Meridional Standard Deviation (m/s)

km	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
100	11	8	19	12	10	6	4	8	7	4	19	13
96	11	11	15	10	5	10	5	9	6	8	12	15
92	12	8	10	9	5	8	6	10	2	10	9	13
88	13	5	6	8	11	4	6	13	4	11	9	11
84	12	7	9	10	13	9	6	13	6	15	8	10
80	7	8	10	14	7	11	4	8	5	23	10	11

Zonal Standard Deviation (m/s)

km	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
100	30	19	12	24	14	14	15	14	8	6	30	18
96	20	19	10	28	12	14	13	14	5	13	27	15
92	15	18	6	28	10	11	10	16	6	12	20	13
88	15	17	4	25	12	8	7	16	10	9	17	19
84	15	17	5	23	11	9	6	16	11	8	20	16
80	16	13	7	23	7	9	7	14	11	10	25	13

Christchurch (44°S, 173°E) Mean Meridional Wind (m/s) June 1978 - Feb 1980

km	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	ОСТ	NOV	DEC
102.5	-11	-13	11	19	2	7	14	10	10	-11	-12	-12
100	-9	-13	10	17	-1	1	11	6	5	-2	-11	-9
97.5	-3	-10	8	12	-1	-2	9	1	5	-3	-7	-5
95	-4	-8	4	5	-4	-7	3	1	4	-1	-3	-4
92.5	-1	-6	1	2	-9	-9	-1	-1	2	0	1	-3
90	-2	-6	-3	0	-6	-8	-3	-4	0	2	2	0
87.5	2	-7	-5	-3	-5	-8	-4	-6	-3	1	4	5
85	6	-9	-9	-4	-4	-6	-7	-7	-2	1	6	11
82.5	11	-7	-17	-7	-8	-8	-10	-8	-4	1	11	19
80	10	-3	-16	-16	-11	-10	-16	-6	-6	-4	5	20
77.5	4	2		-13	-13	-21	-18	-12	-8	-7	8	13
75	9	3		-13	-9	-18	-21	-9	-11	-6	1	11
72.5	9	4		-20	-13	-15	-20	-12	-13	-8	1	8
70	9	4		-15	-19	-7	-21	-11	-15	-8	-1	7
67.5	4	2		-14	-16	-6	-22	-11	-14	-9	0	4
65	6	3		-13	-13	2	-20	-14	-11	-9	0	7

N.B. 1000-2000 values >80 km; 200-400 values <80 km; sd $\mbox{-}7$ m/s at 90 km, increasing to 10 m/s at 80 km.

Christchurch (44°S, 173°E) Mean Zonal Winds (m/s) June 1978 - Feb 1980

km	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
102.5	32	21	-17	-8	-1	-3	-4	-6	-15	15	30	30
100	33	25	-5	-10	6	-5	-8	-7	-7	9	31	33
97.5	26	22	-7	-7	8	1	-6	-3	-6	8	20	23
95	18	18	2	-6	6	6	-4	-2	-5	2	3	18
92.5	15	15	2	-1	9	10	4	0	-4	-1	6	7
90	18	15	6	-1	6	10	3	4	-3	-6	4	10
87.5	12	20	8	4	9	11	6	9	3	-6	2	10
85	0	21	19	11	14	13	11	13	9	-10	-7	4
82.5	-23	13	26	20	21	20	17	20	20	-10	-14	-24
80	-37	1	28	33	33	23	29	26	33	-4	-18	-43
77.5	-56	-11		24	44	42	39	34	36	2	-28	-56
75	-68	-12		38	45	40	44	34	38	0	-23	-62
72.5	-71	-23		43	55	54	46	41	37	3	-25	-68
70	-70	-32		47	56	41	43	40	35	4	-26	-65
67.5	-63	-32		50	57	77	49	38	31	7	-26	-58
65	-46	-29		51	66	84	56	35	27	10	-21	-47

N.B. 1000-2000 values >80 km; 200-400 values <80 km: sd -7 m/s at 90 km, increasing to 10 m/s at 80 km.

Adelaide NS Mean 1978-1983 (35°S, 138°E)

HT	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
100												
98	5	2	8	-13	-7	2	5	7	2	6	3	0
96	5	1	10	-8	-4	0	6	6	3	5	6	1
94	6	2	4	-7	-2	-2	-4	1	0	4	5	2
92	7	2	-1	-8	-3	-3	-6	1	-4	1	6	2
90	7	1	-8	0	-6	-5	-6	-3	-4	-2	6	4
88	8	-1	-11	-3	-9	-7	-5	-1	-4	-6	5	8
86	9	-3	-9	0	-11	-9	-4	-2	-6	-8	6	11
84	7	-6	-9	5	-12	-10	-7	-5	-7	-11	4	11
82	4	-8	-10	10	-8	-8	-12	-3	-2	-19	1	9
80	4	-9	-8	18	-9	-6	-10	-5	-7	-16	1	6
78	5	-5	-3	15	-3		-17	-9	-11	-19	2	6
76	1	-1	-5	8	-10		-1	-5	-12	-16	2	6
74	-2	0	-1	8	-8		1	-5	-12	-14	3	5
72	-3	2	-6	1	-6		-3	1	-13	-11	3	2
70	-2	-1	-6	-4	3		-2	2	-10	-6	-2	-2

Adelaide NS Standard Deviation 1978-1983

HT	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
100												
98	8	6	1		4		1	2	9	4	4	10
96	6	6	8		5		5	2	10	6	3	12
94	5	4	4		3		2	7	5	8	5	10
92	7	5	3		4		2	5	4	6	7	9
90	6	5	1		0		9	3	4	5	9	6
88	2	4	2		4		3	1	6	5	9	6
86	2	6	6		6		4	4	5	5	12	4
84	6	4	8		8		4	5	7	7	9	2
82	9	3	6		13		8	9	5	4	8	3
80	7	5	1		20		6	12	10	3	5	1
78	8	1	0		20		3	9	10	8	2	2
76	3	7	8		14		16	5	10	7	3	5
74	5	14			16		12	8	9	3	5	6
72	2	13			14		10	3	11	5	4	5
70	2	8			8			5		5	4	0

Adelaide	EW	Mean	1978-1983	(35°S,	138°E)

нт	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
100												
98	23	17	15	2	7	4	-6	1	-10	-11	23	34
96	25	17	18	1	9	4	0	6	-2	-11	21	32
94	24	17	11	0	14	2	1	9	0	-13	19	28
92	23	20	15	8	19	4	10	13	5	-15	11	24
90	20	20	17	17	22	5	13	13	7	-14	10	20
88	13	16	16	20	25	10	11	16	10	-10	3	13
86	7	14	17	26	30	16	14	21	11	-8	-1	7
84	-2	12	20	29	36	25	19	24	13	-9	-7	0
82	-13	2	16	35	43	35	30	29	13	-3	-14	-9
80	-24	-1	14	36	49	46	39	36	29	6	-21	-24
78	-35	-13	16	36	50		44	41	36	5	-31	-36
76	-40	-18	17	43	55		49	39	37	9	-38	-46
74	-45	-23	19	50	55		62	48	35	6	-37	-50
72	-48	-27	20	51	51		57	57	28	7	-34	-55
70	-53	-30	20	43	43		69	58	21	7	-30	-60

Adelaide EW Standard Deviation 1978-1983

HT	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	N DV	DEC
100												
98	8	5	7		3		3	11	8	10	9	8
96	7	6	13		4		6	9	7	8	7	5
94	6	6	1		6		4	9	5	8	5	3
92	7	1	6		6		2	8	6	2	4	4
90	12	2	9		6		7	7	9	3	5	7
88	8	4	8		4		6	4	13	2	6	8
86	8	4	11		7		7	3	9	2	6	8
84	8	4	11		10		4	2	8	1	6	9
82	9	3	6		11		8	6	14	6	4	12
80	7	7	6		13		13	5	0	5	5	11
78	6	13	2		15		6	8	12	6	12	4
76	5	6	1		21		15	15	9	4	2	6
74	7	8			14		13	13	7	4	2	7
72	9	5			2		17	15	19	0	1	10
70	9	7			10			18		6	2	8

Townsville NS Mean 1978-1980 (20°S, 147°E)

HT	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
100												
98	12		14		0	0	0	12	9	11	20	
96	13		9		-3	-8	-3	10	7	11	22	
94	13		5		-8	-15	-7	5	4	10	22	
92	12		2		-11	-17	-15	-15	2	6	17	
90	10		-3		-9	-14	-16	-16	-1	6	13	
88	7		-5		-6	-11	-15	-15	-1	2	6	
86	3		-5		-4	-3	-16	-16	-3	-3	-5	
84	-2		0		0	-10	-11	-11	-5	-8	-19	
82	-4		3		9	-9	-3	-3	-7	-9	-31	
80	-3		5		0	2	5	5	-8	-10	-31	
78	0		10		-4	1	15	15	-10	-6	-3	
76			11		-7	-2	12	12	-12	-10	5	
74			5		-6	-4	6	6	-9	-7	4	
72			-6		-1	-10	4	4	-7	-5	0	
70			4		2	-5	3	3	-6	12	-1	

Townsville EW Mean 1978-1980

нт	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
100												
98	15		15		0	-5	-1	-4	-1	0	14	
96	15		10		7	1	0	-2	-2	-6	9	
94	15		0		10	6	5	0	-3	-12	7	
92	14		-5		16	12	6	2	-6	-15	8	
90	- 11		-9		20	17	10	5	-7	-16	3	
88	11		-12		27	22	17	8	-6	-15	0	
86	9		-14		32	29	23	11	-8	-12	-3	
84	2		-14		34	41	28	7	-7	-12	-2	
82	-4		-17		33	47	34	24	-18	-17	-5	
80	-11		-17		30	43	36	23	-18	-22	-21	
78	-5		-10		26	25	39	25	-15	-19	-32	
76			-1		31	24	36	29	-9	-14	-30	
74			5		31	23	28	27	-2	-12	-34	
72			8		37	26	25	23	3	-4	-38	
70			7		40	25	21	22	9	2	-37	

3.2.1 PLANETARY AND GRAVITY WAVES IN THE MESOSPHERE AND LOWER THERMOSPHERE

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INTRODUCTION

Rocket and ground-based studies of the mesosphere and lower thermosphere show that waves play an important role in the dynamics of their region. The waves manifest themselves in wind, temperature, density, pressure, ionization and airglow fluctuations in the 80-120 km height range. Rockets have enabled the density and temperature structure to be measured with excellent height resolution, while long-term studies of wind motions using MST, partial reflection and meteor radars and, more recently, lidar investigations of temperature and density, have enabled the temporal behaviour of the waves to be better understood.

Figure 1 shows a composite of power spectra of wind motions measured near the mesopause at widely separated locations and illustrates how wave energy is distributed as a function of frequency. The spectra show three distinct parts, viz. (i) a long period section corresponding to periods longer than 24 h, (ii) a section between 12 and 24 h period where the spectra are dominated by narrow peaks associated with the semidiurnal and diurnal tides (see FORBES, this volume) and (iii) a section at periods less than 12 h where the spectral density decreases monotonically (except for the 8 h tidal peak). The long period section is associated with transient planetary scale waves while the short period motions are caused by gravity waves.

PLANETARY WAVES

The narrow spectral peak located near 48 h in the Adelaide data in Figure 1 is a manifestation of the quasi-two-day wave. This is one of a series of travelling global scale waves which have been discovered by long-term wind measurements made by ground-based radars. Spectral analyses of long data sets suggest that the wave energy tends to maximize in local summer (SMITH, 1981; MANSON et al., 1982; VINCENT, 1984b). A range of wave periods has been identified but the most commonly reported periods fall into three well-defined intervals which are 10-20 days, 4 to 7 days and 1.9 to 2.2 days. These are often referred to as the "16-day", "5-day" and "2-day" oscillations, respectively, although precise determination of the periods involved is often not possible. Comparative studies made at different longitudes suggest the waves are westward travelling with the best determinations of wave number being made for the 2- and 5-day waves. The inadequate length of many data sets have necessarily restricted studies of the "16-day" wave, although as continuous radar observations become available, this situation will improve. Table 1 summarizes some of the features of those waves which have been extensively reported, but it should be noted that waves of other periods (e.g., 1.6 to 1.7 days) have been found (CEVOLANI et al., 1983; SALBY and ROPER, 1980).

It is usually assumed that these oscillations are caused by Rossby gravity normal modes forced in the lower atmosphere. These modes are evanescent in the vertical except that in certain height ranges with westward winds (easterlies) and equatorward temperature gradients the waves can be locally propagating. SALBY (1984) has recently reviewed the characteristics of normal modes.

Each mode has a well-defined structure with respect to latitude and longtitude, but in practice it has not always been possible to make a positive

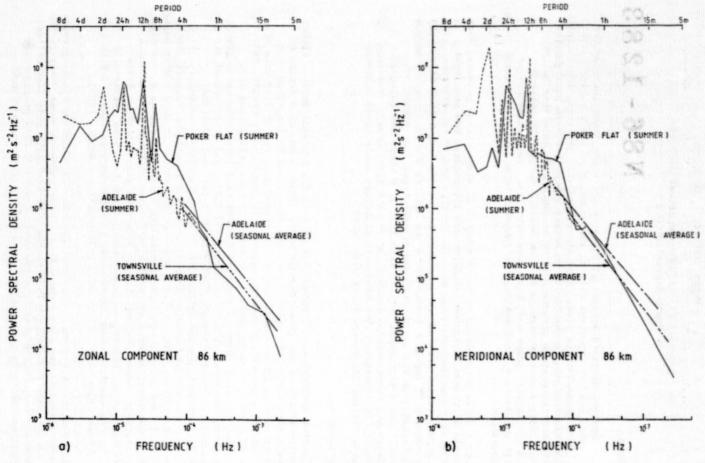


Figure 1. Power spectra of the meridional and zonal wind components observed at Poker Flat (65°S, 138°E) and Townsville (19°S, 147°E). The Poker Flat data is after CARTER and BALSLEY (1982).

Table 1. Characteristics of transient planetary waves

riod(days)	Amplitude(ms-1)	Vertical wavelength(km)	Zonal wave number
10-20	5-10	> 100	1(?)
4-7	5-30	25 to > 100	1
1.9-2.2	10-50	50 to > 100	3

identification from observations in the 80-120 km region because of inadequate geographic coverage. However, an association between 5-day wind oscillations in the mesosphere and a westward travelling wave number one wave in the stratosphere has been found (HIROTA et al., 1983). Satellite radiance studies show evidence for both 5-day and 2-day waves with temperature amplitudes tending to maximize in the lower mesosphere (RODGERS, 1976; RODGERS and PRATA, 1981) with values of about 0.5-0.8 K.

The most extensively studied oscillation is the "2-day" wave and the seasonal and spatial behaviour is now well established. The wave is usually observed in the summer hemisphere reaching maximum amplitudes at about 900 km in July/August in the Northern Hemisphere (MULLER and NELSON, 1978; RODGERS and PRATA, 1981) and in January in the Southern Hemisphere (CRAIG and ELFORD, 1981). Both radar wind measurements and satellite observations show that the wave amplitudes are maximum in the Southern Hemisphere (VINCENT, 1984b; RODGERS and PRATA, 1981). This is illustrated in Figure 2 which shows the mean meridional and zonal wind amplitudes plotted as a function of latitude; it is evident that the maximum response is in the meridional component at southern low-to-mid-latitudes. A hemispheric difference in wave period has also been noted (VINCENT, 1984b) with Northern Hemisphere observations giving periods near 51 h (MULLER and NELSON, 1978; CRAIG et al., 1983) while periods nearer 48 h are reported for the Southern Hemisphere (CRAIG and ELFORD, 1981; CRAIG et al., 1980).

Evidence for travelling planetary waves has also been found in radio soundings of the ionosphere and these often show clear correlations with wave activity in the stratosphere. This is clear evidence for the coupling of wave energy between the stratosphere and ionosphere (BROWN and WILLIAMS, 1971; CAVALIERI et al., 1974; FRASER, 1977). Eastward, as well as westward, travelling waves have been observed.

GRAVITY WAVES

Wave Amplitudes. Figure 1 shows that at a given location, the gravity wave amplitudes are the same for both the zonal (u') and meridional (v') wind componets which show that the perturbation wave amplitudes are on the average isotropic. The spectra show that the energy density (proportional to $\overline{v'^2} = \overline{u'^2 + v'^2}$) follows a power relationship f-k as a function of frequency, f. The exponent k, lies in the range 1.5 to 2.0 (CARTER and BALSLEY, 1982; VINCENT, 1984a) but may change with latitude and season (FREZAL et al., 1981). Averaged over the period range between 12 h and the Vaisala-Brunt period (about 5 min) the rms amplitudes are about 15-20 ms-1 in each component (VINCENT, 1984a) although if the spectrum is assumed to extend out to the inertial frequency (the theoretical lowest frequency for gravity waves) then the rms amplitudes are about 25 ms-1.

Vertical velocity motions are not as easy to measure as the horizontal components. However, measurements made over a range of latitudes with

QUASI 2-DAY WAVE AMPLITUDE / ms-1 IN LOCAL SUMMER AT 95 km

56°N Obninsk 43°N Durham 19°S Townsville 53°N Sheffield (Sh) 34 N Atlanta (A) 35°S Adelaide 52°N Saskatoon (Sa) 34°N Kyoto (K) 43°S Christchurch 47°N Garchy 2°N Mogadishu 67°S Molodezhnaya 45°N Budrio

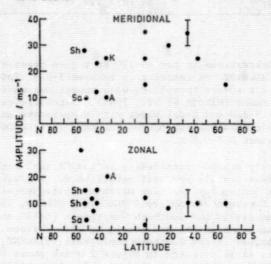


Figure 2. Amplitudes of 2-wave as a function latitude, after VINCENT (1984b).

vertically pointing narrow beam radars give rms amplitudes of the order 1-2 ms⁻¹ (VINCENT, 1984b; FREZAL et al., 1981; WOODMAN and GUILLEN, 1974). Vertical oscillations near the buoyancy frequency are particularly evident (period $^{\circ}5-15$ min).

Temperature and density fluctuations induced by gravity waves have been extensively studied by rockets (THEON et al., 1967; PHILBRICK et al., 1985; PHILBRICK, 1981) and recently by lidars (CHANIN and HAUCHECORNE, 1981). Figure 3 shows vertical profiles of temperature and density. Amplitudes are of the order of 0.5 to 0.1 in fractional density, and these values are consistent with those inferred from the gravity wave motions (VINCENT, 1984a). The figure indicates the very wide range of temperature variations which can be observed at high latitudes with the greatest wave activity occurring in winter (HEATH et al.). Amplitudes as large as 30 K are reached. At midlatitudes the temperature fluctuations are about 10 K.

Seasonal and geographical variations in wave activity are not well known in the 80-120 km height region. What observations are available indicate an annual variation at high latitudes (Figure 3), with maximum amplitudes occurring in winter, and a smaller variation at mid-to-low latitudes with a semiannual variation occurring in the tropics (VINCENT, 1984b; MANSON et al., 1981; FREZAL et al., 1981; THEON et al., 1967; BALSLEY et al., 1983). These observations are in general accord with studies of wave activity in the stratosphere (HIROTA, 1984).

It is emphasized that the amplitudes quoted above are long-term averages. On a time scale of a few hours or so there can be quite significant changes in

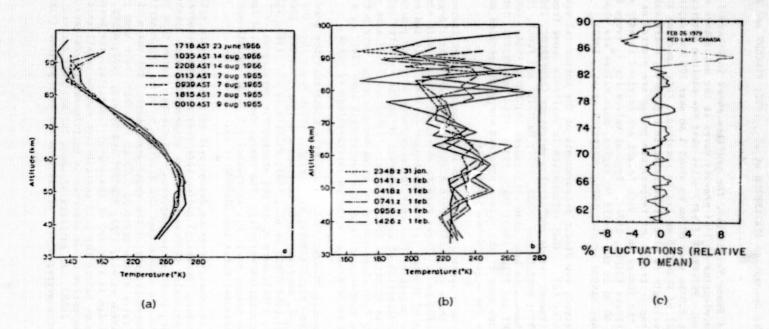


Figure 3. Rocket measurements of temperature in summer (a) and winter (b) at Barrow, Alaska (71°N), after HEATH et al., (c) Vertical profile of neutral density fluctuations (PHILBRICK, 1981).

wave amplitude in the mesosphere (PHILBRICK et al., 1983; VINCENT and REID, 1983).

Wavelengths and Phase Velocities. The profiles shown in Figure 3 indicate that the vertical wavelengths (λ) of gravity waves in the mesosphere are greater than a few km. PHILBRICK (1981) notes that the minimum vertical scale increases from about 1.5 km near 60 km to about 3 km near 100 km despite the fact that scales smaller than 0.5 km can be resolved. This increase in the minimum vertical wavelength is also illustrated in Figure 4a, where values scaled from rocket vapour trails and temperature probes are plotted as a function of height; the change in λ with height are ascribed to eddy and molecular damping effects (HINES, 1974). Typical values for λ range from about 3 km to about 40 km in the 80-120 km region; mean values are about 10 to 12 km (VINCENT, 1984a; MANSON et al., 1982; PHILBRICK et al., 1983).

There are relatively few direct measurements of the horizontal wavelength (λ_h) and phase velocity (c). What information is available comes from photographs of noctilucent clouds and airglow emissions (ARMSTRONG, 1982; FREUND and JACKA, 1979; MOREELS and HERSE, 1977; HAURWITZ and FOGLE, 1969). Indirect estimates have also been made with radars (VINCENT, 1984a; COUNTRYMAN et al., 1981; VINCENT and REID, 1983; REID, 1984; SMITH and FRITTS, 1983). Figures 4a and 4b show some of the values obtained where the periods and phase velocities are given for a ground-based observer.

There seems to be a systematic increase in the mean λ_h with increasing period, whereas the phase velocities do not show any significant change but lie within the range $10-100~{\rm ms}^{-1}$. These results should be treated with some caution for a number of reasons (i) for the longer periods, only indirect estimates are so far possible, (ii) only the magnitudes of \underline{c} are plotted, irrespective of the direction of travel, whereas it is the velocity relative to the mean flow which is important (FRITTS et al., 1984) and (iii) most values of λ_h and c are derived from observations of quasi-monochromatic wave motions, but these may not be representative of the mesospheric wave field as a whole which often appears to consist of a random superposition of waves.

Energy and Momentum Fluxes. It is frequently found that the gravity waves amplitudes do not grow significantly with height, which means that the wave energy, given by $\rho_0 \overline{v}^{-2}$, decreases with increasing height (VINCENT, 1984a; MANSON et al., 1981; COUNTRYMAN et al., 1981; BALSLEY et al., 1983; VINCENT and STUBBS, 1977; HINES, 1965). Here ρ_0 is the atmospheric density and \overline{v}^{-2} is the mean square perturbation velocity. The energy decay is for the form $\exp(-z/h_0)$ where the height scale h_0 , is typically 5 to 12 km although there may be some seasonal variation (MANSON et al., 1981).

The fact that the energy density decays with height indicates either that the waves are saturating (breaking) and/or that they are being externally damped by eddy and molecular processes. Clear evidence for wave breaking may be seen in Figure 3b, which shows temperature gradients greater than the adiabatic lapse rate. In either case the dissipating waves are contributing to the energy and momentum budgets of the upper atmosphere. Estimates of the energy dissipation rates of the order of 0.01 to 0.2 Wkg-1 have been given (VINCENT, 1984a; MANSON et al., 1981; VINCENT and STUBBS, 1977; HINES, 1965). However, more knowledge is required of the energy fluxes into the mesosphere and lower thermosphere before the full contribution can be established. An analysis of 50-60 km period waves observed in noctilucent clouds gave fluxes \(^7.10^{-4}\text{Wm}^{-2}\) (HINES, 1968). An estimate of about 10^{-2}Wm^{-2} was derived for radar measurements averaged over all seasons and wave periods (VINCENT, 1984b).

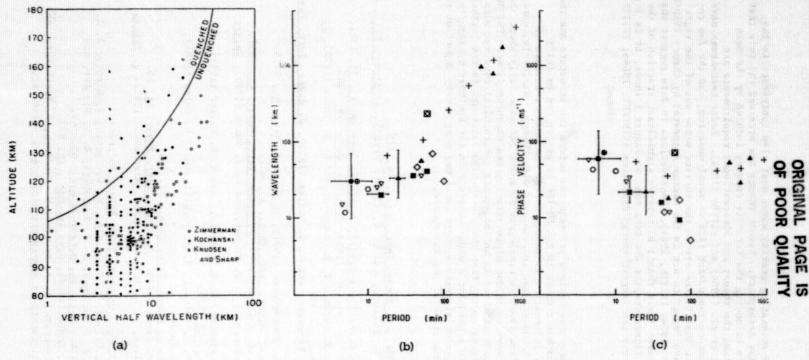


Figure 4. (a) Vertical wavelengths observed in small scale wind structure, the curve shows the theoretical minimum λ_Z (after HINES, 1974).
(b) Plot of gravity wave horizontal wavelength and phase velocity.
(c) As a function of period. Key: ○(FREUND and JACKA, 1979)
○ (HAURWITZ and FOGLE, 1969); ○ (MOREELS and HERSE, 1977); + VINCENT (1984a); ■ (REID, 1984); ● (VINCENT, 1972); ▲ SMITH and FRITTS, 1983);
⊕(COUNTRYMAN et al., 1981); ○ (ARMSTRONG, 1982).

Dissipating and saturating gravity waves must also contribute to the momentum budget of the mesosphere. Recent theory has stressed the role that gravity waves play in balancing the Coriolis torques induced by the mean meridional circulation; the theory and observational requirements are summarized by FRITTS et al. (1984) and FRITTS (1984). Radar techniques have been developed to measure the upward flux of zonal momentum, and the few results to date suggest that fluxes are in the correct sense and of the right magnitude for the wave "drag" to act in the manner suggested by theory (VINCENT and REID, 1983; REID, 1984; FRITTS, 1984). Observations to date suggest that quite short period waves (less than 1 h) carry a significant fraction of the energy and momentum fluxes despite the fact that as Figure 1 shows, it is long period waves which have the largest energy densities (VINCENT, 1984a; FRITTS, 1984).

DISCUSSION

Considerably more observations are required before the structure and the roles played by atmospheric waves in the 80-100 km region can be fully elucidated. Further information is needed before the model structure of planetary waves can be determined and compared with theory. Similarly, more information is required about internal gravity waves and especially about the zonal components of wavelength and phase velocity and momentum fluxes (FRITTS et al., 1984). At present there is an inadequate geographical coverage with many of the observations coming from the mid-to-high latitudes in the Northern Hemisphere. There is a need for a wider coverage in the Southern Hemisphere and especially in equatorial regions where waves may play a very important role in detemining the mean state of the atmosphere.

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3.2.2 ATMOSPHERIC TIDES BETWEEN 80 km AND 120 km

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ABSTRACT

The structure and variability of tides in the 80-120 km height region are reviewed. Particularly emphasized are seasonal-latitudinal variations in the vertical structure of diurnal and semidiurnal winds between 70-110 km as measured by meteor and partial reflection drift radars, and tidal temperatures determined by incoherent scatter radars between 100 and 140 km. Variations in tidal structures with longitude, from day to day, and during equinoctial transition periods are also addressed. A brief summary of the current status of atmospheric tidal modelling is provided.

INTRODUCTION

There are two classifications into which this chapter categorizes tidal observations. The first involves measurements which characterize "average" tidal structures over the period of a month or more, while the second pertains to measurements which delineate variations or deviations from "average" structures over periods from a few days to a month. The data are further subdivided according to the ease with which a particular experimental method determines a specific meteorological variable; that is, winds between roughly 80 km and 100 km in the case of meteor and partial reflection drift radars, and temperatures between 100 and 140 km by incoherent scatter radars. The present review explicitly includes only the more recent observational results and analyses; earlier works may be found in the references cited herein.

AVERAGE TIDAL STRUCTURES

Winds Between 70 km and 110 km. The near-continuous wind data covering the 70-110 km height range over Saskatoon, Canada (52 °N, 107 °W) (MANSON et al., 1981a) are ideal for examining month-to-month and seasonal variations of tides. (Similar studies for previous years at Saskatoon appear in STENING et al., 1978; MANSON et al., 1979, 1984b) Semidiurnal and diurnal tidal winds from winter/summer of 1979/1980 are illustrated in Figure 1. The December-February semidiurnal profiles consistently exhibit a vertical wavelength of order 50 km, with the westerly and northerly velocities in near quadrature. Amplitudes increase from about 10 msec-1 at 70 km to 35 msec-1 at 110 km. During spring equinox there is a transition to typical summer behavior, characterized by velocities of order 5-20 msec-1 and a longer vertical wavelength (>80 km). The diurnal tide exhibits similar features; namely, a near evanescent behavior between April and October and distinctively shorter vertical wavelengths (∿60 km) during the winter months. Amplitudes generally range from 10 to 20 ${
m msec^{-1}}$ from 70 to 110 km, except during January and February when amplitudes attain values of 30 ${
m msec^{-1}}$ at upper levels. The dirunal tide exhibits more variability, however, as indicated (on Figure 1) by the fewer number of days for which a reliable diurnal harmonic was able to be extracted from the fit.

The above seasonal characteristics are generally well established at midlatiude stations. Based on seasonal behaviors reported at Garchy (47°N, 3°E), Urbana (40°N, 88°W), Adelaide (35°S, 139°E), and Atlanta (34°N, 84°W), AHMED and ROPER (1983) find the following picture of the seasonal-latitudinal structure of semidiurnal tides in the meteor wind region: in summer, presence

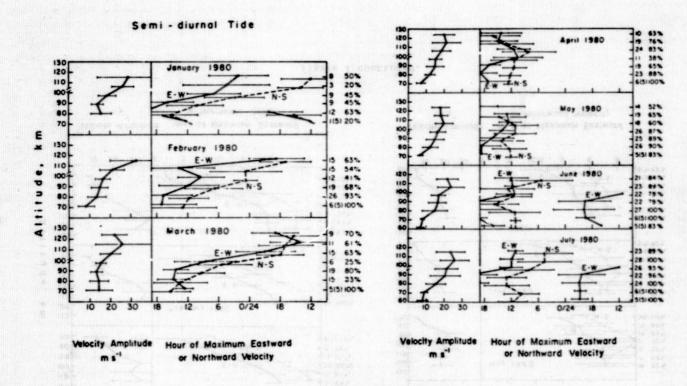


Figure 1. Means and standard deviations of semidiurnal and diurnal tidal winds observed at Saskatoon during 1979-1980.

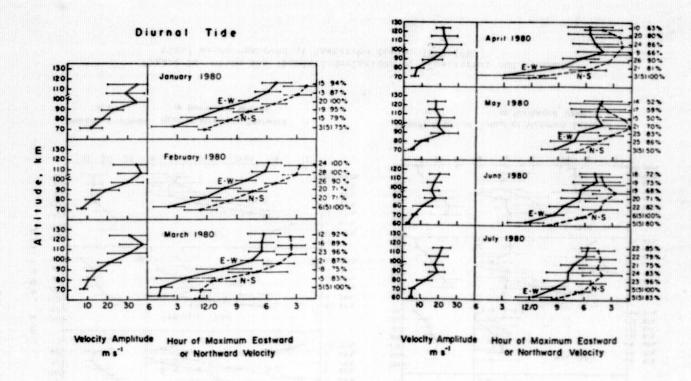


Figure 1 continued.

of long-wavelength ($\lambda \ge 120$ km) structures suggest predominance of the (2,2) and perhaps (2,3) modes. This behavior extends through autumn at all stations, except at Urbana where the observed wavelength is of order 42 km (ENGE and AVERY, 1979). In a recent study of the summer wind field at Poker Flat, Alaska (65°N), CARTER and BALSLEY (1982) find semidiurnal vertical wavelengths of roughly 30 km. This is not necessarily inconsistent with the observed long vertical wavelengths at lower latitudes as indicated by the theoretical models discussed later in this paper. During winter, shorter vertical wavelengths generally prevail: Poker Flat (~15 km), Saskatoon (~60 km), Garchy (~35 km), Urbana (~74 km), Atlanta (~63 km), suggesting presence of the (2,4) and (2,5) modes. It is curious that while the meridional component measured at Atlanta is characterized by λ_z .63 km, λ_z is of order 120 km in the zonal component. The difficulty of ascribing a single mode to observations at a given station is clearly an issue. AHMED and ROPER (1983) further note that evidence exists for even shorter wavelengths during spring: Atlanta (~34 km), and Urbana (~54 km). Irregular phase structures are observed at Garchy during spring. The shift from typically short (~30-60 km) winter/spring wavelengths to long (≥100 km) summertime wavelengths appears to occur over a rather short (~2 weeks) spring transition period. The genernal shift from long wavelength behavior in summer to shorter characteristic wavelengths during winter is also substantiated by a more recent study (TSUDA et al., 1983) of data at the Kyoto, Japan (35°N, 136°E) meteor radar. Early seasonal studies covering several years of meteor wind data include those by MULLER (1966) for three stations in Great Britain and ELFORD (1973) at Adelaide, South Australia. AHMED and ROPER (1983) find it difficult to specify a characteristic seasonal-latitudinal behavior for the diurnal tide. Generally, the diurnal tide is evanescent at high latitudes (Poker Flat, Saskatoon) and propagating with short vertical wavelengths (≤30 km) at low latitudes (Arecibo, Townsville, Jicamarca). At midlatitudes (Garchy, Urbana, Atlanta, Adelaide) a variety of vertical structures can occur depending on phase interference between the evanescent and propagating components (FORBES, 1982a), making it difficult to define a "typical" structure.

Geographically symmetric radars at Kyoto (36°N) and Adelaide (36°S) delineate strongly asymmetric tidal behavior about the equator in both diurnal and semidiurnal components between 80 and 100 km altitude (ASO et al., 1979). Height profiles for the average tidal amplitudes and phases observed at Kyoto, Adelaide, as well as Townsville (19°S) for the period 14-29 March 1979, are illustrated in Figure 2. (Structures are also given on a day-by-day basis by these authors, illustrating strikingly similar characteristics to the mean values in Figure 2.) The diurnal amplitudes at Adelaide and Townsville are twice as large ($^{\vee}20-35~\rm msec^{-1}$) as at Kyoto, and clearly reflect a peak in the amplitude profile near 95 km and downward phase progression with height ($^{\lambda}_{\rm Z}$ 35 km), whereas the Kyoto structures are much more evanescent in nature. Further, the westerly and northerly velocities are in quadrature at Adelaide, but in antiphase at Kyoto. Theoretically one might anticipate that the observed differences could be accounted for by:

 Asymmetric forcing due to insolation absorption by 03 or H20, either in the migrating trapped and propagaing components, or possibly in nonmigrating modes; or

 Latitudinal "distortion" of the (1,1) mode due to asymmetries in background zonal winds (LINDZEN, 1972).

The semidiurnal amplitudes observed at these stations, often less than 10 msec-1, are substantially less than the observed diurnal variations. It is more difficult to say anything definitive about the semidiurnal phases except that they all exhibit substantial latitude asymmetries. It is easier to see the origin of latitudinal asymmetries in the semidiurnal tide than the diurnal tide due to the greater degree of mode coupling due to background zonal winds, and the greater sensitivity of the thermal excitation on solar zenith angle.

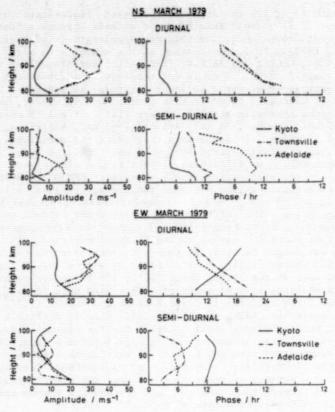


Figure 2. Height profiles of average tidal amplitudes and phases of winds observed at Adelaide, Townsville, and Kyoto for March 1979. (from ASO and VINCENT, 1982).

Evidence of asymmetric semidiurnal tidal components during equinox has been reported previously in the 100-130 km height region (LINDZEN, 1976). ASO and VINCENT (1982) find similar asymmetries during periods in September 1979 and January 1980. Other observations independently reported at Kyoto, Adelaide, and Townsville facilities during the past few years include those reported by ASO et al. (1979, 1980), VINCENT and BALL (1977, 1981), and VINCENT and STUBBS (1977).

TEMPERATURES BETWEEN 100 KM AND 130 KM

Daytime temperature determinations from 151 days of incoherent scatter radar measurements at Millstone Hill (42°N) from 1970 to 1975 are analyzed by WAND (1983) to characterize the semidiurnal temperature oscillation in the lower thermosphere (100-130 km). The annual mean semidiurnal oscillation has a maximum amplitude of 27 K at 115 km and a vertical wavelength of 47 km. Variations associated with season are large, for example, 17 K in amplitude and 1.2 h in phase at 115 km when referred to the annual mean semidiurnal vector. Generally, the altitude of maximum is lowest at the solstices and the longest vertical wavelength occurs in winter. (Note that this seasonal variation in vertical wavelength is opposite that observed in the semidiurnal winds between 80 and 100 km.) Wand notes that semidiurnal temperature measurements from Saint Santin show good agreement with the Millstone Hill

results in winter but some significant amplitude and phase differences are apparent in other seasons.

Between 1972 and 1975 approximately 30 days of simultaneous measurements of E-region neutral temperatures were made at the Arecibo (18°N) and Millstone Hill (42°N) observatories. Many of these results are reported by SALAH and WAND (1974), SALAH et al. (1975), SALAH (1974), and WAND (1976). for the present paper, 25 days of the better quality data with good seasonal coverage have been selected for examination. Seasonal averages of the semidiurnal temperatures measured at Arecibo and Millstone Hill are compared in Figure 3. The Millstone Hill amplitude profile is characterized by a peak near 110-115 km which varies in amplitude from 45 K (summer, equinox) to 60 K (winter). The Arecibo temperatures generally do not exhibit a well-defined peak. Both stations exhibit a downward phase progression with characteristic vertical scales of 30-45 km. Further, the Millstone Hill phases lead those at Arecibo by about 4 hours in summer and lag the Arecibo phases by 4-6 hours during winter. These amplitude and phase characteristics have led to the speculation that the observations reflect the strong presence of (2,4) and 2,5) semidiurnal tidal modes propagating upwards from below 100 km (LINDZEN, 1976).

THE VARIABILITY OF TIDES

Having established gross features of the vertical, latitudinal, and seasonal structures of tides in the upper mesosphere, attention has recently turned toward investigating the variability of tides on shorter time scales. For instance, details of the equinoctial transition of semidiurnal tidal structures (from typical winter to summer characteristics as described previously) has been examined by MANSON et al. (1981a) at Saskatoon. Their

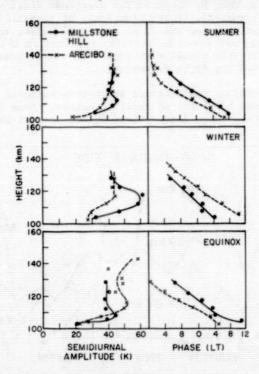


Figure 3. Seasonal averages of semidiurnal temperatures derived from 25 simultaneous daytime experiments at Arecibo and Millstone Hill.

data for the 1981 spring transition are illustrated in Figure 4. The transition from vertical wavelengths typical of March (~35-40 km) to April (\geq 80 km) occurs over a period less than two weeks. The semidiurnal phase near 90 km typically experiences a phase shift from 0600 h to 0300 h over a similar time scale. This can be compared to a total phase shift (over about a month) from about 0800 h and 0300 h from typical winter to summer conditions at Saskatoon. The fall transition occurs over a period at least twice as long as the spring transition. An examination of mean temperature and flow characteristics during the Spring 1981 period indicated that the background atmosphere transition is a much slower process extending into May before completion occurs (MANSON et al., 1981a). This would suggest that seasonal tidal characteristics may be more strongly associated with variations in the thermotidal forcing than coupling effects due to asymmetric mean meridional temperature gradients and zonal winds (see also discussion on theoretical models).

A significant degree of tidal variability over time scales on the order of days has also been established, as clearly illustrated in the band-pass filtered Garchy data in Figure 5 (GLASS et al., 1978). BERNARD (1981) suggests that if the intrinsic time to set up stationarity around the earth for a particular mode is greater than a characteristic time scale associated with the variability, then transient effects would exert some influence over the observed "tidal" behavior. One might then ask to what extent we can discuss the existence of a "mode" and ascribe to it a characteristic horizontal and vertical structure. The horizontal group velocity (VgH) of a tidal mode can be approximated by that of an equivalent gravity wave at the latitude where the vertical group velocity (V__) of the gravity wave is identical to that of the tide (RICHMOND, 1975; SPIZZICHINO, 1969). A charactertistic propagation time (T,) around the earth can then be computed for pertinent tidal modes in the earth's atmosphere and compared with the time scale of variability. Values of can be as great as ten days for the (2,6) and (1,1) modes, and hence the condition of stationarity may never be strictly realized in practice. However, the exact implications of this result with regard to distortions of the normal shape of these "modes" remains to be determined.

The dominant source(s) of the observed short-term temporal variability is basically unknown, and may be global or local in nature. Some possibilities include instability and nonlinear interactions in the case of the diurnal

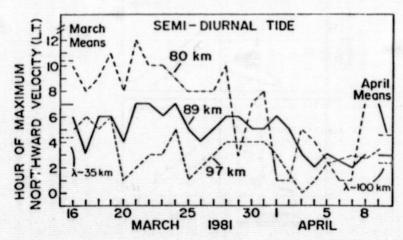


Figure 4. Spring transition of semidiurnal phase at Saskatoon for 1981. (from MANSON et al., 1981a).

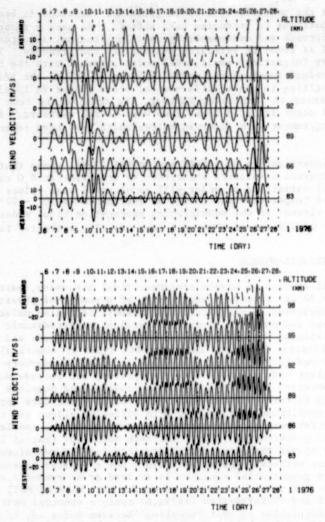


Figure 5. Band-pass filtered westerly velocities from the Garchy radar measurements at the diurnal frequency (top), and semi-diurnal frequency (bottom). (from GLASS et al., 1978).

propagating tide, variations in thermotidal heating (i.e., 03 and H20 concentrations) or background wind and temperature structure, or the tidal modultion of gravity wave momentum deposition into the mean flow (WALTERSCHEID, 1981). The mechanism most plausible to this author is simply that relatively slight changes in the phases of individual modes can result in interference patterns, which cause the day-to-day changes in the total tidal variation to be fairly significant. Such interference effects are discussed extensively by TSUDA et al. (1983).

Relatively few data comparisons have been performed to ascertain the presence of nonmigrating tides, which would give rise to longitudinal differences in tidal structure. Evidence of longitudinal differences in phase up to 1.5 h is reported by GLASS et al. (1975). Since his excitation model reveals little evidence of longitudinal variations in ozone heating, BERNARD

(1981) examines the possible role of longitudinal variation in background atmospheric conditions in producing such effects. He uses a second-order perturbation approach and assumes background longitudinal structure of wave numbers 1 and 2 as found in satellite temperature measurements. Bernard finds that the primary (migrating) semidiurnal modes interact with the background structure to produce nonmigrating modes as large as 50% of the primary tidal amplitudes, resulting in phase difference of order 1 hour in local time over 67 -120 differences in longitude. Further, the coupling is such that the time of maximum will occur later in local time when moving westward. Both of these trends are in agreement with observed values which have been reported (GLASS et al., 1975).

A recent investigation by FORBES and GROVES (1984) shows that longitude variations in diurnal insolation absorption by tropospheric $\rm H_2O$ can account for longitudinal variations of order $\pm 15\%$ about zonal mean values in the diurnal wind and temperature amplitudes at low latitudes (0° - 20°) between 80 and 100 km, by virtue of the nonmigrating propagation tidal modes which are excited. Phase variations of about \pm 1 hour are also estimated to occur.

STATUS OF THEORETICAL MODELS

Theoretical studies of middle atmoshere tidal phenomena, particularly at upper levels (> 70 km) require investigation of a number of physical processes beyond those considered in classical tidal theory, including molecular and eddy diffusion of heat and momentum, Newtonian cooling, electrodynamic forces, compostion variations, and interactions with background winds and meridional temperature gradients. There are basically two types of numerical models which have been developed in recent years to siumulate middle atmoshere tides. The first genre neglect eddy and molecular dissipation, but include mean winds and meridional temperature gradients, Newtonian cooling, and possibly a Rayleigh friction term to filter out small-scale noise or to facilitate application of upper boundary conditions. Dispensing with diffusion allows one to derive a single second order partial differential equation in height and latitude for the perturbation geopotential. The first such model was that of LINDZEN and HONG (1974) who solved the geopotential equation for the semidiurnal tide using finite difference methods. ASO et al. (1982) use a similar approach, except that the lengthy geopotential equation is arrived at by symbolic computer software rather than manual algebraic manipulation. WALTERSCHEID et al. (1980) and WALTERSCHEID and VENKATESWARAN (1979a,b) apply a spectral method of tackling the same problem so that "coupling" between modes can be more explicity studied. The latter two studies, while still restricted to the semidiurnal tide, utilize more detailed specifications of the background atmosphere and thermal excitation than does the LINDZEN and HONG (1974) study.

At the next hierarchal level of modelling pertaining to middle atmosphere tides, FORBES (1982a,b) includes eddy and molecular diffusion of momentum and heat so as to properly address the structural modification of tides in the 80-120 km region and their penetration into the upper thermosphere. This requires numerical solution of the four coupled partial differential equations in the 3 velocity components and temperature, as opposed to a single equation for the geopotential as in the above studies. Forbes provides explicit simulations from the surface to 400 km for the solar diurnal, solar semidiurnal, and lunar semidiurnal tides due to realisitic thermal and gravitational forcing, as well as normalized thermospheric extensions of solar semidiurnal modes above 80 km of use in the fitting, extrapolation, and interpolation of observations data (FORBES and HAGAN, 1982).

An important issue that has been addressed by the above studies concerns the relative importance of tidal mode excitation due to (direct) thermal or (indirect) mode coupling processes. The (2,4) mode appears to receive about equal contributions from direct thermal forcing and mode coupling via the (2,2) mean wind interaction which tend to add in phase. On the other hand, for the (2,3) mode the effect of mode coupling is to interfere with the directly forced component and to substantially reduce the (2,3) response above the level of ozone heating. In the case of (2,5) excitation appears to arise almost exclusively due to direct thermal forcing (mode couling is weak). Difficulties in modelling and interpreting observations of semidiurnal tides in the 80 - 100 km region are expected due to the joint presence of the (2,2), (2,3), (2,4) and (2,5) modes; that is, even slight (~1-2 hours) relative phase shifts among these components can lead to considerable changes in the total semidiurnal variation from day to day and with respect to latitude and height. The specific tidal structure in this region is sensitive to the thermal excitation, background mean wind distribution, and other atmospheric properties that the above models have only attempted to parameterize in a very "average" sense.

ACKNOWLEDGEMENT

Preparation of this work was supported under NSF Grant ATM-8113078.

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3.2.3. TURBULENCE IN THE ALTITUDE REGION 80-120 KM

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ABSTRACT

Measurements of turbulent energy dissipation rates and eddy diffusion coefficients have been collated, and mean height profiles of fundamental turbulence parameters in the region 80-120 km are presented.

INTRODUCTION

It is generally agreed that there is significant turbulence in the region 80-120 km, although there is still some debate as to its temporal and spatial morphology. The main sources of turbulence are probably gravity waves and tides, and these generate turbulence by processes such as nonlinear breaking, shear instabilities, convective overturning and critical-level interactions. (e.g. LINDZEN, 1981; TEITELBAUM and SIDI, 1976; SIDI and TEITELBAUM 1978; HODGES 1969; JONES and HOUGHTON, 1971). Observations of turbulence have often shown turbulence to appear in horizontal laminae of thicknesses of a few kilometres or less, interspersed with nonturbulent regions (e.g. BLAMONT and BARAT, 1967; LLOYD et al., 1972; ROTTGER et al., 1979), and it appears that turbulence is both spatially and temporally intermittent. Turbulence appears to occur in patches (e.g., ANANDARAO et al., 1978). ZIMMERMAN and MURPHY (1977) have presented data to suggest that turbulence occurs from 20% and 80% of the time in the height region 80-100 km. Generally though, turbulence is important up to an altitude of between 95 and 110 km, whereupon the atmospheric viscosity becomes so large that it quickly damps any tendency to turbulence. This transition region is called the "turbopause".

Turbulence is characterized by two important features, which will form the basis of its quantization in this article. Firstly, turbulence causes diffusion, and secondly, it heats its environment. In laminar flow, the rate of diffusion of momentum is represented by the viscosity ν , and the rate of transfer of temperature is represented by the thermal diffusivity k_t . For the case of turbulence, similar equations apply to those of laminar flow, but ν is replaced by the "turbulent eddy viscosity" K_t (also called the momentum diffusion coefficient), and k_t is replaced by the parameter K_t . The ratio K_t/K_t is a constant, written as "Pr", the Prandtl number. In air, $P_t^m \gtrsim 0.7$, so K_t and K_t are very similar, and often both are loosely denoted as "K". The rate of diffusion of minor constituents is controlled by K_t . In much of this paper, we will be looking only at small scales (less than $t \sim 5$ km). The vertical eddy diffusion coefficient obtained at these scales is also the vertical diffusion coefficient over all scales, since vertical eddies of sizes greater than about 1 to 5 km are highly suppressed. This diffusion coefficient is often denoted K_t , to indicate vertical diffusion. Horizontal diffusion occurs at much larger scales, (often denoted K_t K_t and is much faster than vertical diffusion. However, only K_t will be dealt with in this work. For further discussion of K_t , K_t , the reader is referred to EBEL (1980).

For the molecular case for a gas, the viscosity and thermal diffusivity are proportional to the product of the molecular mean free path and the mean molecular speed. It is usual to regard $K_{\underline{t}}$ and $K_{\underline{t}}$ as a similar product of a typical scale and typical velocity, and for approximate calculations it is common to write

$$K_{\underline{L}} \wedge L_{\underline{B}} V_{\underline{L}}$$
 (1)

where $L_{\rm B}$ is a "typical" scale, and $v_{\rm L}$ is the eddy velocity associated with this scale. More will be said of these "typical scales" later.

A general feature of three-dimensional turbulence is the energy transfer direction. Some large-scale feature such as a wind shear or temperature instability becomes unstable, and generates smaller scale cyclic motions. These motions generate smaller rotational random motions, and these new ones generate others. Eventually extremely small scales are reached, at which the small-scale shears are so large that molecular viscous forces become important and the energy is deposited as heat in the atmosphere. The rate at which heat is deposited will be denoted by "ɛ" here. Actually, energy is not only lost from turbulence at the smallest scales. It is lost at all scales, but most of the heat loss is at the smaller scales. Some energy can also be lost at larger scales by the weak radiation of buoyancy waves and also by modification of the temperature profile. These processes will not be parameterized here, but it is important to note that they do occur (e.g., JUSTUS 1967a; LLOYD et al.1972; WEINSTOCK, 1978a).

2. KOLMOGOROFF THEORY

Many of the measurements of K and © presented in this paper were deduced under the assumption that the turbulence being observed obeyed the classical Kolmogoroff theory of inertial-range turbulence (KOLMOGOROFF, 1941; TATARSKI, 1961). Many authors who used this theory commented on the possible inappropriateness of it to the lower thermosphere, but due to lack of alternative theories were forced to use it.

Indeed, it would not be surprising if the Kolmogoroff theory did not apply to the lower thermosphere. For example, the upper part of the region generally has a very stable temperature profile, something like that of the stratosphere, so buoyancy forces could well be important in producing anisotropic turbulence. However, high resolution measurements in the stratosphere (EARAT, 1982) have shown that in any turbulent layer, there is some part of the spatial spectrum which obeys the $k^{-5/3}$ spectrum predicted by Kolmogoroff, and the smallest and largest scales which obey this relation also agree nicely with theory.

A more serious difficulty for the thermosphere is the separation of the smallest and largest scales, or, equivalently, the value of the Reynolds' number. For Kolmogoroff's theory to apply, it is necessary that the Reynolds' number be very large (BATCHELOR, 1953). The Reynolds' number for the atmosphere is defined as

$$R_e \sim \frac{L_B v_L}{v}$$
 , $(\sim K/v \text{ from (1)})$

in analogy with flow in pipes, where L_B is a typical "outer scale", and $_5v_L$ is the velocity associated with scale $_{L_B}$. In the troposphere, $_{\nu}$ $_{\nu}$ $_{10}^{-5}v_L$ m 2 s $^{-1}$, L_B $_{\nu}$ $_{100}$ m $^{-1}$ km and $_{v_L}$ $_{\nu}$ $_{1-10}$ ms $^{-1}$. Hence R_e $_{\nu}$ $_{10}^{7}$ -10 9 , which is satisfactorily large. However, in the lower thermosphere $_{\nu}$ $_{\nu}$ 1 m² s $^{-1}$, (e.g., see Figure 3a) whilst $_{L_B}$ and $_{v_L}$ are similar to the tropospheric values. Hence R_e is < 10 2 -10 4 , and values of 100 or so may not be large enough to maintain an inertial subrange.

Nevertheless, the little experimental data available suggests that the turbulence at least tries to tend to a $k^{-5/3}$ structure (e.g., ZIMMERMAN et

al., 1971; 500KER and COHEN, 1956) at least in conditions of weak to moderate wind shear. For stronger wind shears, other theories (e.g., TCHEN, 1954) have occasionally been invoked.

The region 80-120 km is a difficult region to study. It is too low for insitu satellite measurements, too high for balloons, and too high for satellite remote sensing with adequate vertical resolution. Measurements of and K must be made by somewhat indirect means, and are therefore difficult. Given the apparent tendency for the atmosphere to at least try and approach an "inertial" spectrum, it will be assumed in this article that the Kolmogoroff theory may be approximately applied; this may mean some systematic errors in some of the profiles presented, but certainly the profiles should be applicable to accuracies of, at worst, a factor of 3, if not better.

It is freely admitted that the Kolmogoroff theory may not be an exact description of thermospheric turbulence.

3. RELATIONS BETWEEN K, ε AND THE SCALES OF TURBULENCE

The inertial range theory of Kolmogoroff applies between two scales, L_B and ℓ . The first (larger) is called the outer scale of turbulence, the second the inner scale. Within this range, viscosity has negligible effect. However, at scales less than ℓ , energy dissipation due to viscous forces becomes important. The so-called "Kolmogoroff microscale", $^\eta$, is a scale well within this range of viscous dissipation, and is defined by

$$n = (\sqrt{3}/\varepsilon)^{1/4}.$$
 (3)

It can be shown that $\ell_0 \approx 7.2\eta$ (e.g., HILL and CLIFFORD, 1978). It can also be shown that the outer scale is a function of ϵ , and is given by

$$L_{\mathbf{B}} \approx c_{1} \varepsilon^{1/2} \omega_{\mathbf{B}}^{-3/2} \tag{4}$$

(e.g., WEINSTOCK, 1978b). Here, ω_B is the Brunt-Vaisala angular frequency. Weinstock suggested that $c_1 ~ \% ~ 2\pi/0.62$.

Finally K and ε can be shown to be related by the expression

$$K \approx c_2 \epsilon / \omega_B^2$$
 (5)

and various authors have suggested values for c_2 . WEINSTOCK (1978b) suggested that $c_2 \gtrsim 0.8$, whilst LILLY et al. (1974) suggested $c_2 \gtrsim 0.33$. CHANDRA (1980) took $c_2 = 0.6$. It appears that c_2 lies between 0.2 and 1.0.

Both (4) and (5) only apply in conditions of static stability, when $\omega_{\rm B}^{2}$ is positive. If turbulence is generated by convective processes, then (5) is clearly not valid.

The three equations (3), (4) and (5) together with the expression 2.7.2 η form the main relation to be used in this article. However, it is also useful to note that

$$L_B/\eta \approx (R_e)^{3/4}$$
, (6)

where R is the Reynolds' number (see (2)). Thus the separation of the inner and outer scales is a very simple function of R.

4. THE TURBOPAUSE

The molecular kinematic viscosity ν increases exponentially with increasing height in the atmosphere, and at some height it becomes greater than the eddy viscosity K. The height at which $K \not\approx \nu$ (or equivalently, the Reynolds' number R =1) is the turbopause. When this occurs, it may be seen from (6) that $L_B \sim \eta$. Hence, near the turbopause there can be no inertial range of turbulence whatsoever. The scales at which turbulence generation could occur are comparable to those at which viscous forces are important, and any mechanism which attemps to induce turbulence is very quickly damped.

The height of the turbopause varies because ϵ varies. At the turbopause ν = K, so that $\epsilon^{\gamma} \nu \omega_{\rm p}^{2}$. Larger values of ϵ allow larger ν values, pushing the turbopause height up.

The turbopause was first observed experimentally with rocket vapour trail measurements. The trails appeared turbulent up to the turbopause, and then quite suddenly became laminar above the height. The reason for the rapid change lies largely in the exponential increase in v with height. When a vapour trail forms, it first diffuses by molecular processes, until a time $t_\eta \sim (\frac{\nu}{\varepsilon})^{1/2}$ after release. Then the trail begins to appear turbulent. The kinematic viscosity increases exponentially with height, and near the turbopause, this transition time may typically increase from less than a minute to greater than 2 minutes in less than about 5-6 kms. Thus the trail appears laminar for a considerable time at the higher heights. This, coupled with higher damping which turbulence experiences due to the larger viscosity, results in the appearance of a rapid transition to laminar flow in the vapour trails. However, careful observation has shown that there can be evidence of turbulence up to latitudes as high as v 130 km (e.g. REES et al., 1972). Nevertheless, the turbopause does truly represent a level above which turbulence plays only a minor role. The height of the turbopause as a function of latitude and season would be useful to parameterize, but due to insufficient data no attempt has been made to do this in this paper.

5. METHODS OF DETERMINATION OF ε AND K

Determinations of & and K values can be broadly classified into two types:

- (i) measurements of small scale motions (< 5 km) by direct observation, and
- (ii) large scale studies of the balance of heat and inert ch. wical species in the atmosphere.

The first method usually (though not always) results in direct measurements of ε , whilst the second results in direct measurements of K. It is usually in the first method that it is necessary to assume that the Kolmogoroff spectrum applies. This is not necessary in the second, but the second method suffers from other weaknesses which will be discussed later.

6. DIRECT DETERMINATIONS OF ε .

Most direct measurements of ϵ in the height range 80-120km have been made either by rocket measurements or radar, with one or two measurements by airglow techniques.

(a) Rocket Techniques

Most measurements of ϵ via rocket techniques have involved release of chemoluminescent compounds from a rocket, and then watching these evolve with time. This is a technique initiated by the work of Blamont (e.g., BLAMONT, 1963). These releases have either taken the form of explosions which produced

luminescent clouds, or "slow burns" which released the reactive components slowly as the rocket progressed, resulting in a long trail of luminescence. High resolution photographs of these clouds or trails were then recorded for several minutes after the release. Because of the need to photograph the clouds, these experiments have been restricted to nighttime and twilight periods. The mean drift of the cloud gave the wind velocity, and the growth of the cloud gave information concerning the turbulence. Generally, the trails grew first in a laminar way, with the trails "radius" r (see shortly for more concerning the definition of r) increasing approximately in the manner

$$(r-r_0)^2 \alpha t, \qquad (7)$$

t=0 being the time at which molecular diffusion begins and r_0 the radius at time t=0. Then, after a characteristic time $\tau_\eta \sim (\frac{\nu}{\epsilon})^{1/2}$, turbulence sets in, and the trail expands more rapidly. Theory suggests that the relation

$$r^2 \gtrsim \beta \epsilon t^3$$
 (8)

should be obeyed (e.g., BATCHELOR, 1950). The constant β is known from theory, so one method by which ϵ can be obtained is by examining the expansion of the trail according to (8) and thus finding ϵ .

There are problems with this method. One such problem occurs in defining zero time; the trails and clouds expand initially by nondiffusive mechanisms, such as heat gradients and explosive motions (e.g. ZIMMERMAN, 1968). Problems also exist in defining the trail "radius". The most rigorous definition of r would be to use the trail autocorrelation half width, but this was often difficult to find and was not always used.

REES et al. (1972) did not utilize (8) but rather examined the trail expansion to find the time τ_{η} when the trail_expansion changed from (7) to (8). They then found ε via the relation $\varepsilon= v\tau_{\eta}$. Nevertheless, there are uncertainties in taking this as an equality.

JUSTUS (1967a) did not use either of these methods, but used a more precise formulation which required detailed knowledge of all three components of velocity and their spatial gradients. It is not clear whether adequate accuracy and resolution of these velocity components were actually attained.

ZIMMERMAN and MURPHY (1977) obtained both winds by cloud releases and temperature profiles by grenade experiments, and thus tried to calculate the Richardson number as a function of altitude. However, in connection with this data, it should be noted that grenade experiments cannot achieve a resolution of better than about 1-5 km and this may be too poor to really give good estimates of the Richardson number. Tropospheric observations of relations between Richardson number, wind speed, and turbulence intensity were applied to estimate the mean square eddy velocity, <w >> . Then the relation

$$\varepsilon \stackrel{\sim}{\sim} \frac{1}{3.4} < w^2 > \omega_{\rm B} \tag{9}$$

was used to estimate ϵ . Some later work by WEINSTOCK (1981) suggested that the relation should more appropriately be

$$\varepsilon = 0.4 < w^2 > \omega_{\rm R} \tag{10}$$

and all the values of ZIMMERMAN and MURPHY (1977) have been corrected to suit (10) in this text.

ZIMMERMAN and ROSENBERG (1972) used HINES' (1961) theory of the relation between viscosity and the minimum vertical wavelength of gravity waves to help

extract turbulence parameters, and another method used involved calculations of structure functions from high resolution winds (ROPER, 1966).

It has at times been claimed that rocket measurements of turbulence are unreliable, because the rocket, or even the chemical release itself, could induce the turbulence (e.g. LAYZER and BEDINGER, 1969). This does not appear to be the case, since rocket results show good agreement with remote sensing measurements such as radar observations, which do not suffer from this possibility, but the possibility that the rocket could produce the turbulence must nevertheless be considered.

(b) Radar Techniques

The main two radar techniques involve (i) observations of meteor trails and (ii) medium frequency observations of radar fading times. The former method was originally implemented in detail by ELFORD and ROPER (1967) (based on earlier work done at Jodrell Bank, e.g. GREENHOW and NEUFELD, 1959) and involves firstly measurement or velocities transverse to the meteor trail alignment, and thence formation of the structure function

$$D_{tt}^{2} < |v_t(\underline{x}) - v_t(\underline{x} + \underline{r})|^2 >$$

vt being the velocity perpendicular to r.

According to theory,

$$D_{tt}^2 = 4/3 C_v^2 \epsilon^{2/3} r^{2/3}$$

in the inertial range, and recent measurements give ${\rm C_v}^2$ = 2.0 (e.g. KAIMAL et al., 1972). However, Elford and Roper assumed that

$$D_{tt}^2 = 4.82 \ \epsilon^{2/3} r^{2/3}$$
.

For this paper, values presented by ELFORD and ROPER (1967) have been corrected to satisfy the former formula. McAVANEY (1970) also applied this method, and ϵ values obtained have been similarly adjusted. More recently FELLOUS and FREZAL (1981) have also applied a similar meteor method.

When a backscatter radar with a narrow beam is used, it is possible to measure the mean square fluctuating velocity of the scatters by utilizing the spectral width of the received signal. Both HOCKING (1983a,b) and MANSON et al. (1980, 1981) have applied this technique, and have used a formula similar to (10) to obtain ε . It is important to remove other contaminating effects such as "beam-broadening" when applying this method, and these authors did this. However, MANSON et al. (1980, 1981) used a very wide polar diagram, and as pointed out by HOCKING (1983a,b), this can lead to contamination from larger scale horizontal fluctuating motions (e.g. gravity waves), particularly in conditions of weak turbulence. Thus the values recorded by MANSON et al. (1980 1981) are at best upper limits on ε , and must be treated with caution. In this paper, the results of MANSON et al., and HOCKING (1983a,b) have been adjusted so that (10) is obeyed.

One final way by which energy dissipation rates can be obtained is to examine the decay of gravity wave energy with height, and this has been done by VINCENT and STUBBS (1977), MANSON et al. (1980), VINCENT and BALL (1981) and VINCENT (1984).

7. TYPICAL ENERGY DISSIPATION RATES

All techniques discussed above have some form of possible errors, be they

resolution problems, contamination by gravity waves or uncertainty as to the values of certain constants. Nevertheless, most methods are moderately sound in principle, and all results obtained by such methods are shown in Figure 1, together with plots of the means and medians (where possible) for the three latitude bands 0°-20°, 21°-50° and 51°-90°. The means were taken at 1 km intervals, whilst medians refer to 3 km bands. The horizontal lines represent one standard deviation for the mean. Originally, the data were also divided into three seasons: summer, winter, and equinox. At $21^{\circ}-50^{\circ}$, ϵ appeared to be largely independent of season, and below 20° there was insufficient data to consider each season separately. Thus the three seasons for these latitude belts have been merged. If there was any trend for 21°-50°, it was that summer values were greater than winter which were greater than equinox at 65-90 km, but the total variation was less than a factor of 3. This is a different seasonal trend to that found by ELFORD and ROPER (1967), and it is felt that there is too little data to place any emphasis on it. It is possible that the seasonal trend found by ELFORD and ROPER (1967) was unique to that year of observation. McAVANEY (1970), using a very similar measurement technique, found no seasonal trend, although ROPER (1977) claims to have produced a seasonal variation when the data were re-analysed in a different way to that used by McAvaney.

Notice that medians have been plotted for the band $21^{\circ}-50^{\circ}$, since there was sufficient data to do this. The mean may not be the best way to describe the data, as one large value of ε can seriously affect the mean. The straight edges surrounding the medians represent the lines below which 16% and 84% of the data lie, respectively (i.e., 66% of the data lay within the outlined region). Notice that at times ε values as large as $1-2Wkg^{-1}$ have been observed, but generally ε is of the order of 0.1Wkg. Above \sim 95 km the means and medians agree fairly well, but below this height there are some discrepancies. The median is probably a better measure of typical ε at these heights.

In the $51^{\circ}-90^{\circ}$ region, all the cata are due to ZIMMERMAN and MURPHY (1977) for two stations at $60^{\circ}N$ and $70^{\circ}N$ and MANSON et al. (1980, 1981). The two extreme left profiles in Figure 1 are those due to ZIMMERMAN and MURPHY (1977) for summer. These values get very low in value, although it should be noted that below 80 km (at 75-80 km), Zimmerman and Murphy's values rose somewhat to values of the order of $.01 \text{Wkg}^{-1}$. Hence, all we can say is that the typical values at 80 km are $\sim .005-.01 \text{Wkg}^{-1}$ in summer.

The values due to MANSON et al. (1980, 1981) for summer were > 0.1Wkg⁻¹. If the values due to Zimmerman and Murphy are taken as a reference, then it appears that the Manson values may be contamined by horizontal gravity wave motion as discussed by HOCKING (1983a,b). Thus they have been ignored in forming the summer means. However, during winter, turbulence is much stronger according to Zimmerman and Murphy, so the values due to MANSON et al. (1980, 1981) are therefore probably more reliable, and have been included. It appears that there are larger seasonal fluctuations at high latitudes.

It should also be noted that the "means" above $\sim 100~\rm km$ are almost certainly an overestimate. Much of the time this region is above the turbopause, and so is laminar, but only ϵ values corresponding to turbulent conditions have been included in these means. Thus the profile above $\sim 100~\rm km$ is only representative of occasions when the turbopause is high.

Figure 2 shows the median values of ε for all data collectively, together with 16% and 84% percentiles. The broken arrows on Figure 1 (20°-50°) and Figure 2 are meant to indicate that often the turbopause exists at heights as low as 95-100 km, and often ε profiles actually follow the broken lines rather than continue up to \sim 115 km. The diagonal line in Figure 2 represents the line ε = $\nu\omega_{\rm B}^2$. Any ε values to the left of this curve are meaningless, as

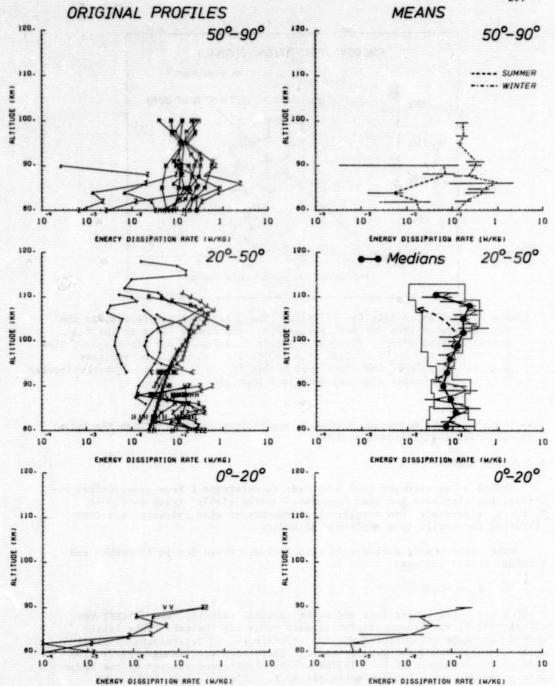


Figure 1. Energy dissipation rates for latitude bands 0-20°, 20-50° and 50-90°. On the left are shown all profiles as extracted from the relevant references, and on the right are the means ((∓ o/√n)) and the medians (heavier lines). Symbols used: Z is used for all profiles involving Zimmerman, M for profiles involving Manson, H for HOCKING (1983b), R for ROPER (1966), J for JUSTUS (1967), + for LLOYD et al. (1972) and REES et al. (1972), V for profiles involving Vincent, B for Blamont and C for McAvaney.

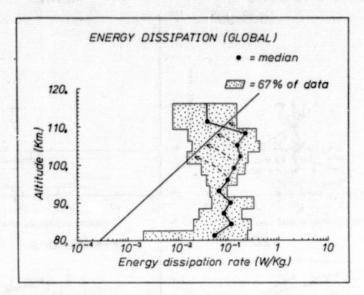


Figure 2. Median profile for all data. The outer boundary represents the region between 16th and 84th percentile. The dashed lines at the top emphasize that often a turbopause exists lower down, and the diagonal line represents $\epsilon \approx \nu \omega_{\rm B}^{-2}$. Values of ϵ to the left of this line indicate meaningless values, and where this occurs it can be concluded that molecular diffusion dominates over any turbulent processes.

this means that the molecular diffusion coefficient is greater than the turbulent diffusion coefficient (by (5)).

8. DETERMINATIONS OF K

Whilst a few attempts have been made to determine K from experimental observations, they have not been frequent. JUSTUS (1967a) tried to obtain K_m and K_s separately from detailed measurements of wind velocity, and from observing the oscillation amplitude of eddies.

Other attempts to determine K have included those due to ZIMMERMAN and KENESHEA (1981) who used

$$K_t = - \overline{w0} / \frac{d0}{dz}$$

O being potential temperature and w the vertical velocity, and VINCENT and STUBBS (1977), who looked at gravity wave decay with height. This latter method has large inaccuracies due to uncertainties in determining "typical" vertical wavelengths for gravity waves. TEITELBAUM and BLAMONT (1977) also made rocket estimates of K. GIBBINS et al. (1982) used studies of the transport of water vapour to give estimates of K.

Some early estimates of K assumed that turbulent diffusion was identical to molecular and diffusion in all aspects, and did not appreciate that turbulent diffusion obeys (8) for scales smaller than the largest scales of turbulence. These estimates have not been included.

More commonly, estimates of K have been made from global temperature and density profile considerations. JOHNSON and WILKINS (1965) noted that the

temperature gradient at 85-110 km is not as steep as it should be if only molecular diffusion acted. They concluded that turbulence must be acting to transfer the heat down from the regions where photodissociation (and therefore heating) take place, to the lower regions. From this concept they were then able to obtain approximate estimates of the expected eddy diffusion coefficient.

In a somewhat similar vein, COLEGROVE et al. (1965) noted that observed ratios of the concentration of 0_2 to that of 0 at 120 km were higher than might be expected. They postulated that eddy diffusion could mix the 0 down from 120 km to ~ 90 km, where the mean free path is less, and so allow greater 0_2 concentrations in the 90-120 km region. These authors also made estimates of K.

These two techniques form the basis of many subsequent estimates of K. Successive authors have included temporal variations (e.g., SHIMAZAKI, 1971; KENESHEA and ZIMMERMAN, 1970) and have looked at latitudinal and seasonal variation (e.g., HESSTVEDT 1968; JOHNSON and GOTTLEIB 1970; BLUM and SCHUCHARDT 1978a). KENESHEA and ZIMMERMAN (1970) pointed out that some of the earlier papers had assumed that turbulence existed above the turbopause and therefore were somewhat in error.

An interesting question arises from this work on energy and oxygen balance. Turbulence produces both heating and diffusion, and it is not at all obvious which process dominates. HUNTEN (1974) and JOHNSON (1975) pointed out that the rates of diffusion and heating are very similar. The question arises as to which is most effective — is diffusion more effective, so that turbulence actually diffuses the heat gradients due to solar effects faster than it causes heating itself (and thus cooling the mesosphere), or is it more efficient at depositing heat, thus heating the mesosphere? It turns out that the answer to this question lies in the value of the constant c₂ in (5).

The reason for the dependence on c_2 can be seen by examining the Richardson number $R_{\hat{i}}$. This is given by

$$R_{i} = \frac{\omega_{B}^{2}}{\langle (\frac{dV}{dz})^{2} \rangle} = \frac{\omega_{B}^{2}}{(\varepsilon/K_{m})} ,$$

since $\epsilon \gtrsim K_{m} < (\frac{dV}{dz})^{2}$ >. (JUSTUS, 1967a)

Here, V is the horizontal velocity.

Thus K = c₂ ϵ/ω_B^2 , where c₂ = $\overline{R_1}$ is the mean R, of all turbulent patches. Hunten showed that the rate of transfer of heat through the mesosphere was F = $nH\rho\omega_B^2$ K, (where n = 7/2, H = scale height, ρ = density), whilst the rate of heating over one scale height was

$$P = \frac{1}{R_4} H \rho \omega_B^2 K$$
. Thus $P/F = (\overline{R}n)^{-1}$.

Clearly heating dominates if $\overline{R}_i \lesssim 0.28$, and diffusion if $\overline{R}_i \gtrsim 0.28$. Hunten claimed that for turbulence to occur, R_i must be less than 0.25 so heating should dominate, whilst JOHNSON (1975) claimed that whilst R_i must be less than 0.25 to initiate turbulence, turbulence may then persist for values of R_i as high as 1.0. Thus Hunten claimed $\overline{R}_i \not\approx 0.2$ - 0.25, whilst Johnson claimed \overline{R}_i is nearer 1.0. The estimates suggested earlier (equation (5)) would imply diffusion dominates.

CHANDRA (1980) has presented a more rigorous treatment of estimation of eddy diffusivities which more properly considers the role of c₂, and assumed c₂ = 0.6. EBEL (1980) has attempted a detailed model to estimate K from theoretical considerations alone, and from considering atmospheric dynamics. CORDIETS et al. (1982) have concluded that the question of whether turbulence heats or cools the atmosphere depends on the height gradient of K, and claim that it heats below about 105 km and cools above.

One problem with these theoretical estimates of K is that they do not consider the effects of vertical winds. For example, atomic oxygen from 120 km could be brought down to 90 km by vertical winds at one location, and lifted back up by vertical winds at another. The possibility of such "cells" of circulation has not been included in any of these analyses. Thus, in principle, all prior estimates are upper limits of K.

The relation (5) offers a means of converting the ε profile of Figures 1 and 2 to K profiles, but a possible problem arises because the lower thermosphere is not always turbulent. This being so, it may be that whilst the relation (5) controls diffusion across a turbulent patch, it may not control diffusion across the whole region 80-120 km. Rather, the rate of diffusion might depend partly on the temporal and spatial frequency of occurrence of turbulent patches in a manner similar to that proposed by DEWAN (1981) and WOODMAN et al. (1981) for the stratosphere. This is a point which needs further examination in the future, but for the present the relation (5) will be utilized.

In Figure 3a all the relevant K profiles due to all the mentioned authors have been presented. These include both theoretical and experimental ones. The approximate molecular viscosity has also been marked, and turbulent viscosities have been stopped when they encounter this region. In Figure 3b, the shaded region represents broadly the range of values in Figure 3a. The solid lines represent K values deduced by applying (5) to the medians of Figure 2. The Brunt-Vaisala periods were taken from GOSSARD and HOOKER (1975). The profile to the right assumes $K = \frac{\varepsilon/\omega}{2}$, and that to the left assumes $K = 0.5 \frac{\varepsilon}{2}$ (equation 5). It is noteworthy that these K profiles derived from experimental estimates of ε agree so well with theoretical valued of K deduced by heating and chemical considerations, which is a good check on the independent procedures used to derive K and ε . It also supplies some support for (5) and although it does not help to significantly resolve the value of ε_2 , it does at least appear to suggest a value of ε_2 of between .5 and 1.0.

9. SEASONAL AND LATITUDINAL VARIATIONS

BLUM and SCHUCHARDT (1978b) and KOROLEV and KOLENIK (1979) have used measurements of the ratio of the densities of 0, to 0 at 120 km to estimated K as a function of season. Both get similar profiles and in particular both find a maximum in K in summer at mid to high latitudes. EBEL (1980) on the other hand, has attempted an entirely theoretical approach, and obtained a maximum in K during winter at $^{\circ}$ 30-40 $^{\circ}$ latitude. Thus although attempts have been made to obtain seasonal and latitudinal variations, these are at too early a stage to be included in this book.

SCALES OF TURBULENCE

Based on the profiles derived earlier, it is possible to estimate ℓ_O and L_B at these altitudes. At 80 km, $\ell_O \sim 10\text{--}20$ m, whilst at 90 km, $\ell_O \sim 20\text{--}40$ m. The outer scale L_B is everywhere about 400-2000 m. Between these scales, turbulence should be largely isotropic — at larger scales significant anisotropy may set in. These ranges are also consistent with experimental observations of ℓ_O (e.g., BOOKER and COHEN, 1956; ROPER 1977). (It should be noted that Booker and Cohen produced unrealistic estimates of ϵ , but neverthe-

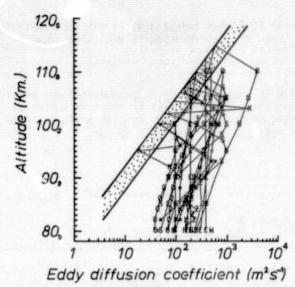


Figure 3a. Collective of all eddy diffusion coefficient profiles from all relevant references. No distinction has been made concerning latitude and season. The dotted region represents K & v , v being molecular viscosity. Symbols used are: K for KENESHEA et al. (1979) and KENESHEA and ZIMMERMAN (1970), and J for JOHNSON and WILKINS (1965), C for papers involving Colgrove, O for JOHNSON and GOTTLIEB (1979), S for SHIMAZAKI (1972), H for HESSTVEDT (1968), W for WOFSY and McELROY (1973), T for TEITELBAUM and BLAMONT (1979), E for EBEL (1980), * for CHANDRA (1980), Z for ZIMMERMAN and KENESHEA (1981), + for GIBBINS et al. (1982), B for BLUM and SCHUCHARDT (1978), S for JUSTUS (1967a).

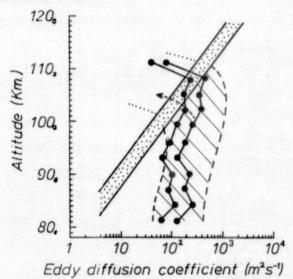


Figure 3b. Envelope of profiles from Figure 3a, together with $\varepsilon/\omega_B^{\ 2}$ (right) and $0.5\varepsilon/\omega_B^{\ 2}$ profiles (equation 5) deduced from the median curve in Figure 2. Note that the two curves deduced from ε both agree with the K profiles, so although this does not solve the problem of better defining C_2 in equation (5), it does appear to support that equation.

less their determination ℓ_0 of was independent of their estimates of ϵ and the method which they used for determinging k_0 was quite sound).

CONCLUSION

Curves of E, and K vs. height have been presented. One point which has clearly emerged is that there is a scarcity of experimental data, and more effort in this direction is strongly urged, so that a clear global and seasonal picture of turbulence variations can be built up.

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4.1 CONTRIBUTION TO THE CIRA MODEL FROM GROUND-BASED LIDAR

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INTRODUCTION

A new technique, the Rayleigh-Lidar Sounding, has been developed recently to probe the Middle Atmosphere and has demonstrated its ability to provide density and temperature profiles in the height range 30-90 km. It has been limited until now to ground-based observations, but it could be used in the future from a space-borne platform. The set of data, as it exists to-day, has been obtained from a unique midlatitude site, the Observatory of Haute-Provence (O.H.P. 44°N, 6°E) and consequently only local information has been obtained with that technique. Even with this limiting factor, it is thought to be a useful complement to a global model, mainly because of its spatial and temporal resolutions, usually not available from global data. Such resolutions give an insight into the atmospheric variability as a function of height and time, for time-scale ranging from minutes to years.

BRIEF DESCRIPTION OF THE METHOD

A description of the Rayleigh-Lidar technique and of the instrument is available in the published literature (HAUCHECORNE and CHANIN, 1980, 1982, 1983; CHANIN and HAUCHECORNE, 1981; BOURG-HECKLY et al., 1982; CHANIN et al., 1983) and its more complete and recent description is published in a previous issue of MAP Handbook (CHANIN and HAUCHECORNE, 1984). The purpose of this brief recall is to ensure that the data will be interpreted and used correctly as a contribution to the new model.

Nature of Measured Parameters. When a monochromatic laser beam is sent into the atmosphere, two processes can provide a backscattered signal: the Rayleigh scattering by atmospheric molecules and the Mie scattering by atmospheric aerosols. Above a level ranging from 30 to 35 km, the Mie contribution (scattering ratio << 1,01). Then the backscattered signal from a given height-range, Z \pm ΔZ , is proportional to the density $\rho(Z)$. A profile of the atmospheric density can be obtained by a time analysis of the echo (with a proportionality constant to be determined). The temperature can be deduced in absolute value from the density profile by using a model value of the pressure at the top of the profile and assuming that the atmosphere is in hydrostatic equilibrium and obeys the perfect gas law. Because of the required fitting with the model at the top of the profile, the range of the temperature profile is reduced by 10 km compared to the density profile.

The main quantity preventing measurement of density in absolute value is the transmission of the atmosphere, which is known to vary widely with a short time constant; to obtain a density profile it requires a calibration at 30 km with another density measurement (radiosondes for example) which was not performed on a regular basis. Due to the fact that the temperature is obtained in absolute value from this technique, all the data mentioned in this contribution will be temperature data.

Altitude Range of the Lidar Sounding. As mentioned before, the lowest height where the backscattered signal can be interpreted directly in terms of density (and then temperature) is fixed by the upper level of the aerosol

layer. This level is usually below 30 km at midlatitudes with the exception of post-volcanic eruption periods. For the years 1981 to 1984 corresponding to the data presented here, such eruptions were quite frequent and care was taken to delete data at the levels where aerosols had been detected. The major disturbance came in 1982 from the El Chichon eruption, but as the aerosols content was monitored by lidar from the same site, it provided a double check to delimit the height range to be used.

The upper limit of the measurement is given by the signal-to-noise ratio, thus explaining the great care taken to reduce the sky-background which is the main contribution to noise. After a succession of improvements through the years, the range was pushed up from 70 km in 1981 to 90 km and occasionally to 95 km. In this altitude range (30-90 km) several tests using double wavelength measurements have been performed to ensure that the contribution of Mie scattering could be neglected. With a still increased sensitivity, one may be able in the future to detect the eventual presence of aerosols of meteoritic origin around 90-100 km, but, as for today, their abundance has never been measured by lidar and is then too small to disturb the measurements.

Resolutions. The lowest possible limit of the height resolution is fixed by the laser pulse duration; in our case 1.5 meter for the laser pulse duration of 10 nsec. Practically, the height resolution is given by the width of the time gate of the photon counting analysis; in the earlier measurements it was fixed at 4 μs giving then ΔZ = 600 m and it has been recently reduced to 2 μs in order to obtain a height resolution of 300 m. For much of the data treatment performed in this analysis, such height resolution was smoothed to 2.4 or 3.0 km by use of a running average. The temporal resolution, theoretically limited by the laser repetition rate (here 10 Hz), is actually defined by the integration time necessary to reach a satisfactory accuracy. In order to reduce the size of the recorded data set, the time resolution has been limited to 5 of 5 minutes. For the lower height range (30-50 km) such an integration time of 5 minutes provides enough accuracy to study short time-scale fluctu- ations. But for the data used in this study the integration time was ranging between 2 and several hours.

Accuracy. The accuracy of the measurements depends on the number of received photons and then on both the time and height resolutions. For the values of those parameters used in this analysis ($\Delta z = 2.4$ km $\Delta t = 2$ H) the typical accuracy would be 0.1, 1 and 10% for the density measured at 35, 65 and 85 km and 0.3, 1 and 10 K for the temperature at 35, 50 and 80 km.

DESCRIPTION OF THE AVAILABLE SET OF DATA AND DATA PROCESSING

The first lidar data from which temperature profile have been deduced date from the year 1977 (HAUCHECORNE and CHANIN, 1980); at that time they were obtained as a by-product of the lidar sounding of sodium and lithium at the mesopause level. Those data were never obtained on a regular basis and their accuracy was lower by far than the present one. Consequently, even though those data can be useful for looking at long-term variations, they have not been used in this work. In June 1980 a new lidar station devoted to Rayleigh scattering measurements was set up at the O.H.P. and was put into service on a routine basis in January 1981. This survey has been going on since that date, with only 2 interruptions of more than a month duration to bring some necessary improvements to the equipment. A noticeable gain in accuracy and range was the consequence of those successive interventions, but the set of data obtained between January 1981 and June 1984 presents a good enough homogeneity to be used as a whole on this study. (The date of June 1st 1984 to end the series of data presented here was chosen because of the presentation of these

results at the COSPAR meeting in June 1984. For a definitive contribution to the CIRA Model in 1985 or 1986 the date set will be completed, as the collection of data has not been interrupted.) These three years and a half of data represent a total number of nights of measurements of 324, namely 67 for 1981, 107 for 1982, 104 for 1983 and 46 for the first 5 months of 1984.

On a regular basis, and when the meteorological conditions are favorable, the lidar operates for 3 consecutive hours during the first part of the night. For this study, most of the temperature data correspond to a 3 hour average. But for 10 cases, the data were obtained for longer periods, between 6 and 13 hours, with the purpose of studying diurnal and semidiurnal tides; in those cases the profile used in this study correspond to the profile averaged over the whole sequence. The reason for using time-averaged profiles was to reduce most of the fluctuations due to gravity waves. It should be mentioned that an instantaneous profile — as the temperature or density rocket profile — is more likely to be influenced by short time-scale fluctuations, as there is no way then to distinguish between short— and long-period waves. In addition, a smoothing function was applied to the lidar vertical profiles in order to suppress the vertical structures of small wavelengths still present after time averaging. The vertical resolution in this study has been reduced to 2.4 km or 3.0 km for that purpose.

From the set of individual profiles covering all the periods described earlier, the seasonal variation of the temperature is obtained using a 45-day half-width Blackman filter to suppress the short-period fluctuations and is then averaged over the 4 years, 1981 to 1984.

The variance of the temperature as a function of time is calculated as the square of the deviation of each individual profile from the averaged temperature. The variance is then smoothed by using the same Blackman filter as for the temperature and averaged over the 4 years of data.

RESULTS OF THE ANALYSIS OF THE PERIOD 1981-1984

Diurnal Variation. Long sequences of data have been recorded especially with the aim to study the diurnal and semidiurnal tides. In half of the cases a regular cooling of the atmosphere is observed with a minimum value at the end of the night; the cooling rate is about 1 K/hour in the stratosphere and up to 3 K/hour in the mesosphere; in the other cases, the amplitude of the gravity waves and/or of the semidiurnal tide being of the same order of magnitude or even larger than the diurnal variation hide completely this cooling effect (amplitudes of the temperature fluctuations as large as 10 to 30 K increasing from 30 to 70 km are not unusual).

A large enough statistics is not yet available to conclude and, at this stage, it looks unjustified to apply a systematic correction to the temperature values as a function of the time of day. The error due to the diurnal variation in this study is limited by the small dispersion of the data with time, as the measurements are usually performed in the early part of the night.

Day-to-Day Variance. A large variability is observed from one day to the next, mainly during the winter (from October to April) when the westerly winds allow the propagation of planetary waves. As the study of the interaction of planetary waves with the general circulation has been one of our main scientific objectives since 1981 (HAUCHECORNE and CHANIN, 1982, 1983), the lidar was due to operate very frequently during wintertime -- each night when the meteorological conditions were satisfactory -- while in summertime, where the variability was observed to be low, the number of observations was willingly

reduced to a few nights a week. From the large number of winter data, the variability of the wintertime temperature has been studied with a time resolution which is usually not available from rocket data (up to 19 nights of data during December 1982).

The height section of the standard deviation (square root of the variance) is shown on Figure 1. These results confirm what had been observed for 3 consecutive winters and indicate the presence of two relatively well-defined maxima of standard deviation centered around January: one at 35-40 km with a maximum of amplitude of 12 K, one at 65-70 km with an amplitude as high as 18 K. Durin; the summer the variability is observed to be very low in the stratosphere (\leq 5 K) but stays quite large in the upper mesosphere near 75 km.

This notion of variance of geophysical quantity has not yet been introduced in the model as it is not available on a global basis. We feel that such results, even limited to a specific site, could be useful to estimate the expected deviation from the mean value as given by the model.

Seasonal Variation. The seasonal variation of the smoothed temperature (Figure 2) show a very similar behaviour for the successive years. A maximum of temperature is observed at the stratopause level around May-June and a minimum around December-January. At this level of the stratopause (45-50 km) the amplitude of the yearly variation is around 20 K. A regular feature also observed in the 3 consecutive winters corresponds to a small warming in the mid-mesosphere around November and is followed by a minimum temperature in January.

The strong similarity between the seasonal variations observed for the data set available, should indicate that the average map covering the whole period (Figure 2) could be used as representative of the seasonal variation for this site and for this part of the solar cycle.

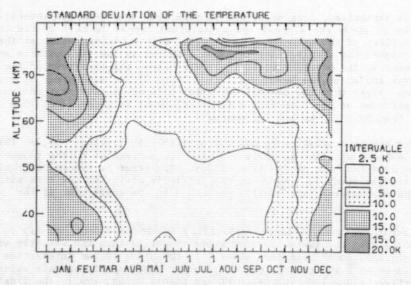


Figure 1. Height section of the temperature standard deviation calculated from the individual daily profile deviation from the 45-day running average for the period 1981-1984.

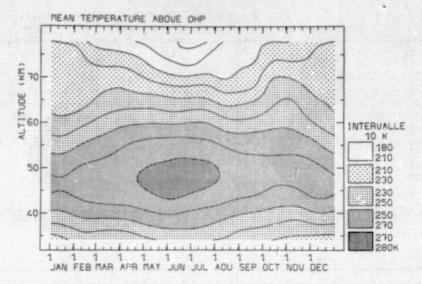


Figure 2. Height section of the mean temperature averaged over 4 years from 1981 to 1984.

These results are also presented in Figure 3 and Table 1 as a series of monthly averaged temperature profiles with an indication of the standard deviation corresponding to the day-to-day variability.

Year-to-Year Variability. As the data are only covering a four-year period, the data set is too small to calculate the year-to-year variance; however, the monthly profiles averaged for each of these years provides an indication on the yearly variability. For this purpose, a winter and a summer set of profiles are given in Figure 4. A large variability is observed as expected in winter as well in the mesosphere and in the stratosphere. The amplitudes of variation observed in February in the stratosphere are of the same order of magnitude as the day-to-day variability (\geq 20 K). In the summer months for the 3 years of data, the variability is larger than the day-to-day standard deviation and reaches a value close to 10 K at all heights.

Deviation From the Model. It is of interest to see how the local mean temperature deviates from the zonal mean as given by the model. The comparison was performed with the CIRA 1972 model by using a linear interpolation between the 40 °N and 50 °N models. Figure 5 presents the deviation from CIRA 72 for the mean temperature observed during the years 1981-1984. Differences as large as 20 K are observed in the mesosphere: the stratosphere at 44°N, 6°E, seems to be on the average warmer during winter and cooler during summer than indicated by the global model, while the situation is opposite for the lower mesosphere (50-65 km). The largest difference is observed in the upper mesosphere \geq 65 km mainly at the beginning of the winter where a small warming is always observed around the October-November period.

The comparison with the revised model, which is of interest in this study, will be performed when the new revised model is available.

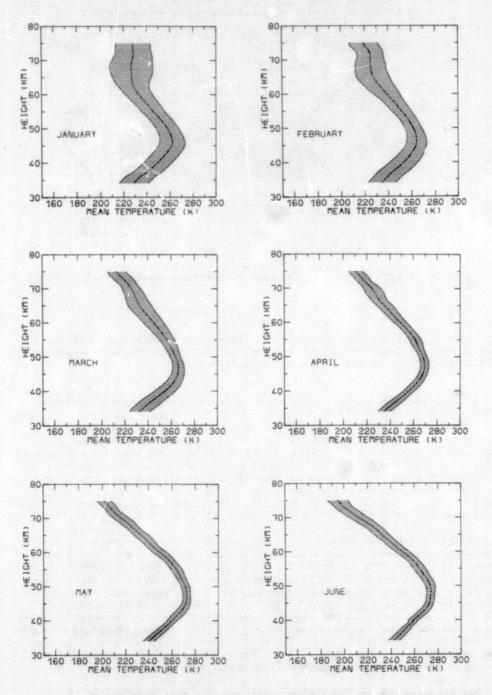


Figure 3. Monthly averaged temperature profiles for the period 1981-1984.

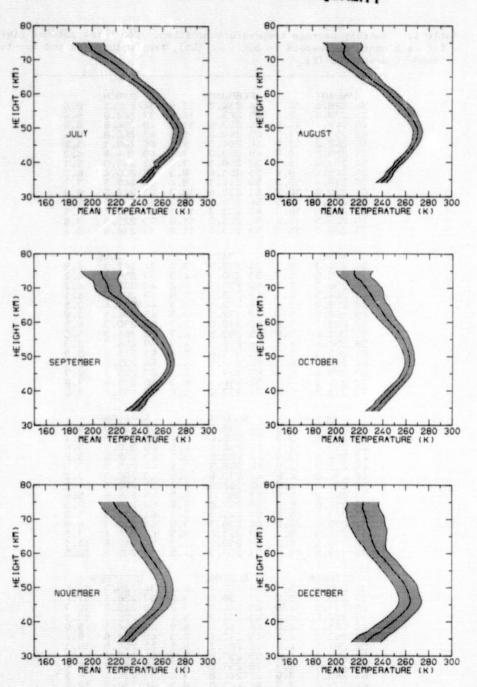


Figure 3 continued.

Table 1. Monthly average temperature profiles. The three columns given for each month correspond to altitude (km), temperature (K) and day-to-day standard deviation (K).

37 239.4 12.2 37 243.1 12.6 37 242.8 40 249.4 11.8 40 253.6 11.8 40 254.6 43 257.3 11.7 43 260.8 9.8 43 262.8 46 262.2 11.0 46 264.5 8.5 46 266.1 49 259.5 9.8 49 263.0 7.1 49 264.8 652 253.6 9.5 52 258.1 7.0 52 261.0 55 245.4 9.8 55 251.4 8.3 55 256.4 9.8 55 251.4 8.3 55 256.4 9.8 238.4 10.8 58 244.1 9.4 58 249.7 61 230.8 12.2 61 235.9 12.3 61 242.6 64 227.3 15.5 64 228.8 13.9 64 235.0 16 67 226.9 18.7 67 225.3 13.1 67 230.1 70 227.5 17.4 70 225.0 11.6 70 225.9	68862313780186
46 263.0 3.4 46 272.5 3.3 46 273.4 49 268.9 3.5 49 272.1 3.5 49 274.1 52 265.1 3.8 52 268.5 3.7 52 270.3 45 52 265.4 5.0 55 263.8 4.7 55 264.3 58 254.4 4.9 58 256.3 4.9 58 256.7 61 245.5 5.7 61 245.6 5.4 61 245.4 64 237.7 6.7 54 237.1 6.0 64 235.0 67 229.4 6.9 67 227.2 5.4 67 225.3 67 227.2 5.4 67 225.3 67 224.2 7.1 70 216.3 6.9 70 211.8	92215850391786
37 250.5 3.3 37 226.2 3.4 37 241.9 4 40 257.1 4.7 40 254.4 4.0 40 250.5 3 43 266.8 3.7 43 262.9 3.0 43 259.3 3 46 272.0 3.9 46 268.7 3.4 46 265.3 3 49 274.0 4.5 49 270.6 4.0 49 266.0 3 52 270.0 4.9 52 266.9 4.6 52 262.5 3 55 263.9 5.9 55 260.5 6.9 55 262.5 3 58 256.0 6.0 58 252.0 6.6 58 249.5 3 61 247.1 6.3 61 243.1 6.1 61 239.3 3 64 235.4 6.5 64 230.7 7.9 64 230.7 66	01820226099915
37 239.1 5.2 37 236.0 7.2 37 238.1 17 40 247.5 4.9 40 244.9 7.0 40 249.3 10 43 256.2 4.4 43 254.7 6.4 43 259.0 10 46 261.4 4.0 46 260.4 6.9 46 264.1 9 49 263.0 4.2 49 262.6 6.3 49 261.6 9 52 261.1 4.8 52 261.2 6.5 52 256.9 10 55 257.3 5.6 55 257.0 7.1 55 249.2 9 58 251.1 6.7 58 251.0 7.1 58 242.1 9 61 243.1 7.6 61 244.8 7.8 61 234.4 8 64 237.4 8.7 64 241.0 8.5 64 230.9 12 67 231.2 9.4 67 236.3 9.1 67 228.7 17 70 225.5 13.2 70 229.8 12.4 70 226.0 15	54718414492186

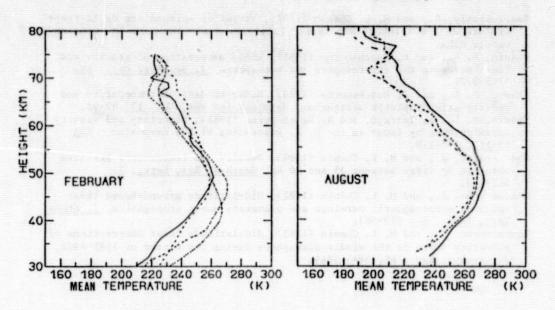


Figure 4. Monthly average temperature profiles February and August for the different years 1981 (-) 1982 (---) 1983 (----) 1984(----).

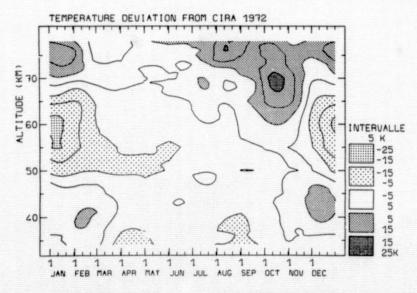


Figure 5. Deviation of the mean average temperature 1981-1984 from the CIRA 1972 model.

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4.2 THE MST RADAR TECHNIQUE

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The past ten years have witnessed the development of a new radar technique to examine the structure and dynamics of the atmosphere between roughly 1-100 km on a continuous basis. The technique is known as the MST (for Mesosphere-Stratosphere-Troposphere) technique and is usable in all weather conditions, being unaffected by precipitation or cloud cover. MST radars make use of scattering from small-scale structure in the atmospheric refractive index, with scales of the order of one-half the radar wavelength. Pertinent scale sizes for middle atmospheric studies typically range between a fraction of a meter and a few meters. The structure itself arises primarily from atmospheric turbulence.

The relative ubiquity of turbulence enables continuous data to be gathered at heights below about 35 km, provided that the radar is sufficiently sensitive. Stipulations to this general statement require: 1) that the spatial resolution of the radar is coarse enough (> 150 m) to ensure that turbulent layers are present within each height interval, and 2) that the radar operating wavelength is sufficiently long to ensure that the pertinent half-wavelength of the scatterers lies in the inertial subrange (if the operating radar wavelength is too short, the half-wavelength structure will be damped out by viscosity in the higher heights).

While it is possible in principle to obtain echoes from atmospheric turbulence above about 35 km, the weaker turbulence at these heights due to a decreasing atmospheric density makes it exceedingly difficult to obtain useful data.

Above about 50 km, however, the presence of free electrons in the atmos phere enhances the radar cross section of the turbulent fluctuations and makes them again observable to a radar of reasonable sensitivity. The atmospheric density is still sufficient to ensure that the free electron motions are controlled completely by the dynamics of the neutral atmosphere. Thus, up to at least 90-100 km it is possible to use these electron-enhanced radar echoes to obtain useful data on neutral motions in the mesosphere and lower thermosphere. Above this height, however, the electron "gas" begins to move independently of the neutral background, so that the radar echoes carry little information on the neutral dynamics.

In the mesosphere-lower thermosphere, turbulent echoes are only observable during daylight (i.e., only when there is sufficient ionization and associated ionization gradients). However, it is possible to supplement the daytime echoes with echoes arising from ionized meteor trails that occur both during day and night. Thus MST meteor echoes are essential to preserve the diurnal continuity of the echo occurrence in the upper mesosphere-lower thermosphere.

In the ten years since the MST technique was first introduced by WOODMAN and GUILLEN (1974), there has been a remarkable increase in the number of radar systems that operate -- at least partially -- in the MST mode. As of this writing, at least 14 existing radars are dedicated to full-time MST studies, seven more systems are operating partially in this mode, and some 77 other systems have been either proposed or are under construction throughout the world. Most of these systems, however, are capable of observing only in the

troposphere and lower stratosphere. The concept of a network of both the less-sensitive (ST) systems and the more-sensitive (MST) systems has been proposed to provide continuous temporal and reasonable spectral coverage of the radar-measurable atmospheric parameters, i.e., winds, waves, turbulence, and atmospheric stability. Such a network of single "point" measurements would be highly complementary to existing satellite data base, which supplies gross features of the geotropic wind field and other parameters on a global scale.

The fundamental parameters measured by MST/ST radars are echc strength, Doppler shift, and Doppler width. Middle atmospheric variables deducible from a continuous measurement of these parameters include mean winds, planetary waves, tides, gravity waves, turbulence structure, and atmospheric stability.

The MST technique is also capable of measuring the vertical wind. High time resolution vertical wind measurements contain a great deal of information on gravity-wave activity, while the long-term mean value potentially is very useful in studying the large-scale circulation pattern. Vertical winds have heretofore been inferred from horizontal wind convergence and continuity agruments. Knowledge of the vertical wind field is of considerable importance in understanding troposphere-stratosphere exchange processes, large scale circulation patterns (e.g., the Hadley and Walker circulations), and wave transport phenomena.

Given the measurement capabilities outlined above, the MST technique appears to have a bright future of middle atmospheric dynamics studies in the coming years. Many preliminary studies designed to examine the limitations and full capabilities of the technique have been undertaken by many experimental groups throughout the world, and the results are very promising. Pertinent review papers, and some specific studies not yet included in the reviews, are listed at the end of this article. The results of more extensive investigations into all of the potential research areas listed below should make major inroads into our understanding of the dynamics of the middle atmosphere.

A partial list of the general areas of study amenable to the MST technique includes:

- 1) The effect of small-scale motions (gravity waves, turbulence, and convection) on the large-scale circulation of the atmosphere. The influence of small-scale motions on the general circulation is known to be appreciable, particularly in the upper mesosphere. Simple models that predict middle-atmospheric temperature structure and zonal mean flow are incapable of reproducing either the measured temperature profiles or the zonal mean flow. In order to produce reasonable results from these models, it is necessary to incorporate dissipation and momentum deposition by upward-traveling gravity waves (and, to a lesser extent, planetary waves and tides).
- A determination of the mean zonal and meridional wind components in the mesosphere and lower thermosphere. The global circulation at these heights is only poorly known, particularly at low latitudes where the Coriolis parameter is either weak or non-existent.
- 3) The delineation of the horizontal wavelengths, phase velocity distributions, and vertical momentum fluxes of middle-atmospheric gravity waves, and a determination of their tropospheric origins. This appears to be a tractable problem using existing MST technology, provided that there are sufficient numbers of radars located at selected geographic locations.
- 4) A study of turbulence in the free atmosphere and its relationship to gravity-wave and tidal breakdown. Estimates of turbulence intensity and turbulent

diffusion appear to be possible using high spatial resolution radars with narrow antenna beams to study the space-time structure of atmospheric turbulence layers. Also, it is possible to examine the idea that the spectral distribution of atmospheric fluctuations may be due to a two-dimensional turbulent cascade process.

- 5) The morphology of atmospheric tides and other large-scale phenomena. Atmospheric tidal processes are currently being studied using a variety of techniques. Data from MST radars, particularly if meteor-echoes are included at the higher heights to improve the continuity of the data base, will provide additional high-quality information for these studies.
- 6) A determination of the dynamic properties of the near-equatorial ionosphere. The equatorial atmosphere within a few degrees of the equator is virtually devoid of Coriolis forcing. As a result, a separate class of relatively long period waves (Kelvin waves and mixed-Rossby gravity waves) can exist in the region. The dynamics of the equatorial atmosphere is thought to be strongly controlled by the evolution and breakdown of these waves. The high-time resolution afforded by continuous observations using a near-equatorial network of MST/ST radars should be extremely beneficial in studying the evolution of these waves.
- 7) The average kinetic energy distribution in the atmosphere. Knowledge of the power spectral density of the atmospheric fluctuations from a few minutes to many hours is available using existing MST data. Combining this kind of data with the mean atmospheric density enables an estimate to be made of the atmospheric kinetic energy $1/2 \text{ pv}^2$ where p is the density and v^2 is the mean square value of the wind field over a specified range of frequencies. Vertical profiles of the atmospheric kinetic energy will be very useful in studies of energy dissipation rates and wave propagation processes (i.e., propagation, reflection, or absorption of planetary waves, tides, gravity waves, etc.).
- 8) Investigation of a possible relationship between solar activity and the mesospheric wind field. A number of existing studies using a variety of techniques (including the MST technique) point to a tenuous but promising relationship between solar activity and mesospheric wind fluctuations. Continuous, high-time resolution MST data will be very useful in such studies.

It is important to point out that, in addition to the MST technique, there are a number of other remote sounding techniques which measure some of the same atmospheric parameters. Both meteor radar systems and partial reflection drifts (PRD) systems have measured mesospheric and lower-thermospheric motions for many years, although their spatial and/or temporal resolution is somewhat more restrictive. Furthermore, horizontal winds, temperature, and humidity are typically measured up to around 30 km by a vast network of meteorological balloons over the entire globe. In addition to these methods, the temperature measuring capability of ground-based lidar systems appears to hold great promise for studying gravity wave propagation in the middle atmosphere, particularly when used in conjunction with radar wind measurements. Both satellite techniques and in situ measurement by rockets and special purpose balloons add new dimensions to the studies. Clearly, the overall picture of the atmospheric motions and energy exchange processes can only be garnered by cooperative, concerted efforts using all available techniques.

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